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# CARRIER LANDING PARAMETERS FROM SURVEY 45, FLEET AND TRAINING COMMAND AIRCRAFT LANDING ABOARD USS ENTERPRISE CVN-65 (MAIN TEXT AND APPENDIX A)

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#### TABLE OF CONTENTS

SUMMARY

LIST OF REFERENCES

LIST OF TABLES

LIST OF FIGURES

LIST OF SYMBOLS

INTRODUCTION

**ACKNOWLEDGEMENT** 

LANDING LOADS SURVEY DEFINITIONS

**BACKGROUND** 

**ANALYSIS** 

CONCLUSIONS

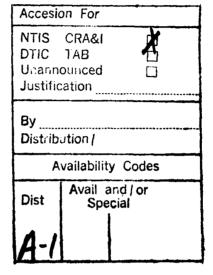
RECOMMENDATIONS

**TABLES** 

**FIGURES** 

## APPENDICES

- A) LANDING PARAMETERS OF INDIVIDUAL AIRCRAFT LANDINGS
- B) FREQUENCY AND PROBABILITY DISTRIBUTIONS, F-14A AIRCRAFT, DAY CARRIER LANDINGS
- C) FREQUENCY AND PROBABILITY DISTRIBUTIONS, F-14A AIRCRAFT, NIGHT CARRIER LANDINGS
- D) FREQUENCY AND PROBABILITY DISTRIBUTIONS, F-18 AIRCRAFT, DAY CARRIER LANDINGS
- E) FREQUENCY AND PROBABILITY DISTRIBUTIONS, F-18 AIRCRAFT, NIGHT CARRIER LANDINGS
- F) FREQUENCY AND PROBABILITY DISTRIBUTIONS, A-6E AIRCRAFT, DAY CARRIER LANDINGS
- G: FREQUENCY AND PROBABILITY DISTRIBUTIONS, A-6E AIRCRAFT, NIGHT CARRIER LANDINGS
- H) FREQUENCY AND PROBABILITY DISTRIBUTIONS, A-7E AIRCRAFT, DAY CARRIER LANDINGS



DTIC QUALITY INSPECTED 4

- I) FREQUENCY AND PROBABILITY DISTRIBUTIONS, A-7E AIRCRAFT, NIGHT CARRIER LANDINGS
- J) FREQUENCY AND PROBABILITY DISTRIBUTIONS, EA-6B AIRCRAFT, DAY CARRIER LANDINGS
- K) FREQUENCY AND PROBABILITY DISTRIBUTIONS, EA-6B AIRCRAFT, NIGHT CARRIER LANDINGS
- L) FREQUENCY AND PROBABILITY DISTRIBUTIONS, E-2C AIRCRAFT, DAY CARRIER LANDINGS
- M) FREQUENCY: AND PROBABILITY DISTRIBUTIONS, E-2C AIRCRAFT, NIGHT CARRIER LANDINGS
- N) FREQUENCY AND PROBABILITY DISTRIBUTIONS, S-3A AIRCRAFT, DAY CARRIER LANDINGS
- O) FREQUENCY AND PROBABILITY DISTRIBUTIONS, S-3A AIRCRAFT, NIGHT CARRIER LANDINGS
- P) FREQUENCY AND PROBABILITY DISTRIBUTIONS, TA-3B AIRCRAFT, DAY CARRIER LANDINGS
- Q) FREQUENCY AND PROBABILITY DISTRIBUTIONS, T-2C AIRCRAFT, DAY CARRIER LANDINGS
- R) FREQUENCY AND PROBABILITY DISTRIBUTIONS, TA-4J AIRCRAFT, DAY CARRIER LANDINGS

#### SUMMARY

As part of a continuing NAVAIRDEVCEN program to monitor the landing performance of naval carrier aircraft, the Aero Structures Division performed a carrier landing loads survey onboard the USS ENTERPRISE in September of 1985. This document formally presents the results of that survey, which were previously provided to NAVAIR informally.

The principle goal of this survey was to compare day and night carrier landing performance. Nearly 900 day and over 500 night landings of fleet aircraft were recorded and analyzed. This survey includes data on F-14, F-18, A-6E, A-7E, EA-6B, E-2C, S-3A and TA-3B aircraft. This survey also provided data on over 1000 carrier landings of student pilots performing day landings of T-2C and TA-4 aircraft. This survey was performed off the west coast of the United States.

## LIST OF REFERENCES

A) NAVAL AIR DEVELOPMENT CENTER REPORT NO. NADC-ST-6706, 27 JAN 68, THE STANDARD ASD PHOTOGRAPHIC METHOD FOR DETERMINING AIRPLANE BEHAVIOR AND PILOTING TECHNIQUE DURING FIELD OR CARRIER LANDINGS.

#### LIST OF TABLES

- DAY / NIGHT MEAN LANDING VALUES COMPARISON DAY / NIGHT LANDING COMPARISON USING A STATISTICAL TEST OF TABLE 2: THE SIGNIFICANTS OF THE DIFFERENCE BETWEEN THE MEAN VALUES OF TWO DATA SAMPLES
- TABLE 3: SURVEY 45 DATA ANALYSIS, GLIDESLOPE ANGLE COMPARISON

TABLE 1:

- SURVEY 45 DATA ANALYSIS, DAY / NIGHT MEAN VALUE COMPARISON TABLE 4:
- TABLE 5: SURVEY 45 DAY CARRIER LANDINGS SUMMARY FOR F-14A MODEL AIRCRAFT
- SURVEY 45 NIGHT CARRIER LANDINGS SUMMARY FOR F-14A MODEL TABLE 6: AIRCRAFT
- SURVEY 45 DAY CARRIER LANDINGS SUMMARY FOR F-18 MODEL TABLE 7: **AIRCRAFT**
- TABLE 8: SURVEY 45 NIGHT CARRIER LANDINGS SUMMARY FOR F-18 MODEL AIRCRAFT
- TABLE 9: SURVEY 45 DAY CARRIER LANDINGS SUMMARY FOR A-6E MODEL AIRCRAFT
- TABLE 10: SURVEY 45 NIGHT CARRIER LANDINGS SUMMARY FOR A-6E MODEL AIRCRAFT
- SURVEY 45 DAY CARRIER LANDINGS SUMMARY FOR A-7E MODEL TABLE 11: AIRCRAFT
- SURVEY 45 NIGHT CARRIER LANDINGS SUMMARY FOR A-7E MODEL TABLE 12: AIRCRAFT
- TABLE 13: SURVEY 45 DAY CARRIER LANDINGS SUMMARY FOR EA-6B MODEL **AIRCRAFT**
- TABLE 14: SURVEY 45 NIGHT CARRIER LANDINGS SUMMARY FOR EA-6B MODEL **AIRCRAFT**
- SURVEY 45 DAY CARRIER LANDINGS SUMMARY FOR E-2C MODEL TABLE 15: AIRCRAFT
- SURVEY 45 NIGHT CARRIER LANDINGS SUMMARY FOR E-2C MODEL TABLE 16: AIRCRAFT
- TABLE 17: SURVEY 45 DAY CARRIER LANDINGS SUMMARY FOR S-3A MODEL **AIRCRAFT**
- SURVEY 45 NIGHT CARRIER LANDINGS SUMMARY FOR S-3A MODEL TABLE 18: AIRCRAFT

TABLE 19: SURVEY 45 DAY CARRIER LANDINGS SUMMARY FOR TA-3B MODEL AIRCRAFT

TABLE 20: SURVEY 45 DAY CARRIER LANDINGS SUMMARY FOR T-2C MODEL AIRCRAFT

TABLE 21: SURVEY 45 DAY CARRIER LANDINGS SUMMARY FOR TA-4J MODEL AIRCRAFT

## LIST OF FIGURES

- FIGURE 1: F-14 DAY LANDINGS \* SURVEY 45, APPROACH SPEED VS WEIGHT FIGURE 2: F-14 NIGHT LANDINGS \* SURVEY 45, APPROACH SPEED VS WEIGHT F-18 DAY LANDINGS \* SURVEY 45, APPROACH SPEED VS WEIGHT FIGURE 3: F-18 NIGHT LANDINGS \* SURVEY 45, APPROACH SPEED VS WEIGHT FIGURE 4: A-6E DAY LANDINGS \* SURVEY 45, APPROACH SPEED VS WEIGHT FIGURE 5: FIGURE 6: A-6E NIGHT LANDINGS \* SURVEY 45. APPROACH SPEED VS WEIGHT A-7E DAY LANDINGS \* SURVEY 45, APPROACH SPEED VS WEIGHT FIGURE 7: FIGURE 8: A-7E NIGHT LANDINGS \* SURVEY 45. APPROACH SPEED VS WEIGHT EA-6B DAY LANDINGS \* SURVEY 45, APPROACH SPEED VS WEIGHT FIGURE 9: FIGURE 10: EA-6B NIGHT LANDINGS \* SURVEY 45, APPROACH SPEED VS WEIGHT E-2C DAY LANDINGS \* SURVEY 45, APPROACH SPEED VS WEIGHT FIGURE 11: FIGURE 12: E-2C NIGHT LANDINGS \* SURVEY 45, APPROACH SPEED VS WEIGHT FIGURE 13: S-3A DAY LANDINGS \* SURVEY 45, APPROACH SPEED VS WEIGHT FIGURE 14: S-3A NIGHT LANDINGS \* SURVEY 45, APPROACH SPEED VS WEIGHT FIGURE 15: T-2C DAY LANDINGS \* SURVEY 45, APPROACH SPEED VS WEIGHT FIGURE 16: TA-4J DAY LANDINGS \* SURVEY 45, APPROACH SPEED VS WEIGHT FIGURE 17: F-14A DAY LANDINGS \* SURVEY 45, ENGAGING SPEED + 20 KNOTS VERSUS LANDING WEIGHT FIGURE 18: F-14A NIGHT LANDINGS \* SURVEY 45, ENGAGING SPEED + 20 KNOTS VERSUS LANDING WEIGHT
- FIGURE 19: F-18 DAY LANDINGS \* SURVEY 45, ENGAGING SPEED + 20 KNOTS VERSUS LANDING WEIGHT
- FIGURE 20: F-18 NIGHT LANDINGS \* SURVEY 45, ENGAGING SPEED + 20 KNOTS VERSUS LANDING WEIGHT
- FIGURE 21: A-7E DAY LANDINGS \* SURVEY 45, ENGAGING SPEED + 20 KNOTS VERSUS LANDING WEIGHT
- FIGURE 22: A-7E NIGHT LANDINGS \* SURVEY 45, ENGAGING SPEED + 20 KNOTS VERSUS LANDING WEIGHT

- FIGURE 23: F-14A DAY LANDINGS \*\* SURVEY 45, SURVEY SPEED VERSUS DESIGN SINK SPEED
- FIGURE 24: F-14A NIGHT LANDINGS \*\* SURVEY 45, SURVEY SINK SPEED VERSUS DESIGN SINK SPEED
- FIGURE 25: F-18 DAY LANDINGS \*\* SURVEY 45, SURVEY SINK SPEED VERSUS DESIGN SINK SPEED
- FIGURE 26: F-18 NIGHT LANDINGS \*\* SURVEY 45, SURVEY SINK SPEED VERSUS DESIGN SINK SPEED
- FIGURE 27: A-7E DAY LANDINGS \*\* SURVEY 45, SURVEY SINK SPEED VERSUS DESIGN SINK SPEED
- FIGURE 28: A-7E NIGHT LANDINGS \*\* SURVEY 45, SURVEY SINK SPEED VERSUS DESIGN SINK SPEED

## LIST OF SYMBOLS

 $V_V$  - Sink speed, feet per second

	Subcripts: N - Nose wheel touchdown P - Port wheel touchdown S - Starboard wheel touchdown A - Average of both main wheels at first main wheel touchdown
KLE	- Wing lift factor
$V_{\mathbf{W}}$	- Wind velocity over deck, knots
$V_{E}$	- Engaging speed, knots
$V_{P'\!AF}$	- Approach speed, knots
$V_{P'A_{\min}}$	- Minimum usable power approach airspeed, knots
$V_{SP'A}$	- Power approach stall speed, knots
$K_{V_{P'Amin}}$	- Ratio of measured approach speed to minimum power approach speed
$K_{VSP'A}$	- Ratio of measured approach speed to power approach stall speed
$\Theta_p$	- Aircraft pitch angle, degrees and (radians); positive values indicate nose up attitude measured from fusclage reference line to horizontal
	Subscripts: td - Touchdown R - Over the ramp
θ,	- Aircraft roll angle, degrees and (radians); positive values indicate starboard wing down
$\dot{\Theta}_{p}$	- Aircraft pitch rate at first main wheel touchdown, degrees per second and (radians per second)
Θ,	- Aircraft roll rate at first main wheel touchdown, degrees per second and (radians per second)
Y	- Aircraft off-centerline distance, feet; positive values indicate port side of deck centerline
$X_{W}$	- Distance from ramp to first main wheel touchdown
$\beta_{v_{_{m{v}}}}$	- Aircraft instantaneous glideslope angle
β <sub>H</sub> ,,	- Aircraft geometric glideslope angle
w	- Landing weight
YAW <sub>td</sub>	- Air aft yaw angle, degrees and (radians)
ф	- Aircraft phi angle

## LIST OF SYMBOLS (cont'd)

F. P. A Aircraft flight path angle	F.	P. A		Aircraft	flight	path	angle
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Hw - Height of main wheels over the ramp

 $H_H$  - Height of the hook at the ramp

 $\delta_{d_p}$  - Angle of flight deck pitch

 $\delta_{4}$  - Angle of flight deck roll

N - Number of Observations in Sample

P - Probability

S - Standard deviation of sample distribution

A<sub>3</sub> - Skewness factor of sample distribution

A<sub>4</sub> - Kurtosis factor of sample distribution

#### INTRODUCTION

The NAVAL AIR DEVELOPMENT CENTER (NAVAIRDEVCEN) utilizes a 70 mm half-frame photoelectronic film system to record day and night aircraft carrier landings for determining approach and touchdown parameters. The information provided in this report was collected onboard the USS ENTERPRISE (CVN-65) during a carrier qualification period for fleet pilots. The ship was operating off the west coast of the United States during this period.

The system consists of a 70 mm half-frame camera to photograph aircraft landings, a covert infrared flasher system to illuminate night landings, and a 70 mm film reader which is used to digitize approaching aircraft position. The analysis techniques of reference (a) are used to develop a statistical presentation of the desired aircraft landing parameters by aircraft model type and series.

Data included in this report was derived from the following sources:

- 1. Day/night photographic records obtained during this survey.
- Ship's logs. (Fuel weights, arresting gear runout)
- 3. Ship's pitch and roll data which is automatically recorded on the 70 mm film from the ship's gyro compass.
- 4. Ship's anemometer for wind over deck measurement.
- 5. Ship's instrumentation for ship speed, barometric pressure and outside air temperature.

The landing parameters included in this report are listed and defined in section 3.0 of this report.

## ACKNOWLEDGEMENT

We express our thanks and appreciation to the Officers and Crew of the USS ENTERPRISE, CVN-65, and in particular to the Air department and V-1 Division, for their outstanding assistance and professional support provided to the NAVAIRDEVCEN Survey Team during this Landing loads Survey.

#### LANDING LOADS SURVEY DEFINITIONS

#### SINK SPEED Vv

The sink speed of the aircraft landing gear wheel just prior to touchdown. Sink speed is reported for each landing gear individually; that is for the Port, Starboard and Nose wheels just prior to individual deck contact. In addition the Average sink speed of the aircraft main landing gear is calculated just prior to touchdown of the first main landing gear wheel. Sink Speed is determined from film data. The symbols used to identify aircraft sink speed are as follows:

 $V_{V_A}$ -average sink speed  $V_{V_S}$ -sink speed of the starboard main wheel  $V_{V_P}$ -sink speed of the port main wheel  $V_{V_B}$ -sink speed of the nose landing gear

The values of aircraft sink speed are reported in Feet per second (ft/sec)

For shipboard landings the values of sink speed are reported with respect to the vessel's flight deck.

## WING LIFT FACTOR KLE

The Wing Lift Factor is calculated from the derivative of the aircraft average sink speed. It is calculated just prior to the touchdown of the first main landing gear. A value of 1.0 for the Wing Lift Factor indicates that a constant sink speed is being maintained. If the value of  $K_{LE}$  is greater than 1.0, this indicates that the sink speed is decreasing and the wing lift is greater than 1.0 G. Conversely, if the value is less than 1.0 then the sink speed is increasing and the lift being generated is less than 1.0 G. The value of Wing Lift Factor is calculated from the equation

$$K_{LE} = \frac{1}{32} \times \frac{d^2Y}{dt^2} + 1.0$$

where the value of Y is the aircraft vertical position with respect to time; the derivative is evaluated at touchdown (t=0). The regression curve is that calculated for the average vertical position of the Aircraft Main Landing Gear and has the form of the equation

Vertical Position  $Y = A + Bt + Ct^2$ 

The symbol for Wing Lift Factor is  $K_{LE}$ 

This quantity is dimensionless.

The value of Wing Lift Factor is measured with respect to the flight deck (this value could be referenced to the horizon by correcting it for deck pitch angle).

## WIND OVER DECK Vw

Wind Over Deck is the wind velocity measured by the ships instrumentation with respect to the flight deck. For aircraft carrier landings, the wind component down the landing deck is utilized. The Positive direction for Wind Over Deck is from the ships bow to the stem, down the angle deck.

The symbol for Wind Over Deck is  $V_{\mathbf{W}}$ 

The value of Wind Over Deck is reported in Knots.

## ENGAGING SPEED $V_E$

The Engaging Speed is the speed with which the aircraft closes on the aircraft carrier's flight deck. Engaging Speed is reported with respect to the flight deck. Engaging Speed is calculated from film measurements.

The symbol for Engaging Speed is  $V_E$ 

The value of Engaging Speed is reported in Knots.

## APPROACH SPEED VPAF

The value of Approach Speed reported is the algebraic sum of engaging speed and component of wind over deck parallel to the centerline of the angle deck. The value of approach speed is the aircraft horizontal velocity with respect to the air mass.

The symbol for Approach Speed is  $V_{PAF}$ 

The value of Approach Speed is reported in Knots.

## MINIMUM POWER APPROACH SPEED $V_{PA_{min}}$

This value is the Minimum Power Approach Speed for a jet aircraft in the power approach configuration (landing gear, flaps, and other high lift devices deployed). This number is determined from the aircraft's aerodynamic characteristics and landing weight per criteria established by NAVAIR.

The symbol for Minimum Power Approach Speed is  $V_{PA}$ 

The value of Minimum Power Approach Speed is reported in Knots.

## POWER APPROACH STALL SPEED $V_{SPA}$

This value is the Power Approach Stall Speed for a propeller driven aircraft in the power approach configuration (landing gear, flaps, and other high lift devices deployed). This number is determined from the aircraft's aerodynamic characteristics and landing weight per criteria established by NAVAIR.

The symbol for Power Approach Stall Speed is  $V_{SPA}$ 

The value of Power Approach Stall Speed is reported in Knots.

## RATIO OF MEASURED APPROACH SPEED TO MINIMUM POWER APPROACH SPEED $K_{V_{p_{Amin}}}$

The ratio of the jet aircraft approach speed determined from film data to the minimum power approach speed for the same landing weight.

The symbol for the Ratio 
$$\frac{V_{PAF}}{V_{PA_{min}}}$$
 is  $K_{V_{PA_{min}}}$ 

This quantity is dimensionless.

## RATIO OF MEASURED APPROACH SPEED TO POWER APPROACH STALL SPEED Kyspa

The ratio of the propeller driven aircraft measured approach speed, determined from film data, to the aircraft power approach stall speed, for the same value of landing weight.

The symbol for the Ratio 
$$\frac{V_{P'AF}}{V_{SP'A}}$$
 is  $K_{V_{SP'A}}$ 

This quantity is dimensionless.

## AIRCRAFT PITCH ANGLE $\theta_{r}$

The Aircraft Pitch Angle measured between the aircraft reference line and a line parallel with the aircraft carrier flight deck. Positive values of Pitch Angle are reported for an aircraft exhibiting a nose up attitude. Pitch Angle is determined from film data.

The symbol used for Pitch Angle is  $\theta_p$ 

The value of this quantity is reported in both Degrees and Radians.

The value of Pitch Angle is reported at two locations; just prior to first wheel touchdown and as the aircraft flies "over the ramp" at the stem end of an aircraft carrier flight deck.

$$\theta_{p_R}$$
 - over the ramp  $\theta_{p_R}$  - at touchdown

## AIRCRAFT ROLL ANGLE $\theta_r$

The Aircraft Roll angle measured between the aircraft reference line and a line parallel with the aircraft carrier flight deck. Positive values of Roll Angle are reported for an aircraft whose starboard wing is down. Roll Angle is determined from film data.

The symbol used for Roll Angle is  $\theta_r$ 

The value of this quantity is reported in both Degrees and Radians.

The value of Roll Angle is reported at two locations: just prior to first wheel touchdown and as the aircraft flies "over the ramp" at the stem end of an aircraft carrier flight deck.

 $\theta_{r_R}$  - over the ramp  $\theta_{r_R}$  - at touchdown

## AIRCRAFT PITCH RATE 0,

The Aircraft Pitch Rate is calculated from the film data. It is reported just prior to the touchdown of the first main wheel. Positive values of this variable indicates that the aircraft nose is pitching down. This rate is determined with respect to the flight deck.

The symbol used for this quantity is  $\dot{\theta}_p$ 

The value of this quantity is reported in both Degrees per second (deg/sec) and Radians per second (rad/sec)

## AIRCRAFT ROLL RATE 0,

The Aircraft Roll Rate is calculated from the film data. It is reported just prior to the touchdown of the first main wheel. Positive values of this variable indicate that the aircraft is rolling to port. This rate is determined with respect to the flight deck.

The symbol used for this quantity is  $\dot{\theta}_r$ 

The value of this quantity is reported in both Degrees per second (deg/sec) and Radians per second (rad/sec)

#### AIRCRAFT OFF-CENTERLINE DISTANCE Y

This is the perpendicular distance measured between the aircraft centerline and the centerline of the flight deck (or runway). This value is calculated from film data just prior to first main wheel touchdown. Positive values of this quanity indicate that the aircraft landed on the Port side of the Flight Deck centerline.

The symbol for this quantity is Y

The value of this quantity is reported in Feet (ft).

## DISTANCE FROM RAMP TO FIRST MAIN WHEEL TOUCHDOWN $X_W$

For aircraft carrier landings the distance between the flight deck ramp (aft end of the flight deck) and the point of first main wheel touchdown is determined from the film data. For land based surveys, this distance can be determined from an appropriate reference line with respect to the camera.

The symbol for this quantity is  $X_w$ 

The value of this quantity is reported in Feet (ft).

## AIRCRAFT INSTANTANEOUS GLIDESLOPE ANGLE βν.,

This angle is determined just prior to first main wheel touchdown. The value of average sink speed  $(V_{V_A})$  and engaging speed  $(V_E)$  are used to define the instantaneous glideslope. These values are entered into the equation

$$\beta_{V_V}$$
 = arctan  $\left(\frac{V_{V_A}}{V_E}\right)$  + deck pitch angle

NOTE: A Consistent set of units must be used in this equation.

The symbol for this quantity is  $\beta_{\nu_{\nu}}$ 

The value of this quantity is reported in Degrees and Radians.

## AIRCRAFT GEOMETRIC GLIDESLOPE ANGLE $\beta_{H_{\mathbf{w}}}$

This angle is determined by utilizing the distance from the ramp to touchdown  $(X_W)$  and height of main wheels at the ramp  $(H_W)$ . These values are substituted into the equation

$$\beta_{H_{\mathbf{w}}} = \arctan \left[ \frac{V_{E_{\mathbf{u}}} - SS}{V_{E_{\mathbf{u}}}} \times \frac{H_{\mathbf{w}}}{X_{\mathbf{w}}} \right] + \delta_{\mathbf{d}}$$

where SS is Ship Speed and  $\delta_d$  is angle of flight deck pitch at touchdown.

The quantity 
$$\frac{V_{E_{nl}}-SS}{V_{E_{nl}}}$$
 is a

correction factor for ship's forward motion during the time the aircraft flies from the Ramp position to Touchdown.

NOTE: A consistent set of units must be used in this equation. The symbol for this quantity is  $\beta_{H_{w}}$ 

5

#### LANDING WEIGHT W

The landing weight reported in the survey is determined from aircraft basic weight and the reported fuel state on aircraft final approach (the Ball State). The type and quantity of any external stores is also included in the determination of landing weight.

The symbol for this quantity is W

The value of this quantity is reported in Pounds.

## AIRCRAFT YAW ANGLE YAW

The Yaw Angle is the angle between the aircraft centerline and the aircraft flight path at the point of first main wheel touchdown. Positive YAW Angle is defined to be that orientation where a clockwise rotation of the flight path vector causes the vector to coincide with the aircraft centerline using a minimum angular rotation. Yaw Angle is determined from film data.

The symbol for this quantity is YAW ...

The value of this quantity is reported in Degrees and Radians.

#### AIRCRAFT PHI ANGLE 6

The phi angle is the angle between the aircraft centerline and the flight deck (or runway) centerline at the point of first main wheel touchdown. Positive Phi angle is defined to be that orientation where a clockwise rotation of the flight deck centerline causes it to coincide with the aircraft centerline using a minimum angular rotation. Phi angle is determined from film data.

The symbol for this quantity is  $\phi$ 

The value of this quantity is reported in Degrees and Radians.

#### AIRCRAFT FLIGHT PATH ANGLE F. P. A.

The Flight Path Angle is the angle between the aircraft flight path and the flight deck centerline at the point of touchdown. This measurement is determined from film data. Positive Flight Path Angle is defined to be that orientation where a clockwise rotation of the flight path vector causes the vector to coincide with the flight deck centerline using a minimum angular rotation.

The Symbol for this quantity is F. P. A.

The value of this quantity is reported in Degrees and Radians.

## HEIGHT OF MAIN WHEELS OVER THE RAMP $H_W$

The average height of the aircraft main landing gear wheels as it flies over the aircraft carrier ramp (aft end of flight deck) is determined from the film data. This information can also be provided for land based surveys utilizing an apppropriate reference line on the runway.

The symbol for this quantity is  $H_{\mathbf{w}}$ 

The value of this quantity is reported in Feet.

## HEIGHT OF THE HOOK AT THE RAMP $H_H$

The height of the aircraft arresting gear hook as it flies over the aircraft carrier ramp (aft end of flight deck) is determined from the film data. This quantity is only reported on carrier surveys.

The symbol for this quantity is  $H_H$ 

This quantity is reported in Feet.

## ANGLE OF FLIGHT DECK PITCH $\delta_{d_a}$

This angle is the pitch angle of the aircraft carrier flight deck with respect to the horizon. This data is recorded from the Ships Inertial Navigation System utilizing inputs to the Fresnel Lens (Mirror Landing Aid System). This data is reported at the time of the aircraft first main wheel touchdown. This parameter is reported only for carrier landings. The positive value of this quantity indicates that the stem of the ship is up.

The symbol for this quantity is  $\delta_{4}$ 

This quantity is reported in Degrees and Radians.

## ANGLE OF FLIGHT DECK ROLL $\delta_4$

This angle is the roll angle of the aircraft carrier flight deck with respect to the horizon. This data is recorded from the Ships Inertial Navigation System utilizing inputs to the Fresnel Lens (Mirror Landing Aid System). This data is reported at the time of the aircraft first main wheel touchdown. This parameter is reported only for carrier landings. The positive value of this quantity indicates that the starboard side of the ship is down.

The symbol for this quantity is  $\delta_{\alpha}$ 

This quantity is reported in Degrees and Radians.

## LIST OF SUBSCRIPTS

- FFE Free Flight Engagement
  - F Indicates that the data source is film data
  - R indicates data reported at the "over the ramp" position.
  - P Port
  - S Starboard
  - N Nose Wheel
  - A Average
  - r Roll
  - p Pitch
  - td Data reported at aircraft touchdown
  - d Data referenced to the Flight Deck

## STATISTICAL SYMBOLS

- N Number of Observations (data points)
- $\bar{x}$  Mean Value of a parameter
- P Probability
- S Standard Deviation of sample distribution
- $\alpha_3$  Skewness factor of sample distribution
- α<sub>4</sub> Kurtosis factor of sample distribution

## ANALYSIS

The relationship between the various parameters determined during a carrier landing loads survey is complex. Successfully performing a carrier landing is a significant accomplishment. The pilot is assisted in this effort by a system of instruments and landing aids which has evolved over the years. The sensitivity and accuracy of these instruments and equipment have a direct impact on the ability of the pilot to properly execute a carrier landing.

The principle instrumentation available to the pilot is the "Angle of Attack" indexer, the various cockpit glideslope displays and his observation of the fresnel lens system installed on the aircraft carrier. In addition, on many aircraft models, the pilot is assisted by an "Approach Power Compensator" or "Automatic Throttle Control". This equipment adjusts engine thrust to maintain a 1.0 g flight condition in response to various measured inputs, e.g normal acceleration, angle of attack and control surface position.

Table I is a listing of the mean values of principle landing parameters determined for the fleet aircraft covered by this survey. It provides data for both day and night landings.

Statistical tests were performed on the data. These were to determine if a significant difference exists in the mean values of the measured parameters for day and night landing operations. This was done for each model of aircraft. Table II identifies those combinations of parameters and aircraft models which exhibit statistically significant differences in mean values at a 95% confidence limit or higher.

The interrelationships between the various flight parameters involved in carrier landings is described in Table II. Those aircraft models which have a significant difference in landing weight should also show a significant difference in approach speed. Approach speed and landing weight are linearly related. When a significant difference between the values of "wind over deck" for day and night landings occurs, then engaging speeds should change for landings of the same landing weight. If landing weight and wind over deck change, then engaging speed and approach speed must change. Glideslope angle should remain constant, any change in sink speed should be accompanied with a corresponding change in engaging speed.

The only parameter which should remain constant during a carrier landing is glideslope angle. See Table III. The pilot is attempting to fly down a prescribed glideslope, normally 3.5 degrees, which is maintained by the carrier's fresnel lens system. Glideslope should be independent of aircraft landing weight, wind over deck or even aircraft type. Table I indicates that the survey data varies from the expected result. The mean value of instantaneous glideslope was 2.9 degrees during the day and 3.1 degrees at night. The small variations of survey glideslope angle from the expected value of 3.5 degrees can

be attributed to the tolerances on the measured values of sink speed  $(\pm \ 1.0 \ \text{ft/sec})$  and engaging speed  $(\pm \ 2.0 \ \text{knots})$  for individual landings used in the calculation, along with rounding errors in the recorded deck pitch and minor angular misalignments in camera installation.

The value of instantaneous glideslope determined from our analysis program is calculated from the value of the tangent of the ratio of the average sink speed at touchdown with the engaging speed at touchdown.

 $B_{VV}$  = tan (Vva/Ve) + flight deck pitch angle

This equation correctly provides the angle of the aircraft with the horizon. This is the same angle that the pilot is following as he attempts to land by following the 3.5 degree angle established by the fresnel lens system. At any instant in time, the pilot observes the "ball" centered in the lens. The lens mechanism is stabilized to compensate for carrier flight deck motion, (pitch and roll).

Review of the measured approach speed listed in table I indicates that these values are higher than would be expected for the reported value of mean landing weight. These values were compared with the appropriate NATOPS approach speed curves. These comparisons are listed in table IV. Plots of the individual landings approach speed versus landing weight were generated and are provided as figures 1 throught 16. Day and night plots are provided for all model aircraft in this Survey except the TA-3, which had only 23 landings recorded. The corresponding NATOPS curves were included in the plots. As can be seen from these curves, the aircraft are flying approach speeds higher than the recommended NATOPS values.

The recommended NATOPS approach speed curves provide a relationship between aircraft approach speed and landing weight. The typical variation is to add one to two knots of approach speed for each additional thousand pounds of aircraft landing These curves are prepared from flight test data for an aircraft flying an "on-speed" approach at the proper aircraft "angle of attack" and descending on the prescribed 3.5 degree These curves also must assume a value of "wind over glideslope. deck" to convert the recommended approach speed to a value of aircraft engaging speed. The engaging speed limits are established by limits on the aircraft arresting gear hook loads, as well as the energy absorption capabilities of the arresting gear on the aircraft carrier. If any of these variables are different during an actual carrier landing, then the reported approach speed will vary from the NATOPS value.

The sensitivity of aircraft approach speed to angle of attack varies considerably for different aircraft models. The difference in a "slightly fast" approach over an "on-speed" approach for an A-7E can be as much a six knots in approach speed. Other models vary by two or three knots for the same

range of angle of attack variation. The Approach Speed for an A-6 Aircraft increases by 4.5 knots if external stores are carried during the landing. These variations account for asignificant portion of the differences in A-6 and A-7 engaging speeds listed in table I.

Similarly, the tolerances in glideslope angle can have an effect on the reported value of aircraft approach speed. The aircraft carrier provides glideslope information to the pilot by means of an Automatic Carrier Landing System. This information is provided to the pilot both on cockpit displays and on the "HEADS UP DISPLAY". The full scale deflection of these displays indicate a vertical misalignment of the aircraft to the glideslope of  $\pm$  1.4 degrees. For small values of glideslope misalignment, the instrumentation will provide a proportional deflection of the glideslope displays. Given the range of this proportional indication, a variation of 10 % , (  $\pm$  0.14 degrees ) would not be an unreasonable tolerance to expect on the angle being maintained by the pilot. A similar or greater tolerance would be expected if the pilot was flying without using the ACLS system and making a non-precision visual approach.

As an additional check on the survey results, the values of aircraft engaging speed plus 20 knots were plotted against landing weight for the F-14, F-18 and A-7E aircraft. These plots are included as figures 17 thru 22. The value of twenty knots was chosen since MIL-A-8863 defines engaging speed to be approach speed minus twenty knots. Our program calculates approach speed from engaging speed and reported value of "wind over deck". Engaging speed is derived directly from our film image data. These plots show considerably better agreement between the reported data and the NATOPS curves, particularly for the night landing data.

Aircraft sink speed was also plotted as a function of engaging speed for the F-14, F-18 and A-7 aircraft. These plots are included as figures 23 thru 28. A tolerance band generated from the sink speed equations of table I of MIL-A-8863 was included on the these plots. The sink speed data from this survey does fall in the band defined by the specification.

In light of the above considerations, the observed variations in aircraft landing performance observed in this survey can readily be ascribed to these instrumentation tolerances and the various flight conditions experienced by the pilots. The observed differences between day and night landings, higher glideslope angle, higher sink speeds and better agreement of the data with the recommended NATOPS approach speed at night, can be explained by the increased time that the pilot has to "fine tune" his approach. At night, the pace of landing operations is considerably slower and the pilot is established on his glideslope at a significantly greater distance from the ship than during daylight visual flight operations. Typically, the pilot turns onto the glideslope at a distance of 3 to 3.5 miles at night compared to distance of from one to one and one half miles from the

ship during the day. Additionally, it must be noted that the approach speed reported from our survey depends on the accuracy of the "wind over deck" measurement taken onboard the aircraft carrier. Local disturbances caused by the ships configuration and motion can cause this value to vary from the wind conditions experienced by the aircraft in the air mass behind the ship. The value of NATOPS Approach Speed depends on an accurate estimate of Aircraft Landing Weight which is based on fuel state reported by the pilot on final approach, basic weight of the aircraft involved and the weight of any external stores carried on the aircraft. An error of several hundred pounds could be made in this weight calculation. These considerations, coupled with a loss of visual references at night, which may focus the pilots attention on his landing aids, are sufficient to account for the minor differences between day and night landings observed during this survey.

#### CONCLUSIONS

The data analyzed from Survey 45 leads to the following conclusions:

- 1. Statistically significant differences in the mean values of sink speed, engaging speed and glideslope angle exist between day and night landing of the F-14, F-18 and A-6E aircraft. Of these three parameters, only the difference in engaging speed was significant for the A-7E. Only the F-18 and EA-6B showed an increase in the variation of glideslope angle at night when compared to the Fresnel lens setting. For the bulk of the night landings observed (80%), the pilots maintained glideslope more accurately at night than during the day. This may reflect the reduced pace of night flight operations, and the longer night landing patterns which gives the pilot a greater opportunity to establish his glideslope and angle of attack.
- 2. The mean values of aircraft approach speeds determined by this survey are higher than would be expected from review of the appropriate NATOPS approach speed versus landing weight curves. This variation ranged from sixteen knots for the F-18 night landings to six knots for the E-2C day landings of this survey. The distribution of measured values of sink speed are less than the sink speed values calculated from measured engaging speed as described in Mil-A-8863. The difference in mean sink speed ranged from 4.5 ft/sec lower for both day F-14 and night F-18 landings to 2.0 ft/sec lower for night F-14 landings.
- 3. The NATOPS approach speed curves consider only the effect of landing weight on approach speed. Individual landings are not fully defined by the NATOPS guidance. The variation in aircraft approach speed with landing weight, wind over deck conditions, external stores configuration and aircraft angle of attack are more complex than indicated by the NATOPS approach speed curves. The skill and training of the pilots are also significant in interpreting these survey results.

## RECOMMENDATIONS FOR ADDITIONAL ANALYSIS AND INVESTIGATIONS

Review of the results of this survey lead to the following recommendation to the NAVAL AIR SYSTEMS COMMAND for additional analysis and investigations of aircraft landing loads:

- 1. That additional studies and analysis of carrier landings be authorized to determine the effect of variations in ship speed and "wind over deck" conditions on aircraft landing performance.
- 2. That an analytical method be developed to establish aircraft engaging speed from carrier arresting gear ram runout. This would provide an supplementary means of monitoring aircraft engaging speeds from the arresting gears recovery log sheets, which are routinely recorded on the ship and forwarded to the NAVAL AIR ENGINEERING CENTER, Lakehurst N.J. This would permit adverse trends and potential problems to be identified prior to performing a full scale carrier survey. This would aid in planning and directing future survey efforts.
- 3. The substantial data base of carrier landings included in this report provide an excellent source of input data for the analysis of carrier landings. The data base on field landings for carrier aircraft, which account for 50% of all landings of these aircraft, is a candidate for further study. The analysis of field landings performed during 1981 at NAS OCEANA during Survey 39 identified significantly higher sink speeds than expected for those landings. Additional surveys should be authorized to verify the adequacy of the field landings sink speed distribution in the aircraft design specification MIL-A-8866(ASG).
- 4. An additional area of study is the short take off and landing (STOL) operation of the AV-8B Harrier. Operational landings of this model have never been recorded by this activity, and only hover landings of the AV-8A have been surveyed.

TABLE 1: DAY/NIGHT MEAN LANDING VALUES COMPARISON

Parameter		AIRCRAFT TYPE						
		F-14	<b>F-18</b>	A-6E	A-7E	EA-6B	B-20	8-3A
NO. OF	DAY	157	190	68	151	56	79	165
LANDINGS	NIGHT	95	76	39	58	37	80	133
AVG. SINK	DAY	10	12	10	12	10	8	8
SPEED	NIGHT	12	11	11	11	10	8	9
ENGAGING	DAY	113	119	102	119	107	84	94
SPEED	NIGHT	109	121	101	112	109	85	91
LANDING	DAY	47788	30659	32722	23798	39132	43302	36764
WEIGHT	NIGHT	47953	30920	34146	23524	40086	43281	36740
GLIDE	DAY	2.8	3.1	3.2	3.1	3.0	2.9	2.8
SLOPE	NIGHT	3.4	2.7	3.5	3.3	2.8	3.2	2.8
APPROACH	DAY	140	145	129	145	134	108	122
SPEED	NIGHT	140	148	127	140	137	109	122
PITCH	DAY	7.8	4.6	8.3	8.2	10.8	7.6	4.5
ANGLE	NIGHT	7.5	4.7	8.2	8.0	10.2	7.6	4.7
PITCH	DAY	1.8	0.3	0.5	1.0	1.6	-0.1	-0.
RATE	NIGHT	1.2	0.8	0.8	0.4	2.4	0.2	-0.0
WIND	DAY	28	26	26	26	27	24	2
OVER	NIGHT	31	26	26	29	29	24	32

TABLE 2: DAY/NIGHT LANDING COMPARISON USING A SIGNIFICANTS

STATISTICAL TEST FOR THE MEAN DIFFERENCE OF TWO

DATA SAMPLES (95% CONFIDENCE OR HIGHER)

			AIRCRAI	TT TYPE			
PARAMETER	F-14	F-18	A-6E	A-7E	EA-6B	B-2C	S-3A
AVG. SINK SPEED	99%	99%	99%			98%	
ENGAGING SPEED	99%	99%	95%	99%			99%
LANDING WEIGHT			99%		99%		
GLIDE SLOPE	99%	99%	95%		· · · · · · · · · · · · · · · · · · ·	95%	
APPROACH SPEED		99%	95%	99%	98%		
PITCH ANGLE							
PITCH RATE	95%						
WIND OVER DECK	99%			99%	99%		99%

TABLE 3: SURVEY 45 DATA ANALYSIS

AIRCRAFT MODEL	LANDING TYPE	BETA VV INSTANTANEOUS GLIDESLOPE	BETA HW GEOMETRIC GLIDESLOPE	Ships Deck Pitch
F-14A	DAY NIGHT	2.8 3.4	3.1	-0.3 -0.3
F-18	DAY NIGHT	3.1 2.7	3.2	-0.3 -0.4
A-6E	DAY NIGHT	3.2 3.5	3.3	-0.4 -0.4
A~7E	DAY NIGHT	3.1 3.3	3.4	-0.2 -0.2
EA-6B	DAY NIGHT	3.0 2.8	3.1	-0.3 -0.4
E-2C	DAY NIGHT	2.9 3.2	3.2	-0.1 -0.2
S-3A	DAY NIGHT	2.8 2.8	3.2	-0.3 -0.4
TA-3	DAY	3.2	3.7	-0.3
T-2C	DAY	3.0	2.8	-0.1
TA-4	DAY	2.8	3.2	-0.3

TABLE 4: SURVEY 45 DATA ANALYSIS

				NATOPS		EXCESS	NATOPS	
		MEAN	MEAN	RECOMMENDED	WIND	WIND	PLUS	
AIRCRAFT	LANDING	APPROACH	LANDING	APPROACH	OVER	OVER	<b>EXCESS</b>	
MODEL	TYPE	SPEED	WEIGHT	SPEED	DECK	DECK	WIND	DELTA
F-14A	DAY	140	47788	129	28	8	136.5	3.9
	NIGHT	140	47953	129	31	11	139.8	-0.1
F-18	DAY	145	30659	132	26	6	137.6	7.6
	NIGHT	148	30920	132	27	7		8.82
A-6E	DAY	129	32722	114	26	6	119.88	8.82
A-0E.	NIGHT	127	34146	116	26	6	122.48	4.22
						_		
A-7E	DAY NIGHT	145 140	23798 23524	128 128	26 29	6 9	134.3 136.6	10.6 3.8
	10.00							0.0
EA-6B	DAY	134	39132	120	27	7	127.2	6.8
	NIGHT	137	40086	122	29	9	130.6	6.7
E-2C	DAY	108	43302	102	24	4	105.63	1.97
- <u></u>	NIGHT	109	43281	102	24	4	105.6	2.9
S-3A	DAY	122	36764	111	27	7	118.36	3.34
<b>0</b> -0/1	NIGHT	122	36740	111	32	12	123.32	-0.92

# TABLE 5: SURVEY 45 DAY CARRIER LANDINGS SUMMARY FOR F-14A MODEL AIRCRAFT

	number Of		STANDARD	ALPHA	ALPHA
Parameter	LANDINGS	MEAN	DEVIATION	3	4
Vvp	158	10.4	2.59	-0.58	3.48
Vvs	157	10.2	2.69	-0.33	3.66
Vva	157	10.3	2.55	-0.66	3.61
Vva ff	30	9.3	3.13	-0.34	2.49
Vvn	158	9.7	2.57	-0.43	3.81
Kle	158	1.1	0.10	0.26	2.95
Kle ff	30	1.09	0.11	0.73	3.70
Vw	158	28	3.40	0.39	1.89
Vef	158	113	4.44	-0.01	2.65
Vpaf	158	140	4.03	-0.01	2.80
Vpamin	156	121	2.06	-0.35	2.24
Kvpamin	156	1.17	0.03	0.04	2.65
PITCH ramp	156	9.2	1.15	0.04	3.12
PITCH td	158	7.8	1.17	0.61	4.62
PITCH td ff	30	8.1	1.18	0.79	3.07
ROLL ramp	156	-0.2	2.50	0.33	3.44
ROLL td	158	-0.6	2.10	0.10	3.34
ROLL td ff	30	-0.5	1.39	0.82	3.46
PITCH RATE	157	1.78	2.18	1.10	3.82
ROLL RATE	157	0.4	5.22	-1.55	10.54
DECK PITCH	153	-0.3	0.20	0.36	3.64
DECK ROLL	153	-0.3	1.17	0.17	2.55
OFFCENTER	158	-12.9	4.16	0.21	3.69
RAMP TO					
TD DISTANCE	158	246	42.8	-0.78	4.35
WEIGHT	156	47788	1629	-0.32	2.22
WHEEL HEIGHT	156	15.4	3.52	0.14	3.20
HOOK HEIGHT	156	10.7	3.60	0.13	3.23
GEOMETRIC					
GLIDESLOPE	156	3.1	0.58	0.13	2.76
INSTANTANEOUS					
GLIDESLOPE	157	2.8	0.78	-0.61	3.51
WIRE #	113	2.6	0.92	-0.08	2.17
PHI RATE	158	0.5	2.31	-2.30	22.45
PHI TD	158	1.8	1.74	-0.62	3.70
F.P.A.	158	-3.1	1.10	-1.02	6.04
YAW	158	4.9	2.17	-0.27	3.40

TABLE 6: SURVEY 45 NIGHT CARRIER LANDINGS SUMMARY
FOR F-14A MODEL AIRCRAFT

	NUMBER OF		STANDARD	ALPHA	ALPHA
Parameter	LANDINGS	MEAN	DEVIATION	3	4
Vvp	95	12.1	2.93	-0.11	3.22
Vvs	95	11.6	2.92	-0.28	2.92
Vva	95	11.9	2.76	-0.45	3.38
Vva ff	7	12.2	1.99	0.58	1.89
Vvn	95	10.9	2.75	-0.06	3.75
Kle	95	1.05	0.11	0.96	4.99
Kle ff	7	1.04	0.5	0.29	1.08
Vw	95	31	5.00	-0.08	1.38
Vef	95	109	6.56	0.75	4.15
Vpaf	95	140	5.88	1.16	6.94
Vp'amin	95	121	1.93	-0.31	2.99
Kvp'amin	95	1.16	0.05	0.92	5.91
PITCH td	95	7.5	1.34	0.67	5.89
PITCH td ff	7	8.4	1.19	-0.07	2.04
ROLL td	95	-0.3	2.71	-0.02	3.78
ROLL td ff	7	0.2	1.12	-0.02	1.25
PITCH RATE	95	1.2	1.96	1.15	4.19
ROLL RATE	95	1.3	6.85	0.20	3.48
DECK PITCH	95	-0.3	0.20	0.14	3.04
DECK ROLL	95	-0.4	1.42	-1.64	9.47
OFFCENTER	95	-12.6	5.07	0.88	7.45
RAMP TO					
TD DISTANCE	95	256	42	-0.29	2.68
WEIGHT	95	47953	1525	-0.26	2.93
INSTANTANEOUS					
GLIDESLOPE	95	3.36	0.89	-0.57	3.49
WIRE#	69	2.8	0.94	-0.40	1.81
PHI RATE	95	-0.1	2.72	-0.96	7.94
PHI TD	95	2.8	1.63	0.02	2.44
F.P.A.	95	-3.4	1.9	-0.19	4.96
YAW	95	6.2	2.88	0.27	2.79

# TABLE 7: SURVEY 45 DAY CARRIER LANDINGS SUMMARY FOR F-18 MODEL AIRCRAFT

	number of		STANDARD	ALPHA	ALPHA
PARAMETER	LANDINGS	MEAN	DEVIATION	3	4
Vvp	196	12.0	2.27	0.02	3.79
Vvs	196	12.0	2.30	-0.34	4.65
Vva	196	12.0	2.17	-0.05	3.95
Vva ff	100	12.0	1.91	0.58	2.11
Vvn	196	10.6	2.33	-0.07	3.40
Kie Kle ff	196	1.1	0.08	0.00	3.43
<del></del>	<del></del>	26	0.06	-0.37	2.29
Vw	195		2.89	0.21	1.76
Vef	196	118	7.62	-2.31	12.05
Vpaf	195	······	7.31	-2.15	11.56
Vpamin	185	134	2.53	-0.49	2.48
Kvpamin	185	1.08	0.05	-2.58	15.09
PITCH ramp	191	4.8	0.99	-1.68	10.59
PITCH td	196	4.6	1.11	-0.30	3.11
PITCH td ff	10	5.4	0.53	-1.39	4.25
ROLL ramp	191	0.4	3.28	0.12	3.03
ROLL td	196	0.2	2.49	0.43	5.08
ROLL td ff	10	0.2	1.88	-0.51	2.20
PITCH RATE	196	0.25	1.91	-0.22	4.09
ROLL RATE	196	0.2	7.15	-0.34	5.83
DECK PITCH	195	-0.3	0.17	0.00	2.97
DECK ROLL	195	-0.4	1.07	-0.47	3.29
OFFCENTER	196	-9.4	5.14	0.99	6.17
RAMP TO			İ		
TD DISTANCE	196	254	38.3	0.11	2.64
WEIGHT	185	30659	1151	-0.45	2.44
WHEEL HEIGHT	191	16.8	2.78	0.17	3.07
HOOK HEIGHT	191	13.6	2.77	0.20	2.99
GEOMETRIC			:		
GLIDESLOPE	191	3.2	0.50	-0.07	3.82
INSTANTANEOUS			<u> </u> 		
GLIDESLOPE	196	3.1	0.63	-0.04	3.74
WIRE #	152	2.9	0.72	0.03	2.14
PHI RATE	191	2.9	3.31	-0.59	5.01
PHI TD	191	-1.5	3.19	0.54	2.22
F.P.A.	196	1.7	3.44	0.53	4.95
YAW	196	-3.1	1.21	0.55	2.90

TABLE 8: SURVEY 45 NIGHT CARRIER LANDINGS SUMMARY
FOR F-18 MODEL AIRCRAFT

	NUMBER OF		STANDARD	ALPHA	ALPHA
PARAMETER	LANDINGS	MEAN	DEVIATION	3	4
Vvp	77	10.6	2.69	0.08	2.91
Vvs	77	10.7	2.78	0.19	2.77
Vva	77	10.7	2.74	0.15	2.89
Vva ff	2	9.5	1.14	0.00	1.00
Vvn	77	9.8	2.53	-0.27	2.70
Kle	77	1.1	0.15	2.28	13.39
Kle ff	2	1.1	0.05	0	1.00
Vw	77	27	3.10	-0.71	2.35
Vef	77	121	5.36	0.28	3.08
Vpaf	77	148	6.30	0.02	2.57
Vp'amin	77	135	4.19	5.47	41.32
Kvp'amin	77	1.1	0.05	-0.77	5.17
PITCH td	77	4.6	0.86	-0.47	4.75
PITCH td fr	2	6.0	0.35	0.00	1.00
ROLL td	77	0.2	2.61	-0.64	5.58
ROLL td ff	2	1.8	0.40	0.00	1.00
PITCH RATE	77	0.6	3.50	-2.69	17.22
ROLL RATE	77	-0.6	7.53	0.58	5.84
DECK PITCH	77	-0.4	0.19	-0.33	2.58
DECK ROLL	77	-0.3	0.84	-0.55	3.66
OFFCENTER	77	-12.5	4.35	-0.05	3.43
RAMP TO					
TD DISTANCE	77	252	39	-0.11	2.68
WEIGHT	77	30920	989	0.24	2.95
INSTANTANEOUS					
GLIDESLOPE	77	2.62	0.78	0.13	3.21
WIRE#	63	2.9	0.75	0.21	1.82
PHI RATE	76	2.5	5.01	-1.31	8.64
PHI TD	76	-0.9	2.99	0.33	2.09
F.P.A.	77	-2.9	7.45	7.48	62.61
YAW	77	2.1	7.61	-5.28	40.54

## TABLE 9: SURVEY 45 DAY CARRIER LANDINGS SUMMARY FOR A-6E MODEL AIRCRAFT

PARAMETER	NUMBER OF LANDINGS	MEAN	STANDARD DEVIATION	Alpha 3	ALPHA
Vvp	68	10.0	1.66	-0.08	2.73
Vvs	68	9.8	1.41	0.06	3.09
Vva	68	9.9	1.44	-0.05	3.13
Vva ff	6	10.1	1.62	-0.03	1.67
Vvn	68	8.3	2.40	-0.70	5.59
Kle	68	1.0	0.07	-0.05	2.33
Kle ff	6	1.0	0.07	-0.23	2.11
Vw	68	26	2.08	0.06	2.53
Vef	68	102	3.92	0.01	2.59
Vpaf	68	129	4.52	0.20	2.76
Vpamin	68	109	2.80	-0.18	2.17
Kvpamin	68	1.19	0.04	-0.21	2.98
PITCH ramp	68	9.8	0.88	0	3.25
PITCH td	68	8.3	1.17	-0.27	2.60
PITCH td ff	6	8.6	1.16	-0.17	1.43
ROLL ramp	68	0.4	2.17	0.86	4.11
ROLL td	68	0.2	1.79	1.28	6.25
ROLL td ff	6	0.3	1.58	-0.11	1.83
PITCH RATE	68	0.51	2.06	-0.21	2.96
ROLL RATE	68	0.6	5.08	0.01	4.53
DECK PITCH	51	-0.2	0.21	-0.16	3.91
DECK ROLL	51	-0.4	0.63	1.00	8.12
OFFCENTER	68	-11	2.88	0.65	3.77
RAMP TO					
TD DISTANCE	68	268	23.4	-0.20	2.18
WEIGHT	68	32722	1080	-0.15	2.18
WHEEL HEIGHT	68	16.6	2.50	0.88	4.39
HOOK HEIGHT	68	11.3	2.55	0.84	4.20
GEOMETRIC					
GLIDESLOPE	68	3.3	0.44	0.29	3.01
INSTANTANEOUS					
GLIDESLOPE	68	3.2	0.50	-0.44	2.91
WIRE#	54	3.3	0.68	-0.41	2.17
PHI RATE	68	2.7	2.66	0.45	2.42
PHI TD	68	-2.7	3.78	0.17	1.64
F.P.A.	68	-3.2	0.89	1.07	5.55
YAW	68	0.6	3.53	0.08	1.76

TABLE 10: SURVEY 45 NIGHT CARRIER LANDINGS SUMMARY
FOR A-6E MODEL AIRCRAFT

	Number Of		STANDARD	ALPHA	ALPHA
PARAMETER	LANDINGS	MEAN	DEVIATION	3	AUFRA 4
Vvp	39	10.9	2.06	-0.09	2.83
Vvs	39	10.8	1.99	-0.27	3.28
Vva	39	10.9	2.01	-0.26	3.09
Vva ff	7	8.7	2.16	-1.22	2.95
Vvn	39	9.3	2.38	-0.03	2.82
Kle	39	1.0	0.11	0.83	3.53
Kle ff	7	1.1	0.11	0.88	2.23
Vw	39	26	2.75	1.46	3.53
Vef	39	101	3.65	0.65	3.45
Vpaf	39	127	3.96	0.24	2.64
Vp'amin	39	111	1.92	-2.14	9.66
Kvp'amin	39	1.14	0.03	0.22	2.44
PITCH td	39	8.2	1.18	0.53	4.94
PITCH td ff	7	8.5	0.70	0.09	2.06
ROLL td	39	0.4	1.75	-0.04	2.28
ROLL td ff	7	0.2	1.63	-0.04	1.33
PITCH RATE	39	0.8	2.82	0.27	3.51
ROLL RATE	39	0.9	4.61	0.17	3.99
DECK PITCH	39	-0.2	0.32	0.07	1.21
DECK ROLL	39	-0.4	0.69	-0.63	6.97
OFFCENTER	39	-11.0	3.87	-0.04	2.89
RAMP TO					
TD DISTANCE	39	265.38	28	0.52	2.52
WEIGHT	39	34146	1161	-2.04	9.07
INSTANTANEOUS					
GLIDESLOPE	39	3.50	0.79	-0.18	2.40
WIRE #	31	3.1	0.80	-0.12	1.57
PHI RATE	39	2.3	2.26	2.47	3.01
PHI TD	39	-1.5	4.37	-0.71	2.2
F.P.A.	39	-2.8	1.18	0.67	3.12
YAW	39	1.3	4.19	-0.61	2.54

## TABLE 11: SURVEY 45 DAY CARRIER LANDINGS SUMMARY FOR A-7E MODEL AIRCRAFT

	number of		STANDARD	ALPHA	ALPHA
PARAMETER	LANDINGS 151	MEAN 11.6	DEVIATION	2 0.06	0.70
Vvp Vvs	151	11.4	1.80 1.87	-0.06 -0.29	2.73 3.09
Vva	151	11.5	1.77	-0.29	3.09
Vva ff	7	10.5	1.34	0.36	1.67
Vvn	151	11.5	2.00	-0.73	5.59
Kle	151	1.1	0.98	0.73	2.33
Kle ff	7	1,1	0.08	-0.27	2.11
Vw	151	26	1.93	1.34	2.53
Vef	151	119	5.36	-0.35	2.59
Vpaf	151	145	5.30	0.08	2.76
Vpamin	141	134	2.63	-0.47	2.17
Kvpamin	141	1.08	0.04	-0.17	2.98
PITCH ramp	147	8.8	1.05	0.03	3.25
PITCH td	151	8.2	1.38	0.23	2.60
PITCH td ff	7	10.3	1.32	0.70	1.43
ROLL ramp	147	0.6	2.57	-0.17	4.11
ROLL td	151	-0.6	1.98	0.22	6.25
ROLL td ff	7	0.3	1.50	-1.57	1.83
PITCH RATE	151	1.04	3.00	-0.06	2.96
ROLL RATE	151	1.9	5.40	0.06	4.53
DECK PITCH	128	-0.2	0.17	-0.49	3.91
DECK ROLL	128	-0.5	0.63	1.41	8.12
OFFCENTER	151	-9.2	4.16	1.08	3.77
RAMP TO					
TD DISTANCE	151	253	32.9	-0.14	2.18
WEIGHT	141	23799	927	-0.44	2.18
WHEEL HEIGHT	147	16.3	2.48	0.02	4.39
HOOK HEIGHT	147	12.9	2.50	-0.06	4.20
GEOMETRIC					
GLIDESLOPE	147	3.4	0.45	-0.33	3.01
INSTANTANEOUS					
GLIDESLOPE	151	3.1	0.52	-0.05	2.91
WIRE #	119	2.9	0.73	-0.24	2.17
PHI RATE	151	3.1	2.33	0.06	2.42
PHI TD	151	-2.3	2.71	0.61	1.64
F.P.A.	151	-3.4	0.8	-0.64	5.55
YAW	151	1.2	2.86	0.56	1.76

TABLE 12: SURVEY 45 NIGHT CARRIER LANDINGS SUMMARY
FOR A-7E MODEL AIRCRAFT

PARAMETER	number of Landings	MEAN	STANDARD DEVIATION	ALPHA 3	ALPHA
Vvp	58	11.3	2.54	-0.05	2.02
Vvs	58	11.2	2.51	-0.01	2.75
Vva	58	11.3	2.46	-0.04	2.36
Vvn	58	11.2	2.40	-0.36	2.76
Kle	58	1.1	0.10	0.74	3.20
Vw	58	29	3.71	-0.20	1.16
Vef	58	112	8.72	0.70	5.26
Vpaf	58	140	9.49	1.20	5.34
Vp'amin	58	134	3.71	-1.56	6.08
Kvp'amin	58	1.05	0.07	1.00	4.28
PITCH td	58	8.0	1.59	0.63	3.36
ROLL td	58	-0.6	1.72	-0.42	3.03
PITCH RATE	58	0.4	3.00	0.18	3.60
ROLL RATE	58	0.9	8.10	-0.46	3.12
DECK PITCH	58	-0.2	0.23	-0.23	2.68
DECK ROLL	58	0.2	0.84	1.1	3.89
OFFCENTER	58	-8.5	4.01	0.12	3.54
RAMP TO					
TD DISTANCE	58	271	36	-0.51	2.78
WEIGHT	58	23524	1280	-1.45	5.64
INSTANTANEOUS					
GLIDESLOPE	58	3.25	0.82	0.02	2.68
WIRE #	47	3.2	0.87	-0.67	2.50
PHI RATE	58	-0.5	2.97	0.51	3.99
PHI TD	58	2.3	1.46	-2.14	11.51
F.P.A.	58	-3.3	2.22	0.72	4.51
YAW	58	5.5	2.68	-0.37	2.58
PHI RATE	39	2.3	2.26	2.47	3.01
PHI TD	39	-1.5	4.37	-0.71	2.2
F.P.A.	39	-2.8	1.18	0.67	3.12
YAW	39	1.3	4.19	-0.61	2.54

## TABLE 13: SURVEY 45 DAY CARRIER LANDINGS SUMMARY FOR RA-6B MODEL AIRCRAFT

	NUMBER	_			
	OF		STANDARD	ALPHA	ALPHA
Parameter	LANDINGS	MEAN	DEVIATION	3	4
Vvp	56	10.6	1.86	-0.17	2.76
Vvs	56	10.3	1.81	0.51	3.39
Vva	56	10.4	1.73	0.03	2.77
Vva ff	5	8.2	1.63	0.22	_1.38
Vvn	56	6.6	3.42	-0.23	1.79
Kle	56	1.0	0.09	0.19	2.18
Kle ff	5	1.1	0.07	0.34	1.85
Vw	56	27	3.66	0.02	1.62
Vef	56	107	5.32	0.53	3.23
Vpaf	56	134	6.08	0.16	2.55
Vpamin	53	119	2.39	0.29	3.22
Kvpamin	53	1.13	0.05	0.28	2.98
PITCH ramp	56	12.3	1.32	-0.27	3.07
PITCH td	56	10.8	1.41	0.07	2.46
PITCH td ff	5	11.7	0.40	-0.41	2.20
ROLL ramp	56	0.7	2.91	0.19	2.40
ROLL td	56	0.0	2.62	1.03	4.84
ROLL td ff	5	-0.8	0.42	0.12	1.75
PITCH RATE	56	1.6	2.33	0.68	3.30
ROLL RATE	56	1.1	4.84	0.31	3.78
DECK PITCH	56	-0.3	0.17	-0.19	3.40
DECK ROLL	56	-0.4	0.86	-0.44	4.05
OFFCENTER	56	-9.6	4.60	0.43	3.57
RAMP TO				· · · · · · · · · · · · · · · · · · ·	
TD DISTANCE	56	246	33.8	-0.81	3.93
WEIGHT	53	39132	1579	0.35	0.36
WHEEL HEIGHT	56	15.8	2.27	0.71	3.46
HOOK HEIGHT	56	9.8	2.41	0.60	3.20
GEOMETRIC					
GLIDESLOPE	56	3.1	0.52	0.86	5.44
INSTANTANEOUS					
GLIDESLOPE	56	3.0	0.57	-0.47	3.04
WIRE#	49	3.1	0.69	-0.16	2.10
PHI RATE	56	1.1	3.01	-0.34	3.54
PHI TD	56	0.1	2.2	-0.71	2.81
F.P.A.	56	-2.9	1.43	-0.69	6.25
YAW	56	3.0	2.60	0.31	4.65

TABLE 14: SURVEY 45 NIGHT CARRIER LANDINGS SUMMARY
FOR EA-6B MODEL AIRCRAFT

PARAMETER	number of Landings	MEAN	STANDARD DEVIATION	ALPHA 3	ALPHA
Vvp	37	10.3	2.49	-0.01	1.98
Vvs	37	9.9	2.12	0.20	2.17
Vva	37	10.1	2.21	0.02	2.08
Vva ff	3	9.3	2.96	0.34	1.50
Vvn	37	6.7	3.41	0.31	2.81
Kle	37	1.1	0.09	0.47	2.59
Kle ff	3	1.1	0.09	-0.71	1.50
Vw	37	29	1.62	-0.63	2.42
Vef	37	109	6.63	1.77	9.45
Vpaf	37	137	6.65	2.20	10.97
Vp'amin	37	120	2.22	-0.62	3.42
Kvp'amin	37	1.14	0.07	2.79	13.86
PITCH td	37	10.2	1.63	0.21	2.50
PITCH td ff	3	11.8	1.05	-0.63	1.50
ROLL td	37	1.1	2.33	-0.07	2.65
ROLL td ff	3	-1.5	2.00	0.02	1.50
PITCH RATE	37	2.4	3.20	0.71	2.70
ROLL RATE	37	1.9	5.99	0.41	2.86
DECK PITCH	37	-0.4	0.20	0.69	4.23
DECK ROLL	37	-0.1	0.83	0.01	2.68
OFFCENTER	37	-11.8	3.88	0.46	3.66
RAMP TO					<del></del>
TD DISTANCE	37	249	40	0.08	2.90
WEIGHT	37	40086	1476	-0.57	3.32
INSTANTANEOUS					
GLIDESLOPE	37	2.74	0.69	-0.23	2.23
WIRE#	27	2.6	0.82	0.78	1.92
PHI RATE	37	3.7	4.27	-0.43	2.89
PHI TD	37	-1.7	3.07	0.18	1.76
F.P.A.	37	-3.9	1.8	1.15	5.27
YAW	37	2.2	3.62	0.36	2.23

TABLE 15: SURVEY 45 E-2C DAY CARRIER LANDING DATA SUMMARY

	NUMBER OF		STANDARD	Alpha	ALPHA
PARAMETER	LANDINGS	MEAN	DEVIATION	3	4
Vvp	79	7.7	1.93	-0.08	2.77
Vvs	79	7.5	1.94	0.09	4.09
Vva	79	7.5	1.75	-0.32	3.17
Vva ff	4	6.7	1.17	0.38	1.93
Vvn	79	6.2	2.29	-0.39	3.11
Kle	79	1.0	0.11	0.46	3.16
Kle ff	4	1.1	0.8	0.49	1.63
Vw	79	24	1.24	-1.43	4.51
Vef	79	83	4.24	-0.69	7.45
Vpaf	79	108	4.30	-0.72	8.75
Vsp'a	78	86	1.10	0.29	2.76
Kvsp'a	78	1.25	0.03	0.42	3.61
PITCH ramp	75	9.0	1.54	-1.83	11.78
PITCH td	79	7.6	1.18	-1.03	7.78
PITCH td ff	4	8.9	1.46	0.45	1.69
ROLL ramp	75	1.0	2.82	0.69	3.54
ROLL td	79	0.4	2.34	0.41	4.06
ROLL td ff	4	1.8	1.01	-0.04	1.10
PITCH RATE	79	-0.1	2.23	0.37	4.80
ROLL RATE	79	0.3	4.95	-0.34	3.75
DECK PITCH	79	-0.1	0.21	0.29	3.09
DECK ROLL	79	0.2	0.77	0.46	3.88
OFFCENTER	79	-11.1	3.61	-0.30	2.63
RAMP TO					
TD DISTANCE	66	253.18	4.74	0.57	3.60
WEIGHT	78	43302	1115	0.33	2.78
WHEEL HEIGHT	75	15.2	2.44	0.16	2.70
HOOK HEIGHT	75	9.4	2.57	0.31	2.66
GEOMETRIC					
GLIDESLOPE	75	2.7	0.49	0.53	3.45
INSTANTANEOUS					
GLIDESLOPE	79	2.9	0.75	-0.05	2.81
WIRE #	65	2.6	0.68	0.54	2.60
PHI RATE	79	-0.1	2.23	0.37	4.80
PHI TD	79	-0.1	1.96	-0.04	2.38
F.P.A.	79	-2.6	1.64	0.10	3.62
YAW	79	2.4	2.57	-0.22	2.77

TABLE 16: SURVEY 45 NIGHT CARRIER LANDINGS SUMMARY
FOR B-2C MODEL AIRCRAFT

PARAMETER	NUMBER OF LANDINGS	MEAN	STANDARD DEVIATION	ALPHA 3	ALPHA
Vvp	80	8.2	2.31	-0.23	3.00
Vvs	80	8.0	2.45	-0.16	3.23
Vva	80	8.3	2.18	-0.20	3.20
Vva ff	6	9.5	1.24	0.60	2.13
Vvn	80	6.3	2.57	-0.14	2.90
Kle	80	1.0	0.12	0.63	2.83
Kle ff	6	1.1	0.16	0.53	1.55
Vw	80	24	2.76	0.57	2.26
Vef	80	85	5.04	-0.06	3.72
Vpaf	80	108	5.34	0.26	2.68
Vsp'a	80	86	1.03	0.80	4.28
Kvsp'a	80	1.26	0.06	0.23	2.83
PITCH td	80	7.6	1.14	0.14	2.45
PITCH td ff	6	8.6	0.79	-0.06	1.93
ROLL td	80	1.2	3.06	1.02	5.05
ROLL td ff	6	0.5	0.98	0.54	3.08
PITCH RATE	80	0.2	1.98	0.15	4.48
ROLL RATE	80	1.1	4.95	-0.68	4.17
DECK PITCH	80	-0.2	0.16	0.50	3.67
DECK ROLL	80	0.0	0.92	-0.64	3.41
OFFCENTER	80	-11.9	4.20	0.73	_4.20
RAMP TO					· · · · · · · · · · · · · · · · · · ·
TD DISTANCE	80	254	5.65	-0.16	2.53
WEIGHT	80	43281	1047	0.84	4.36
INSTANTANEOUS					
GLIDESLOPE	80	3.2	0.89	0.03	3.44
WIRE#	71	3.1	0.62	-0.08	2.56
PHI RATE	80	0.6	3.27	0.24	4.15
PHI TD	80	0.6	2.27	-0.39	2.92
F.P.A.	80	-3.5	2.22	1.13	4.39
YAW	80	4.0	3.26	-0.80	3.50

## TABLE 17: SURVEY 45 DAY CARRIER LANDINGS SUMMARY FOR S-3A MODEL AIRCRAFT

	NUMBER				
PARAMETER	OF LANDINGS	MEAN	STANDARD DEVIATION	ALPHA 3	ALPHA
Vvp	165	8.5	2.07	0.31	3.58
Vvs	165	8.2	2.00	0.48	3.89
Vva	165	8.4	1.96	0.47	4.27
Vva ff	13	6.9	1.98	0.30	2.96
Vvn	165	8.1	1.70	0.47	3.73
Kle	165	1.0	0.09	0.32	3.52
Kle ff	13	1.1	0.07	-0.13	2.70
Vw	165	27	4.58	0.29	3.00
Vef	165	94	5.38	0.09	2.61
Vpaf	165	122	4.75	-0.21	2.54
Vp'amin	164	105	2.14	0.29	2.37
Kvp'amin	164	1.16	0.05	0.18	2.74
PITCH ramp	161	5.5	1.19	0.55	3.89
PITCH td	165	4.5	1.20	0.18	3.57
PITCH td ff	13	5.1	0.89	0.00	2.40
ROLL ramp	161	-0.1	2.08	0.48	3.65
ROLL td	165	-0.6	1.89	0.57	4.48
ROLL td ff	13	-0.5	1.17	0.34	2.05
PITCH RATE	165	-0.1	2.57	-0.11	4.87
ROLL RATE	165	1.0	4.10	0.07	3.81
DECK PITCH	149	-0.3	0.21	-0.04	2.37
DECK ROLL	149	-0.4	1.09	0.12	3.59
OFFCENTER	165	10.6	4.52	0.22	2.97
RAMP TO					
TD DISTANCE	165	248	32.93	-0.39	2.85
WEIGHT	164	36764	1501	0.33	2.39
WHEEL HEIGHT	161	15.5	2.56	0.71	3.57
HOOK HEIGHT	161	12.8	2.57	0.64	3.50
GEOMETRIC					
GLIDESLOPE	161	3.23	0.67	0.74	4.01
INSTANTANEOUS					
GLIDESLOPE	165	2.80	0.70	0.45	3.20
WIRE#	131	2.6	0.76	0.47	2.34
PHI RATE	165	1.6	2.65	0.10	4.09
PHI TD	165	-1.3	2.82	0.03	2.02
F.P.A.	165	-3.1	1.13	0.60	4.30
YAW	165	1.8	2.92	0.05	2.72

TABLE 18: SURVEY 45 NIGHT CARRIER LANDINGS SUMMARY
POR 8-3A MODEL AIRCRAFT

PARAMETER	number of Landings	MEAN	STANDARD DEVIATION	ALPHA 3	ALPHA
Vvp	133	8.6	1.97	-0.06	3.16
Vvs	133	8.4	2.20	0.02	2.54
Vva	133	8.6	1.92	-0.13	2.66
Vva ff	7	7.7	2.23	-0.59	2.06
Vvn	133	8.2	1.80	-0.08	2.63
Kle	133	1.0	0.09	-0.06	3.97
Kle ff	7	1.0	0.05	0.95	1.90
Vw	133	32	2.04	0.01	1.98
Vef	133	91	5.87	-0.17	3.39
Vpaf	133	122	5.64	-0.38	4.99
Vp'amin	133	105	2.55	-0.05	2.19
Kvp'amin	133	1.17	0.05	-0.26	4.00
PITCH td	133	4.7	1.23	-0.57	5.40
PITCH td ff	7	5.1	0.78	1.27	3.63
ROLL td	133	-1.0	2.23	0.22	3.43
ROLL td ff	6	-1.0	1.63	0.73	1.96
PITCH RATE	133	-0.4	2.33	-0.42	3.45
ROLL RATE	133	0.6	5.91	0.55	4.06
DECK PITCH	133	-0.4	0.21	0.15	2.17
DECK ROLL	133	-0.3	1.04	-0.28	3.55
OFFCENTER	133	10.7	5.34	0.36	3.81
RAMP TO					
TD DISTANCE	133	276	38.32	-0.28	2.65
WEIGHT	133	36741	1782	0.00	2.19
INSTANTANEOUS					
GLIDESLOPE	133	2.84	0.71	-0.37	2.78
WIRE #	98	3.0	0.77	-0.20	2.34
PHI RATE	133	1.4	3.71	0.80	5.10
PHI TD	133	-0.5	3.36	0.21	1.85
F.P.A.	133	-3.5	1.58	1.50	10.27
YAW	133	3.1	3.68	0.27	2.45

## TABLE 19: SURVEY 45 DAY CARRIER LANDINGS SUMMARY POR TA-3B MODEL AIRCRAFT

	NUMBER				
	of		STANDARD	ALPHA	ALPHA
PARAMETER	LANDINGS	MEAN	DEVIATION	3	4 0.00
Vvp	23	9.9	2.10	0.22	2.36
Vvs	23	10.0	2.23	-0.10	2.72
Vva ff	23	7.6	2.13 2.50	-0.14 0.00	2.57
Vvn	23	10.3	1.63	-0.07	1.00 2.15
Kle	23	1.1	0.11	0.17	2.15
Kie ff	23	1.1	0.0	0.17	0.0
Vw	23	24	1.88	0.32	2.91
Vef	23	100	4.51	0.52	1.94
Vpaf	23	125	4.47	0.40	2.27
Vp'amin	22	113	2.14	-0.81	2.92
Kvp'amin	22	1.11	0.05	0.75	2.66
PITCH ramp	23	3.1	1.21	0.17	2.71
PITCH td	23	2.9	1.07	0.52	2.74
PITCH td ff	2	4.5	0.05	0.00	1.00
ROLL ramp	23	-1.0	1.45	0.03	2.75
ROLL td	23	-0.7	1.65	-0.44	3.17
ROLL td ff	2	-3.3	1.40	0.00	1.00
PITCH RATE	23	1.7	2.62	-0.27	2.66
ROLL RATE	23	-0.2	2.79	-0.09	2.50
DECK PITCH	19	-0.3	0.13	-0.60	2.04
DECK ROLL	19	0.58	0.40	-0.73	2.68
OFFCENTER	23	-8.9	4.08	-0.24	1.99
RAMP TO		<del></del>			
TD DISTANCE	23	243	34.93	-0.28	3.76
WEIGHT	22	48109	1808	-0.77	2.83
WHEEL HEIGHT	23	17.2	2.66	-0.10	2.10
HOOK HEIGHT	23	13.8	2.80	-0.11	2.11
GEOMETRIC		<del></del>			
GLIDESLOPE	23	3.71	0.73	0.18	2.56
INSTANTANEOUS					
GLIDESLOPE	23	3.15	0.75	-0.20	2.32
WIRE #	16	2.6	0.86	0.39	2.21
PHI RATE	23	-0.8	1.22	0.12	2.63
PHI TD	23	3.2	2.31	-0.98	3.71
F.P.A.	23	-3.4	1.25	0.49	4.22
YAW	23	6.6	2.93	-0.58	2.53

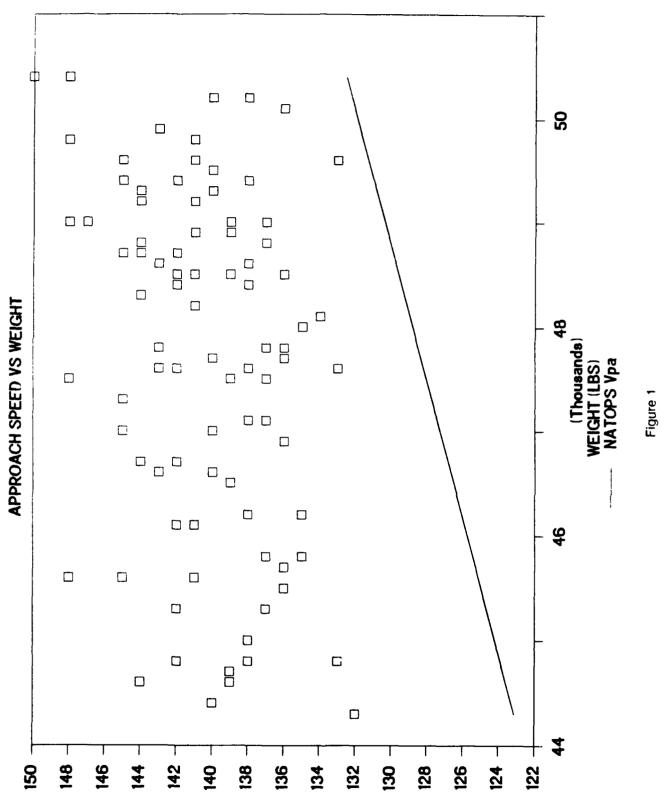
## TABLE 20: SURVEY 45 DAY CARRIER LANDINGS SUMMARY FOR T-2C MODEL AIRCRAFT

Parameter	number of Landings	MEAN	STANDARD DEVIATION	Alpha 3	Alpha 4
Vvp	498	7.9	2.28	0.42	4.44
Vvs	498	7.2	2.15	0.59	4.17
Vva	498	7.5	1.94	0.62	4.48
Vva ff	28	7.0	1.86	1.46	5.85
Vvn	498	7.5	1.94	0.37	4.02
Kle	498	1.0	0.10	0.85	6.53
Kle ff	28	1.1	0.08	-0.5	2.9
Vw	498	24	1.91	0.12	3.44
Vef	498	82	5.42	0.32	4.33
Vpaf	498	106	5.41	0.31	3.83
Vp'amin	496	95	1.84	0.73	6.29
Kvp'amin	496	1.12	0.06	0.59	4.97
PITCH ramp	490	6.0	1.29	0.36	4.15
PITCH td	498	4.8	1.57	0.37	3.22
PITCH td ff	28	5.8	1.22	0.84	3.76
ROLL ramp	490	-0.2	2.81	0.09	3.57
ROLL td	498	0.1	2.93	0.57	3.62
ROLL td ff	28	-0.9	1.36	-0.07	2.54
PITCH RATE	498	0.9	3.56	-0.02	4.80
ROLL RATE	498	1.8	6.59	0.10	3.68
DECK PITCH	493	-0.1	0.21	-0.39	3.03
DECK ROLL	493	-0.1	0.95	0.13	4.35
OFFCENTER	498	-11.1	5.23	-0.01	4.12
RAMP TO					
TD DISTANCE	498	248	44.5	-0.33	2.66
WEIGHT	496	9433	367	0.87	6.67
WHEEL HEIGHT	490	15.7	3.04	0.20	2.93
HOOK HEIGHT	490	13.2	3.08	0.14	2.92
GEOMETRIC					
GLIDESLOPE	498	2.8	0.66	0.97	5.59
INSTANTANEOUS					
GLIDESLOPE	498	3.00	0.83	0.57	4.08
WIRE#	310	2.9	0.80	0.22	1.61
PHI RATE	498	-0.2	5.45	-1.08	16.05
PHI TD	498	0.8	2.11	0.04	4.06
F.P.A.	498	-2.8	2.26	0.38	10.10
YAW	498	3.6	3.41	-0.19	4.86

## TABLE 21: SURVEY 45 DAY CARRIER LANDINGS SUMMARY FOR TA-4J MODEL AIRCRAFT

	NUMBER				
	OF		STANDARD	ALPHA	ALPHA
Parameter	LANDINGS	Mean	DEVIATION	3	4
Vvp	635	10.4	2.33	0.18	3.13
Vvs	635	10.0	2.28	0.07	3.15
Vva	635	10.3	2.25	0.16	3.23
Vva ff	120	9.3	2.52	0.05	3.39
Vvn	635	10.2	2.33	-0.32	3.70
Kle	635	1.1	0.10	2.75	35.05
Kle ff	120	1.1	0.12	2.66	19.74
Vw	635	26	3.30	0.31	3.44
Vef	635	113	6.68	0.49	8.05
Vpaf	635	140	6.73	0.46	6.09
Vp'amin	624	129	1.47	-1.10	3.30
Kvp'amin	624	1.09	0.05	0.46	6.01
PITCH ramp	617	14.2	1.48	-0.01	3.23
PITCH td	635	11.9	1.50	-0.14	3.61
PITCH td ff	120	12.3	1.49	0.35	3.53
ROLL ramp	617	0.6	3.40	0.46	3.87
ROLL td	635	-0.9	2.83	0.29	3.94
ROLL td ff	120	-0.6	2.30	0.27	3.65
PITCH RATE	635	3.8	3.27	0.43	4.61
ROLL RATE	635	1.7	7.80	0.05	4.01
DECK PITCH	553	-0.3	0.20	0.40	3.54
DECK ROLL	553	0.15	1.17	0.27	3.28
OFFCENTER	635	-9.2	6.13	-0.33	4.58
RAMP TO					
TD DISTANCE	635	254	42.11	0.01	2.68
WEIGHT	624	14062	320	-1.08	3.25
WHEEL HEIGHT	617	15.8	3.20	0.66	3.57
HOOK HEIGHT	617	12.2	3.21	0.61	3.42
GEOMETRIC					
GLIDESLOPE	617	3.16	0.59	0.16	3.31
INSTANTANEOUS					
GLIDESLOPE	635	2.84	0.72	-0.11	3.41
WIRE #	452	2.8	0.88	-0.40	2.50
PHI RATE	635	3.0	3.87	0.26	6.79
PHI TD	635	-3.3	3.07	-0.8	3.43
F.P.A.	635	-3.8	1.89	0.07	6.23
YAW	635	0.6	3.64	-0.13	3.21

## F-14A DAY LANDINGS \* SURVEY 45



**APPROACH SPEED (KNOTS)** 

36



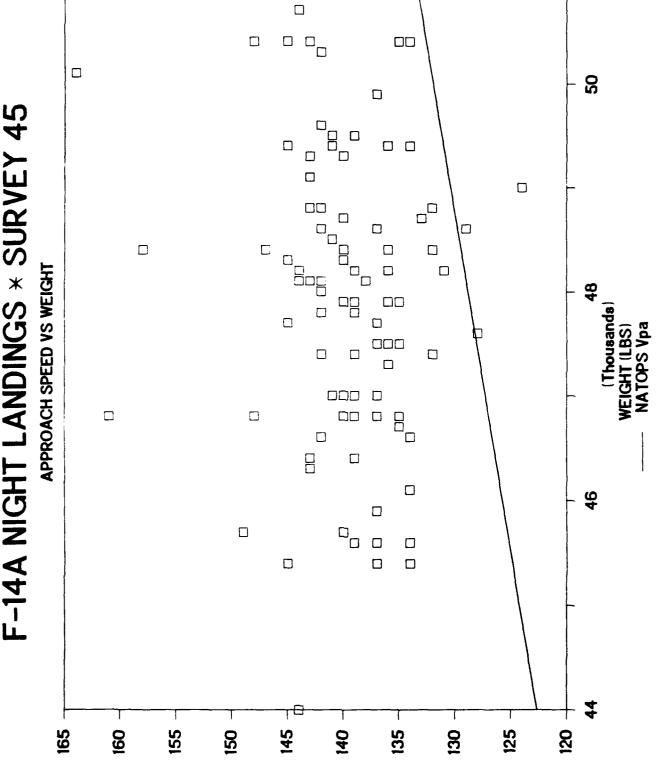
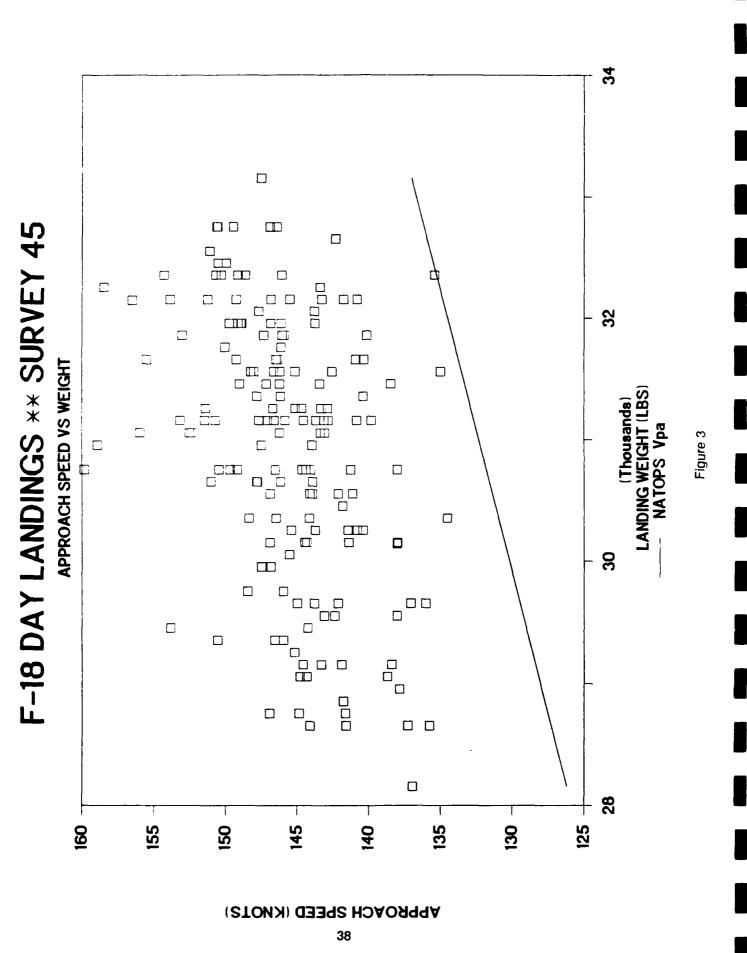


Figure 2



## F18 NIGHT LANDINGS \*\* SURVEY 45

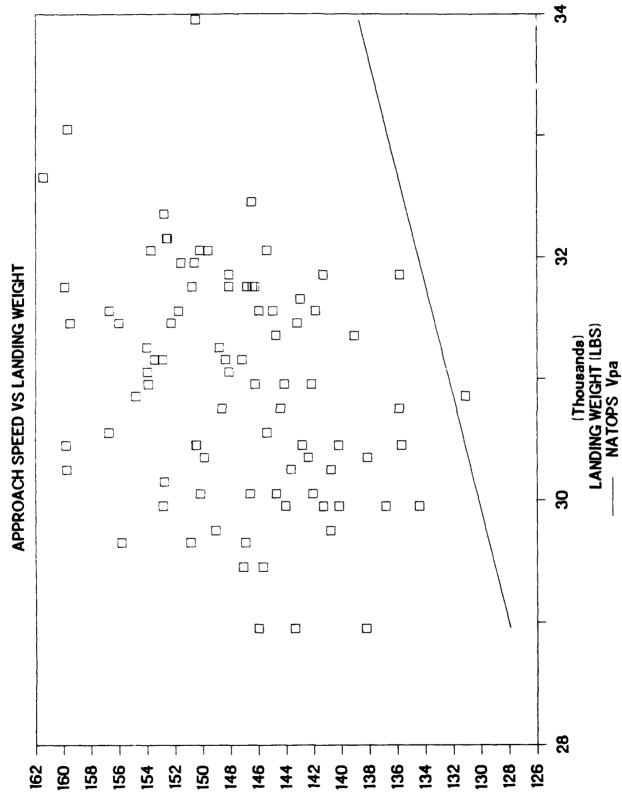
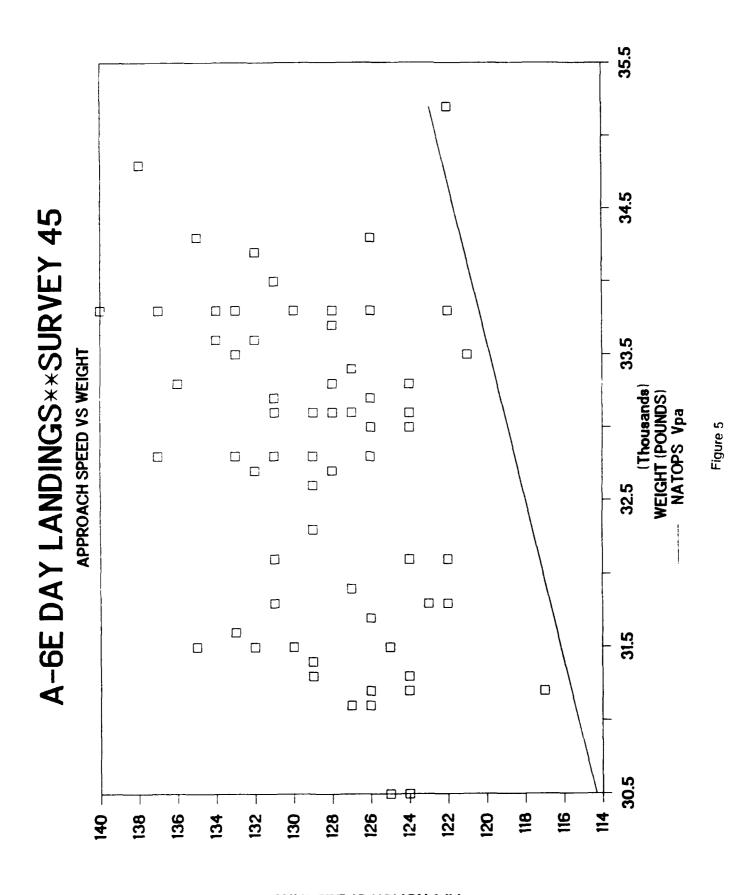
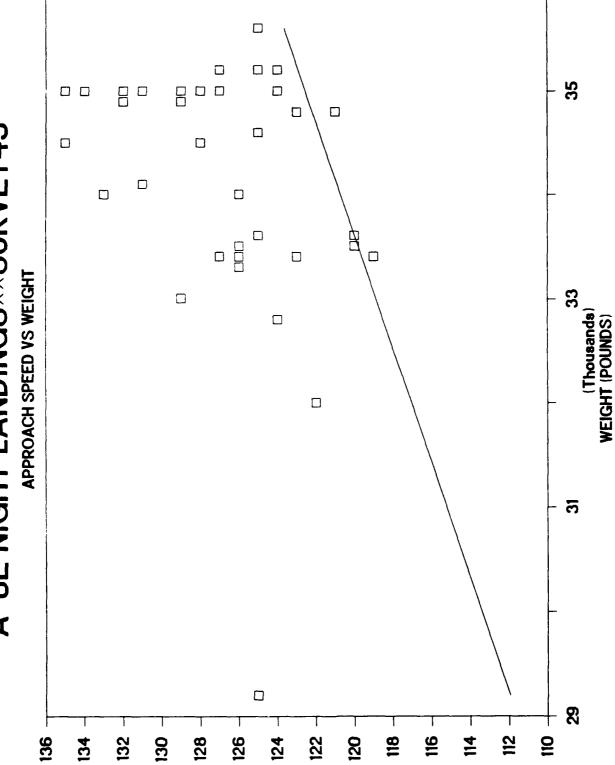


Figure 4



APPROACH SPEED (KNOTS)

## A-6E NIGHT LANDINGS\*\*SURVEY45



**APPROACH SPEED (KNOTS)** 

41



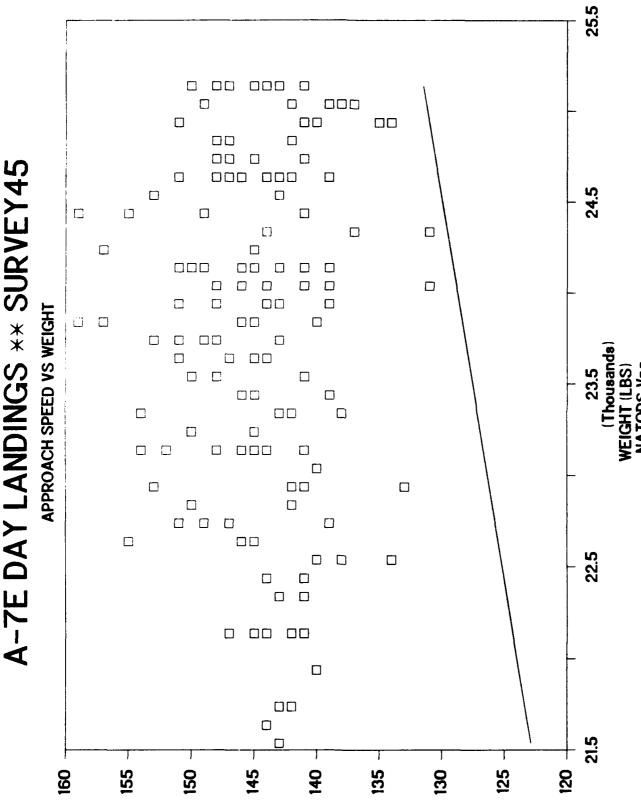
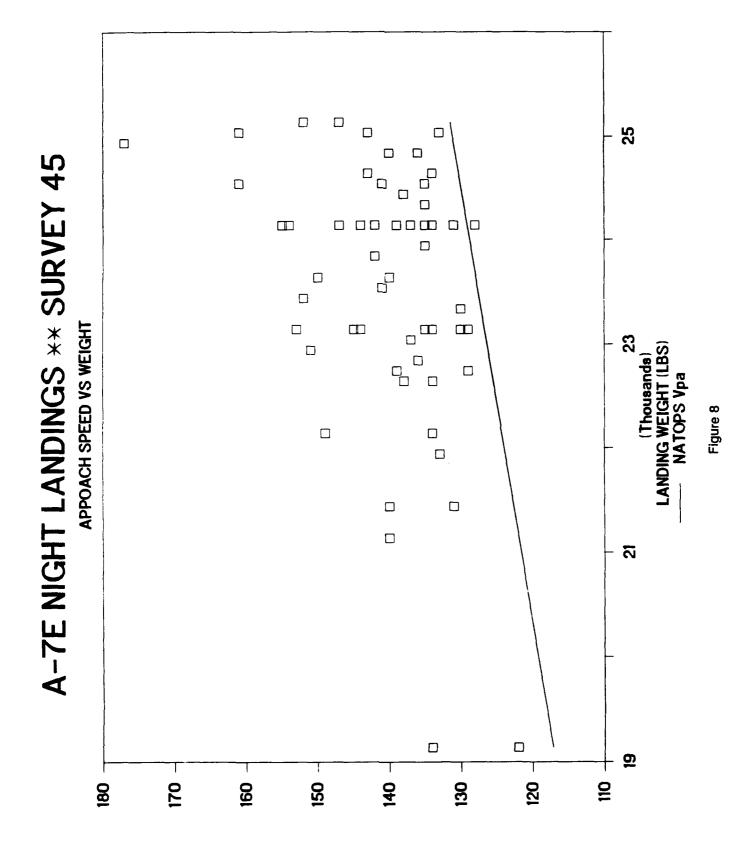
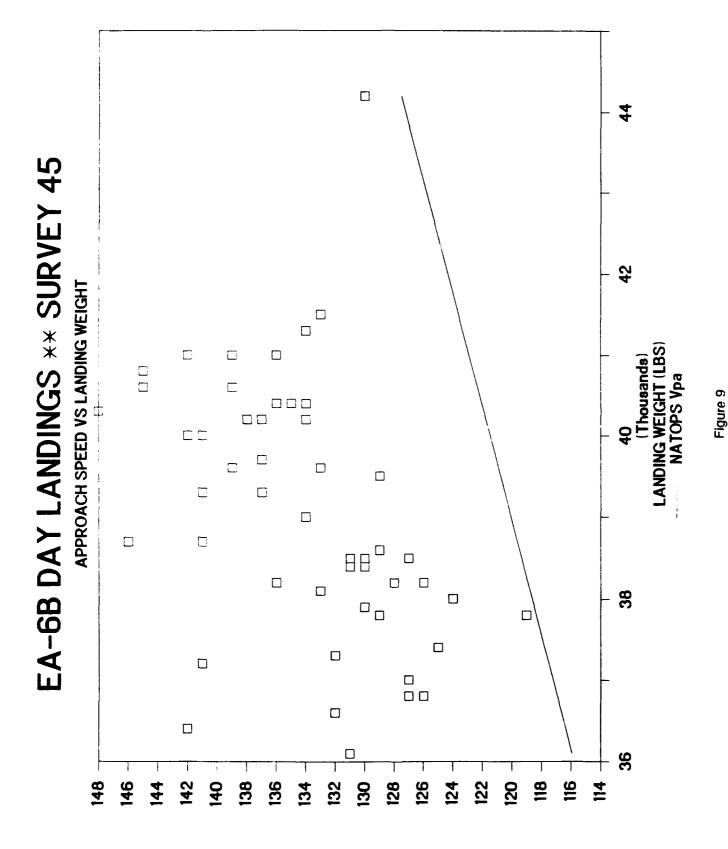


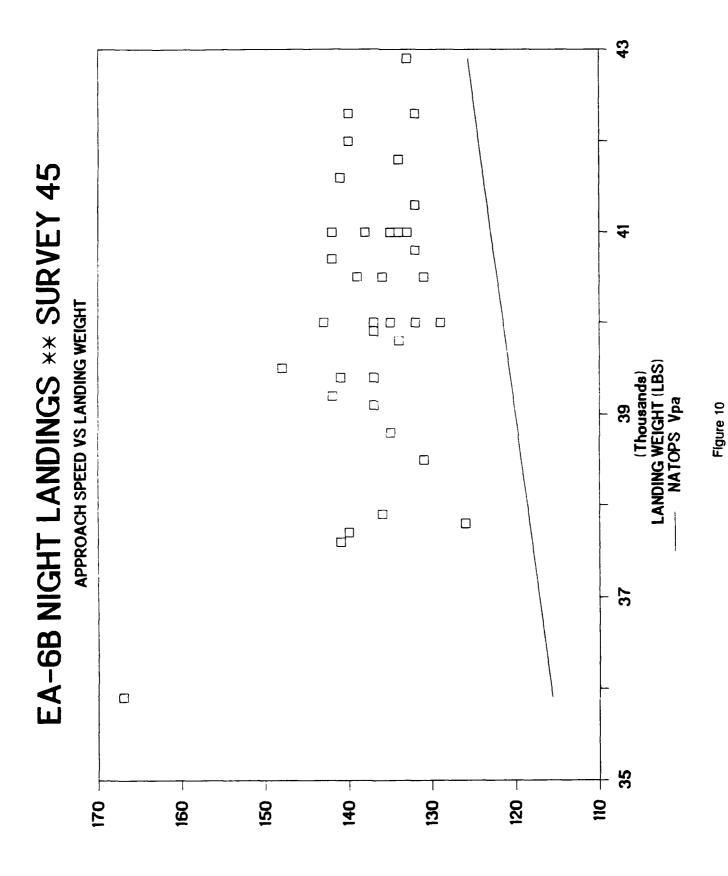
Figure 7

42





**PPPROACH SPEED (KNOTS)** 



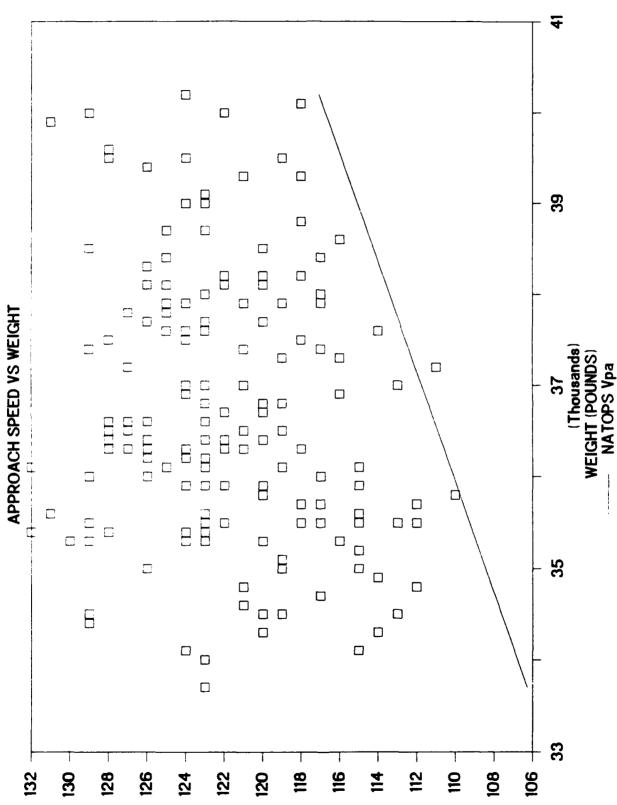
### E-2C DAY LANDINGS \*\* SURVEY 45 APPROACH SPEED VS LANDING WEIGHT (Thousands) LANDING WEIGHT (LBS) NATOPS Vpa <u>6</u>

Figure 11

### E-2C NIGHT LANDINGS \*\* SURVEY 45 APPROACH SPEED VS LANDING WEIGHT (Thousands) LANDING WEIGHT (LBS) — NATOPS Vpa

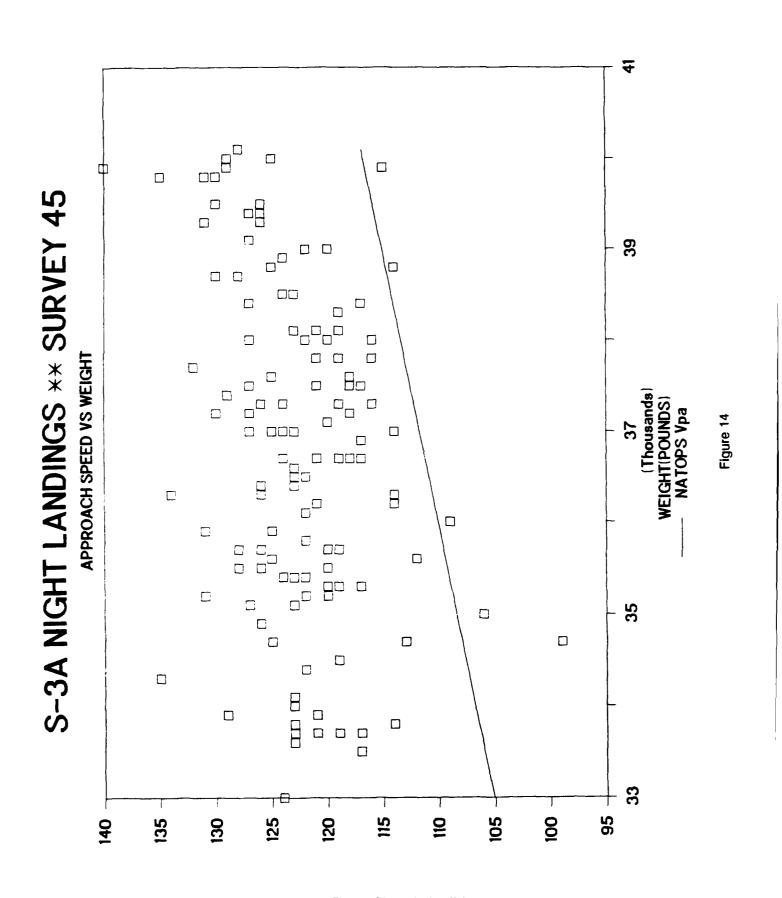
Figure 12



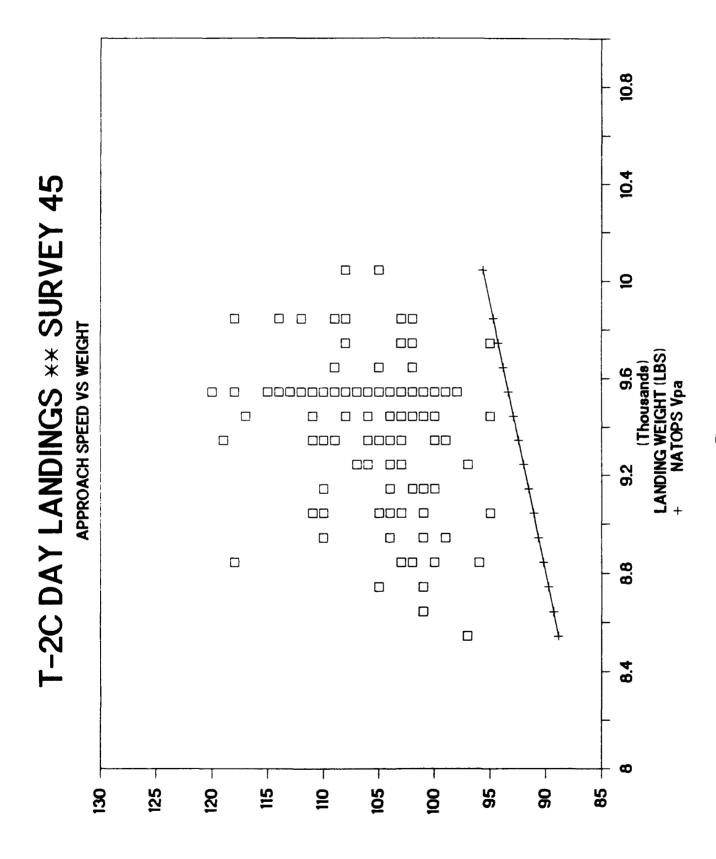


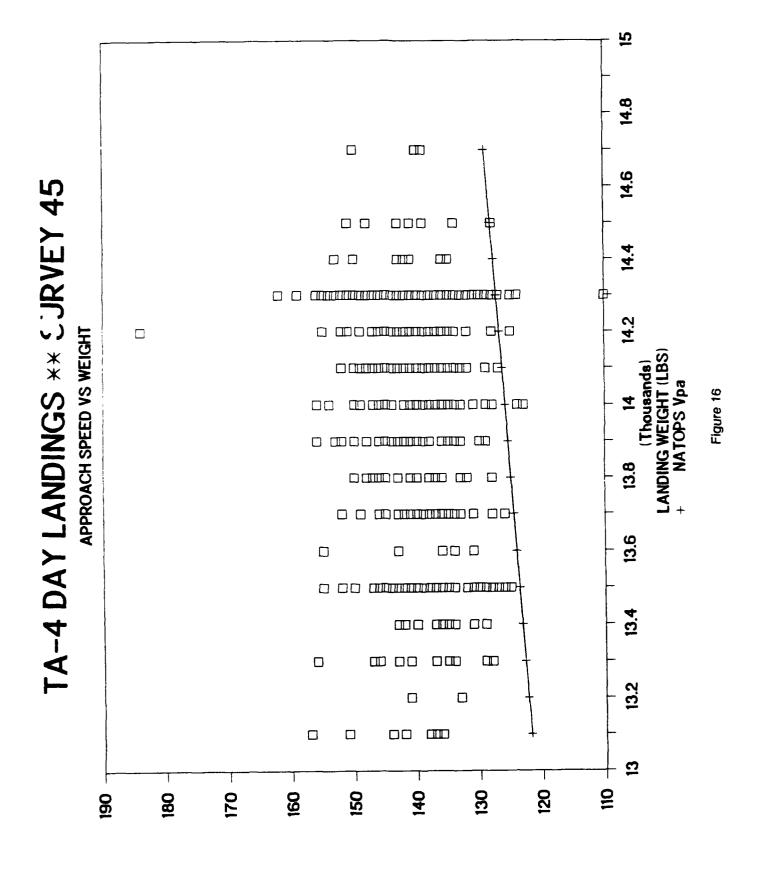
APPROACH SPEED (KNOTS)
89

Figure 13



APPROACH SPEED (KNOTS)





APPROACH SPEED (KNOTS)

## F-14A DAY LANDINGS \* SURVEY 45

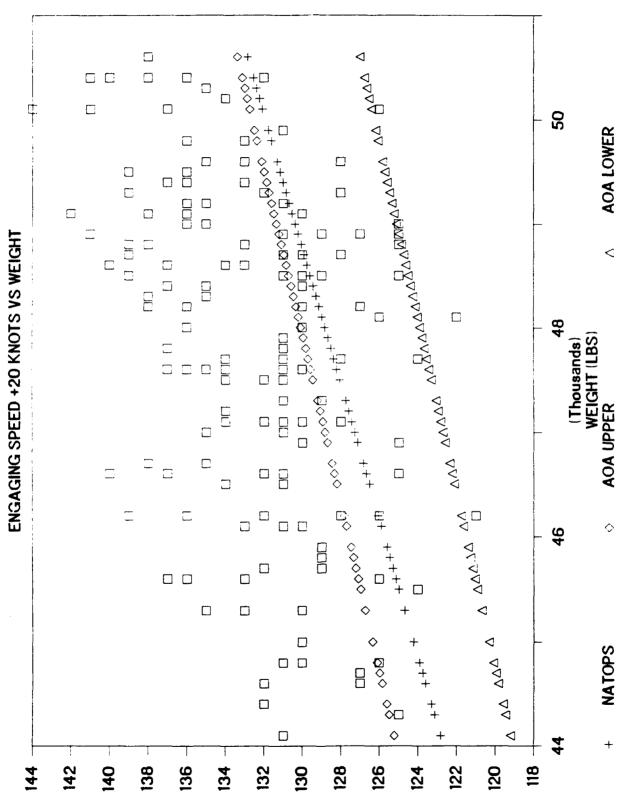
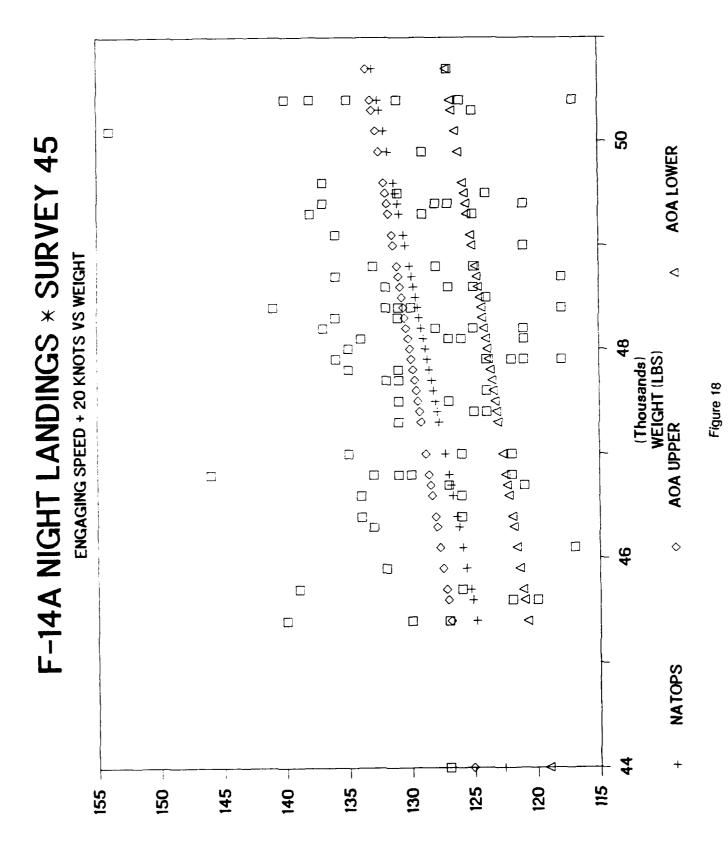
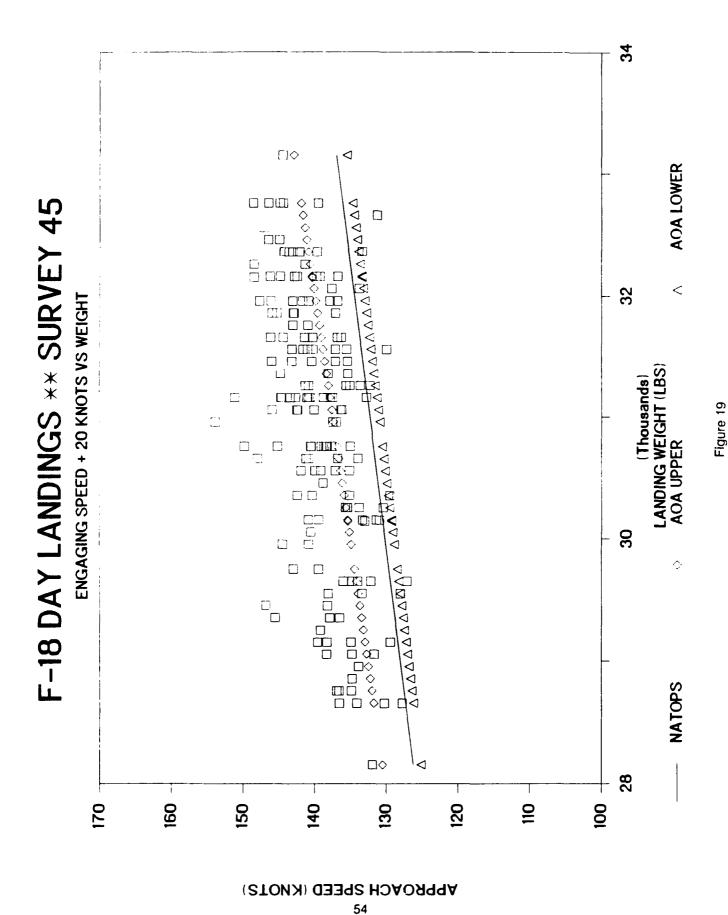


Figure 17



APPROACH SPEED (KNOTS)



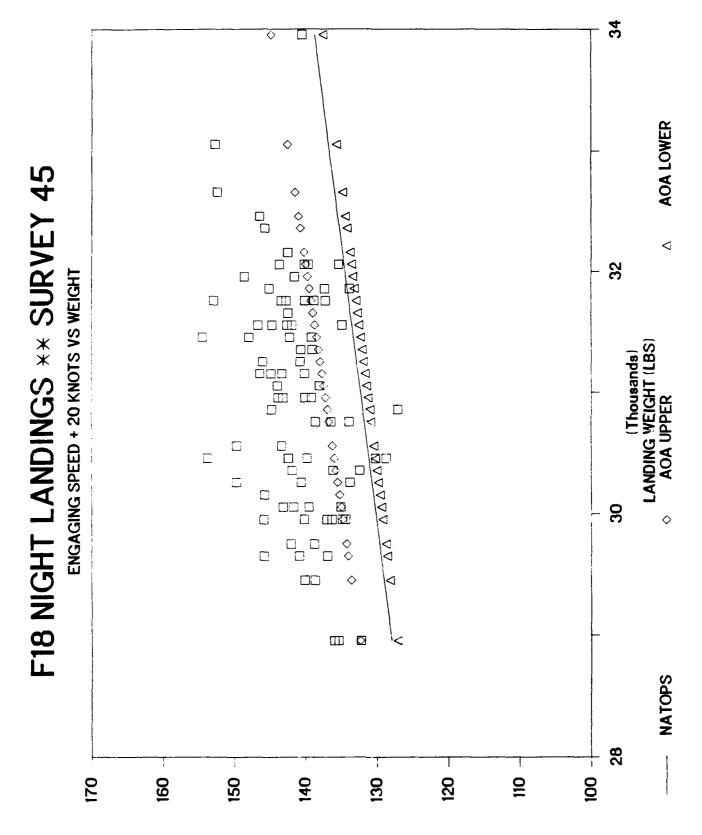
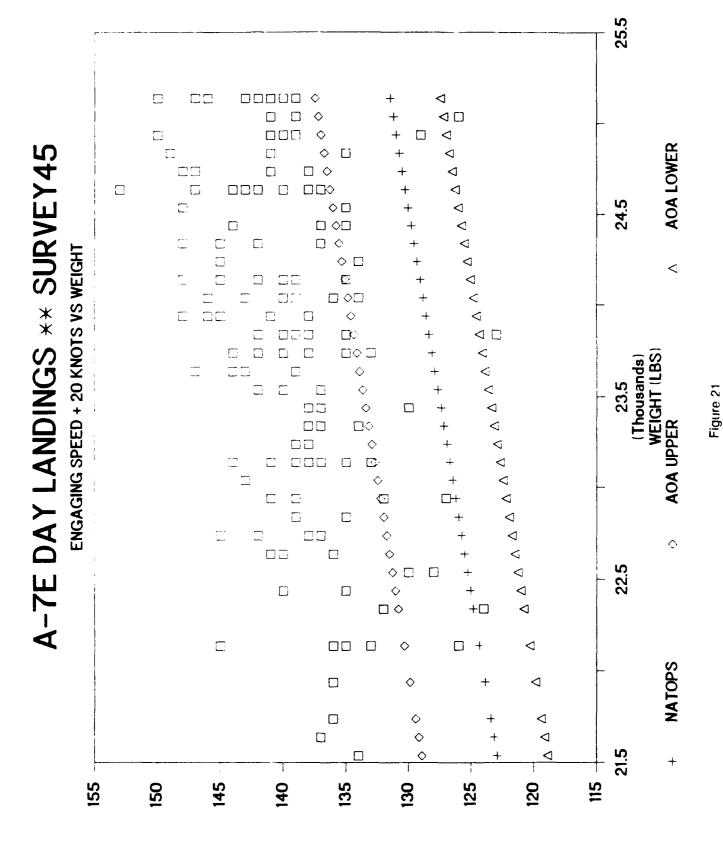


Figure 20



APPROACH SPEED (KNOTS)

# A-7E NIGHT LANDINGS \*\* SURVEY 45

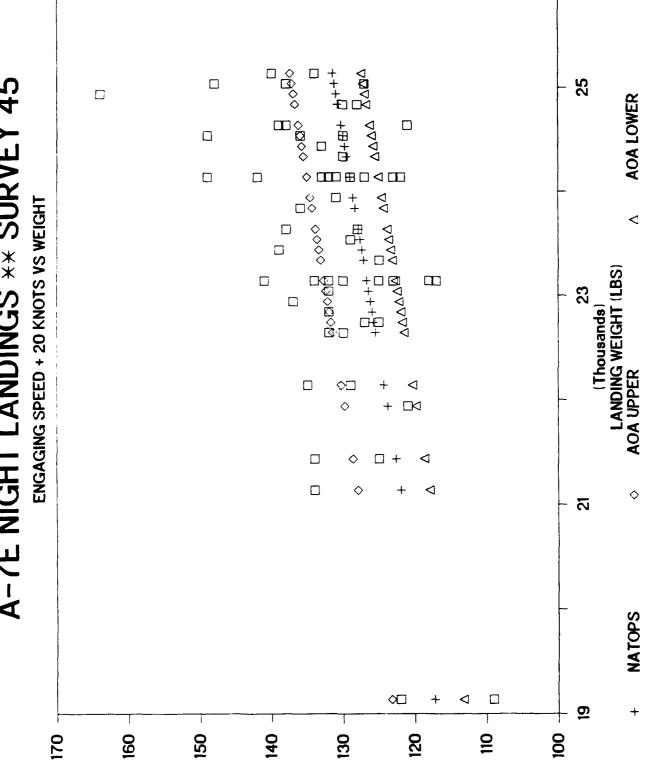
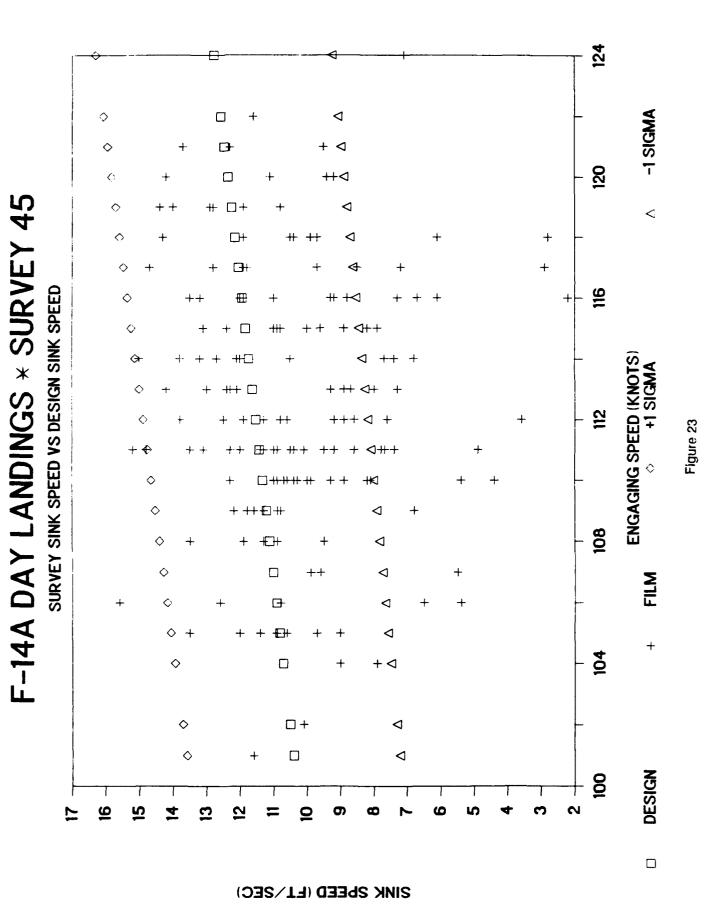
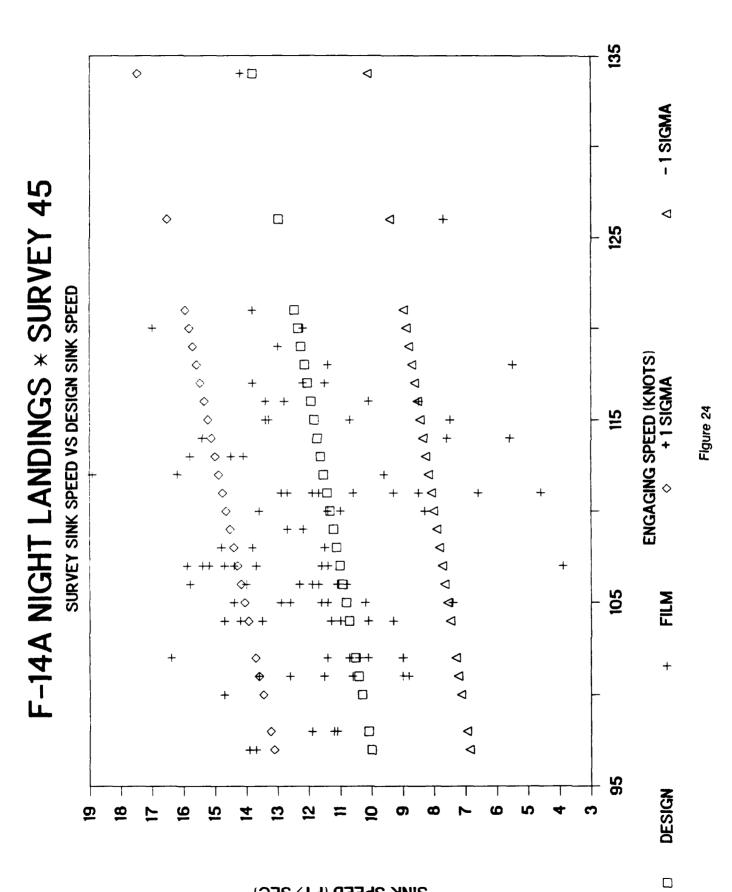
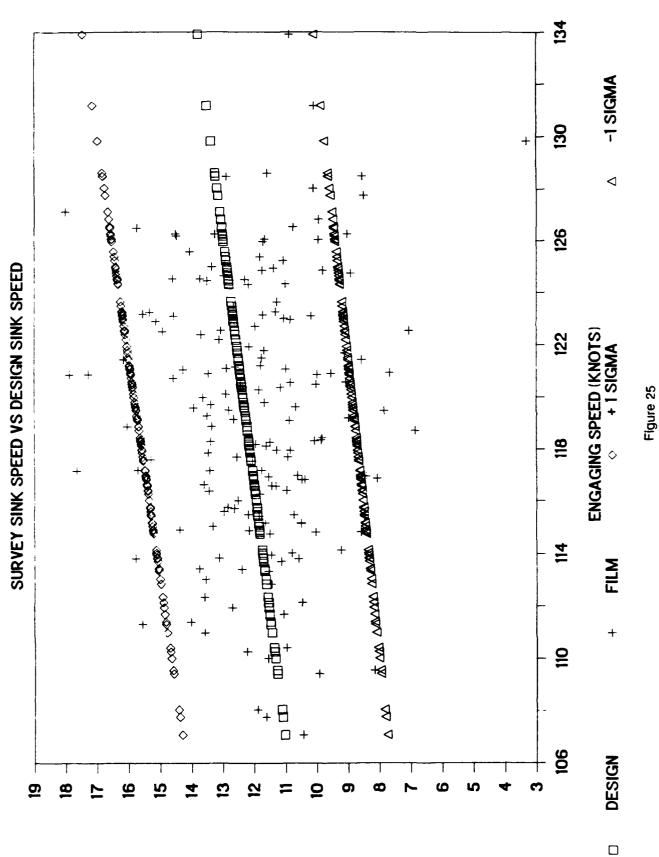


Figure 22





### F-18 SURVEY 45 DAY LANDINGS



SINK SPEED(FT/SEC)

## F18 NIGHT LANDINGS\*\*\*SURVEY 45

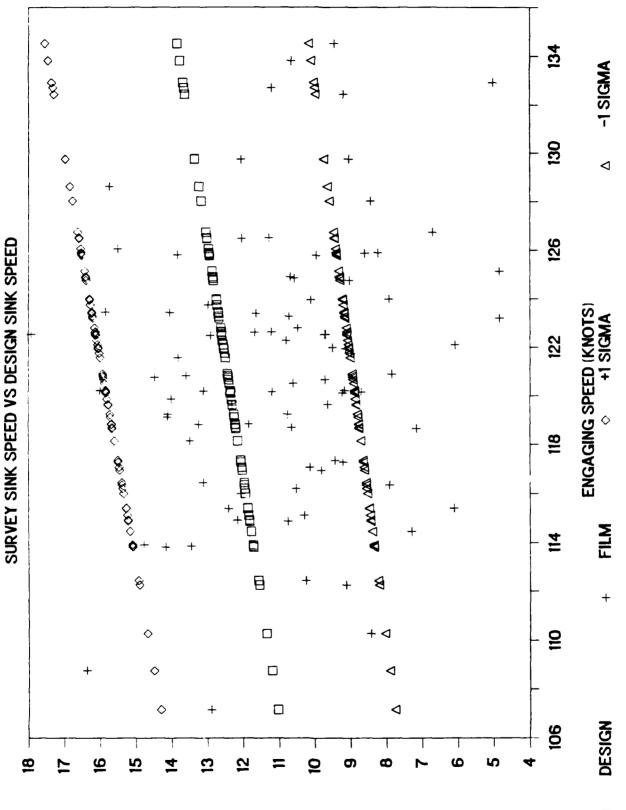
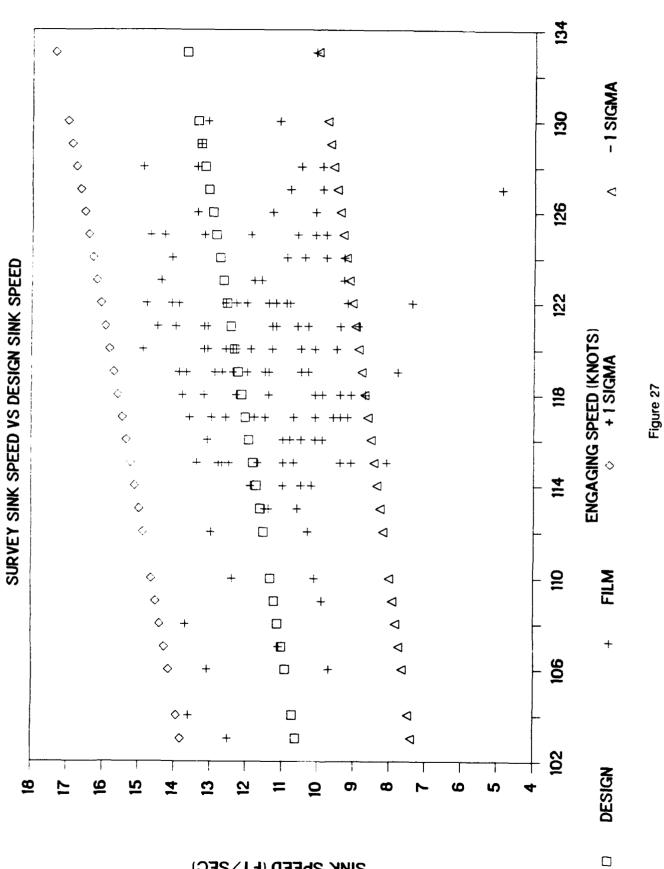


Figure 26

SINK SEED (LINSEC)

## A-7E DAY LANDINGS \*\* SURVEY 45



SINK SPEED (FT/SEC)

# A-7E NIGHT LANDINGS \*\* SURVEY 45

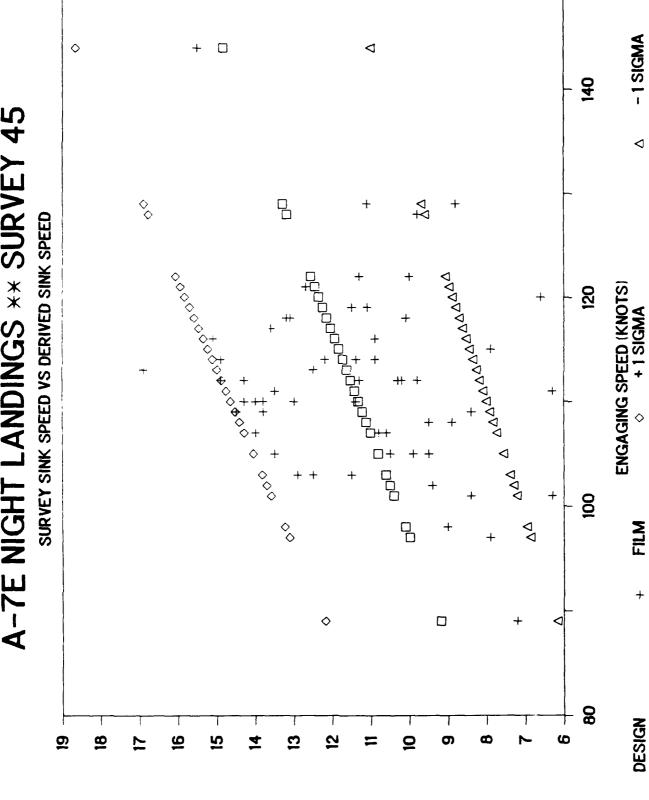


Figure 28

SINK SEED (LINSEC)

### APPENDIX A

### LANDING PARAMETERS OF INDIVIDUAL AIRCRAFT LANDINGS

USS ENTERPRISE CVN-65

### **F-14 DAY**

CNDG	\$	VPAF	2	VE-FIUM		WIN	WIND-VEL		7	VEOR	ΑdΛ	VPAMIN	VSP.4	.<	KVPA	\$	LIFT	LIFT	ME.	WEIGHT
<del>2</del>	_	ē			-	PAR.	PE	PERP.							Z Z	SP. A	5	4		
	ž	M/S	\$	I W/S	\$	K S	\$	K/S	₹	S/M	₹ 2	s/n	3	S/M					LBS	ĸĠ
-	7	n	4	n	•	7	€	<b>O</b> h	19	=	12	5	<b>±</b>	5	91	17	81	19	20	21
663	144	-	112	800	32	16	r	8	113	88	122	23			1.18		1.99		49300	22362
603	148		=		32	16	n	7	118	19	122	63			1.21		1.30		4966	22226
909	7	•			32	16	n	7	103	53	122	63			1.18		1.10		49300	22362
697	<b>4</b>	-			32	16	n	7	Ξ	57	122	63			1.14		1.00		49300	22362
808	137	70	195	54	32	9	n	7	Ξ	22	122	63			1.13		96		48800	22136
609	7	•			32	9	r)	7	116	99	,	ļ					96			
6	147	-			32	9	<b>17</b> )	7	Ξ	57	122	63			1.21		8		43666	22226
- 5	137				32	9	<b>r</b> ) (	7	104	23	122	63			1.12		.00		49000	22226
612	142				32	9	י מי	~	108	26	121	62			1.17		1.00	1	48500	22000
513	=				32	9 !	n	7	107	ဂ္ဂ	121	62			9 !		86.	96.	48500	22000
<del>2</del>	142				7	17	<b>o</b>	S I	99	2	122	63			1.17		- 19		48700	22090
616	139				#	4	<b>o</b>	<b>1</b> 0	102	52	121	62			<b>*</b> :		- 10	;	48500	22000
617	<del>-</del>	•			4	17	o ·	in i	107	55	122	63			- 18		.00	- 00	48700	22090
618	<b>5</b>				4	17	<b>o</b>	<b>د</b> د	105	4	122	63			- 19		1.20		48700	22090
619	48				<del>,</del>	2!	<b>o</b>	ın ı	123	5	120	62			1.23		1.10		47500	21546
629	<b>*</b>				<b>†</b>	_ :	<b>5</b> 0 (	י מ	69	8	120	79			1.23		99.		47566	21546
621	7				<b>*</b>	17	<b>o</b>	<b>6</b>	103	3	122	3			1.16		1.39	;	48966	22181
622	= = = = = = = = = = = = = = = = = = = =	,			Ħ.	1	<b>o</b>	<b>ن</b> د	103	23	121	62			5.16			1.10	48200	21864
623	± 5		•		,	<u>.</u>	<b>o</b>	<b>ا</b> د	13	5	120	62			1.21		1.00	;	47300	21455
624	5				ň i	17	<b>o</b>	ın ı	86	20	120	62			1.21		1.20	1.20	47999	21319
625	52.	•			7	2:	<b>o</b> n (	n •	•	2	122	g :			1 4. 6		99.		48900	22181
879	741	•			3 5	9	o 4	) r	• •	) ()	0 0	<u>.</u> :			97.1		9 6		40104	71617
670	2 5	•			3 5	2 4	<b>.</b>	) P	80	9 40	1.8	7 7							45.500	20639
635	2 2	•	•		32	16	ω (	) P)	105	5 4	1 2 3	6 5			1.12		.00		46200	20956
636	145	•	•		32	16	9	n	105	54	118	61			1.23		1.10		45600	20684
637	134	_	•		35	16	9	n	103	53	121	62			1.1		1.00		48100	21818
638	139	•	•		32	16	ø	n	103	53	117	99			1.20		1.20	1.20	44700	20276
640	148	•	•		32	16	ဖ	۲3	110	21	118	61			1.26		1.10		45600	20684
644	139	•	•		32	9	ø	n	105	54	116	69			1.20		1.20		44600	20231
646	142	•	•		32	9	φ	m	112	88	117	60			1.22		1.30	1.20	44800	20321
647	<del>+</del>	•	•		32	16	ဖ	n	107	55	116	69			1.23		1.30	1.30	44699	20231
650	150	•	•		32	16	ဖ	n	109	26	124	64			1.21		1.20	1.49	50400	22861
655	148	•	•		32	16	9	n	118	61	123	63			1.21		1.20		49800	22589
658	143	•	•		32	16	9	n	103	53	123	63			1.16		1.10		49900	22635
629	<del>-</del> <del>2</del> <del>2</del> <del>2</del>	•	•		32	16	စ	m	120	62	123	63			±. ₩		1.00		49600	22499
665	138	•	-		24	12	7	-	112	58	124	<b>64</b>			1.12		1.00		59200	17722
999	-	•	•		24	12	7	-	117	69	123	63			1.14		1.00		49500	22453
667	139	•	•		<b>54</b>	12	7	-	109	26	122	63			1.13		1.00		49666	22226
468	140	•			26	13	7	-	120	62	124	64			1.13		1.00		59200	17722

										_					_							_			_	_	_					_	_			_	_	_	_	_			
WEIGHT		¥	21	22408	22666	22499	22136	22000	21773	22408	21864	22045	21954	21682	22499	21319	21546	21365	21092	21546	20911	21138	20412	20775	21183	20730	20548	20321	20231	20956	20321	20094	20548	22861	22725	20140	22589	20684	22499	215 54	22317	22408	21591
WE		<b>188</b>	20	49466	48500	49600	48800	48500	48000	49400	48200	48600	48400	47800	49600	47000	47500	47100	46599	47500	46160	46600	45000	45800	46700	45700	45300	44800	44600	46200	44800	44300	45300	50400	50100	44400	49800	45600	49600	48400	49200	49400	47600
LIFT	<u>u</u>		6																		1.10	1.10			1.18						1.00				1.10						1.10		
LIFT	5		<del>2</del> 0	1.10	1.00	1.00	1.10	96.	1.00	1.00	1.00	1.00	1.10	1.00	1.00	96.	1.00	1.10	1.00	1.10	1.10	1.10	1.00	1.10	1.66	1.00	1.00	1.00	1.10	1.00	1.00	96.	1.10	1.10	1.00	1.00	1.10	1.10	1.10	96.	1.10	1.10	1.00
\$	V .⊌S		17																																								
KVPA	N I		16	1.15	1.12	1.15	1.18	1.12	1.12	1.12	1.16	1.13	1.17	1.13	1.08	1.17	<del>*</del>	1.15	1.17	1.16	1.19	1.17	1.18	1.16	1.28	1.15	1.21	1.14	1.19	1.1	1.18	<del>*</del>	1.17	1.20	1.10	1.21	1.15	1.20	1.15	1.14	1.18	1.18	<u>+</u> . <u>+</u>
V.dSA		s/m	5																																								
8		¥	<b>±</b>																																								
VPAMIN		N/S	5	63	62	5 63		62		63		63		62				62		62	19	61	. 69	19	_	19	99	69			99	99 9	69	1 64	63								62
>		₹	12	123	121	123	122	121	121	123	121	122	121	121	123	120	120	120	119	120	118	119	117	118	119	118	117	117	116	118	117	116	117	124	123	116	123	118	123	121	122	123	120
VEOR		M/S	Ξ	62	59	62	59	26	26	55	99	53		55	53	62	57	57	55	57	26	69	55	57	57	52	58	56	26	53	5	53	55	29	54	5	26	4	36	26	26	99	57
		š	6	120	115	121	115	109	109	106	117	104		106	104	120	=	Ξ	107	=======================================	108	116	106	110	==	102	112	108	109	104	100	104	107	114	105	118	109	124	109	109	109	116	=
	PERP.	K/S	01	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	7	8	-	-	-	-	-	-	-	-
WIND-VEL	ā	\$	60	7	7	7	~	7	7	7	7	7	8	7	7	7	Ci	7	7	7	7	7	7	7	7	7	7	7	7	7	8	7	7	n	n	7	7	7	7	7	7	7	. 7
X	PAR.	K/S	7	2	13	13	7	13	13	5	2	13	5	<u></u>	5	5	5	<u>*</u>	<u>*</u>	<del>+</del>	+	<u>*</u>	<u>*</u>	<u>*</u>	<b>*</b>	<del>*</del>	<del>*</del>	<del>*</del>	<b>*</b>	<b>*</b>	<b>*</b>	<b>*</b>	<del>*</del>	5	15	<b>±</b>	<b>±</b>	<b>*</b>	=	+	<del>*</del>	*	<b>±</b>
	_	\$	•	26	26	26	25	25	25	25	22	22	25	25	25	22	25	28	28	28	28	28	28	28	27	27	27	27	27	27	27	27	27	30	30	28	78	8	78	28	78	28	78
VE-FILM		¥/s	60	99	57	29	61	57	57	8	66	88	60	27	26	28	88	57	57	57	8	58	21	56	29	28	59	55	88	26	57	ž	57	5	55	58	28	8	58	57	69	99	22
<b>∠</b> €		\$	•	116	110	115	119	=======================================	110	113	-	113	117	=	168	115	112	110	Ξ	=======================================	113	112	110	109	115	169	115	166	112	108	11	105	110	118	106	112	113	113	113	110	116	117	110
VPAF	5	K/S	n	•			7 1	•					23		3 68											8 70							•		•		23		-	•	7	5 75	2 7
	•	Š	7	•	•	•-	•		•	_	_	•	_	•	_	•	_	_		•	_		_	•	•	•	•	•	_	_	_	_	_	_	_	-	<u>+</u>	•	=	_	_	_	138
TAGG	3		-	699	671	673	674	675	676	677	678	679	689	681	682	685	687	688	689	692	695	969	697	698	700	701	702	705	706	797	708	709	710	719	721	724	725	728	729	730	731	732	2

DAY LANDINGS

USS ENTERPRISE (CVN-6

LANDING DATA - MODEL F-14

WEIGHT		ğ	21	21591	21591	22317	21682	21909	21682	21274	21637	22045	21128	21181	21365	20775		21365	21365	20730	21138	20956	20956	22000	21410	22136	07/77	22725	21591	22181	21864	21591	22952	20956	20684	20548	21138	20956	22272	22272	22045
¥ ¥E]		LBS	20	47600	47600	49200	47800	48300	47800	46900	47700	48688	45566	45700	47100	45800		47100	47100	45700	46600	46200	46200	48599	47200	48800	20100	50100	47600	48900	48200	47600	50600	46200	45600	45300	46600	46200	49100	49100	48600
LIFT	<u>1</u>		19			1.20	1.20			,	96.	99.	9	4	2											,	90.										1.00		1.00		1.10
LIFT	TD F		81	1.10	96.	1.10	1.10	1.00	1.60	1.10	86.	95.	9				5 5	96	1.00	1.00	1.00	1.10	1.10	1.20	1.00	 6 :	9 .		1.19	1.20	1.10	1.10	1.20	1.10	1.10	1.20	96	1.00	1.00	1.00	1.10
\$	V .dS		17																																						
KVPA	N N		16	1.10	1.19	1.15	1.19	1.19	1.13	7.1	1.16	e	97.		17.		<u>:</u>	1.16	1.16	1.15	1.21	1.18	1.15	1.19	1.16	1.12	2	0 . t	1.18	1.21	1.17	1.12	1.15	1.21	1.20	1.19	1.1	1.09	1.1	1.18	1.17
VSP.A		s/m	15																																						
×S		X	<b>±</b>																																						
VPAMIN		N/S	13	62	62	53	62	62	62	61	62	3 :	<u>.</u>	70	<u>.</u>	7 7	5	63	62	19	19	5	19	62	62	3	3 :	4 4	2 2	3	62	62	<b>9</b>	19	61	60	19	61	63	63	63
À		ኟ	12	120	120	122	121	121	121	119	120	122	61.	27 :	120	2 .	2	128	120	1.8	119	118	<b>=</b>	121	120	122	23	124	120	122	121	120	124	118	118	117	119	118	122	122	122
VEOR		s/m	Ξ	59	29	59	5. 4.	69	24	28	26	800	9 ;	- 6	3 6	3 6	9 4	. ec	န္	36	29	23	œ	26	23	88	ç	<b>8</b> 9	2 2	29	58	57	69	20	62	22	53	26	62	62	65
VE		Š	9	115	115	115	195	117	105	112	109	112	9 :	» «	7 7	118	- F	2 2	1 + 1	109	115	114	112	108	115	112	,		120	114	113	110	117	97	121	107	104	108	121	121	127
	ية.	s/w	o	~	0	0	0	0	0	•	<b>6</b>	<b>5</b> 0 (	<b>5</b> 0	<b>9</b>	<b>9 4</b>	• 6	> 6	9 6	. 0	6	0	0	•	7	7	<b>-</b> ·	_ ,			_	_	_	-	_	_	_	-	-	-	-	-
VEL	PERP	ž	€	+	•	0	0	0	0	0	•	<b>S</b>	<b>S</b>	<b>D</b> 6	9 6	• 6	> 6	•	•	•	0	0	0	*	4	~	~ 0	, c	. ~	~	7	7	7	7	7	7	7	7	7	7	7
WIND-VEL	PAR.	s/m	7	12	13	13	13	13	13	2	5 ;	2 :	2:	2 #	2 =	2 5	2 =	2 12	13	12	12	12	12	13	13	12	2 5	2 2	<u> </u>	*	12	12	12	12	13	<del>*</del>	<del>*</del>	<b>±</b>	12	=	Ξ
	ď	Š	•	23	26	26	26	26	26	<b>5</b> 6	56	26	9 5	9 4	, k	2 4	9 6	9 6	<b>5</b> 2	75	24	<b>5</b> *	24	22	52	2	3 3	3 5	2	7	24	<b>5</b> 4	<b>5</b> 4	<b>5</b> 4	22	27	27	28	23	22	22
VE-F1UM		S/N	တ	57	69	23	69	61	57	21	29	66	9 9	9	- £	9 4	3 6	3 5	80	8	62	69	58	5	29	82 (S	<b>B</b> (	2 2	28	62	19	57	61	61	69	58	54	25	69	63	62
VE-1		Š	*	110	117	115	117	118	=	110	<b>±</b>	2:	2 :	o	2 =	90	2 6	112	112	12	120	116	112	119	=	2	2	126	115	121	118	Ξ	118	119	117	=	105	101	116	122	120
le.		N/S	m	89	*	23	*	*	92	70	72	<b>*</b> i	<b>*</b> ;	2 5	, t	2 0	9 6	2 5	: =	20	*	72	79	7.	72	9	2 :	* *	2 2	92	2	69	22	74	23	72	68	99	72	*	73
VPAF	5	₹	7	133	143	=	143	++	137	136	40	7	2	?		5 5	2 4	2	138	136	=======================================	140	136	<del>+</del> + + + + + + + + + + + + + + + + + +	139	136	40	? :	14.5	148	142	135	142	143	142	. 40	132	129	139	141	142
CNDC	ġ		-	1098	1099	1188	1011	1102	1103	1104	1105	1106	1107	99	80	2 :	::	7117	1 4	1115	1116	1117	1118	1122	1125	1128	1129	1138	2	1136	1137	1139	1142	1143	1146	1155	1157	1163	1185	1186	, 39

DAY LANDINGS

USS ENTERPRISE (CVN-6

-LANDING DATA - MODEL F-14

				_																																	_				
WEIGHT		æ	21	22090	21773	21092	21909	22861	22861	22453	22136	22272	22045	20684	21138	20004	21637	21365	20548	21864	21591	22816	22861	22861	22181	22362	21954	22317	22272	21365	22181	21818	21727	21455	21637	20011	20820	21274	22725	21365	21637
WE		TBS	20	48700	48000	46500	48300	50490	50438	49500	48800	49100	48600	45600	46600	44100	47700	47100	45300	48200	47600	50300	50400	59499	48900	49366	48400	49200	49100	47100	48300	48100	47900	47300	47700	46100	45900	46900	50100	47100	47700
LIFT	<u>.</u>		19										1.00		1.10			1.00		1.10														1.00			1.00				
LIFT	5		18	1.00	96	96		1.00	1.20	1.10	1.00	1.10	1.00	96.	1.10	96	1.00	1.00	1.10	1.10	1.10	96	1.20	96	1.00	1.20	1.10	1.00	1.19	1.10	1.10	96.	96.	1.00	1.00	1.00	1.00	96.	1.20	1.20	1.10
\$	SP. A		11																																						
KVPA	Z Z		16	1.16	1.16	1.17	1.15	1.16	1.13	1.16	1.17	1.17	1.16	5::5	-:-	1.17	1.1	1.13	1.19	-:	1.14	1.15	1.20	1.13	1.14	1.20	1.17	1.13	1.16	1.22	1.15	<b>1</b> . <b>1</b>	1.19	1.18	1.19	1.20	1.19	1.1	1.20	1.18	1.19
VSP'A		R/S	<del>5</del>																																						
YS.		ž	<b>±</b>																																						
VPAMIN		R/S	5	63	62	61	62	49	9	63	63	63	63	61	وَ	60	62	62	60	62	62	49	64	<b>9</b>	63	63	62	63	63	62	63	62	62	62	62	61	19	61	63	62	62
Š		\$	12	122	121	119	121	124	124	123	122	122	122	118	119	116	120	120	117	121	120	124	124	124	122	122	121	122	122	120	122	121	121	120	120	118	118	119	123	120	120
VEOR		N/S	=	29	29	28	69	61	53	69	53	62	55	26	55	56	29	57	57	26	57	58	26	59	61	65	23	26	26	58	59	58	69	99	58	55	57	5	69	54	25
>		¥	6	=	114	115	116	118	122	116	<del>*</del>	120	107	109	107	168	115	Ξ	Ξ	108	=======================================	112	169	<b>*</b>	119	127	=======================================	168	169	113	13	112	117	116	113	107	110	100	117	105	102
	PERP.	N/S	0	-	-	-	0	0	0	0	0	0	60	-	6	0	0	0	0	-	-	-	-	-	-	-	_	-	n	n	n	n	n	n	n	n	n	-	6	20	n
WIND-VEL	<u> </u>	×	40	~	7	7	0	0	Φ	6	0	0	0	-	•	•	•	0	0	7	7	ч	8	8	7	~	64	7	ø	••	ø	9	v	ø	w	ဖ	ø	8	0	O	9
X	PAR.	¥	7	=	5	5	12	12	12	12	5	13	7	5	2	5	7	5	5	13	12	7	<u>+</u>	<b>±</b>	<b>*</b>	<u></u>	<b>±</b>	<b>±</b>	16	9	9	16	16	16	16	16	16	<del>*</del>	12	17	9
_		\$	•	22	22	25	24	74	24	24	22	<b>97</b>	27	29	22	22	22	25	22	25	23	28	28	28	28	28	78	28	32	32	32	32	32	32	32	32	32	27	<b>5</b>	ħ	32
VE-FILM		Ş	10	2	8	29	20	62	9	5	5	6	29	55	57	57	28	5	8	57	8	Š	62	8	52	5	ŝ	57	52	29	56	8	57	<b>8</b>	57	57	26	<b>3</b>	3	36	57
ώ >		\$	*	119	16	=	=======================================	120	116	119	118	118	==	106	Ξ	Ξ	5	==	=======================================	110	=	115	12	112	Ξ	119	=======================================	Ξ	19	114	109	106	=======================================	109	111	=======================================	109	105	124	108	Ξ
L.	6	M/S	n	23	22	72	72	7,	72	7,	7.4	7.	23	69	2	2	8	79	72	69	70	7	11	72	72	76	*	72	2	75	73	7	7.	2	7.4	7.4	2	89	76	2	7
VPAF	5	Š	~	=	=	139	139	144	140	143	143	7	==	135	136	136	55	136	140	135	137	143	149	140	139	147	1	139	142	146	=	35	3	1	143	1	===	132	148	142	143
CNDC	ġ		-	1192	1198	1199	1371	1373	1374	1380	1383	1384	1385	.386	1426	1425	1435	1437	1443	1520	1525	1724	1725	1726	1729	1730	1733	1734	1735	1738	1749	1741	1744	1747	1750	1753	1754	4153	4375	4625	4628

Main   Main	200			AIRCRAFT	S	KING :	SPEED AT	INKING SPEED AT TOUCHDOWN	N			GLIDE	GLIDE PATH ANGLE AT TD	NGLE A	0T T	WHEEL HEIGHT	EIGHT	HOOK HEIGHT	IGHT.
24         25         26         27         28         29         39         31         32         33         34         35         55         39         31         32         33         34         35         36         37         38         39           3.2         16.5         3.2         19         3.1         3.2         33         34         35         35         35         39 <t< th=""><th></th><th><u>¥</u></th><th>SE</th><th>8</th><th>RT</th><th>ίν</th><th>180</th><th>¥</th><th>(3</th><th>FREE-FL</th><th>16H1</th><th><b>.</b></th><th>¥</th><th>8</th><th>&gt;</th><th>OVER R</th><th>Ale P</th><th>OVER</th><th>(AMP</th></t<>		<u>¥</u>	SE	8	RT	ίν	180	¥	(3	FREE-FL	16H1	<b>.</b>	¥	8	>	OVER R	Ale P	OVER	(AMP
24         25         26         27         29         39         31         32         33         34         35         36         37         38         39<		F/S	K/S	F/S	s/m	F/S	s/m	F/S	M/S	F/S	N/S	DEG	<b>RAD</b>	DEG	8	E	×	t.	3
3.2         16.5         3.2         16.6         3.2         16.6         3.2         16.8         3.3         2.6         .645         2.7         .647         12.7         3.9         8.1           2.6         6.3         2.2         2.6         6.3         2.6         .611         3.5         11.4         3.5		23	24	22	<b>36</b>	27	28	53	30	3.	32	33	<b>4</b> 0	35	36	37	38	39	94
1.6         2.6         2.7         2.2         8.93         6. 811         8.4         2.6         5.9           2.6         2.6         2.1         3.5         1.7         2.7         2.3         2.2         8.93         2.1         3.9<		10.5	3.2	10.5	3.2	10.9	×.	10.8	3.3			2.6	. 645	2.7	.047	12.7	3.9	89	2.5
2.6         6.9         2.1         7.7         2.4         7.6         2.3         3.4         6.66         3.5         6.9         3.5         1.9         3.5         1.9         3.5         1.9         3.5         1.9         3.5         1.9         3.5         1.9         3.5         1.9         3.5         1.9         3.5         1.9         3.5         1.9         3.5         1.9         3.5         1.9         3.5         1.9         3.5         1.9         3.5         1.9         3.5         1.9         3.5         1.9         3.5         1.9         3.5         3.6         3.5         3.6         3.5         3.6         3.5         3.6         3.5         3.6         3.5         3.6         3.6         3.5         3.6         3.6         3.6         3.7         3.6         4.6         3.5         3.6         4.6         3.5         3.6         4.6         3.5         3.6         4.6         4.5         3.5         3.6         3.6         3.6         3.5         3.6         3.6         3.7         3.6         3.7         3.6         3.7         3.6         3.7         3.6         3.6         3.6         3.6         3.6         3.6 <th></th> <th><b>4</b></th> <th>+</th> <th>2.0</th> <th>9.</th> <th>2.4</th> <th>7.</th> <th>2.5</th> <th></th> <th></th> <th></th> <th>2.5</th> <th>.039</th> <th>9</th> <th>.011</th> <th>4.8</th> <th>5.6</th> <th>6.0</th> <th>1.2</th>		<b>4</b>	+	2.0	9.	2.4	7.	2.5				2.5	.039	9	.011	4.8	5.6	6.0	1.2
1.2.         3.6         1.1.         3.5         1.1.         3.5         1.1.         3.5         1.1.         3.5         1.1.         3.5         1.1.         3.5         1.1.         3.5         1.1.         3.5         1.1.         3.5         1.1.         3.5         1.2.         3.6         3.5         3.7         3.7         3.6         3.5         3.6         3.5         3.7         3.6         3.5         3.6         3.5         3.7         3.6         3.5         3.6         3.7         3.7         3.6         3.7         3.7         3.6         3.7         3.7         3.7         3.6         3.7         3.7         3.7         3.7         3.7         3.7		6.7	2.0	6.9	2.1	7.7	2.4	7.6	2.3			2.8	.048	2.1	.037	10.9	3.3	5.7	1.7
3.3         11.6         3.5         11.4         3.5         11.6         3.5         10.9         3.		2.5	æ	12.4	8	+ ==	3	11.9	3.6			3.4	.060	3.5	. 961	12.8	6.5	7.8	2.4
1.9         11.1         3.4         9.5         2.9         10.4         3.2         10.4         3.2         10.4         3.2         10.4         3.2         10.6         3.0         3.0         69.2         3.7         3.0         1.6         10.1         3.1         9.2         3.0         1.6         10.6         3.2         9.4         13.1         4.6         4.5         9.2         3.4         13.1         4.6         4.5         9.2         3.4         13.1         4.6         4.5         9.6         9.2         3.6         13.1         13.1         4.6         8.2         3.2         9.6         13.2         9.4         13.1         4.6         8.2         3.2         9.6         9.2         9.6         9.2         9.6         9.2         9.6         9.2         9.6         9.2         3.6         9.2         9.6         9.2         9.6         9.2         9.6         9.2         9.6         9.2         9.6         9.2         9.6         9.2         9.6         9.2         9.6         9.2         9.6         9.2         9.6         9.2         9.6         9.2         9.6         9.2         9.6         9.2         9.6         9.2		10.7	3.3	1.0	4.6	11.6	3.5	<b>+</b> .=	3.5			2.8	. 049	3.3	.057	13.5	<del>-</del>	8.7	5.6
2.7         18.6         3.9         6.9         2.1         7.9         2.4         1.6         628         2.3         644         9.2         2.8         4.6         9.7         2.6         9.4         9.2         2.6         9.9         2.7         2.6         9.6         2.3         944         14.6         4.6         9.2         2.6         9.6         9.4         9.8         3.4         9.6         3.4         9.6         3.4         9.6         3.4         9.6         3.4         9.6         3.4         9.6         9.7         2.2         9.6         9.7         2.2         9.6         9.7         2.2         9.6         9.7         3.2         9.6         9.7         3.2         9.6         9.7         3.2         9.6         9.7         3.6         9.7         3.6         9.7         3.6         9.7         3.6         9.8         3.7         9.6         9.7         3.6         9.7         3.6         9.8         3.7         9.6         9.7         3.6         9.8         3.7         9.6         9.8         3.7         3.6         9.8         3.7         9.6         9.8         3.7         9.8         9.8         9.8         9.8 </td <td></td> <td>6.3</td> <td>6.</td> <td>=</td> <td>4.8</td> <td>9.3</td> <td>2.9</td> <td>10.4</td> <td>3.2</td> <td></td> <td></td> <td>2.6</td> <td>.045</td> <td>3.0</td> <td>.052</td> <td>9.7</td> <td>3.0</td> <td>4.9</td> <td>5.</td>		6.3	6.	=	4.8	9.3	2.9	10.4	3.2			2.6	.045	3.0	.052	9.7	3.0	4.9	5.
1.6         19.1         3.1         3.5         2.6         9.7         3.6         9.7         3.6         9.8         2.6         9.8         2.6         9.8         2.6         9.8         2.6         9.8         3.5         2.6         9.8         3.5         1.6         9.7         3.5         9.8         3.5         9.8         9.8         3.6         9.8         3.7         3.6         9.8         3.7         3.6         3.7         3.7         3.7         3.7         3.8         3.8         3.8         3.8         3.8         3.8         3.8         3.8         3.8         3.8         3.8         3.8         3.8         3.8         3.8         3.8         3.8         3.8         3.8 <td></td> <td>g. 6.</td> <td>2.7</td> <td>10.0</td> <td>3.0</td> <td>6.9</td> <td>2.1</td> <td>7.9</td> <td>2.4</td> <td></td> <td></td> <td>5.</td> <td>.028</td> <td>2.3</td> <td>. 949</td> <td>9.2</td> <td>2.8</td> <td>4.6</td> <td><del>+</del>:</td>		g. 6.	2.7	10.0	3.0	6.9	2.1	7.9	2.4			5.	.028	2.3	. 949	9.2	2.8	4.6	<del>+</del> :
2.6         9.3         2.5         6.6         2.7         3.6         6.4         2.4         6.6         13.1         4.0         8.2           2.4         1.2         16.6         3.6         1.3         1.4         6.6         2.4         6.6         2.6         2.7         6.6         2.7         6.6         2.7         6.6         2.7         6.6         2.7         6.6         2.7         6.6         2.7         6.6         2.7         6.6         2.7         6.6         2.7         6.6         2.7         6.6         2.7         6.6         2.7         6.6         2.7         6.6         2.7         6.6         2.8         6.6         2.7         6.6         2.7         6.6         2.7         6.6         2.7         6.6         2.7         6.6         2.7         6.6         2.7         6.7         2.7         6.6         2.7         3.7         6.6         2.7         3.7         6.7         3.7         6.8         3.7         6.7         3.7         6.7         3.7         6.6         3.7         3.7         6.7         3.7         3.7         3.7         3.7         3.7         3.7         3.7         3.7         3.7 <td></td> <td>5.2</td> <td>1.6</td> <td>10.1</td> <td>3.1</td> <td>9.3</td> <td>2.8</td> <td>9.7</td> <td>3.0</td> <td></td> <td></td> <td>3.1</td> <td>.053</td> <td>2.5</td> <td>.044</td> <td>14.6</td> <td>4.5</td> <td>9.5</td> <td>2.9</td>		5.2	1.6	10.1	3.1	9.3	2.8	9.7	3.0			3.1	.053	2.5	.044	14.6	4.5	9.5	2.9
3.4         12.6         3.8         10.9         3.3         10.9         3.3         10.9         3.5         10.9         3.5         13.5         4.6         6.9         13.5         4.6         6.9         13.5         4.6         6.9         2.3         10.9         13.5         2.6         9.9         2.3         10.9         13.5         2.6         9.9         2.3         10.9         13.5         2.9         6.9         2.3         10.9         13.5         2.9         6.9         2.3         10.9         13.5         2.9         6.9         2.3         10.9         13.5         2.9         6.9         2.3         6.9         13.5         2.9         6.9         2.3         6.9         13.5         2.9         13.5         14.5         13.5         14.5         13.5         14.5         13.5         13.5         13.5         13.5		8.5	2.6	9.3	2.8	8.5	5.6	<b>8</b> .9	2.7			5.6	.046	2.3	.041	13.1	<b>4</b> .0	8.2	2.5
2.6         9.2         9.2         9.9         9.6         3.4         9.9 <td></td> <td>1.1</td> <td>4.0</td> <td>12.6</td> <td>3.8</td> <td>10.0</td> <td>ر ا</td> <td>10.9</td> <td>n.</td> <td>10.9</td> <td>3.3</td> <td>3.0 0</td> <td>.053</td> <td>4.6</td> <td>. 059</td> <td>13.2</td> <td>6</td> <td>8.7</td> <td>2.7</td>		1.1	4.0	12.6	3.8	10.0	ر ا	10.9	n.	10.9	3.3	3.0 0	.053	4.6	. 059	13.2	6	8.7	2.7
2.6         9.2         2.6         9.2         2.7         0.55         2.3         0.66         1.3         0.5         2.3         0.65         2.3         0.66         1.3         0.5         2.3         0.65         2.3         0.66         1.3         0.5         0		<b>4</b> .4	۳.	<b>.</b> 6	3.2	- - -		۳. ت	4.5			o	.068	4.4	. 060	7.3	2.5	2.0	٠.
2.8         9.8         3.8         19.1         3.1         3.2         1835         2.9         12.3         3.7         17.2           2.9         9.8         3.8         19.1         3.1         3.1         3.2         3.9         1.2         3.9         3.9         1.2         3.3         1.2         3.4         7.1         3.4         7.1         3.4         7.1         3.4         7.0         3.4         7.0         3.4         7.0         3.4         7.0         3.4         7.0         3.4         7.0         3.4         7.0         3.4         7.0         3.4         7.0         3.4         7.0         3.4         7.0         3.4         7.0         3.4         7.0         3.4         7.0         3.4         7.0         3.4         7.0         3.4         7.0         3.5         3.2         4.7         1.0         4.7         7.1         7.1         7.1         7.1         7.1         7.1         7.1         7.1         7.1         7.1         7.2         7.1         7.1         7.2         7.1         7.2         7.1         7.2         7.1         7.2         7.2         7.1         7.2         7.2         7.2         7.2<		<b>8</b> .5	5.6	9.5	7. 9.	80 j	2.6	Ø :	2.7	:		2.9	.050	2.3	.040	= :	9 1	6. 6.	2.7
2.9         8.8         2.6         2.6         2.6         2.6         3.7         3.6         3.7         3.6         3.7         3.6 <td></td> <td>6.7</td> <td>7.0</td> <td>න න</td> <td><b>5</b></td> <td>10.3</td> <td>٠. م</td> <td>ල. ල</td> <td>S. 0</td> <td>10.1</td> <td>J.</td> <td>3.2</td> <td>. 055</td> <td>5.9</td> <td>. 959</td> <td>12.3</td> <td>3.7</td> <td>7.2</td> <td>2.2</td>		6.7	7.0	න න	<b>5</b>	10.3	٠. م	ල. ල	S. 0	10.1	J.	3.2	. 055	5.9	. 959	12.3	3.7	7.2	2.2
1.9         7.2         2.2         6.0         1.8         6.8         2.1         2.3         640         1.8         6.8         7.1         2.3         6.0         2.9         7.4         2.3         3.0         6.0         2.9         7.4         0.7         2.8         669         1.2         3.4         7.0         2.2         1.4         7.1         2.4         7.1         2.4         1.6         4.7         1.6         1.7 <td></td> <td>9.9</td> <td>7.0</td> <td>8. 8.</td> <td>2.7</td> <td><b>8</b>0</td> <td>2.6</td> <td>9.8</td> <td>5.6</td> <td></td> <td></td> <td>5.9</td> <td>.050</td> <td>2.5</td> <td>. 039</td> <td>6.7</td> <td>2.7</td> <td>ω ( Β</td> <td>1.2</td>		9.9	7.0	8. 8.	2.7	<b>8</b> 0	2.6	9.8	5.6			5.9	.050	2.5	. 039	6.7	2.7	ω ( Β	1.2
2.1         8.3         2.5         6.6         2.9         7.4         2.3         2.1         .037         1.9         .033         11.1         3.4         7.0         2.2         1.4         2.3         11.1         3.4         7.0         2.2         1.4         3.5         2.2         2.2         1.4         3.5         2.2         2.2         1.4         3.5         2.2         2.8         3.9         3.0		۰. در	6.	7.2	2.5	6.9	<del>-</del>	<b>6</b> 0	2.1			2.3	.040	æ. ·	.032	11.2	4.0	7.1	2.2
2.8         9.4         2.9         19.5         3.0         9.8         3.0         3.3         .677         2.8         .694         7.2         2.2         1.4         9.8         3.0         3.3         .697         2.8         1.6         4.7         1.6         4.7         1.6         4.7         1.6         4.7         1.6         4.7         1.8         4.9         1.5         4.9         1.5         2.4         .667         2.8         1.6         1.5         5.3         12.9         12.9         1.6         1.5         9.6         1.5         9.7         1.6         1.5         9.7         1.6         1.5         9.6         1.5         9.6         1.5         9.6         1.5         9.7         1.6         1.5         9.7         1.6         1.5         9.7         1.6         1.5         9.7         1.6         1.5         9.7         1.6         1.5         9.7         1.6         1.5         9.7         1.6         1.5         9.7         1.6         1.5         9.7         1.6         1.5         9.7         1.7         1.6         1.6         1.7         1.7         1.6         1.8         1.9         1.6         1.8		7.0	2.1	<b>6</b>	2.5	9.	5.0	7.4	2.3			2.1	.037	e: (	.033	- ; = ;	4.0	7.0	2.1
3.1         10.4         3.2         9.7         3.0         9.8         3.0         3.3         .057         2.8         .050         15.5         4.7         10.4           3.2         3.2         3.7         3.0         9.8         3.0         3.3         .057         2.8         .050         15.5         4.7         10.4         15.5         10.3 <t< td=""><td></td><td>9.5</td><td>7.8 9.8</td><td><b>→</b></td><td>2.9</td><td>10.3</td><td>3.2</td><td>o.</td><td>ا ا</td><td>,</td><td>1</td><td><b>4</b> .</td><td>.077</td><td>2.8</td><td>.649</td><td>7.2</td><td>2.2</td><td><b>+</b> :</td><td>• (</td></t<>		9.5	7.8 9.8	<b>→</b>	2.9	10.3	3.2	o.	ا ا	,	1	<b>4</b> .	.077	2.8	.649	7.2	2.2	<b>+</b> :	• (
3.2         3.8         3.7         3.8         3.7         3.8         3.7         3.8         3.7         3.8         3.7         3.7         3.4         3.6         3.8         3.9         3.5         3.7         3.8 <td></td> <td> </td> <td> </td> <td>10.4</td> <td>3.2</td> <td>9.7</td> <td>. G</td> <td>ص ص</td> <td>ы. 6</td> <td>8. 8.</td> <td>S. 0</td> <td>۳. ا</td> <td>.057</td> <td>2.0</td> <td>.050</td> <td></td> <td>· ·</td> <td>4.6</td> <td>2.5</td>		 	 	10.4	3.2	9.7	. G	ص ص	ы. 6	8. 8.	S. 0	۳. ا	.057	2.0	.050		· ·	4.6	2.5
2.2         3.5         1.2         6.6         1.8         4.9         1.5         2.4         666         3.6         3.6         2.9         2.9         3.7         3.4         666         3.6         3.4         2.9         3.7         3.4         3.4         3.6         3.7         3.7         666         3.8         3.6         3.7         3.6         3.7         3.6         8.4         2.9         3.7         3.6         3.7         3.6         8.4         2.6         3.7         3.6         8.4         3.6         3.4         3.6         3.7         3.6         8.7         3.6         3.7         3.6         8.7         3.6         3.7         3.6         8.7         3.6         8.7         3.6         3.7         3.6         8.7         3.7         3.7         3.6         8.7         3.7         3.7         3.7         3.6         8.7         3.7 <td></td> <td>10.4</td> <td>3.2</td> <td>8.5</td> <td>2.8</td> <td>\. S</td> <td>9 ·</td> <td>2.5</td> <td>2.8</td> <td>•</td> <td>,</td> <td>2.7</td> <td>.04/</td> <td>۲.5 د .</td> <td>949</td> <td>17.5 0.6</td> <td></td> <td>6.21</td> <td>, ,</td>		10.4	3.2	8.5	2.8	\. S	9 ·	2.5	2.8	•	,	2.7	.04/	۲.5 د .	949	17.5 0.6		6.21	, ,
2.6         9.6         5.6         9.6         5.7         9.6         5.7         9.6         5.7         9.6         5.7         9.6 <td></td> <td>7.7</td> <td>2.5</td> <td>ر و . و</td> <td>1.2</td> <td>6.9</td> <td> ·</td> <td><b>4</b>.6</td> <td>- ·</td> <td>6.</td> <td>5.5</td> <td>2.4</td> <td>.042</td> <td>٠. د</td> <td>.023</td> <td>φ· σ</td> <td>5 5 6</td> <td>o .</td> <td></td>		7.7	2.5	ر و . و	1.2	6.9	·	<b>4</b> .6	- ·	6.	5.5	2.4	.042	٠. د	.023	φ· σ	5 5 6	o .	
2.6       9.6       2.7       9.6       3.2       9.5       9.7       9.6       9.5       9.7       9.6       9.5       9.7       9.6       9.5       9.7       9.6       9.5       9.7       9.6       9.5       9.7       9.6       9.5       9.7       9.6       9.6       9.7       9.6       9.5       9.5       9.7       9.6       9.7       9.6       9.7       9.6       9.7       9.6       9.7       9.6       9.7       9.6       9.7       9.6       9.7       9.6       9.7       9.6       9.7       9.6       9.7       9.6       9.7       9.6       9.7       9.6       9.7       9.6       9.7       9.6       9.7       9.6       9.7       9.6       9.7       9.6       9.7       9.6       9.7       9.7       9.7       9.7       9.7       9.7       9.7       9.7       9.7       9.7       9.7       9.7       9.7       9.7       9		- ;		12.6	۵ ر د د	* ·	n. •	12.0				٠ ٠ ٠	900	o e	000.	+ + • •	0 4 4	, ē	
2.6         9.6         2.7         9.6         3.7         .064         3.0         9.5         1.3           2.6         9.6         2.7         9.6         3.7         .064         3.0         9.5         11.8         7.3         9.6         2.9         9.9         3.1         .054         2.2         .053         12.4         3.8         7.3         9.6         2.9         9.9         3.1         .054         2.2         .053         12.4         3.8         11.8         4.1         8.4         2.7         9.6         4.1         8.4         1.8         4.1         8.4         1.8         4.1         8.4         1.8         8.7         3.7         9.6         4.1         8.4         1.3         9.9         3.9 <td< td=""><td></td><td>9 6</td><td>0 F</td><td></td><td></td><td>2 -</td><td>. c</td><td>5 v</td><td>. ·</td><td></td><td></td><td>6.4 4.4</td><td>. 626</td><td></td><td>20.0</td><td>- 4</td><td></td><td>4 -</td><td>- «</td></td<>		9 6	0 F			2 -	. c	5 v	. ·			6.4 4.4	. 626		20.0	- 4		4 -	- «
3.2         10.8         3.3         10.8         3.3         10.8         3.2         .058         3.2         .055         16.2         4.9         11.8           3.2         9.6         2.8         8.7         2.7         3.1         .054         2.2         .039         14.0         4.3         9.6           2.1         10.2         3.1         8.4         2.6         10.1         3.1         8.4         2.2         .039         1.2         0.53         17.3         5.3         12.8           2.6         1.7         6.1         1.9         6.1         1.9         2.2         .039         1.2         0.21         13.8         4.2         9.7           2.3         1.6         2.9         3.9         3.9         3.8         10.7         3.7         7.4           3.0         2.5         1.7         5.5         1.7         5.3         1.6         2.4         0.9         10.3         3.7         7.4           3.0         2.5         1.7         2.8         1.9         3.4         1.0         2.2         0.0         1.0         3.0         3.0         3.0         3.0         3.0         3.0 <t< td=""><td></td><td>. 6</td><td></td><td>. 6</td><td></td><td>. 6</td><td></td><td></td><td></td><td></td><td></td><td></td><td>964</td><td>10.</td><td>.053</td><td>12.4</td><td>80</td><td>7.3</td><td>2.5</td></t<>		. 6		. 6		. 6							964	10.	.053	12.4	80	7.3	2.5
3.2         9.0         2.8         8.4         2.6         8.7         2.7         3.1         .054         2.2         .039         14.0         4.3         9.6           2.1         10.2         3.1         8.4         2.6         10.1         3.1         2.8         .067         3.0         .053         17.3         5.3         12.8           2.6         10.5         3.6         2.9         3.9         3.0         3.0         .053         17.3         5.3         12.8           2.5         1.7         6.1         1.9         2.2         .039         1.2         .021         13.8         4.2         9.7           2.3         1.7         6.1         1.9         2.2         .039         1.2         021         13.8         4.2         9.7           2.3         1.6         2.4         1.7         5.5         1.7         2.8         1.0         5.3         13.8         4.6         13.9         3.7         4.6         4.6         4.6         13.3         3.0         3.0         3.0         3.0         3.0         3.0         3.0         3.0         3.0         3.0         3.0         3.0         3.0		2.9	6.	10.8	. r.	10.7	3.0	19.8	<b>5</b>			3.3	.058	3.2	.055	16.2	₽.	11.8	3.6
2.1       10.2       3.1       8.4       2.6       10.1       3.1       2.8       .049       2.7       .048       13.6       4.1       8.4         2.6       10.5       3.6       2.9       3.9       3.6       3.8       .067       3.0       .053       17.3       5.3       12.8         1.8       5.7       1.7       6.1       1.9       2.2       .039       1.2       .021       13.8       4.2       9.7         2.3       6.2       1.9       3.9       3.6       1.7       5.5       1.7       7.4         3.1       5.3       1.6       2.4       .042       1.3       .022       9.9       3.7       7.4         3.0       2.5       1.7       3.6       1.1       3.8       1.1       2.2       0.38       .9       .016       9.1       2.8       4.6         3.1       5.3       1.6       2.4       .042       1.3       .022       9.9       3.0       5.3       4.6         3.1       5.3       1.6       2.4       .042       1.3       0.2       8.0       5.3       4.6       6.5         3.1       5.3       1.6       2		10.6	3.2	9.6	2.8	4.8	2.6	8.7	2.7			3.1	.054	2.2	. 039	14.0	4.3	9.6	2.9
2.6     10.5     3.2     8.2     2.5     9.6     2.9     3.0     3.8     .067     3.0     .053     17.3     5.3     12.8       1.8     5.7     1.7     6.1     1.9     2.2     .039     1.2     .021     13.8     4.2     9.7       2.3     6.2     1.9     5.4     1.7     5.5     1.7     5.3     1.6     2.4     .042     1.3     0.22     9.9     3.7     7.4       3.1     5.3     1.6     2.4     .042     1.3     0.2     9.9     3.0     3.0     3.0       3.1     5.3     1.6     2.4     .042     1.3     0.2     9.9     3.0     3.0     3.0       2.1     3.5     1.1     3.8     1.1     2.2     0.3     0.1     0.3     0.1     2.8     4.6       3.1     5.3     1.6     7.1     2.2     2.3     1.6     2.4     0.0     1.7     2.8     4.6       3.1     5.3     1.3     3.5     2.2     2.8     0.0     1.5     0.2     13.0     4.6     10.3     13.0       3.1     5.3     1.3     3.5     1.3     3.5     1.4     4.4     4.4     9.3 <td></td> <td><b>6</b>.8</td> <td>2.1</td> <td>10.2</td> <td>٠. ۲.</td> <td>4.8</td> <td>2.6</td> <td>19.1</td> <td>J. 1</td> <td></td> <td></td> <td>2.8</td> <td>.049</td> <td>2.7</td> <td>.048</td> <td>13.6</td> <td><b>+</b>.1</td> <td>4.8</td> <td>5.6</td>		<b>6</b> .8	2.1	10.2	٠. ۲.	4.8	2.6	19.1	J. 1			2.8	.049	2.7	.048	13.6	<b>+</b> .1	4.8	5.6
1.8     5.7     1.7     6.1     1.9     6.1     1.9     2.2     .039     1.2     .021     13.8     4.2     9.7       2.3     6.2     1.9     5.4     1.7     5.5     1.7     5.8     1.7     5.9     3.7     7.4       3.1     5.3     1.6     2.4     .042     1.3     .022     9.9     3.0     5.3       3.0     2.6     1.1     3.8     1.1     2.2     .038     .9     .016     9.1     2.8     4.6       3.1     5.3     1.6     2.4     .042     1.5     .026     9.7     3.1     5.6       3.1     5.3     1.6     2.4     .042     1.5     0.6     17.2     13.0       3.1     5.3     1.6     2.4     1.0     2.9     1.6     1.7     2.1     13.0       3.1     5.3     1.6     2.7     2.2     2.8     0.40     2.4     0.05     1.4     4.4     9.3       3.5     5.2     2.0     2.0     0.05     1.7     0.29     9.7     3.0     5.2       3.2     11.9     3.4     10.5     3.4     0.65     11.0     3.4     6.8       3.2     11.5 </td <td></td> <td>8.6</td> <td>5.6</td> <td>10.5</td> <td>3.2</td> <td>8.2</td> <td>2.5</td> <td>9.6</td> <td>5.9</td> <td>6.6</td> <td>3.0</td> <td>3.8</td> <td>. 067</td> <td>3.0</td> <td>. 053</td> <td>17.3</td> <td>5,3</td> <td>12.8</td> <td>a.9</td>		8.6	5.6	10.5	3.2	8.2	2.5	9.6	5.9	6.6	3.0	3.8	. 067	3.0	. 053	17.3	5,3	12.8	a.9
2.3       6.2       1.9       5.4       1.7       5.5       1.7       2.8       .048       1.6       .029       12.3       3.7       7.4         3.1       5.3       1.6       2.4       .042       1.3       .022       9.9       3.9       5.3         3.0       2.8       1.1       3.8       1.1       2.2       9.9       3.0       5.2       8.6       5.3         2.1       3.3       1.6       2.4       .042       1.3       .06       9.1       2.8       4.6         3.1       5.3       1.6       2.4       .042       1.5       .05       17.2       2.8       4.6       4.6       9.3       3.1       5.6       13.0       5.2       13.0       4.1       8.2       13.0       4.1       8.2       13.0       4.4       4.4       9.3       3.2       10.5       3.2       10.5       3.2       10.5       3.2       10.5       3.2       10.5       3.2       10.5       3.2       10.5       3.4       10.9       3.4       6.9       9.7       3.0       5.2       13.0       3.2       10.5       3.4       10.5       1.0       3.2       10.5       3.2		5.9 9.9	<b>8</b> .	5.7	1.7	6.1	6.	6.1	1.9			2.2	. 039	1.2	. 921	13.8	4.2	9.7	y.0
3.1       5.3       1.6       2.4       .042       1.3       .022       9.9       3.0       5.3         3.0       2.5       .7       4.1       1.2       3.6       1.1       3.8       1.1       2.2       .038       .9       .016       9.1       2.8       4.6         2.1       3.3       1.6       2.4       1.7       2.8       1.1       3.8       1.1       2.2       0.38       .9       0.06       9.1       2.8       4.6         3.1       5.3       1.6       7.1       2.2       7.3       2.2       2.8       1.6       1.5       0.5       1.1       5.2       13.0         3.1       5.9       2.7       2.2       2.8       .048       1.5       0.4       4.1       8.2       13.0		7.6	2.3	8.2	6.	4.0	1.7	5.5	1.7			2.8	.048	9.	.029	12.3	3.7	7.4	2.3
3.0       2.5       .7       4.1       1.2       3.6       1.1       3.8       1.1       2.2       .038       .9       .016       9.1       2.8       4.6         2.1       3.3       1.6       2.4       .7       2.8       .9       3.4       1.0       2.0       .034       .4       .007       10.3       3.1       5.6         3.1       5.3       1.6       7.1       2.2       7.3       2.2       7.2       13.0       3.1       5.6       13.0       4.1       8.2       13.0       4.1       8.2       13.0       4.1       8.2       13.0       4.6       10.5       3.2       10.5       3.4       .051       14.4       4.4       9.3       3.2       11.0       3.4       6.8       3.2       10.5       3.2       10.5       3.2       10.5       3.2       10.5       3.4       6.8       9.7       3.0       5.2       3.0       5.2       3.0       5.2       3.0       5.2       3.0       5.2       3.0       5.2       3.0       5.2       3.0       9.5       3.4       6.8       9.7       5.3       13.0       4.8       4.4       9.3       3.2       11.0       3.4<		10.3	J. 7	5.3	1.6	2.8	<u>o</u> .	<b>+</b> .+	 	5.3	9.	2.4	. 042	٠. د.	. 022	6. 6	3.0	5.3	9.
2.1 3.3 1.0 2.4 .7 2.8 .9 3.4 1.0 2.0 .034 .4 .007 10.3 3.1 5.6 3.1 5.3 1.6 7.1 2.2 7.3 2.2 2.8 .049 1.5 .026 17.2 5.2 13.0 3.1 5.3 1.6 7.1 2.2 7.3 2.2 7.3 2.2 2.8 .049 1.5 .026 17.2 5.2 13.0 3.1 9.0 2.7 12.2 3.7 11.3 3.5 4.0 3.5 2.8 8.6 2.6 8.9 2.7 2.8 9.4 9.4 9.4 9.5 12.0 3.7 11.9 3.6 12.0 3.7 3.7 3.2 .055 3.4 .059 14.4 4.4 9.3 2.1 6.4 1.9 3.1 12.2 6.7 2.1 2.2 .039 1.7 0.29 9.7 3.0 5.2 2.1 3.4 10.5 3.2 11.0 3.4 6.8 4.0 14.5 4.4 11.6 3.5 13.2 4.0 3.1 .055 3.4 .060 17.4 5.3 13.0		6.6	3.0	2.2	۲.	<del>-</del>	1.2	3.6	-:	3.8	<u>-</u>	2.2	. 038	o.	.016	9.1	2.8	4.6	<b>+</b> .
3.1     5.3     1.6     7.1     2.2     7.3     2.2     2.8     .049     1.5     .026     17.2     5.2     13.0       3.1     9.0     2.7     12.2     3.5     4.0     .070     3.4     .059     13.4     4.1     8.2       3.2     9.3     2.8     8.6     2.7     2.8     .048     2.4     .042     15.0     4.6     10.5       3.2     12.0     3.7     3.2     .055     3.4     .059     14.4     4.4     9.3       2.1     6.4     1.9     7.1     2.2     6.7     2.1     2.2     .039     1.7     .029     9.7     3.0     5.2       3.2     11.3     3.4     10.5     3.4     10.6     17.4     5.3     13.0       4.0     14.5     4.4     11.6     3.5     13.2     4.0     3.1     .055     3.4     .060     17.4     5.3     13.0		7.0	2.1	J. J	<b>6</b> .	7.4	۲.	2.8	σ.	4.6	9.	2.0	.034	₹.	.007	10.3	J.1	2.6	1.7
5.1     9.0     2.7     12.2     3.7     11.3     3.5     4.0     .070     3.4     .059     13.4     4.1       3.3     9.3     2.8     8.6     2.6     8.9     2.7     2.8     .048     2.4     .042     15.0     4.6       3.2     12.0     3.7     3.2     .055     3.4     .059     14.4     4.4       2.1     6.4     1.9     7.1     2.2     6.7     2.1     2.2     .039     1.7     .029     9.7     3.9       3.2     11.3     3.4     10.5     3.4     2.9     .051     2.9     .050     11.0     3.4       4.0     14.5     4.4     11.6     3.5     13.2     4.0     3.1     .055     3.4     .060     17.4     5.3		10.2	3.1	5.3	9.	7.1	2.5	7.3	2.2			2.8	.049	5.	. 026	17.2	5.2	13.0	4.0
3.3 9.3 2.8 8.6 2.6 8.9 2.7 2.8 .048 2.4 .042 15.0 4.6 3.2 12.0 3.2 12.0 3.7 11.9 3.6 12.0 5.7 3.2 .055 3.4 .059 14.4 4.4 2.1 6.4 1.9 7.1 2.2 6.7 2.1 2.2 .039 1.7 .029 9.7 3.0 3.2 11.3 3.4 10.5 3.2 11.0 3.4 2.9 .051 2.9 .050 11.0 3.4 4.0 14.5 4.4 11.6 3.5 13.2 4.0 3.1 .055 3.4 .060 17.4 5.3		19.2	3.1	<b>8</b> .6	2.7	12.2	3.7	₽. E.	3.5			4.0	.070	4.	. 629	13.4	<del>-</del> -	8.2	2.5
5     3.2     12.0     3.7     3.2     .055     3.4     .059     14.4     4.4       8     2.1     6.4     1.9     7.1     2.2     6.7     2.1     2.2     .039     1.7     .029     9.7     3.0       5     3.2     11.3     3.4     10.6     3.4     3.4     3.4     3.4       1     4.0     14.5     4.4     11.6     3.5     13.2     4.0     3.1     .055     3.4     .060     17.4     5.3     6.3		19.8	3.3	9. 5.	2.8	8 9	2.6	න ග	2.7			2.8	.048	7.4	.042	15.0	4.6	- 10°.5	3.2
.8 2.1 6.4 1.9 7.1 2.2 6.7 2.1 2.2 .039 1.7 .029 9.7 3.0 .5 3.2 11.3 3.4 10.5 3.2 11.0 3.4 2.9 .051 2.9 .050 11.0 3.4 .1 4.0 14.5 4.4 11.6 3.5 13.2 4.0 3.1 .055 3.4 .060 17.4 5.3		10.5	3.2	12.0	3.7	11.9	3.6	12.0	3.7			3.2	. 055	4.6	.059	14.4	<b>₹</b>	9 .u	2.8
.5 3.2 11.3 3.4 10.5 3.2 11.0 3.4 2.9 .051 2.9 .050 11.0 3.4 4.0 14.5 4.4 11.6 3.5 13.2 4.0 3.1 .055 3.4 .060 17.4 5.3		6.8	2.1	4.9	6.	7.1	2.5	6.7	2.1			2.5	. 039	7.7	. 629	9.7	ы. Ө.	2.5	9.
.1 4.8 14.5 4.4 11.6 3.5 13.2 4.8 3.1 .055 3.4 .060 17.4 5.3 '		19.5	3.5	1.3	4.4	10.5	3.5	1.0	4.6			2.9	.051	5.9	. 050	11.0	٠, b	8. 8.	2.1
		13.1	4.0	14.5	<b>+</b> . <b>+</b>	11.6	3.5	13.2	4.0			3.1	.055	4.5	. 060	17.4	5.3	13.0	4.0

PAGE         PAGE         FAGE         ANG         FREE-FILLIGHT         BMA         OVER RAMP         OVER RAMP         OVER RAMP         OVER RAMP         PAGE																		
24         25         26         27         105         F/5         M/5	Š	14	8	RT	STI	8	ž	y	FREE-F	LIGHT	æ	HA	ĒΦ	Š	OVER	RAMP	OVER	RAMP
24         25         26         27         28         29         31         32         33         35         36         37         38         39<		K Z	53	M/S	F/S	K/S	F/S	s/m	F/S	s/x	DEG	RAD	DEG	8	Ħ	3	E	3
1.3         13.6         4.2         12.5         5.8         13.2         4.0         3.7         .064         3.2         .055         17.5         5.3         13.0           1.8         11.5         3.5         10.8         3.3         3.7         .065         3.2         .065         13.7         4.7         10.8           3.5         10.2         3.2         10.8         3.3         3.2         .065         3.2         .065         13.7         4.7         10.8           3.5         10.2         3.2         10.8         3.3         3.2         .065         13.7         4.7         10.4           3.5         10.2         3.2         10.8         3.3         10.8         3.2         10.4         3.2         10.8         3.2         10.4         3.2         10.8         3.2         10.8         3.3         10.8         3.2         10.8         3.3         10.8         3.2         10.8         3.3         10.8         3.3         10.8         3.3         10.8         3.3         10.8         3.3         10.8         3.3         10.8         3.3         10.8         3.3         10.8         3.3         10.8         3.3	_	<b>5</b>	22	26	27	28	53	30	3	32	33	ų,	35	36	37	88	39	40
3.7         1.1.         3.5         1.1.         3.5         1.5.         4.7         10.5           3.5         10.2         3.5         10.8         3.3         3.4         2056         2.8         605         13.1         4.7         10.5           3.5         10.2         3.5         10.8         3.3         2.8         6.6         2.8         605         14.9         4.5         10.4           2.5         9.5         3.6         11.3         3.7         2.8         6.5         2.8         605         14.9         4.5         10.4           3.1         8.8         2.7         11.2         3.7         2.8         6.8         2.8         10.4         10		£.	13.6	4.2	12.5	S. 50	13.2	4.0			3.7	.064	3.2	. 055	17.5	5.3	13.0	4.0
1.8 11.5 3.5 10.5 3.2 10.8 3.3 3.4 4060 5.2 6.055 13.1 4.0 7.9 7.5 10.5 5.2 10.8 13.1 4.0 7.9 7.5 10.5 5.2 10.8 13.3 4.0 7.5 10.5 5.2 10.8 13.1 4.0 7.5 10.5 5.2 10.8 10.8 5.2 10.8 5.2 10.8 5.2 10.8 5.2 10.8 5.2 10.8 5.2 10.8 5.2 10.8 5.2 10.8 5.2 10.8 5.2 10.8 10.8 5.2 10.8 10.8 5.2 10.8 10.8 5.2 10.8 10.8 5.2 10.8 5.2 10.8 10.8 5.2 10.8		3.7	11.7	3.8	19.3	3.1	11.0	3.3			3.2	. 056	4.6	. 059	15.4	4.7	10.5	3.2
3.5         19.5         3.5         19.6         2.8         649         14.9         4.5         10.4           3.5         19.5         3.9         19.5         2.8         649         14.9         4.5         10.4           2.5         9.9         3.0         19.5         3.4         3.7         2.9         10.5         2.4         641         1.1         4.4         4.9         11.4           3.1         8.6         2.6         9.9         3.2         8         2.9         10.5         1.0         652         1.4         4.4         4.9         11.4         4.5         11.4         4.5         11.6         4.2         11.6         3.7         10.6         10.5         3.1         10.6         3.2         10.6         3.3         10.6         3.3         10.6         4.2         11.6         4.3         11.6         4.3         11.6         4.3         10.6         3.3         10.6         3.3         10.6         3.3         10.6         3.3         10.6         3.3         10.6         3.3         10.6         3.3         10.6         3.3         10.6         10.6         3.3         10.6         10.6         10.6 <t< td=""><td></td><td><b>8</b>.</td><td>11.5</td><td>3.5</td><td>10.5</td><td>3.2</td><td>10.8</td><td>3.3</td><td></td><td></td><td>4.5</td><td>. 060</td><td>3.2</td><td>.056</td><td>13.1</td><td>4.0</td><td>7.9</td><td>2.4</td></t<>		<b>8</b> .	11.5	3.5	10.5	3.2	10.8	3.3			4.5	. 060	3.2	.056	13.1	4.0	7.9	2.4
2.5         3.6         3.2         1.3         3.4         3.1         653         3.6         653         14.3         4.4         9.7           2.5         3.6         3.6         3.5         3.6         3.6         3.6         16.6         5.1         11.4           3.5         12.5         3.6         2.7         3.6         6.5         3.6         6.6         5.1         11.4           2.8         8.4         2.6         9.8         2.7         2.8         6.6         13.8         4.2         9.7           2.8         8.4         2.6         9.8         2.7         3.6         6.6         13.8         4.2         9.7           2.8         1.6         3.5         11.6         3.5         10.4         3.5         10.6         4.7         9.7         11.4           2.5         1.6         3.5         10.4         3.5         10.6         3.5         10.6         3.5         10.6         3.5         10.6         3.5         10.6         3.5         10.6         3.5         10.6         3.5         10.6         3.5         10.6         3.5         10.6         3.5         10.6         3.5		3.5	10.2	3.1	11.5	3.5	10.8	3.3			3.2	. 056	2.8	.049	14.9	4.5	10.4	3.2
2.5         9.9         9.3         2.8         9.5         1.4         16.1         4.9         11.4           3.3         18.8         2.6         9.3         2.8         9.5         12.1         3.6         12.1         3.7         3.9         655         12.6         5.1         11.9         3.3         18.8         2.7         2.4         .64         2.1         3.9         18.9         2.7         9.3         11.9         3.3         18.9         18.9         3.3         18.9         18.9         3.3         18.9         18.9         3.3         18.9		3.3	12.5	3.8	9.6	3.2	11.3	4.5			J. 7	.053	3.0	.853	14.3	<b>+.</b> +	9.7	3.0
3.3         12.5         3.6         12.1         3.7         3.6         13.9         3.6         13.9         13.9         3.6         13.9         3.6         13.9         3.6         13.9         3.6         13.9         4.2 <t< td=""><td></td><td>2.5</td><td>ø.</td><td>3.8</td><td>æ 9.</td><td>2.6</td><td>٠. د.</td><td>2.8</td><td></td><td></td><td>2.9</td><td>.051</td><td>4.7</td><td>.041</td><td>16.1</td><td>4.9</td><td>1.4</td><td>3.5</td></t<>		2.5	ø.	3.8	æ 9.	2.6	٠. د.	2.8			2.9	.051	4.7	.041	16.1	4.9	1.4	3.5
3.1         8.8         2.7         2.4         .041         2.1         0.05         13.8         4.2         9.2         3.9         14.0         3.9         3.8         2.7         2.8         4.4         2.0         13.8         4.2         3.8         17.7         3.1         12.2         3.9         14.0         3.1         10.6         3.2         10.4         3.2         10.4         3.2         10.4         3.2         10.4         3.2         10.4         3.2         10.4         3.2         10.6         3.3         10.8         3.2         10.4         3.2         10.6         3.3         10.8         3.2         10.4         3.2         10.6         3.2         10.6         3.3         10.8         3.2         10.4         3.2         10.6         3.3         10.8         3.2         10.6         3.3         10.8         3.2         10.6         3.3         10.8         3.3         10.8         3.2         10.6         3.3         10.8         3.3         10.8         3.3         10.8         3.2         3.2         3.2         3.2         3.2         3.2         3.2         3.2         3.2         3.2         3.2         3.2         3.2		3.3	12.5	а. В	11.7	3.6	12.1	3.7			3.0	.053	3.0	.052	16.6	5.1	11.9	3.6
2.8         8.4         2.6         9.3         2.8         9.4         2.6         9.3         1.8         9.3         2.8         9.4         2.6         9.3         9.3         9.8         9.3         9.3         9.3         9.3         9.3         9.3         9.3         9.3         9.3         9.3         9.3         12.6         3.9         9.3         12.6         3.9         9.3         12.6         3.9         12.7         9.4         10.6         17.5         5.3         12.6         3.3         12.6         3.3         12.6         3.3         12.6         3.3         12.6         3.3         12.6         3.3         12.6         13.7         4.1         13.5         12.6         13.6         9.3         12.6         13.7         12.6         13.7         12.6         13.7         13.7         13.7         13.7         13.8         <		J. 1	<b>8</b> .8	2.7	8.5	<b>5.6</b>	89 89	2.7			2.4	.041	2.1	.036	13.8	4.5	9.5	2.8
2.7         11.4         3.5         11.8         3.6         3.5         10.8         3.7         11.4         3.5         11.8         3.5         11.8         3.5         11.8         3.5         11.8         3.5         11.8         3.5         11.8         3.5         12.4         3.6         66.5         3.7         10.6         17.5         5.3         12.6           2.9         11.9         3.5         12.4         3.6         66.5         3.7         0.6         17.7         5.3         12.6           2.9         11.9         3.5         10.6         3.5         3.6         13.6         13.7         4.1         18.6         13.5         12.6         13.6         13.5         12.6         13.5         12.6         13.5         12.6         13.5         12.6         13.5         12.6         13.5         12.6         13.5         12.6         13.5         12.6         13.5         12.6         13.5         12.6         13.5         12.6         13.5         12.6         13.5         12.6         13.5         12.6         13.5         12.6         13.5         13.6         13.5         13.6         13.5         14.1         18.6         13.5		2.8	<b>8</b> .4	5.6	6.6	3.0	9.3	2.8			2.8	.048	2.5	. 038	14.0	4.3	8.7	2.7
2.7 18.2         3.1 18.5         3.2 18.4         3.2         3.6         .65.3         3.9         .65.2         12.7         3.9         7.7           3.5 13.4         3.6         .65.3         3.4         .66.3         3.4         .66.3         3.4         .66.3         3.4         .66.3         3.7         13.6         4.1         8.6         12.5         3.5         13.5		3.1	12.2	3.7	1.4	J.5	1.8	3.6					3.3	. 058				
3.3         12.0         3.6         10.5         3.4         10.6         13.4         10.6         13.5         12.6         13		2.7	10.2	J. 7	10.5	3.2	10.4	3.2			3.0	.053	3.0	.052	12.7	3.9	7.7	2.3
3.6         13.4         4.1         11.5         3.5         12.4         3.8         3.9         .052         3.2         .055         19.7         6.0         15.3           2.9         8.3         2.5         8.8         2.7         8.6         2.6         .059         2.8         .047         13.6         4.1         8.6           2.9         11.0         3.3         11.0         3.3         10.9         3.3         3.4         .059         2.8         .047         13.6         4.4         9.3           2.9         12.5         3.7         1.0         3.2         1.0         3.5         1.6         4.4         9.3         1.5         1.2         3.4         .059         2.1         0.05         1.4         4.4         9.3         1.5         1.2         1.2         3.4         .059         2.1         0.05         1.4         4.4         9.3         1.5         1.6         9.3         1.5         1.6         9.3         1.2         1.5         2.2         2.2         2.2         2.3         1.4         4.4         9.3         1.3         1.6         9.3         1.3         1.6         9.3         1.3         1.6		3.3	12.0	3.6	10.5	3.2	11.3	4.5			3.6	.063	4.4	. 969	17.5	5.3	12.6	J. 8
2.9         8.3         2.5         8.8         2.7         8.6         2.9         .651         2.7         .647         13.6         4.1         8.6           2.9         11.0         3.4         11.0         3.3         11.0         3.3         11.0         3.3         11.0         3.3         11.0         3.3         11.0         3.3         11.0         3.3         11.0         3.3         10.0         3.5         12.0         3.6         3.7         .65.7         4.4         9.7         2.0         2.0         13.9         3.2         3.6         13.9         3.7         .65.7         14.4         9.7         2.6         6.05         13.9         14.2         9.5         13.9         14.2         9.5         13.9         14.2         9.7         3.6         6.05         3.1         .65.5         14.4         9.7         2.6         6.05         14.7         2.7         14.7         2.7         14.7         2.7         14.7         2.7         14.7         2.7         14.7         2.7         14.7         2.7         14.7         2.7         14.7         2.7         14.7         2.7         14.7         2.7         14.7         2.7         14.7 </td <td></td> <td>3.6</td> <td>13.4</td> <td><del>-</del></td> <td>11.5</td> <td>3.5</td> <td>12.4</td> <td>3.8</td> <td></td> <td></td> <td>3.0</td> <td>.052</td> <td>3.2</td> <td>. 055</td> <td>19.7</td> <td>6.9</td> <td>15.3</td> <td>4.7</td>		3.6	13.4	<del>-</del>	11.5	3.5	12.4	3.8			3.0	.052	3.2	. 055	19.7	6.9	15.3	4.7
2.9         11.0         3.4         10.5         2.8         049         17.4         5.3         12.5           3.4         11.0         3.3         11.0         3.3         11.0         3.3         11.0         3.5         12.5         3.4         .059         3.1         0.5         14.4         4.4         9.5         12.5         12.5         12.5         3.5         12.5         3.2         7.5         2.5         2.7         9.1         2.8         4.4         .077         2.4         .042         23.8         13.9         4.2         9.5         13.9         4.2         9.5         13.9         4.2         3.8         4.2         9.5         13.5         10.5         2.7         9.1         2.8         4.4         .077         2.4         .042         23.8         4.2         9.5         10.9         3.3         10.8         4.2         10.2         4.4         .077         2.4         0.44         2.0         .035         13.9         10.2         10.2         10.2         2.7         2.7         2.7         2.7         3.7         10.9         3.9         10.9         3.9         10.9         3.9         10.9         3.9         10.9		2.9	8.3	2.5	8.8	2.7	8.6	2.6			2.9	.051	2.7	.047	13.6	<del>+</del> .+	8.6	5.6
3.4         11.6         3.3         11.6         3.3         11.6         3.5         11.6         3.5         12.6         3.5         12.6         3.6         3.5         12.6         3.6         3.6         3.6         13.9         3.7         14.4         9.3         3.7         13.9         3.5         12.9         3.6         18.5         3.7         18.7         3.6         18.9         2.7         3.6         18.9         2.7         3.6         18.9         2.7         3.6         18.9         2.7         3.6         18.9         2.7         3.7         3.7         3.7         3.7         3.7         3.7         3.8         3.7         3.8         3.7		2.9	11.0	4.6	10.3	3.1	10.4	3.2			4.6	.059	2.8	.049	17.4	5.3	12.5	3.8
2.9         12.3         3.7         11.6         3.5         12.0         3.4         .059         3.1         .055         18.5         5.6         13.9           2.5         7.6         2.3         7.9         2.7         9.1         2.8         4.4         .075         13.9         4.2         9.5           3.6         8.3         2.7         9.1         2.8         4.4         .075         2.4         2.8         4.5         9.7           3.6         8.3         2.5         7.9         2.7         9.1         2.8         4.4         9.7         2.4         2.8         4.7         9.7         9.7         9.7         3.9         9.8         1.9         4.5         9.7         3.9         9.8         1.9         6.5         9.9         9.8         9.8         1.9         6.5         2.9         9.9         9.8         1.9         9.7         1.9         9.2         9.9         9.8		4.5	11.0	3.3	11.0	3.3	10.9	3.3			4.6	. 059	3.2	.057	<b>+</b> . <b>+</b>	4.4	9.3	2.8
2.5         7.6         2.3         7.9         2.1         7.3         2.2         7.5         2.3         2.6         0.05         13.9         4.2         9.5           3.6         8.8         2.7         9.1         2.8         4.4         0.77         2.4         0.42         23.8         7.3         18.7           2.6         8.3         2.7         9.1         2.8         4.4         0.77         2.4         0.42         23.8         7.3         18.7           2.6         8.3         2.7         9.1         2.8         4.4         0.77         2.4         0.45         23.8         7.3         18.7         2.4         4.4         8.7         2.4         6.5         3.9         18.9         2.7         9.1         2.8         3.2         0.65         1.6         4.5         19.2         2.8         19.2         2.9         3.2         10.6         4.5         10.2         4.7         10.2         3.2         10.6         4.5         10.2         4.5         10.2         3.2         10.6         4.5         10.2         3.2         10.6         4.2         3.2         10.6         4.2         3.2         0.65         17.2<		2.9	12.3	3.7	1.6	3.5	12.0	3.6			4.6	.059	3.1	. 055	18.5	9.0	13.9	4.2
3.0         8.8         2.7         9.1         2.8         4.4         .077         2.4         .047         2.5         .047         2.7         .047         2.2         .038         14.5         4.4         9.7           2.6         8.3         2.5         7.9         2.4         8.1         2.5         8.9         2.7         .047         2.2         .038         14.5         4.5         9.9           3.6         8.4         2.6         8.1         2.5         8.9         2.4         2.3         .039         14.6         4.5         9.7           2.8         12.9         3.5         1.6         2.7         3.2         .057         2.9         .056         17.2         5.2         12.8         9.2           2.8         1.3         1.6         3.5         3.2         .057         3.2         .056         17.2         5.2         12.8         9.2           2.8         1.3         1.6         3.5         4.1         3.6         10.5         3.2         10.8         9.2         10.8         9.2         14.8         9.2         10.8         9.2         10.8         10.8         10.8         10.8         10.8		2.5	7.6	2.3	7.0	2.1	7.3	2.2	7.5	2.3	2.2	.044	2.0	.035	13.9	4.5	9.5	2.9
2.6         8.3         2.5         7.9         2.4         8.1         2.5         2.7         .047         2.2         .038         14.3         4.4         9.7           3.2         9.8         3.6         11.7         3.6         10.8         3.3         9.5         2.9         .059         14.9         4.5         9.9           3.6         8.6         2.5         8.0         2.5         8.0         2.4         2.7         3.6         4.5         10.2         3.2         10.2		3.0	8.8	2.7	9.	2.8	8.9	2.7	9.1	2.8	4.4	. 677	7.4	.042	23.8	7.3	18.7	5.7
3.2         9.8         3.0         11.7         3.6         10.8         3.3         .057         2.9         .050         14.6         4.5         9.9           3.0         6.4         2.6         8.1         2.5         8.0         2.4         2.3         .057         2.9         .053         1.8         .052         14.6         4.5         19.2           2.8         12.9         2.5         8.0         2.7         3.0         .055         3.2         .044         13.9         4.2         12.8         3.2         12.8         17.2         9.2         12.8         3.2         3.0         17.2         9.5         17.2         9.5         17.2         9.5         17.3         17.3         3.2         17.2         10.4         13.9         4.2         13.9         14.2         14.2         13.2         14.2         13.2         14.2         13.2         3.7         17.3         3.7         17.3         3.7         17.3         3.7         17.3         3.7         17.3         3.7         17.3         3.7         17.3         3.8         13.1         4.1         10.2         3.9         10.6         2.0         13.2         3.9         10.6 <td></td> <td>2.6</td> <td>8.3</td> <td>2.5</td> <td>7.9</td> <td>4.2</td> <td>8.1</td> <td>2.5</td> <td></td> <td></td> <td>2.7</td> <td>.047</td> <td>2.2</td> <td>. 038</td> <td>14.3</td> <td>4.4</td> <td>9.7</td> <td>3.0</td>		2.6	8.3	2.5	7.9	4.2	8.1	2.5			2.7	.047	2.2	. 038	14.3	4.4	9.7	3.0
3.6         6.4         2.6         6.1         2.5         8.0         2.4         2.3         .039         1.8         .032         14.6         4.5         160.2           2.8         12.9         3.9         11.6         3.5         8.0         2.4         2.3         .056         17.2         5.2         12.8           2.9         3.1         11.6         3.5         8.0         8.2         17.2         9.2         12.8         3.7         7.7         3.2         12.8         3.2         12.8         3.2         17.3         4.2         13.2         4.2         13.2         4.2         13.2         4.2         13.2         4.2         13.2         4.2         13.2         4.2         13.2         4.1         3.2         3.6         .065         2.6         0.45         12.2         3.7         7.7         3.2 <td></td> <td>3.2</td> <td><b>6</b>0</td> <td>3.0</td> <td>11.7</td> <td>3.6</td> <td>10.8</td> <td>3.3</td> <td></td> <td></td> <td>3.3</td> <td>. 057</td> <td>2.9</td> <td>. 050</td> <td>14.9</td> <td>4.5</td> <td>6. 6</td> <td>J. 0</td>		3.2	<b>6</b> 0	3.0	11.7	3.6	10.8	3.3			3.3	. 057	2.9	. 050	14.9	4.5	6. 6	J. 0
2.8         12.9         3.9         10.3         3.1         11.6         3.5         3.2         .057         3.2         .056         17.2         5.2         12.8           2.9         8.9         2.7         8.6         2.7         8.6         2.7         4.2         9.2           2.8         7.3         2.2         8.9         2.7         3.1         .054         13.9         4.2         9.2           3.4         9.1         2.2         8.9         2.7         3.1         .059         8.5         2.6         3.7         7.7           3.5         4.2         13.5         4.1         3.9         3.8         .066         3.9         .068         22.0         6.7         7.7           2.8         13.7         4.1         4.1         67.2         4.3         .066         20.3         6.2         15.8         17.3           2.8         13.7         4.1         4.1         67.2         4.3         6.6         20.3         6.6         20.3         6.6         20.3         17.3         14.8         12.2         3.7         17.3         3.8         11.9         3.6         11.9         3.6         11.9		ъ. В.	4.8	5.6	<b>.</b>	2.5	8.2	2.5	8.8	2.4	2.3	. 039	<b>.</b> .	. 032	14.6	4.5	10.2	ы Т.
2.9         8.9         2.7         8.6         2.6         8.9         2.7         3.0         .053         2.5         .044         13.9         4.2         9.2           2.8         7.3         2.6         1.9         6.5         2.0         2.0         .035         1.7         .029         8.5         2.6         3.2           2.4         9.1         2.8         9.2         2.8         3.1         .054         2.6         .045         12.2         3.7         7.7           2.9         13.8         4.2         13.5         4.1         4.1         .072         3.4         0.66         20.3         6.7         17.3           2.8         13.1         4.2         13.5         4.1         4.1         .072         3.4         0.66         20.3         6.2         15.8         11.3           2.8         13.1         4.2         13.5         4.1         4.1         .072         3.4         0.66         20.3         6.2         11.9           2.8         10.9         3.3         4.1         .072         3.4         0.59         16.9         4.6         10.5           2.1         2.2         11.9		2.8	12.9	g.8	10.3	٦. ٢.	11.6	3.5			3.2	. 057	3.5	. 056	17.2	5.2	12.8	3.9
2.8         7.3         2.2         6.5         2.9         6.5         2.9         9.5         1.7         029         8.5         2.6         3.2           2.4         9.1         2.8         9.2         2.8         3.1         .054         2.6         .045         12.2         3.7         7.7           3.9         13.8         4.2         13.5         4.1         4.0         12.9         3.9         .068         2.9         6.7         17.3           2.8         13.7         4.2         13.5         4.1         4.1         .072         4.3         .076         17.7         5.4         12.7           2.8         13.1         4.0         12.9         3.9         3.8         .066         20.3         6.2         15.8           2.8         13.1         4.1         1.7         0.7         4.1         17.7         5.4         10.7           2.8         13.1         4.1         1.0         2.3         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0		2.9	6.0	2.7	8.6	5.6	8.9	2.7			J. 0	. 053	2.5	.044	13.9	4.2	9.5	2.8
2.4     9.1     2.8     9.3     2.8     9.2     2.8     3.1     .054     2.6     .045     12.2     3.7     7.7       3.9     13.8     4.2     13.5     4.1     3.6     .065     3.9     .068     22.9     6.7     17.3       2.5     13.7     4.2     13.5     4.1     4.1     .072     4.3     .076     17.7     5.4     12.7       2.8     13.1     4.0     13.8     4.2     13.5     4.1     .072     4.3     .076     17.7     5.4     12.7       2.8     13.1     4.0     13.5     4.1     .072     3.4     .059     16.9     5.2     11.9       2.7     7.1     2.2     4.6     1.4     5.4     1.6     5.1     .057     3.4     .059     16.9     5.2     11.9       2.1     7.1     2.2     4.6     1.4     5.4     1.6     2.1     .057     3.4     10.5     4.1     11.9       2.9     1.3     3.6     1.2     3.6     3.2     .055     3.2     .055     15.9     4.8     11.0       2.9     4.1     1.3     3.6     1.2     3.6     3.9     3.6     3.9		2.8	7.3	2.5	6.2	<del>1</del> .9	6.5	2.0			7.0	. 035	1.7	. 029	8.5	2.6	3.5	1.0
3.9       13.6       4.2       13.5       4.1       3.6       .065       3.9       .068       22.0       6.7       17.3         2.5       13.7       4.2       13.1       4.0       12.9       3.9       3.8       .066       3.8       .066       22.0       6.7       17.3         2.8       13.1       4.0       13.5       4.1       4.1       .072       4.3       .076       17.7       5.4       12.7         2.8       13.1       4.0       13.5       4.1       .072       3.4       .059       16.9       5.2       11.9         2.7       8.2       2.5       10.4       3.2       9.9       3.0       2.9       .056       2.5       .044       15.6       4.6       10.5         2.7       8.2       2.5       10.6       3.5       1.6       2.1       03.7       13.4       4.1       10.5         2.9       11.3       3.6       12.4       3.6       3.6       2.1       0.055       3.2       055       15.9       4.8       11.0         2.9       2.4       12.6       3.8       13.5       3.6       3.9       0.65       3.9       0.66		2.4	<b>9</b> .	2.8	9.3	2.8	9.5	2.8			3.1	.054	5.6	. 945	12.2	3.7	7.7	2.3
2.5     13.7     4.2     12.5     3.8     13.1     4.0     12.9     3.9     3.8     .066     3.8     .066     20.3     6.2     15.8       2.8     13.1     4.0     13.5     4.1     4.1     .072     4.3     .076     17.7     5.4     12.7       2.8     10.9     3.3     10.7     3.3     4.1     .072     3.4     .059     16.9     5.2     11.9       2.7     8.2     2.5     10.4     3.2     9.9     3.0     2.9     .056     2.5     .044     15.0     4.6     10.5       2.1     7.1     2.2     4.6     1.4     5.4     1.6     5.2     1.6     2.1     .057     1.5     0.6     10.5       2.9     11.3     3.4     12.9     3.6     13.9     3.6     13.9     4.1     11.0       2.9     13.1     4.0     13.1     3.6     13.9     3.6     10.0     3.9     4.1     15.5       3.7     13.1     4.0     2.4     2.6     0.04     2.1     0.05     13.9     6.1     15.5       4.1     13.5     3.6     13.9     3.6     13.9     0.06     19.2     5.9     14.8		3.9	13.8	4.2	13.2	4.0	13.5	<del>-</del>			3.6	. 963	9. 6.	. 968	22.0	6.7	17.3	5.3
2.8     13.1     4.0     13.8     4.2     13.5     4.1     .072     4.3     .076     17.7     5.4     12.7       2.8     10.9     3.3     10.7     3.3     4.1     .072     3.4     .059     16.9     5.2     11.9       2.7     8.2     2.5     10.4     3.2     9.5     9.4     15.0     4.6     10.9       2.1     7.1     2.2     4.6     1.4     5.4     1.6     5.2     1.6     2.1     .037     1.5     .026     13.4     4.1     8.6       2.1     7.1     2.2     4.6     1.4     5.4     1.6     5.2     1.6     2.1     .055     13.4     4.1     1.0       2.0     11.3     3.4     12.6     3.8     11.9     3.6     13.4     8.6     14.8     11.9       4.1     13.1     4.0     13.4     10.7     3.9     .068     19.9     6.1     15.5       3.7     13.1     4.6     1.7     3.6     13.9     3.6     13.3     3.6     13.3       4.1     13.5     3.4     12.3     3.6     11.9     3.6     13.4     4.7     11.1       2.6     13.7     3.5 <t< td=""><td></td><td>2.5</td><td>13.7</td><td>4.2</td><td>12.5</td><td>J. 8</td><td>13.1</td><td>4.0</td><td>12.9</td><td>3.9</td><td>3.8</td><td>990.</td><td>3.8</td><td>990.</td><td>20.3</td><td>6,2</td><td>15.8</td><td>4.8</td></t<>		2.5	13.7	4.2	12.5	J. 8	13.1	4.0	12.9	3.9	3.8	990.	3.8	990.	20.3	6,2	15.8	4.8
2.8     16.9     3.3     16.7     3.3     4.1     .072     3.4     .059     16.9     5.2     11.9       2.7     8.2     2.5     16.4     3.2     9.9     3.6     2.9     .056     2.5     .044     15.0     4.6     10.5       2.1     7.1     2.2     4.6     1.4     5.4     1.6     5.2     1.6     2.1     .037     1.5     .026     13.4     4.1     8.6       2.0     11.3     3.4     12.6     3.6     3.2     .055     3.2     .055     15.9     4.8     11.0       4.1     13.1     4.0     11.9     3.6     13.9     4.1     10.0     3.9     14.8       4.1     13.1     4.0     4.2     .074     3.9     .068     19.9     5.1     15.5       3.7     13.1     4.0     4.0     4.2     .074     3.9     .068     19.9     5.1     15.5       4.1     13.5     3.4     12.3     3.6     11.9     3.6     19.4     5.9     14.8       5.5     11.2     3.5     11.9     3.6     19.9     966     19.4     5.9     14.8       5.8     11.7     3.5     10.6		2.8	13.1	4.0	13.8	4.2	13.5	<del>-</del>			<del>-</del>	. 072	4.3	920.	17.7	4.6	12.7	3.9
2.7     8.2     2.5     10.4     3.2     9.9     3.0     2.9     .050     2.5     .044     15.0     4.6     10.5       2.1     7.1     2.2     4.6     1.4     5.4     1.6     5.2     1.6     2.1     .037     1.5     .026     13.4     4.1     8.6       2.0     11.3     3.4     12.6     3.6     12.4     3.8     11.9     3.6     13.9     4.8     11.0       4.1     13.1     4.0     11.9     3.6     12.4     3.8     1.6     2.1     .036     19.2     5.9     14.8       5.9     14.1     13.1     14.0     14.2     3.6     13.9     4.0     3.6     13.9     6.1     15.5       4.1     13.5     3.4     12.3     3.6     13.9     3.6     13.4     3.9     14.8       5.0     14.2     3.5     11.9     3.6     13.9     3.6     13.4     13.3       2.6     8.2     2.5     13.9     3.6     13.7     3.9     15.4     4.7     11.3       2.6     8.2     2.5     2.2     2.3     3.041     1.7     3029     15.4     4.7     11.3		2.8	10.9	J. J.	10.8	J. J	10.7	3.3			<del>-</del> -	.072	4,5	. 059	16.9	5.2	11.9	3.6
2.1     7.1     2.2     4.6     1.4     5.4     1.6     5.2     1.6     2.1     .037     1.5     .026     13.4     4.1       2.0     11.3     3.4     12.6     3.8     11.9     3.6     12.4     3.8     4.1     .072     3.8     .067     19.2     5.9       4.1     13.1     4.0     11.9     3.6     12.4     3.8     2.4     8.0     2.4     8.0     2.4     8.0     3.0       3.7     13.1     4.0     11.7     3.6     13.9     4.0     4.2     3.9     .062     3.8     19.4     5.9       4.1     12.5     3.8     11.9     3.6     11.9     3.6     3.3     .041     1.7     .029     15.4     4.7		2.7	8.2	2.5	10.4	3.2	6.6	3.0			5.9	. 050	2.5	.044	15.0	<b>4</b> .6	10.5	3.2
2.0 11.3     3.4 12.6     3.8 11.9     3.6     3.2     .055     3.2     .055     3.2     .055     15.9     4.8       4.1 13.1     4.0 11.9     3.6 12.4     3.8     4.1     .072     3.8     .067     19.2     5.9       2.9     8.0     2.4     8.0     2.4     8.0     2.4     8.0     3.0       3.7     13.1     4.0     11.7     3.6     13.0     4.0     4.2     .074     3.9     .068     19.9     6.1       4.1     12.5     3.8     11.2     3.4     12.3     3.8     3.5     .062     3.8     .066     19.4     5.9       2.6     8.1     2.5     6.8     2.1     7.2     2.2     2.3     .041     1.7     .029     15.4     4.7	_	2.1	7.1	2.2	4.6	<b>+</b> . <b>+</b>	5.4	9.	5.2	1.6	2.1	. 037	5.5	. 026	13.4	4.4	8.6	5.6
4.1 13.1 4.0 11.9 3.6 12.4 3.8 4.1 .072 3.8 .067 19.2 5.9 2.9 8.0 2.4 7.9 2.4 8.0 2.4 2.0 2.6 .046 2.1 .036 10.0 3.0 3.7 13.1 4.0 11.7 3.6 13.0 4.0 4.2 .074 3.9 .068 19.9 6.1 4.1 12.5 3.8 11.2 3.4 12.3 3.8 3.5 .062 3.8 .066 19.4 5.9 2.8 11.7 3.6 11.6 3.5 11.9 3.6 11.9 3.6 3.9 .068 3.3 .057 17.8 5.4 4.7 2.6 8.2 2.5 6.8 2.1 7.2 2.2 2.3 .041 1.7 .029 15.4 4.7		2.0	11.3	4.6	12.6	3.8	11.9	3.6			3.5	. 055	3.5	. 055	15.9	₩.	11.0	4.6
2.9 8.0 2.4 7.9 2.4 8.0 2.4 2.6 .046 2.1 .036 10.0 3.0 3.7 13.1 4.0 11.7 3.6 13.0 4.0 4.2 .074 3.9 .068 19.9 6.1 4.1 12.5 3.8 11.2 3.4 12.3 3.8 3.5 .062 3.8 .066 19.4 5.9 2.8 11.7 3.6 11.6 3.5 11.9 3.6 11.9 3.6 3.9 .068 3.3 .057 17.8 5.4 4.7 2.6 8.2 2.5 6.8 2.1 7.2 2.2 2.3 .041 1.7 .029 15.4 4.7	_	-	13.1	4.0	11.9	3.6	12.4	3.8			<del>-</del> :	.072	3.8	.067	19.2	8.S	14.8	4.5
3.7 13.1 4.0 11.7 3.6 13.0 4.0 4.2 .074 3.9 .068 19.9 6.1 4.1 12.5 3.8 11.2 3.4 12.3 3.8 3.5 .062 3.8 .066 19.4 5.9 2.8 11.7 3.6 11.9 3.6 11.9 3.6 3.9 .068 3.3 .057 17.8 5.4 2.6 8.2 2.5 6.8 2.1 7.2 2.2 2.3 .041 1.7 .029 15.4 4.7		2.9	8.0	7.4	7.9	7.4	8.0	2.4			5.6	. 046	2.1	. 036	10.0	გ. ტ.	5.5	1.7
4.1 12.5 3.8 11.2 3.4 12.3 3.8 3.5 .062 3.8 .066 19.4 5.9 2.8 11.7 3.6 11.6 3.5 11.9 3.6 11.9 3.6 3.9 .068 3.3 .057 17.8 5.4 2.6 8.2 2.5 6.8 2.1 7.2 2.2 2.3 .041 1.7 .029 15.4 4.7		3.7	13.1	4.0	11.7	3.6	13.0	4.0			4.2	.074	3.9	. 968	19.9	6.1	15.5	4.7
2.8 11.7 3.6 11.6 3.5 11.9 3.6 11.9 3.6 3.9 .068 3.3 .057 17.8 5.4 2.6 8.2 2.5 6.8 2.1 7.2 2.2 2.3 .041 1.7 .029 15.4 4.7		<del>-</del> -	12.5	ъ. В.	11.2	4.6	12.3	3.8			3.5	. 062	3.8 8.	990.	19.4	5.9	14.8	4.5
2.6 8.2 2.5 6.8 2.1 7.2 2.2 2.3 .041 1.7 .029		2.8	11.7	3.6	11.6	3.5	11.9	3.6	11.9	3.6	3.9	.068	ы. Б.	.057	17.8	5.4	13.3	4.0
		9.6	,		9	•	•	•			•		1	**			•	•

EIGHT	RAMP	3	40	3.1	3.6	3.9	2.0	4.7	3.3	J. 1	4.6	4.6	2.7	2.5	3.9	2.9	<b>-</b> .+	3.6	3.2	3.1	3.2	<b>+</b> . <b>+</b>	3.1	2.2	4.6	3.2	2.3		2.8	2.3	ы Б.	<b>4</b> . <del>L</del>	3.2	2.8	8.1	6.8	3.6	4.3	2.9	<b>+</b> . <b>+</b>	3.6	J.6	2
HOOK HEIGHT	OVER RAMP	E	39	10.1	11.8	12.8	9.9	15.3	10.8	10.2	=:	11.1	8 8.8	8.3	12.9	9.4	13.4	11.8	10.6	19.2	10.6	14.5	10.3	8.2	7.7	10.4	7.5		დ დ	7.4	11.4	4.6	10.4	9.5	6.9	22.3	11.8	14.1	<b>†</b> .0	13.5	11.7	1.8	4 4
WHEEL HEIGHT	OVER RAMP	3	38	4.6	5.1	5.2	3.5	6.9	4.8	4.7	<b>4</b> .8	4.8	4.0	<b>6</b> .4	5.J	<b>+</b> . <b>+</b>	5.5	6.4	4.7	4.5	4.7	5.6	4.5	4.0	<b>4</b> .8	4.7	3.9		<del>+</del> .+	3.6	ø. <del>4</del>	2.9	4.5	4.3	3.2	8.1	4.9	5.7	4.5	5.7	5.0	1.	7
WHEEL	OVER	E	37	15.2	16.6	17.2	<b>1</b> .4	19.7	15.6	15.5	15.8	15.7	13.2	13.1	17.3	14.3	18.2	16.2	15.4	14.8	15.4	18.4	14.8	13.1	15.7	15.3	12.7		13.5	11.7	16.2	4.6	14.8	14.2	10.5	26.7	16.2	18.6	14.9	18.7	16.5	16.6	7 71
AT 70	AM.	SAD O	36	.052	.053	.044	. 668	.061	.074	.051	.051	.054	. 034	.045	.049	. 072	.058	.053	. 969	.047	.054	. 050	.041	.059	.056	.070	.061	.071	. 042	. 040	.049	.060	.047	.042	.029	990.	.046	.064	.057	. 059	. 056	.051	0,0
ANGLE ,	á	DEG	35	3.0	٦. ۲.	2.5	ĸ.	3.5	4.2	2.9	2.9	3.1	7.0	5.6	2.8	+.1	3.3	3.0	4.6	2.7	J. 1	2.8	2.3	4.5	3.5	4.0	3.5	4.0	7.4	2.3	2.8	3.5	2.7	2.4	1.6	3.8	5.6	3.6	3.5	4.6	3.5	5.9	,
GLIDE PATH ANGLE AT TD	BHW	₽¥D	ņ	.059	.048	.058	.032	.069	.072	.056	.048	. 050	.041	. 055	. 056	.074	.051	. 056	.051	. 050	.049	. 049	. 048	. 063	.067	. 072	.064		.048	.046	. 059	. 069	.060	.059	.046	.078	. 059	. 082	.054	.061	.051	. 045	776
GLIDE	ā	DEG	33	4.5	7. 8.	3.3	8.	3.5	4.2	3.5	2.7	2.9	7.4	3.2	3.2	4.3	2.9	3.2	2.9	2.9	2.8	2.8	2.8	3.6	3.8	<del>-</del>	3.7		2.7	2.7	3.4	4.0	3.4	3.4	2.7	4.4	4.6	4.7	3.1	3.5	5.9	5.6	2 5
	LIGHT	S/M	32			3.0	ø.				3.5	3.7	2.6		3.0													4.6											3.1		3.7		4
	FREE-FLIGHT	F/S	2			6.6	J. 1				10.4	12.3	8.5		6.6													15.1											10.3		12.1		7
NAMO	O	S/M	30	3.2	3.6	3.0	σ.	<b>+</b> . <b>+</b>	4.5	3.3	3.5	3.9	2.6	2.8	3.0	<b>+</b>	4.0	3.5	3.5	3.2	3.6	4.5	2.8	3.8	g. 5	4.5	3.7	4.5	2.8	2.9	J.	3.8	3.2	2.4	8.	4.4	3.0	4.3	3.2	3.5	3.7	3.5	c
NKING SPEED AT TOUCHDOWN	AVG	F/S	29	10.6	11.9	10.0	2.9	14.3	14.8	10.9	10.5	12.8	8.5	9.5	7.6	13.5	11.3	11.6	11.3	10.6	11.9	1.1	9.°3	12.5	12.8	13.8	12.3	14.7	9.5	9.5	19.9	12.3	10.4	7.8	6.1	14.4	7.6	14.2	19.6	11.6	12.0	11.6	•
PEED A1	8	M/S	28	2.9	3.7	2.9	1.2	4.2	<b>+</b> .	3.3	4.6	3.6	2.7	2.7	5.9	4.3	4.6	3.2	4.6	3.3	3.7	4.7	5.9	3.9	4.2	<b>+</b> .+	3.2	<b>+</b> . <b>+</b>	2.5	J. J.	J. 0	4.0	3.2	2.5	<b>.</b>	<del>-</del> .	5.6	3.9	3.0	3.4	3.8	3.5	9
KING SI	STBO	F/S	27	ø.	12.2	9.6	3.8	13.9	14.5	11.0	11.2	12.0	9.6	<b>8</b> .8	4.6	14.1	11.1	10.5	11.3	10.7	12.1	15.4	4.6	12.9	13.9	14.3	10.6	14.5	<b>8</b> .1	10.7	10.0	13.3	10.4	7.4	5.8	13.3	9.8	12.9	8.6	1.1	12.5	11.3	9
SI	E	M/S	<b>56</b>	3.2	4.6	J. 1	1.5	<b>+</b> .	÷.5	n. n	5.9	<del>-</del> :	7.4	2.9	٦. م	<b>6</b> .4	3.5	3.7	3.6	J. 7	3.8	2.9	3.0	3.5	3.5	<del>-</del> -	3.8	4.5	3.0	2.8	3.0	4.5	3.1	2.6	6.	4.7	3.2	4.5	3.5	3.7	3.5	3.6	,
AIRCRAFT	PORT	5	25	10.6	1.2	10.2	8.4	4.5	4.7	10.8	9.7	3.6	8.0	9.0	9.0	3.1	4.1	2.1	1.7	6.3	2.4	9.4	9.9	9.	9.	4.5	12.4	6.4	9.B	9.1	8.	1.1	9.5	4.8	9	5.5	5.6	6.4	4.	2.1	1.6	6.1	o a
	LJ.	N/S	24	2.9	3.6	2.8	2.1	2.5	4.7	3.3	3.2	3.9	5.6	2.5	3.6	4.4	3.7	3.1	80	80	ø.	<u>ه</u>	3.4	3.8	3.0	4.0	3.0	3.6	2.8	2.5	3.0	2.5	3.1	2.6	6.	4.5	2.9	2.8	2.2	3.5	3.4	3.7	-
	NOSE	F/S	23	4.6	11.7	9.3	6.9	8.1	15.4	11.0	4.0	12.7	4.4	<b>8</b> .3	1.7	4.4	12.2	19.1	11.6	9.5	12.9	12.9	1.3	12.3	8. 8.	13.2	8.6	9.1	9.5	7.3	9.0	8.1	1.0	9.6	6.1	8.4	9.5	9.5	7.2	r. =	11.2	12.1	
CNDC	2		22	1698						104						1110	1111	1112	1113	1114	1115	1116	1117				1128			131											1185	1186	280

		AIRCE	AIRCRAFT SINKI	MKING S	PEED A	NG SPEED AT TOUCHDOWN	NWO			GLIDE	GLIDE PATH ANGLE AT TD	NGLE A	OT T	WHEEL HEIGHT	EIGHT	ноок нетсит	CHT
	NOSE	8	PORT	ST	STBO	AVG	<i>(</i> 2	FREE-FLIGHT	IGHT	BHW	ž	BW.	>	OVER RAMP	AWP.	OVER RAMP	de la
F/S	S <del>X</del>	5.	X X	£/s	R/S	<b>E/S</b>	N/S	F/S	N/S	DEG	RAD O	DEG	3	E	3	E	×
23	24	25	<b>58</b>	27	28	29	38	31	32	33	#	33	36	37	38	39	64
	3.1	14.2	4.4	14.0	4.4	14.0	4.3			3.0	.052	3.5	.061	18.2	5.5	14.0	4.3
E	3.5	15.2	4.6	11.7	3.6	13.5	<del>-</del> -			3.6	. 063	4.0	.070	16.9	5.2	12.4	3.8
7:	3.6	13.1	4.0	= -	4.0	12.1	3.7			2.9	.051	3.3	. 058	18.6	5.7	14.1	4.3
2	4.0	13.1	4.0							3.1	.054			20.4	6.2	15.4	4.7
15.5	5 4.7	10.3	3.1	17.3	5.3	14.2	4.3			4.2	. 673	3.8	990.	21.7	9.9	17.3	5.3
-	2.5	10.8	3.3	1.3	4.5	11.0	3.4			3.7	. 965	3.0	. 053	10.6	3.2	5.7	1.7
12.3	1 3.7	1.1	4.5	12.9	3.9	11.9	3.6			4.0	.070	3.2	. 056	20.1	6.1	15.3	4.7
9	1 2.9	12.3	3.7	11.5	3.5	11.9	3.6			3.2	.055	3.0	. 053	15.2	4.6	19.6	3.2
9.	3.2	1.0	3.3	9.6	2.7	10.5	3.2			3.5	. 061	5.9	.051	17.6	5.4	13.0	3.9
12.1	3.7	14.2	4.3	14.8	4.5	15.0	4.6	14.9	4.5	4.9	.070	4.3	.074	22.2	6.8	17.5	5.3
2.8	3.9	12.5	3.8	13.0	4.0	12.6	3.8			3.2	.056	3.8	.067	18.4	5.6	13.1	6.4
2.5	3.8	16.5	3.2	10.5	3.2	10.5	3.2	10.6	3.2	3.5	.061	2.8	.049	20.3	6.2	15.5	4.7
7.	3.8	10.2	3.1	13.3	<del>-</del> -	<b>+</b> .=	3.5			3.2	.055	4.6	. 059	16.8	5.1	11.6	3.5
2.6	3.7	<b>9</b> .0	5.8	10.7	3.3	10.9	J. J			3.1	.053	3.1	. 054	17.5	5.3	12.6	3.8
2.2		12.1	3.7	12.6	3.8	12.3	3.7	12.5	3.8	3.2	.056	3.3	.057	19.2	6.6	14.7	4.5
	2.9	<b>8</b> .0	5.6	10.6	3.5	9.6	2.9			2.8	.048	2.5	.044	17.5	5.3	13.0	3.9
9.3		8.5	2.5	8.2	2.5	8.2	2.5	4.8	2.5	2.4	. 042	<del>.</del> 6.	. 034	14.5	<b>+</b> . <b>+</b>	4.6	2.9
S	2.7	<b>8</b>	2.5	7.3	2.2	7.7	2.3			3.2	.056	2.8	.049	14.1	<b>4</b> .4	8.9	2.7
2		<b>-</b>	4.6	10.5	3.2	10.8	J.3			3.1	.054	J. 1	.054	15.7	<b>4</b> .8	10.9	3.3
5.7	+:-	13.4	<del>-</del> .	14.1	4.3	13.7	4.2			3.9	.068	3.2	. 056	19.9	6.1	15.9	6.4
£.		14.1	4.4	13.4	<b>-</b> .	13.8	4.2			3.6	.063	4.0	690.	22.2	6.8	17.6	5.4
4		14.0	4.3	17.7	4.6	15.2	4.6			3.5	.062	4.0	. 979	21.9	6.7	17.7	5.4
12.9	3.9	13.4	<b>+</b> .+	12.3	3.7	12.9	3.9			4.0	690.	3.2	. 955	20.3	6.2	16.3	5.0
		10.4	3.5	11.2	4.6	10.9	3.3			3.6	. 062	3.0	. 053	17.5	5.3	12.9	3.9
3.		12.0	3.7	9.6	2.9	11.0	3.3			3.5	.061	3.1	. 053	16.7	5.1	12.1	3.7
9.		9. 9.	1.5	5.4	6	5.4	1.7			5.6	.046	<del>*</del> .	.024	14.5	<b>4</b> .4	9.3	2.8
7.8	3 2.4	12.0	3.7	13.5	<del>-</del> -	12.7	3.9			3.7	. 065	3.3	.057	20.5	6.2	15.8	8.4
2.6		13.5	<del>-</del>	10.5	3.2	12.2	3.7			3.7	. 065	4.6	.059	19.7	6.9	15.0	4.6
14.9		15.2	4.6	15.9	4.9	15.6	4.7			3.9	.068	4.6	. 686	23.9	7.3	19.3	5.9
6	•	9.1	2.8	9.5	2.9	9.5	2.9			2.7	.047	2.8	.049	16.5	5.0	11.6	3.5
12.9		1.6	3.5	12.1	3.7	1.8	3.6	11.6	3.5	3.1	. 055	٦. ٦.	. 054	19.4	6.9	14.7	4.5
9.6	3.3	6.6	3.0	10.4	3.2	19.1	3.1			2.9	. 051	2.9	. 050	14.4	<b>+</b> . <b>+</b>	9.6	2.9
8	3 2.7	7.5	2.3	7.3	2.2	7.4	2.3			2.4	.041	1.6	. 627	15.0	4.6	10.5	3.2
7.4	_	6.9	2.1	9.9	2.0	<b>8</b> .9	2.1	6.8	2.1	2.6	. 045	6.	. 033	16.4	5.0	11.9	3.6
6	2.8	10.5	3.2	11.3	3.5	10.9	3.3			3.1	.054	3.1	.054	16.9	5.2	11.7	3.6
6		7.9	2.4	6.5	2.0	7.1	2.5			2.7	.048	1.7	. 030	14.7	4.5	10.2	3.1
8.8	1 2.1	19.3	7.	8.5	2.6	5.6	2.9			3.2	. 055	2.7	.047	12.4	3.8	7.8	2.4
3	1.7	7.1	2.5	8.8	2.7	7.7	2.3			3.2	.056	2.3	.041	13.9	4.2	ø. 6	2.8

200		<u> </u>	H C H	Z V	n m			ROL	۷	N G L	ш	•	PITCH RATE	RATE	ROLL RATE	MTE	٠. م	÷	YAW	
2	2		8				5	•	క		44		AT TD	5	AT TD	٥	AT TD	5	AT TD	٩
	DEG	3	DEG	8	DEG	8	930	<b>§</b>	DEG	8	DEG	RAD	930	RAD	DEG	RAD O	DEG	8	DEG	<b>§</b>
÷	42	2	‡	45	46	47	<b>\$</b>	6	20	5	52	53	25	22	26	57	28	59	99	19
603		. 145		.166		T	-2.9	- 159	-3.0	.052		•	ø.	.000 -2.		042 -3	ø.	068	6.1	. 106
603		169		. 164			7		2	.040		•	.0	0.000 -1.4	_			037	2.7	.847
999	9.5	. 166		. 195		•		-	-2.4 -	. 042		_	6		6		- 0.9-	105	8.9	. 155
607	9.2	161		. 169		1		636	ø.	.010		•	9		*		o,	033	5.2	. 091
698		.154		.173		1	- 6:1-	033	<b>+</b> .	. 624		•	0.0	1	+		9	063	5.2	. 091
603		124		176			o.	.016	ر ا	.054		~	*		<b>.</b>			042	<b>-</b> (	.072
616			7.0	. 178		•	بر 1.00	.052	ا د ده	960.		60 P	رة وي	0.000 7	 	124 -1.2		021	- · ·	.030 
612				9 6		Ì				1 995		) <b>(</b> 2	, 6		. 6			. 045	9 4	.113
613		5			9.0	.140			_		-1.9.1-	.033	80	_			·	026	5.1	. 689
<b>6</b> 14		169		.176		•	2.6		1.7	. 030		מי	r.	.058 -1.1		019 -3	-3.0 -	052	3.5	.061
616		166	10.0	.175		ï		649		005		4	9				· -	054	2.3	.040
617		.147		.183	9.6	.158 -	-1.7	838	6.9	.0681	'-	. 030	۲.		7	012 -3	7	056	-:	.019
618		87		. 175			<b>-</b>		æ. ;	.014		▼ 1	ın ı				· - ·	054	3.8	996
619		<u> </u>		9 !		1	, e, (		2.0 1.0	.035		יט פי	۰ ب	.063 2	<b>ب</b>		•	637	4.2	.073
				<u>}</u>		•	' ' ' '	. 663 1 64	•	719.		<b>7</b>	. e	-		0.7- 020 -			• •	. 986 886
623		148			œ	154	· ·		- v		1	- A26 -	e P		٠.			1961	. O	898
623		122			)							9	6				•	460	6	.155
624		2			8.7	. 152					4.4	007 6	60	.119 -7.2			' ده ٠	676	5.6	860.
625		181				•	ر. ا						80				·	045	6.4	980.
628		112		.176			₹.	. 007	- 6	016		_	о О		2	.003 -2.	1	047	6.5	.113
629		127		.218		•	, ,	005		.016		6	6				7	. 073	6.8 8.9	119
633		.173		.173		•	4.0	.059	ا. ا	. 023		K)	6	.087 -1.7			•	. 035	7.5	.621
635		<b>8</b>		. 140		•	o.	•	•	031		- (	κi .		<b>.</b>		•	. 649	ю. Ф.	
656		82		<u> </u>		7	• •	/00 00 1		. 168 565		9 (	ء م	2 681.	- 0	. 62. 10. 10. 10. 10. 10. 10. 10. 10. 10. 10			• •	211.
2 5		95	2	136	8.5	161			-2.4 -	-	0	016	. 6					042	. 4	.079
649		5										8	0				-3.8	066	7.6	.133
644		. 147		.175		Ì		624	7	. 003		N	7					038	3.9	.068
646		. 185		_	6.3		1.6		-2.8 -	ł	ı	024	9.					035	5.6	. 698
647		. 159	•		9.6							. 956 7	•	•	ŀ		<b>.</b>	068	7.5	<u></u>
659		168	10.4	181	9.	. 192 –		021	7.		 B.:	014 0	6					037	ا رو د رو	. 692
655		134	<b>.</b>	138		••	2.9	. 035		002		_	· •				•	056	7.4	. 129
658		.178	_	. 169		-				024		in i	7		ı		•	049 6.69	9.1	.115
629		.117	•	. 155		•		ı	•	061		6	6					.045	3.7	.065
665		. 147	10.5	. 183					9.1	.028		,		,			· - ·	054	4.1	.677
999		.113	4.6	. 164		•	•	9.000		~.075		in '		1	1	.847 -3	دن من	066	7.7	134
299		. 126	<b>%</b>	. 136		1	· • :		ص ص	.033		7			<b>o</b> (	. 935 - 3	۱ ۲۰	065	ر ب ب	999.
<b>\$</b> 68		. 122	8.2	. 143		ĩ	-2.5	0442	7	038		5	e e	0.000 B.	on .	.155 -3	1 7	.054	X 9	991.

YAW	AT TD	DEG RAD	19	. 652	1112	101.		126											000				3 . 166															. 108	
			89	J. 0	4.9			7.2											7.0				9.5			9 v				_					_			6.2	
F. P. A.	AT TD	ο <b>γ</b>	92	044	065	072	979	045	056	965	965	070	091	956	033	047	635	014	1.000	1 1	1,632	098	106	045	065	1,0,1	663	037	079	147	965	056	063	087	045	033	DAR.	3	959
u.	<	OEG	28	-2.5	-3.7	7		-2.6	-3.2		7.7	6.4	-5.2	-3.2	6.1	-2.7	9.7-	ю с 1	3 5	9 7		-5.6	-6.1			+			-4.5	<b>4</b> .	7.7		-3.6	-5.0	-2.6	-1.9	ני ק	?	7 17
RATE	5	RAD	57	.056	. 689	.042	072	.079	. 686	. 040	662	068	.054	017			+.014	7/9.	100.1	9.6	3 6	. 924	115	.016	. 159	. 66. 	012	. 042	. 072	049	005	070	. 094	694	. 077	. 009	613		400
ROLL	AT	930 0	26	3.2	5.1	7.4	- 7	4.5	4.9	2.3	7	6.5	٠. د.	6, 1	<b>4</b> .8	4.0	 	÷ .	+ c	7	• <del>-</del>	*	9.9-	o.	 	، د د	7.1	2.4	<b>+</b>			6.4	5.4	-5.4	<b>+</b> .	ĸ.	r	:	: -
PITCH RATE	5	RAD	55	.010	0.00	.019	.031	.051	. 089	. 073	0.000	. 086	.061	.042	0.000	9.999	999.9		500.	900	900.0	.075			.024	979.	.047	9.66	.014	. 024	7:0.	0.000	0.000	.010	0.000	0.000	900	0.000	999
PITCH	AŢ	DEG	40	9.	0.0	<u>-</u>	8.1	2.9	5.1	4.2	9.0	4.9	J. 5	4.4				5 G	7.7		9 6		4.3	9.0	4.	- a			₩.	<b>+</b> :-		0.0	0.0				9		
	14.	8	53																	000	1.003			. 885					.012				. 035						
w	i.	DEC	25																		יי מינו וווו			r.					۲.				2.0						
S Z		8	15	. 045	. 023	. 030	054	960.	9.99	052	663	. 077		.014	014	.012	012	677	9.9.6		200.0	916	019	.009	.010	609 -	919	.024	916	. 082	.031	012	005	030	.021	010	9	7	1.003
۲	8	930	20	2.6	٦. ٦	1.7	1.7	5.5		-3.0	2	1 +		œ.	ا د:						7.0	9 0	7.7	ιċ		 	•	1	o.	1.7	8.			-1.7 -	1.2	6		י	֓֞֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֓֓֓֓֓֜֜֜֜֜֜֜
ROL		8	6	024	014	998			. 667			.019 -4	028	007	051			•			. 210			. 003		072		026 -	. 999	898	. 033	. 021	. 619	710.		992		7	
	5	930	89	+:	8.1	3.9			4		•				•	~					i (		,	'n		1   - •				•					3.2	-			
		3	41	Ī	•	••	•	•		ï	•	-	ī	•	ï			ï	•	, ,			ï	.115		7 7	ʻ.	ī	113	7	_	_	154	_	7	•	ï	ì	i i
L	4	DEG	9																	•		•		. 6					'n				<b>*</b> 0						
S Z		2	45	5	168	186	147	154	161	159	168	197		178	162	145	186	156	0				175	161 E	.143	191	150	148	136 6	. 159	157	. 155	181	169	127	157	128		9 9
I O	8	DEG	<b>‡</b>	•	•	n	*	·	Ī	Ī	Ī	·		•	•	•	•	•																	•	•	r	•	
P 1 7		2	3	152 8		_				127 9.1		-	. 129						9.91 /21								133 8.6						-				7 001	20	
-	5	DEG	42	•																							7.6											•	•
			•	<b>(E)</b>	•	Ġ,	•	•	~	_		Q1	~	•	<b>U</b>	-	<b>•</b> 0 1	-	• :	•	- r	. 47	•	40	•	- 1	. ~	•	•	~	•	•0	40	_	40	~	_	۰	•

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	DEG	3	DEG	3	DEG	<b>8</b>	930	SA O	DEC	gA.	DEC	RAD	DEG	RAD 0	DEG	8	DEG	3	DEG	3
<b>∓</b>	42	\$	‡	\$	\$	47	<b>\$</b>	6	20	5	22	53	\$	55	26	22	88	29	99	5
			•	.175		J.	7	072	<b>+</b> :	007			3.7			962 -	-2.0	035	-2.0	035
			<b>6</b> .6	.173		ı	-2.5	944 -	5.7	099				0.000			6.		7.7	.134
			•	138	7.5	- 131 -	9	028			4.11	024			1.7				6.1	. 106
		_	۰	. 185	8.5	. 148 –	-3.2	056	6.9		-1.0	017			12.8			047	6.7	.117
				.134		•		019	1.2	. 021			1.9		4.			051	6.2	. 108
103	6.9	. 120	8.5	.148		•	-2.0	035	2	003			4.0					045	4.2	. 673
		_		188			2	003	J. 1	.054			4.2					045	<del>-</del> -	. 672
				. 164	4.9	.112	10.	009	<b>+</b> .	. 024		012	2.5	•			n	058	3.6	. 963
			ĸ.	.161	6.8	119	80. 1		۲.	012	ŗ.	. 005	3.6					. 038	9.	. 028
				.157	6.8	119	39.		6	035	. J.	005	5.1				'n	061	ø. ₹	.086
			9.3	.162			7								3.1			079	<b>4</b> .9	.112
				. 140	7.1	. 124 –	ņ		•		-1:1	019			2.1		0	070	3.5	.061
		. 122		. 148					4.5	059				ı	- 0. <del>1</del>		,	047	8.8	. 119
				.168		'	7		4.	077					7.5		•	042	o. <del>1</del>	.086
112				<del>-</del>		•		051	5.8 8	101					3.7		•	033	4.5	. 073
				. 168				. 961	7	012					n		80	049	7	012
				. 161		'		628	"	. 005					6		0	035	9.	.010
5		25.		. 168		1	ņ	056	r.	. 005				999		. 629		033	2. 2.	.040
			7.0	.122			6.9 9.9	. 105	<b>+</b>	007				ņ				056	n .	.058
				. 155					•	017			ر ا ا					047	1.7	. 030
		134		191		•			<b>+</b>	059			4.7					056	4.8	.084
				131			ທຸ	. 993	o, i	033			 8					068	4 i	.075
				.152					'n	061			<b>4</b> .0					044	ر ا	. 058
128	9.6	.157 1		. 180			<b>.</b>		-7.7	054			8		۲.			038	2.3	.040
		28	+		 	14.		012	,	;	, 10	014		.030	<b>+</b> :			021	<b>+</b> (	.024
		7	7.8	136		1	- 1		<b>m</b>	.014					ى ت			635	ر د و	.058
		91		2		•			<b>+</b> (	024			ر. د د	•	- 5.6			۱. وقع	: :	124
		9		161			~ .			169.			9 1		÷ :		•	 		999
	7.9		_	48			2.7			087			<u>.</u> ;			3		440	9 G	/80.
		=	_	.138		1	_	037	7	.003			2.9		•			6/9		. 120
_			.7	. 169			_	.037	3.6	.063			4.6		3.5		<u>,</u>	030	ω	996
			6.0	. 155				016	۲.	.012					'n		۲.	047	9.9	. 035
				. 119			20	.669	œ.	.010					7.6		<del>-</del> .	054	2.3	.040
		112	7.8	. 136		•	-2.4	042	J. J.	. 023			3.9		5.1		*	059	<b>†</b> .	. 077
		.147		. 120		•	<b>+</b> . <del>-</del>		4.5-	059					4.6			035	4.5	.079
	'n			. 204	8.3	145	7		6.1	017	2	003 -	-1.2	021	5.7			058	6.3	.110
	∞.	•		.178				.014	2	003			9.9		3.6		-3.0	052	6.6	.115
. 281	•				8.5	. 148	6.6	0.000	8.1	031	5.3	005	2.1	. 037	ن. ا		- -	054	7.3	.127
98	6.9	_	-	.176			κi	- 600	-1.2	021			9.9	999.	8.	. 031	.80	031	3.0	. 052

	F		5		క		4		¥	5	AT	5	Υ	AT T0	AT TD	2
5	DEG	RAD	930	8	DEC	RAD O	DEG	SAD.	DEC	<b>S</b>	DEG	RAD	DEG	8	DEG	SA SA
4		47 48	<b>s</b> o	64	28	5.	22	53	\$	55	26	22	28	29	99	19
		-1.3		623 -1.3	ı	. 023		•	-	002	1.3	. 623 -	-3.5	061	9.9	.115
		6.			:	024		-		.028	12.1		80	084		.086
		-3.0	ı			061		•		9.99	6.3			031	2.7	. 947
		-2.8				636								058	6.1	. 106
		3.5				035		•	0.0	0.000-21.7		379 -		040	7.0	.122
			ı			005			₩.	.014 -1.8				658	4.7	.082
		3.0			1.0.1	670		•	9.9	0.000			-2.2	038	6.4	. 086
		7				037		.4	2.6	. 045	2.7	- 047	-4.5	061	4.6	.059
		7	_			.012		a)	0.0	0.000	2.9		-1.6	028	1.9	. 033
6.8	-	.119 -1.6		828 -		903 -2	1 -	037	1.0	- 710.	-5.3		-3.0	052	5.7	660.
		2.2		.038 -6.1		106			0.0	9.666 -	-2.6	045 -	1 5.4	075	6.3	.110
7.6	Τ.	133 -1.4	١		_	ī	.7 -	. 030	9.9	9.000	;		-4.2 -	073	5.9	. 103
		-5.0				003			9.9					061	6.2	. 108
				.037 -3.4	1	059		•						058	9.2	.161
7.8 .136	=	ï				.003 -3.1	•	054 6					60	035	ы Т.	.054
		•	•			. 023								059	4.4	.042
0.7 .187	=	.2		.003 -2.0		٠	_	. 992		0.000	<del>-</del> .			061	<b>+</b> :	. 624
		i			<b>.</b>	007		•		000.0	2.7			006	•	. 126
		Ξ				. 924		_				333		037	7.4	.042
		J. J.			_	051		0						031	4. U	.075
		9.		ī	_	017		0						051	9.4	.086
		9.7-				600.		<b>.</b>						092	9	. 105
		<b>T</b>			5.6	. 045		o.	9.0			- 898		045	5.3	. 692
		1.2			ĸ.	.044		0						047	2.5	.044
		-1.2	•	621 7	o.	. 138		•		.075	7.1			044	ы Б	.061
		<b>.</b> .			9	.010		0		0.000	<b>~</b>			052	3.7	.065
		В.		014 -2.	0	051		•	9.0					086	<b>4</b> .6	. 989
		<b>→</b> .?			2	663		0						031	3.6	. 063
		1.0		017	· •	.007		•	9.9	9.000			-4.2 -	073	<b>4</b> .8	. 684
		-1.7		838 3.0	6	.063		•	0.0					056	5.2	.091
7.4	Τ.	.129 -1.2			_	.012 -1.5		026 0	9.9	0.000			-4.0	070	<b>+</b> .	. 677
				-	0				_					010	₹.	. 667
		7	1			.051		8		999				058	8.4	.084
7.7		134 2.2			. 60	0.000 2.1	_	637 6		000.0	1.3		4	059	8.	.084
			•	•					2.5		-3.0			077	8.2	. 143
		2.1	•			.054		0			3.8		_	023	ا ن	609
					_	.002		~	2.2	.038	5.5			35	0.0	0.000

REREAD	NUMBER			6	0	0	-	•	-	0	0	-	0	-	-	6	0	-	-	7	0	0	-	-	0	0	-	0	•	-	60	-	0	-	-	-	0	-	-	60	0	0	0
ARR GEAR	RUNOUTS	3	82	9.0	9.9	9.0	<b>6</b> .6	9.9	<b>6</b> .6	0.0	•	9.9	<b>0</b> .0	<b>6</b> .0	436.9	436.9	436.9	0.0	<b>0</b> .0	<b>6</b> .0	31.8	429.3	436.9	<b>9</b> .	<b>6</b>	<b>0</b> .0	434.3	426.7	431.8	426.7	431.8	429.3	431.8	436.9	434.3	442.0	<b>0</b>	436.9	431.8	436.9	0.0	<b>6</b> .0	431.8
AR	25	ž	8	0	•	0	0	0	0	0	0	0	0	0		172	172	0	0	0	170	169	172	6	0	Φ	5	<b>2</b>	170	89	170					174			170	172	0	0	170
BAROMETRIC	PRESSURE	¥ <b>₹</b>	80	760.0	760.0	760.0	760.0	760.0	760.0	760.0	760.0	760.0	769.0	760.0	760.0	760.0	760.0	760.0	760.0	9.097	9.092	760.0	760.0	760.0	760.0	760.0	760.0	760.0	769.0	760.0	760.0	760.0	769.0	760.0	760.0	760.0	760.0	760.0	760.0	769.5	760.5	769.5	760.5
BARON	PRES	N HG	79	29.92	29.92	29.92	29.92	29.92	29.92	29.92	29.92	29.92	29.92	29.92	29.92	29.92	29.92	29.92	29.92	29.92	29.92	29.92	29.92	29.92	29.92	29.92	29.92	29.92	29.92	29.92	29.92	29.92	29.92	29.92	29.92	29.92	29.92	29.92	29.92	29.94	29.94	29.94	29.94
TEMP		ပ	78	18	18	₩	18	₽	8	8	<b>8</b>	<b>∞</b>	<b>∞</b>	<b>5</b>	18	<del>6</del>	<b>6</b>	18	<b>6</b>	18	8	₩	8	18	₽	<del>6</del>	₽	<b>18</b>	<b>∞</b>	<u> </u>	₽	<b>6</b>	<del>2</del>	₩	18	18	<del>.</del>	<b>6</b>	<del>1</del> 8	₩	8	8	18
=		<b>L</b>	71	64	64	<b>\$</b>	<b>\$</b>	<b>5</b>	49	4	<b>5</b>	4	3	<b>9</b>	<b>9</b>	64	49	64	<b>64</b>	49	64	49	49	4	49	<b>9</b>	49	4	<b>5</b>	4	<b>6</b>	4	49	49	49	<b>5</b>	49	<b>5</b>	64	49	<b>7</b>	64	4
DECK ROLL		RAD	76	023	. 023	9.000	0.000	.016	.017	024	.012	003	.028	.016	031	012	. 003	9.000	003	017	662	021	021	005	. 667	009	. 021	033	033	028	019	016	.012	024	005	031	005	016	021	. 002	.009	010	014
DEC		DEG	75	1.3	1.3	0.0	0.0	6.	- 0	<del>*</del> . [	.7	1.2	7.6	o.	1.8	7:-	4	0.0	2	1.0	7	-1.2	-1.2	٦.	₹.	1.5	1.2		-1.9	-1.6			_	<del>*</del> : <del>-</del> -		1.8		6.		-	٠.	9	œ.
реск РІТСН		RAD	7.	010	0.000	003	003	007	003	0.00	010	007	0.000	002.	010	003	007	003	005	005	005	009	003	902	003	007	. 002	005	007	010	0.000	010	002	002	003	007	010	002	995	003	005	007	009
DECK		DEG	23	9.1	0.0	2	2	<b>+</b> :	2	9.0	9.	₹.	9.0	-	9.	2	<b>+</b>	2	۳.	ا. د	٦.	٥.	2	7	2	*		ا. ا	<b>+</b> :	9	0.0	9.	7	-	2	4.1	9.	-		2	٠. ت	4	٦.
	SPEED	M/S	72	~		~	~	~	~	7	~	~	~	~	~	α.	~	7	~		7	~	~	~	~	~	7	и	~	М.	~	~	~	~	8	и.	~	~	~	~		~	7
SHIP	S	ž	7	n	n	n	n	n	n	n	n	'n	n	4	4	4	4	*	*	4	4	4	4	4	4	*	4	4	4	*	4	4	4	4	4	4	4	4	4	m	m	•7	m
3	CODE		70																																								
SON	TYPE		69	70100	76288	70200	70100	70100	70200	70200	70120	70100	50100	70200	59100	50100	59129	69199	69129	70120	50100	50100	50120	79129	50120	69120	50200	50100	59199	50100	50100	50100	50100	50100	50200	50100	60200	59299	50120	58288	70120	79199	50100
SIDE	₹		68	446	440	450	447	446	445	440	450	447	446	445	450	447	445	440	440	443	459	447	440	443	440	450	447	443	445	450	447	443	447	443	445	440	440	459	440	440	446	450	443
WIRE	ġ		67										7		-	-	-				7	4	-		*		-	4	8	7	8	4	8	-	-			-	4	7			2
TO TD	DISTANCE	3	99	67	3	62	99	72	23	97	89	2	*	30	26	5	<del>.</del>	23	71	26	72	9	62	<b>4</b>	82	88	58	74	67	99	73	<b>.</b>	72	99	65	7,	98	55	83	72	65	95	<b>6</b>
RAMP TO TD	DIST	E	65	221	211	204	196	236	195	317	222	241	242	<u>1</u>	185	201	147	245	254	<b>8</b>	237	299	204	130	269	289	189	244	228	218	247	267	236	216	212	242	281	179	271	237	212	184	266
TER	S.	3	<b>3</b>	s,	7	ŋ	'n	'n	မှ	7	ņ	Ϋ́	†	က္	'n	7	†	ņ	7	'n	7	†	7	ģ	မှာ	7	٠	†	7	φ	ę,	ģ	7	φ	ξ	φ	7	'n	77	1	-7-	1 PG	<b>, †</b>
OFF-CENTER	DISTANCE	<b>1</b>	3	-13	-		-17	-	-7 <b>9</b>							. 51-	· *-	· =	· =	-17			•	•	. 51-	·	·	•	<u>,</u>		·	٠			-	-19		·			· •	9	. <del>.</del> .
9	ġ.		62			•	-		-		Ī	•	•	•	•	•	Ť	٠	٠	٠	٠	•								-										'			- 899

REREAD	NUMBER			0	6	•	•	0	60	-	0	-	•	0	-	0	-	0	6	0	0	•	0	-	•	0	0	-	6	0	0	0	60	0	0	•	60	60	60	0	0	0	0
ARR CEAR	RUNOUTS	3	82	0.0	0.0	9.0	0.0	431.8	431.8	9.0	434.3	431.8	431.8	431.8	0.0	431.8	431.8	426.7	426.7	431.8	431.8	434.3	431.8	426.7	434.3	431.8	0.0	<b>0</b> .0	434.3	429.3	431.8	426.7	431.8	436.9	434.3	434.3	434.3	<b>0</b>	9.	431.8	434.3	9.0	0.0
AR	\$	×	8	•	0	0	•	170	170	0	17	170	170	170	0	170	170	168	168	170	170	17	170	168	17	170	0	0	17			168	170	172	7	17	17	0	0	170	171	0	0
BAROMETRIC	PRESSURE	MA HG	80	760.5	760.5	760.5	760.5	760.5	760.5	760.5	760.5	760.5	769.5	760.5	760.5	769.5	760.5	760.5	760.5	760.5	760.5	769.5	769.5	760.5	769.5	760.5	760.5	760.5	760.5	760.5	760.5	760.5	769.5	760.5	760.5	760.5	760.5	761.2	761.2	761.2	761.2	761.2	761.2
BARON	PRES	N N	79	29.94	29.94	29.94	29.94	29.94	29.94	29.94	29.94	29.94	29.94	29.94	29.94	29.94	29.94	29.94	29.94	29.94	29.94	29.94	29.94	29.94	29.94	29.94	29.94	29.94	29.94	29.94	29.94	29.94	29.94	29.94	29.94	29.94	29.94	29.97	29.97	29.97	29.97		29.97
TEMP		ပ	78	8	82	82	₽	₩	82	18	8	18	8	8	8	8	18	8	8	8	₽	18	<del>2</del>	₩	₽	8	₩	₽	8	18	₩	18	8	18	<del>1</del> 8	18	8	19	19	19	19	19	19
ĭ		<b>L</b>	11	49	\$	49	79	\$	<b>5</b>	64	<b>6</b>	64	<b>5</b>	\$	<b>2</b>	49	49	64	<b>9</b>	64	4	64	4	4	<b>\$</b>	49	49	5	5	64	49	64	49	<b>64</b>	49	64	64	99	99	99	99	99	99
DECK ROLL		RAD	76	014	.007	. 038	.016	. 023	. 007	. 021	.045	600.	.017	844	042	.018	028	031	037	003	003	0.000	. 031	. 037	600.	.010	. 026	019	.016	. 003	. 026	. 035	. 026	. 662	.044	0.000	0.000	. 003		007	.009	. 005	. 003
DEC		DEG	75	1	₹.	2.5	o.	1.3	₹.	1.2	5.6	'n	1.0	-2.5	-2.4	9.	9.1-	- - -	-2.1			9.0	<del>.</del>	2.1	'n	9.	7.5	<del>-</del> <del>-</del> <del>-</del>	<del>ه</del> .	7	5.	5.0	5.5	-:	2.5	0.0	9.9	7		<b>†</b> .	s.	<u>ب</u>	.5
DECK PITCH		RAD O	7.	012	0.000	0.000	005	007	869	012	009	010	002	003	002	869	. 002	007	002	009	003	005	005	009	010	007	662	007	003	005	003	9.00	. 002	005	003	007	. 002	005		0.000	003	007	007
DECK		DEG	22	7	9.0	0.0	. u	*:	S.	7	٠ د	9.	-	- -	-	'n		+	-	'n		ņ	٦.	'n	0	*	-	· •			.2	9.0	<del>-</del> .	i.	. 7	*	Ξ.	'n		_	. 7	*	+
	9	M/S	72	7	~	~	~	~	~	7	7	Ч	~	~			7	~	~	7		ς		7			~			α,	~	7	7	,	8	7	7	7	7	7		7	
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### F-14 NIGHT

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	WEIGHT		LBS	20	47000	49400	49500	47400	48600	46300	50100	48800	45400	200	47700	47500	46800	45900	47300	000	46400	0000	50400	48300	49400	48700	48800	47600	48600	48 100	46700	20400	46600	45,600	40500	49900	47800	49000	48200
L.AND INGS	LIFT	11		19		:	<u>-</u>																				3									6			
NIGHT L	1111	10		18	1.10	- 0	88	38	3 =	1.20	1.10	<del>-</del> 8	e .	38	3 8	1.20	- 10	- 30	- 0	1.20	88	3 5	3 2	1.50	-8	<u>۔</u> و	8 9	2 2	88	<del>-</del> 8	- - -	6.	1.20	2 8	3 5	2 6	1.20	<del>-</del>	<del>-</del>
-	<b>×</b>	Sp. A		1.7																																			
	KVPA	Z		91	1.17	1. 18	5. 5	6 6		1.30	1.33	1. 18	1.24	2.5	? :		- 13	1. 16	1. 13	1.17	1.17		- 6	1. 16	1. 15	5.	60.		90	1.17	1.13	1.16	61 .	9 9	2 :	<u> </u>	. 1.	1.02	1.08
(2)	SP'A		S/W	15																																			
(CVN-65	VSF		Z	7																																			
	VPAMIN		S/W	13	62						63												9 4																
ENTERPRISE	Α		Z	12	120	123	123	120	777	1 1 1 9	123	122	117	121	122	2 2	119	8-	120	120	119	123	124	121	123	122	122	121	220	121	119	124	119	120	119	123	2 2 2	122	121
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	-		Z X	ō																																			
7		PERP.	S/W I	6										-				-	-	_	<b>-</b> ·	- •	<b></b>		_	-	-	- •			-	-	-	_	_				7
MODEL F-14	WIND-VEL		S	₩		(7)	(*)	(7)	., .	7 (*	, (7)	"	.4	<b>C</b>				1 (7						• • •		•			•	• • •		•	``	•••	••		•	•	•
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	WEIGHT		¥	21	22362	21864	20593	21228	21228	20593	22408	21546	22861	21773	21954	22272	21682	20730	21546	
	3		LBS	20	49300	48200	45400	46800	46800	45400	49400	47500	50400	48000	48400	49100	47800	45700	47500	) )
NOINGS	LIFT	FF		6																
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	<b>×</b>	SP'A		1.1																
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55)	VSP'A		M/S	15																
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ENTERPRISE (CVN-65)	VP		¥	12	•	77.	7.	- :	7 (	7 7	- 6	223		7 .	7	7 6	771		911	120
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- MODEL F-14	WIND-VEL	ă	X	•	•	₹	ស (	io i	ומו	ומ	S.	in i	ហ	n (	~	~	7	Ν.	n	7
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AND ING DA	VE-FILM		M/S	บา		9	9	en En	57	S)	57	S.	55	-	39	20	ဝွ	59	9	52
LAND	VĒ.		X	•		18	117	<b>†</b> 04	9	=	9	101	107	- 18	- 5	112	116	115	19	107
	VPAF	70	M/S	, m	1		7.4	_				_								
	2	<b>F</b>	Z	~	l	143	144	134	137	-	137	134	137	148	142	140	143	142	149	135
	LNDG	2		-		9429	9433	9437	9438	9439	9441	9449	9455	9497	9504	9539	9545	9555	9564	9593

	HOOK HEIGHT	OVER RAMP	Σ	40	
	HOOK +	OVER	FI	39	
v	HE I GHT	RAMP	Z	38	
NIGHT LANDINGS	WHEEL MEIGHT	OVER	FT	37	
NIGHT	01 11	>	RAD	36	062 005 005 005 005 005 005 005 005 005 00
	GLIDE PATH ANGLE AT TD	BVV	DEG	35	αφυνηψηφυνησημος συμφημος ανασμησημος συμφονηση αν Βυνου- ανου Βυνου να 400 ανου ανου το ανου 4 στο 4 ανου 4 ανου Ευνου - ανου Βυνου να 400 ανου ανου ανου 4 ανου
	PATH	ВНМ	RAD	34	
65)	GL IDE	80	DEG	33	
(CVN-65)		LIGHT	M/S	32	6 6 6 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7
ENTERPRISE		FREE-FLIGHT	F/S	31	7. 0 0 1. 1 1. 9 2. 2 1. 2 1. 2 1. 2 1. 2 1. 2
USS ENTI	NMOO	G	S/W	30	$\begin{array}{c} \mathbf{u} \mathbf{u} \mathbf{u} \mathbf{u} \mathbf{u} \mathbf{u} \mathbf{u} u$
2	10UCH	AVG	F/S	29	
F - 14	INKING SPEED AT TOUCHDOWN	20	M/S	28	ろうようとよれるひょくひりひとひとよるひろうよようのよれ!とれようようのものもの この! ここまな を
MODEL F	KING S	STBD	F/S	27	0       0
•	S	<b>≒</b>	M/S	56	こうこくこうようこうこうこうこうそうよう こうそうじゅん うしゅん しゅうしゅうしょう こうこう ちょうしゅう ちゅうしゅう ちゅうしゅ ひゅう ちゅう より ほんりょう しょう しょう しょう しょう しょう しょう しょう しょう しょう し
LANDING DATA	AIRCRAFT	PORT	F/S	25	
LAN		w	M/S	24	ほうほうほうみようようようほうひゅん ままままます。 ようきゅうき ~のようほう 本書 見!これ ~ ○ うらら カー・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・
		NOSE	F/S	23	
	LNDG	2		22	99929999999999999999999999999999999999

		נא	LANDING DATA	1	MODEL F	F - 14	uss		ENTERPRISE (	(CVN-65)	5)			NIGHT	NIGHT LANDINGS	v		
S ON			AIRCRAFT	AFT SINKI	옃	PEED AT	SPEED AT TOUCHDOWN	NAO		J	GLIDE PATH ANGLE AT	ATH A	NGLE A	T 10	WHEEL HEIGHT	HE I GHT	HOOK HEIGHT	EIGHT
9	NOSE	SE	PORT	FA	STBD	80	AVG		FREE-FLIGHT	1641	BHW	_	BVV	>	OVER	RAMP	OVER	RAMP
	F/S	M/S	F/S	M/S	F/S	S/M	F/S	M/S	F/S	M/S	DEG	RAD	DEG	RAD	FT	¥	13	¥
22	23	24	25	<b>36</b>	27	28	29	30	31	32	33	34	35	36	37	38	39	40
283	10.4	•	•				9.0	2.7					2.8	.048				
284	- 6	•	•		•		5.5		9				- •	.054				
286	r	ω ω υ 4	. 4 . 4	. 4 	- ¢	ים רי ים מ	0.6			ى ت				.003				
287	6.					3.7	- - -						6	.067				
292	5.9	•					3.9	•					_	.013				
337	14.2	•	•		•	4.	•	•					ص ص ا	690.				
342	0.0				•	4 .	14.2	 					טינ	<u>.</u>				
240	7 C				•	•	- 2	. n.						080				
1 5						4		9						.058				
353	. F					4		9						.075				
900	9.6					2		5 69						.094				
354	5.8					3.		3.5						.053				
355	10.9					2.7	89 .3	2.5						.041				
356	6.5	•	-			2.7	9.6	2.9						.042				
359	2.8	•				9.0	12.7	9.6						.061				
360	9 · e					ლ <b>ი</b>	10.1							050				
796	7 c				•	ع ب ب	4.0							0.00				
364	77.7					9 E	5.0	ى د م ن					, e	055				
367	12.6						12.9	6						.065				
368	6.6					2.8	10.1	-						.041				
369	13.6					4.2	13.8	4.2						.063				
370	<b>8</b>					2.7	т. С.	9.6	•					.037				
- 6		٠				0.1	0.4	n -	0.	4. U								
7 10	2.5						. F.	- 10						.055				
375	-					9.0	12.6	3.8						.062				
376	-		•			<del>1</del> .8	7.6	2.3						.041				
377	12.7		•			3.3		3.5						. 056				
378	13.2	•	17.4			3.5	13.3	<b>4</b> 0					•	.065				
379	9.5	•	٠			6. 6.		1.7					-	.027				
380	12.2		•					-					-	080				
381	0. -	•			•	4 ·		ه. ن						.074				
382	<b>8</b> 0	•	•			2.5	•	01						020				
383	13.6	•				ю 0 г	12.2	7.0	12.0	3.7			n 6	. 06.				
786	• •		•			÷ (		9 6					, ,	946				
777	2.5	•	٠				. <u>.</u>						9 6	9.0				
97.0	n. 7	•	٠			7.	•	٠					0	,				

Name		LANG	LANDING DATA	•	MODEL F	41		USS ENT	ENTERPRISE	E (CVN-65)	-65)			Ž	GHT LA	NIGHT LANDINGS				
NATION         FF         AT TO         A		-	U	z	_			0	⋖	ט	w	-	PITCH	RATE		RATE			<b>*</b>	>
4.3         4.6         4.0         0.6         RAD         DEG         RAD <th>10</th> <th></th> <th>S</th> <th></th> <th>4</th> <th></th> <th>10</th> <th></th> <th>OR</th> <th></th> <th></th> <th></th> <th><b>-</b></th> <th>õ</th> <th>AT</th> <th>10</th> <th>AT</th> <th>10</th> <th>AT</th> <th>5</th>	10		S		4		10		OR				<b>-</b>	õ	AT	10	AT	10	AT	5
1.   1.   1.   1.   1.   1.   1.   1.	DEG	RAD	DEG	RAD		RAD	DEG	RAD	DEG	RAD	DEG	RAD	DEG	RAD	DEG	RAD	DEG	RAD	DEG	RAD
1.6   0.005   1.7   0.005   1.7   0.005   1.7   0.005   1.7   0.005   1.7   0.005   1.7   0.005   1.7   0.005   1.7   0.005   1.7   0.005   1.7   0.005   1.7   0.005   1.7   0.005   1.7   0.005   1.7   0.005   1.7   0.005   1.7   0.005   1.7   0.005   0.005   1.7   0.005   1.7   0.005   1.7   0.005   1.7   0.005   0.005   1.7   0.005   1.7   0.005   1.7   0.005   1.7   0.005   0.005   1.7   0.005   1.7   0.005   1.7   0.005   1.7   0.005   0.005   1.7   0.00			4	<b>4</b>		47	48			_	52	53	54	52	26	57	28	59	9	61
1.4   0.02   0.00   0.0   0.00   0.0   0						•	ď	2				_	c	000	1.7	0	3.1	.05		.094
1.0   1.0							? <	•				-	ی د	045		60	~	.040		101
1.0   1.0		56.					•					_	· c	•		.073	9	٠,		.058
1.   1.   1.   1.   1.   1.   1.   1.		129				27	•			•	,		, c	Ŧ		176	4	0.		101
1.0   0.073   0.014		141		•	•	C .	•				•		מ כ	•		. 4	6			.113
1.0   1.0		191					• •					r	) r		•		9			.054
10.3   10.3		50.				•	•					•	. "		-	000	9			.086
230 240 250 251 260 271 260 272 260 272 260 272 272 273 273 273 273 273 273 274 275 275 275 275 275 275 275 275 275 275		9					٠	100.				•	•	200		3		6		.061
1.0   1.0		. 230				•	•	.037				•	•	55.	e c	5 6	. ע	•	•	
1.0   1.0		. 136					•	610.					0.		ا زد	3	0 0	٠		
1.0   1.0		126					•	. 105							. 7	030	6.6	•	•	2.00
10.3   180   1.4   .024   .1.2   .021   .2.6   .0215   .1.9   .033   .1.9   .1.9   .1.9   .1.2   .021   .0.2   .2.7   .0.6   .1.2   .0.2   .1.9   .0.2   .1.2   .0.2   .1.9   .0.2   .0.2   .0.2   .1.9   .0.2   .		148				150	1.7	.030		-	₹.	_	٠			. 213	-	•	٠	4.0
10.3   180   -1.5   -0.056   -1.2   -0.01   3.7   -0.055   -1.06   -1.5   -0.055   -1.06   -1.5   -0.055   -1.06   -1.5   -0.055   -1.06   -1.5   -0.055   -1.06   -1.5   -0.055   -1.06   -1.06   -1.0   -0.033   -1.0   -0.033   -1.0   -0.033   -1.0   -0.033   -1.0   -0.055   -0.055							4	.024				•	9	045	6.	•	•	.003	٠	.01
1.5   0.09   0.00   0.1   0.04   0.44   0.		7 2		=				026		-	,	021	۲.	. 590	~	108	S. 55	•	٠	- 10
1.0				•			:	500				_	0	800	۲.	.012	~	•		.077
1.5   1.05   1		7.					? -	220				-	6	103	•	.054		.056	•	.017
122						•	0	•				-		680			4.6	.05		.080
127 128 129 129 129 129 129 129 129 129 129 129							n c	•					· c	200	•		3.6	90		. 124
133 3		. 124					7 U	•				-	) c			072	-	80		. 141
131 132 133 134 135 136 137 138 138 138 138 138 138 138 138 138 138		. 133				•		•				•	, (	•	•		_	030		101
136		. 127				•	ָ פּי	•				•	، د		•		. ~	•		960
133		136					٥.	•				. •	, (							. 103
131 136 136 137 138 138 139 139 139 139 139 139 139 139 139 130 130 130 130 130 130 130 130 130 130		= :					2.0					•	> > <	•	•		. <b>(</b>	028		710.
136 126 127 128 129 129 120 120 120 120 120 120 120 120 120 120		131				•	<b>50</b> (	•				•	۰ د د	•	•		. 4	950	•	084
126		. 136				•	n.	•				- '			n e			, i		850
1.06  1.07  1.08  1.09		. 126					<del>-</del> ,	•					5.6		P P	2 5	) e	200		800
127		106					o.	•					<b>20</b> 1		- (	200	, ,	2 4		V 00
152 9.2 161 .7 .012 1.3 .023 .4 .007 3.9 .008 5.8 .008		. 127					₹.	•					3.3		7 (	7.0		565	•	72.
154 - 7.4 - 129		. 152		-		191.	۲.	.012		_	m			,000	ית.	9 6	* (	5	•	
087 0.0 0.000 0.000 0.0 0.000 0.2.4		154				•	٩.	. 129					<b>5</b> 0.	- 60	7	25.	n c	36		
124 - 3.1054		.087					0	•				-	0	8	4	2 5	? ?	6.00	٠	
152 <th></th> <th>124</th> <th></th> <th></th> <th></th> <th>•</th> <th>_</th> <th></th> <th></th> <th></th> <th></th> <th></th> <th></th> <th></th> <th></th> <th>90</th> <th>'n</th> <th>040</th> <th>٠</th> <th>000</th>		124				•	_									90	'n	040	٠	000
138								500						.014	9	0.0		•	٠	.094
138		71.						•								059	3.3	•		.089
120 115 115 117 117 118 118 118 118 118 118		86.				•		•				•				073		. 026		.082
115 -1.3023		. 120						•				•	٠.	100	•	257	ď			080
167 - 7.7 - 134 - 1.2 . 021 - 6.5 - 113 - 6.8 - 119 11.7 . 114 1 124 024 024 024 021 027 033 4.3 . 124 021 021 021 021 021 021 021 031 4.3 . 157 038 - 2.7 038 - 2.7 047 5.5 . 0.0 0.00 0.000 - 2.6 045 - 3.8 066 4.3 . 120 0.5 0.26 0.26 0.26 0.27 045 - 2.6 045 6.2 039		. 1.15				•	ر س	٠					•	55	•			•	•	200
141		187				•	۲.	•					7	•	n.	•	0.0	•	•	
124						•	4					•	0	•	∞.	•	D.	٠	٠	60.
124		: :						5						.047	۲.	.003	0	•	•	.075
0.0 0.000 -2.6045 -3.8066 4.3 -1.5026 -0.000 2.8 .049 -2.6045 6.2 -1.5026		124						٠				•				138		.047	•	960.
0.0 0.000 2.8 .049 -2.6045 6.2		. 157					Ŋ,	•					ų (			•	•		•	.075
-1.5026 0.00 0.000 2.8 .049 4.6 .043 0.5		120					0	•					٠,	•		٠		3	•	200
		000				•		•				-	0		•	.049	٠	. 040	٠	

TO 08 FF AT TO AT	Name		LANDING	ING DATA	1	MODEL F.	4					(CAN-65)			Z	NIGHT LANDINGS	NNO I NO	vo			
RAD         DEG         RAD <th>## FF</th> <th></th> <th>Ç</th> <th>I</th> <th>z</th> <th></th> <th></th> <th></th> <th>0</th> <th></th> <th>ပ</th> <th>w</th> <th></th> <th>РІТСН</th> <th>RATE</th> <th>ROLL</th> <th>RATE</th> <th></th> <th></th> <th>YAY</th> <th>_</th>	## FF		Ç	I	z				0		ပ	w		РІТСН	RATE	ROLL	RATE			YAY	_
45         46         47         48         96         RAD         DEG	Main   Dec   Rad   Dec			g		FF		7	_	OR					TD	AT	10	AT	5		۵
6.7 117 2.0 0.05 6.4 112 2.7 0.04 5.1 1.6 0.08 6.4 112 2.7 0.04 5.1 1.4 1.4 1.4 1.4 1.4 1.4 1.4 1.4 1.4 1	6.7 117 2 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	RAD		DEG	RAD	w	RAD	DEG	RAD	DEG	RAD	DEG	RAD	DEG	RAD	DEG	RAD	30	RAD	DEG	RAD
7.7         117         2.0         0.00         6.4         112         2.7         0.04         5.1         0.08         6.9         115         2.7         0.09         7.1         1.2         2.7         0.04         2.7         0.04         3.5         1.9         1.5         1	7. 117         2.0.4        059         1.6         0.000         6.4         +112         2.7        047         5.1        040         +1.2         2.7        047         1.6         0.02         2.0         0.05         5.3        045         1.5         0.02         2.0         0.05         1.5         0.05         2.7         0.04         1.6         0.05	43 4	4	4		46	47	48	49	20	51	52	53	24	22	99	57	28	53	09	61
7. 117 24077  4.4077  1.5025  1.6028	7. 117 2.0         0.077         1.6 .028 5.1 .089 8.9 .155 5.3 .002 7.9         1.5 .002 7.9	122					'	4	•				Ū	0			. 112	2.7	•		680.
7. 117         2.0         0.032         1.6         0.028         3.0         0.052         2.3         0.044         0.05         3.5         0.08         7.6         0.09         4.5         0.08         7.6         4.5         0.08         7.6         0.08         7.6         0.08         7.6         0.08         7.6         0.08         7.6         0.08         7.6         0.08         7.6         0.08         7.6         0.08         7.6         0.08         7.6         0.08         7.6         0.08         7.6         0.08         7.6         0.08         7.6         0.08         7.6         0.08         7.6         0.08         7.6         0.09         7.0         0.09         0.00 <t< td=""><td>7. 117         2.0         0.032         1.6         .028         3.0         .032         1.3         .044         .024         3.5           2. 7         .047         .047         .047         .047         .047         .056         1.6         .057         1.6         .057         1.6         .058         7.6         1.6         .058         <t< td=""><td>138</td><td></td><td></td><td></td><td></td><td>•</td><td>٩.</td><td>•</td><td></td><td>•</td><td></td><td></td><td>٠</td><td></td><td>6.8</td><td>សួ</td><td>5.3</td><td>•</td><td>٠.</td><td>. 138</td></t<></td></t<>	7. 117         2.0         0.032         1.6         .028         3.0         .032         1.3         .044         .024         3.5           2. 7         .047         .047         .047         .047         .047         .056         1.6         .057         1.6         .057         1.6         .058         7.6         1.6         .058 <t< td=""><td>138</td><td></td><td></td><td></td><td></td><td>•</td><td>٩.</td><td>•</td><td></td><td>•</td><td></td><td></td><td>٠</td><td></td><td>6.8</td><td>សួ</td><td>5.3</td><td>•</td><td>٠.</td><td>. 138</td></t<>	138					•	٩.	•		•			٠		6.8	សួ	5.3	•	٠.	. 138
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5      009       4.3       .075       -7.4      129       -5.9      103       11.1        1       .002	500950095009103120053005400750160016	134							.8					80	•	9.3	~	1.2	.021		108
1       .002       6.0       .105       5.2       .091       -1.9      033       4.7         1       .005       .005       .003       .1       .002      065       7.5         .7       .152       .2       .003       .2       .003       -1.0      017       -1.0      017       -5.3      092       8.6         -2.1      037       .006       .2       .007       .000       1.0      017       -1.0      017      03       8.2         .9       .016       .000       0.000       1.0       .175       -2.1      035       9.8         .9       .016       .000       0.000       10.9       .175       -2.1      037       4.2         .9       .016       .000       0.000       4.6       .080       -2.4      042       2.9         .9       .016       .000       0.000       4.6       .080       -2.4      042       2.9         .9       .016       .000       0.000       4.6       .080       -2.8      049       6.7         .9       .016       .000       0.000       0.000       -2.8      049 <td>1. 1 .002 1. 1 .002 1. 1 .002 1. 1 .002 1. 1 .002 1. 1 .002 1. 1 .002 1. 1 .002 1. 1 .002 1. 1 .002 1. 1 .002 1. 1 .002 1. 1 .002 1. 1 .002 1. 1 .003 1. 2 .003 -1.0 -0.17 -1.0 -0.03 18.5 1. 1 .002 1. 1 .003 1. 1 .002 1. 1 .003 1. 1 .002 1. 1 .002 1. 1 .003 1. 1 .002 1. 1 .003</td> <td>. 143</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>•</td> <td></td> <td></td> <td></td> <td>•</td> <td></td> <td>- 270.</td> <td>٩.</td> <td>. 129</td> <td>5.9</td> <td>. 103</td> <td>•</td> <td>194</td>	1. 1 .002 1. 1 .002 1. 1 .002 1. 1 .002 1. 1 .002 1. 1 .002 1. 1 .002 1. 1 .002 1. 1 .002 1. 1 .002 1. 1 .002 1. 1 .002 1. 1 .002 1. 1 .002 1. 1 .003 1. 2 .003 -1.0 -0.17 -1.0 -0.03 18.5 1. 1 .002 1. 1 .003 1. 1 .002 1. 1 .003 1. 1 .002 1. 1 .002 1. 1 .003 1. 1 .002 1. 1 .003	. 143							•				•		- 270.	٩.	. 129	5.9	. 103	•	194
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	_	<u>e</u>	RAD	61	.094 .155 .192 .192 .239 .239 .239 .049 .068
	YAW	AT TD	DEG	9	4 8 9 0 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
	F. P. A.	5	RAD	23	
	Ĩ.	AT	DEG	58	2,0,0,4,0,0,0,0,0,0,0,0,0,0,0,0,0,0,0,0,
NIGHT LANDINGS	RATE	10	RAD	57	201 248 259 259 259 259 259 250 250 250 250 250 250 250 250 250 250
GHT LA	ROLL RATE	AT	DEG	56	
Z	PITCH RATE	10	RAD	55	0.000 11.5 0.000-14.2 0.003 -2.0 0.033 -9.7 0.000-13.6 0.000 -1.6 0.000 -1.6 0.000 2.4 0.000 2.4 0.000 2.4 0.000 2.4 0.000 2.4 0.000 2.4 0.000 2.4 0.000 2.4
	РІТСН	AT	DEG	54	0001-0-0000048-8
			RAD	53	
N-65)	¥	FF	DEG	52	
, Е (С	N G L		RAD	51	
USS ENTERPRISE (CVN-65)	⋖	OR	930	20	
JSS EN	ROLL		RAD	69	042 .021 .092 .092 .052 .093 .099 .097 .091
		5	DEG	8	
<b>4</b>			RAD	4.7	
MODEL F-14	n m	7.	DEG	<b>4</b> 6	<b>;</b>
¥ - ¥L	Z		RAD	<b>4</b> 5	<b>;</b>
LANDING DATA -	ĭ	č	DEG	4	;
LAND	P 1 C		RAD	. <b>4</b>	27 20 20 20 20 20 20 20 20 20 20 20 20 20
		£	DEG	42	. 6676887788787767 487878787878787878787878787878787878787
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### NADC-91124-60

		Ţ	LANDING DATA	٠	MODEL	F - 14		USS E	NTER	ENTERPRISE	E (CVN-65	1-65)			Z	NI GHT	LANDINGS	v			
LNDG	OFF.	OFF-CENTER	RAMP TO	TO TD	WIRE	SIDE	LNDG	FLAP	SHIP		DECK P	PITCH	DECK	ROLL	TEMP	a	BAROMETRIC	TRIC	ARR	GEAR	REREAD
Š	013	STANCE	018	DISTANCE	₽.	Š.	TYPE	CODE	SPEED	ED							PRESSURE	URE	RUNDUTS	UTS	NUMBER
	FT	I	1	*					z	M/S	DEG	RAD	DEG	RAD	<u>u</u>	ပ	IN HG	MM HG	Z	S.	
62	63	4	65	99	67	89	69	70	7.1	72	73	74	75	9/	7.7	78	79	80	18	82	
16	9	-2	209	64		440	70100		4				œ.	010	63		ę.	7.69.7	0		0
		e.	255	7.3		450	70120		₹		-	•	ლ :	.005	63		6.0	759.7	00	0.0	0 (
9	თ	n	307	94		445	70200		毋 ⋅		₹.(	•	, ب	•	63		o	759.7	•	, c	00
9169	7 :	- 1	289	60 r	∢ (	440	80120		٧,	~ ~			0 4	•	2 6		29.91	759.7		34.0	0
- :	? -	* 5	200	2,2	,	447	50120		. 4				, m	.005	63		. 6	759.7	170		0
: _	. 4	· <del>-</del>	247	5.	n ا	445	50200		4		, E.	•	- 5.9 -	.051	63		6	759.7	-	*	o ·
9180	-	ŗ	183	26	-	447	50120		4		9	٠	- 1.3	.023	63		6	759.7	-		<del>-</del> c
9181	- 12	7	227	69	7	440	50200		₹,		٠	•	٠.	36	9		o	750.7		- 0	> 0
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9266	- 12	7	250	16	ო	440	50120		4	7	7	.003	m	.003	63	<u>.</u>		760.7		- c	o <del>-</del>
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XN         M/S         DEG         RAD         F         C         IN HG         MM HG         IN         CM           71         72         73         74         75         76         77         78         79         80         81         82           71         72         73         74         75         76         77         78         79         80         81         82           4         2             17         29         95         760. 7         169         479. 3         1           4         2             17         29         95         760. 7         169         479. 3         1           4         2             17         29         95         760. 7         11         4         17         29         95         760. 7         11         4         17         29         95         760. 7         11         4         17         29         95         760. 7         11         4         18         7         18         7	LANDING DATA - MODEL F-14 OFF-CENTER RAMP TO TO WIRE SIDE	DING DATA - MODEL F RAMP TO TO WIRE	- MODEL F TO WIRE	u w	<b>LL</b>	la.i	LNDG	USS E	SHIP D	۵	DECK	РІТСН	DECK	ROLL	-	TEMP	BAROM	BAROMETRIC	ARR	GEAR	REREAD
M/S         DEG         RAD         F         C         IN         HG         HM         HG         IN         CM           72         73         74         75         76         77         78         79         80         81         82           2          5        003         -1.4        024         63         17         29.95         760.7         169         429.33           2             14        024         63         17         29.95         760.7         169         429.33           2              17         29.95         760.7         169         429.33           2             17         29.95         760.7         170         413         18         20         29.99         760.7         170         413         18         20         29.99         760.7         170         413         18         20         29.99         760.7         170         413         20         20         20         20         20         20	DISTANCE DISTANCE NO. NO. TYPE CODE	DISTANCE NO. NO. TYPE CODE	E NO. NO. TYPE CODE	. NO. TYPE CODE	. TYPE CODE	CODE			SPE	ED							PRES	SURE	S	auts	NUMB
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2         -5         -009         -6         -010         63         17         29         95         760.7         169         479.3           2         -2         -0003         -1         -0024         63         17         29.95         760.7         170         434.3           2         -4         -007         -1         0.002         63         17         29.95         760.7         170         431.8           2         -6         -000         -1         -0002         63         17         29.95         760.7         170         431.8           2         -1         -0002         -1         -0002         68         20         29.89         759.2         170         436.9           2         -1         -0002         68         20         29.89         759.2         170         436.9           2         -003         -5         -003         68         20         29.89         759.2         170         431.8           2         -003         -6         -003         68         20         29.89         759.2         170         431.3           2         -003         -7         -003	-4 3C	30 92 4 450	92 4 450	0	0	50100	4	4		7	2	003		•	63	17	29.95	7.097		29.	0
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NO.         DISTANCE         NO.         VIPE         CODE         SHIP         DECK PITCH         TEKY         RARDHERIC         ARR GEAR         REREAD           NO.         DISTANCE         DISTANCE         DISTANCE         NO.         TYPE         CODE         SPEED         PRESSURE         RUNDUTS         NUMBER           FT         M         FT         M         NO.         TYPE         CODE         SPEED         RAD         DEG         RAD         F         C         IN HG         MM HG         IN         CM           42         62         64         65         66         67         68         69         70         71         72         74         75         76         77         78         79         80         81         82           9439         -17         -5         283         86         -4         201         50.200         7         4         -6         -010         -1.2         70         7         7         4         -6         -010         -1.2         70         7         7         4         -6         -010         -1.2         70         7         7         4         -6         -010 <td< th=""><th></th><th></th><th>LAM</th><th>O DNIC</th><th>LANDING DATA - MODEL</th><th>MODEL</th><th>F - 14</th><th></th><th>USS</th><th>NTER</th><th>ENTERPRISE (CVN-65</th><th>C (C</th><th>N-65)</th><th></th><th></th><th><u>د</u></th><th>NIGHT</th><th>LANDINGS</th><th>S</th><th></th><th></th><th></th></td<>			LAM	O DNIC	LANDING DATA - MODEL	MODEL	F - 14		USS	NTER	ENTERPRISE (CVN-65	C (C	N-65)			<u>د</u>	NIGHT	LANDINGS	S			
FT         M         FT         M         VPE         CODE         SPEED           FT         M         FT         M         M/S         DEG         RAD         DEG         RAD         F         C         IN         HG         IN         CM           63         64         65         66         67         68         69         70         71         72         73         74         75         77         78         79         80         81         82           17         -13         -4         320         98         4         201         50100         7         4         -6         -007         -9         -016         71         72         73         74         -7         74         -7         74         -7         -007         -9         -016         71         72         29         90         759         9         10         00         00           -10         -3         265         81         3         201         7         4         -6         -010         1.5         026         71         78         17         18         80         81         82           -10	LNOG	OFF-CE	ENTER		TO TD	WIRE	SIDE		FLAP	SHI				DECK		16	Ę.	BAROME	TRIC	ARR	GEAR	REREAD
FT         M         FT         M         KN         M/S         DEG         RAD         DEG         RAD         F         C         IN         HG	9	0157	ANCE	018	TANCE	Š.	8	•	CODE	SPE	ED :							PRESS	URE	NO.	JUTS	NUMBER
63         64         65         66         67         68         69         70         71         72         73         74         75         76         77         78         79         80         81           -13         -4         320         98         200         70200         74        6        007         .9         .016         71         22         29.90         759.5         170           -10         -3         265         81         3         447         50200         7         4        6        010        2        016         71         22         29.90         759.5         170           -13         -4         263         80         3         201         50120         7         4        6        010        7        010         71         22         29.90         759.5         171           -15         -25         305         93         201         70200         7         4        6        010         71         22         29.90         759.5         171           -10         -3         205         90         7         4        6		F	I	F	=					Z	M/S	DEG	RAD	DEG	RAD	u.	υ		MM HG	z	<b>∑</b> O	
-13         -4         320         98         200         70200         7         4        0        0        0         11         22         29.90         759.5         170           -17         -5         283         86         4         201         50100         7         4        6        010        2        003         71         22         29.90         759.5         170           -19         -3         265         81         3         447         50200         7         4        6        010         15         .026         71         22         29.90         759.5         171           -15         -305         93         -4         50200         7         4        6        010         15         .026         759.5         171           10         -3         209         70200         7         4        6        010         1.         20         29.90         759.5         170           -11         -3         308         94         201         70200         7         4        6        010        1        0         22         29.90	62	63	64	65	99	67	68	69	70	1.1	72	73	74	75	97	77	7.8	79	80	-	82	
-17         -5         283         86         4         201         50100         7         4        6        010        2        003         71         22         29.90         759.5         170           -10         -3         265         81         3         447         50200         7         4        6        010         1.5         .026         71         22         29.90         759.5         171           -15         -5         305         93         4         450         50200         7         4        6        010         1.5         .026         71         22         29.90         759.5         170           -10         -3         209         70         7         4        6        010         1.5         .02         29.90         759.5         170           -11         -3         308         94         201         70200         7         4        6        010         .1         .002         71         22         29.90         759.5         170           -11         -3         308         94         201000         7         4        6         -	Φ	-13	7	320	96		200	70200		7	4	₹.	007	6.	.016	7.1	22	29.90	759.5		0.0	0
-10         -3         265         81         3         447         50200         7         4        6        010         1.5         .026         71         22         29.90         759.5         171           -13         -4         263         80         3         201         50120         7         4        6        010         71         22         29.90         759.5         171           -10         -3         308         94         201         70200         7         4        6        010         7         22         29.90         759.5         170           -11         -3         308         94         201         70200         7         4        6        010         .1         .002         71         22         29.90         759.5         170           -11         -3         308         94         201         70200         7         4        6        010         .1         .002         71         22         29.90         759.5         170           -11         -3         308         94         201200         7         4        6        010         -	<del>ر</del>	- 17	'n	283	86	4	201	50100		7	4	9.	010	. 2	003	7.1	22	29.90	759.5		131.3	-
-13         -4         263         80         3         201         50120         7         4        6        010         71         22         29.90         759.5         171           -15         -5         305         93         4         450         50200         7         4        6        010         71         22         29.90         759.5         170           -10         -3         305         93         201         70200         7         4        6        010         71         22         29.90         759.5         170           -11         -3         308         94         201         70200         7         4        6        010         -1         202         29.90         759.5         170           -11         -3         308         94         201         70200         7         4        6        007         1.9         .033         71         22         29.90         759.5         0           -11         -3         207         4         4         2        6        010        2        03         760.0         760.0         760.0 <t< td=""><td>7</td><td>- 10</td><td>٠.</td><td>265</td><td>8</td><td>e</td><td>447</td><td>50200</td><td></td><td>7</td><td>, 4</td><td>9.</td><td>010</td><td><u>.</u></td><td>.026</td><td>7</td><td>22</td><td>29.90</td><td>759.5</td><td></td><td>134.3</td><td>0</td></t<>	7	- 10	٠.	265	8	e	447	50200		7	, 4	9.	010	<u>.</u>	.026	7	22	29.90	759.5		134.3	0
-15         -5         305         93         4         450         50200         7         4        5        009         .4         .007         71         22         29·90         759·5         170           -10         -3         239         73         2         200         50120         7         4        3        005         -2.8        049         71         22         29·90         759·5         170           -11         -3         308         94         201         70200         7         4        6        007         1.9         .033         71         22         29·90         759·5         170           -12         -4         30         101         450         70120         7         4        6        010        2        033         71         22         29·90         759·5         0           -11         -3         297         91         4         4         2        6        007        2        003         71         22         29·92         760·0         172           -18         -5         24         50100         4         2	60	- 13	7-	263	80	n	201	50120		7	4	4.	007	9	010	7.5	22	29.90	759.5		134.3	-
-10         -3         239         73         2         200         50120         7         4        3        005         -2.8        049         71         22         29.90         759.5         170           -12         -4         305         93         201         70200         7         4        6        010         1         .002         71         22         29.90         759.5         170           -11         -3         308         94         201         70200         7         4        0         1         .002         71         22         29.90         759.5         0           -11         -3         297         91         4         450         50100         4         2        4         .007         .9         .016         71         22         29.92         760.0         170           -11         -3         214         65         50100         4         2        5        009        1        002         71         22         29.92         760.0         171           -11         -3         214         65         50100         4         2        5 <td>6</td> <td>- 15</td> <td>ŗ.</td> <td>305</td> <td>6</td> <td>4</td> <td>450</td> <td>50200</td> <td></td> <td>7</td> <td>4</td> <td>۲.</td> <td>600</td> <td>4</td> <td>.00</td> <td>7.1</td> <td>22</td> <td>29.90</td> <td>759.5</td> <td></td> <td>131.8</td> <td>0</td>	6	- 15	ŗ.	305	6	4	450	50200		7	4	۲.	600	4	.00	7.1	22	29.90	759.5		131.8	0
-12         -4         305         93         201         70200         7         4        6        010         .1         .002         71         22         29.90         759.5         0           -11         -3         308         94         201         70200         7         4        6        010         .1         .003         71         22         29.90         759.5         0           -11         -3         310         91         4         450         50100         4         2        6        010        2        007         71         22         29.92         760.0         70           -18         -5         279         85         3         450         50100         4         2        6        007         71         22         29.92         760.0         171           -11         -3         214         65         2         447         50100         4         2        5        002        6        010         71         22         29.93         760.2         171           -9         -3         232         747         50100         4         2 <td>-</td> <td>- 10</td> <td>ę.</td> <td>239</td> <td>73</td> <td>7</td> <td>200</td> <td>50120</td> <td></td> <td>7</td> <td>4</td> <td>е.</td> <td>005</td> <td>-2.8</td> <td>049</td> <td>7.1</td> <td>22</td> <td>29.90</td> <td>759.5</td> <td></td> <td>131.8</td> <td>-</td>	-	- 10	ę.	239	73	7	200	50120		7	4	е.	005	-2.8	049	7.1	22	29.90	759.5		131.8	-
-11         -3         308         94         201         70200         7         4         -10         -10         1.9         .033         71         22         29.92         760.0         0           -12         -4         330         101         4         450         50100         4         2         -6         -010         -7         -033         71         22         29.92         760.0         0           -18         -5         279         85         3         450         50100         4         2         -6         -007         71         22         29.92         760.0         171           -11         -3         214         65         2         447         50100         4         2         -1         -002         -6         -010         71         22         29.93         760.0         171           -9         -3         232         71         2         447         50100         5         3         -6         -010         -1,2         -02         171         2         29.93         760.2         171           -9         -3         2         4         4         5         3 <td>6</td> <td>- 12</td> <td>7</td> <td>305</td> <td>6</td> <td>1</td> <td>201</td> <td>70200</td> <td></td> <td>7</td> <td>· •</td> <td>9.</td> <td>010</td> <td>-</td> <td>.002</td> <td>7.1</td> <td>22</td> <td>29.90</td> <td>759.5</td> <td></td> <td>0.0</td> <td>0</td>	6	- 12	7	305	6	1	201	70200		7	· •	9.	010	-	.002	7.1	22	29.90	759.5		0.0	0
-12         -4         330         101         450         70120         4         2        6        010        2        003         71         22         29.92         760.0         0           -11         -3         297         91         4         450         50100         4         2        6        007         9         .016         71         22         29.92         760.0         170           -18         -5         279         85         3         450         50100         4         2        5        009        1        002         71         22         29.92         760.0         171           -9         -3         234         65         50100         4         2        1        002        6        010         71         22         29.93         760.0         172           -9         -3         23         69         20100         5         3        6        010        1        02         29.93         760.2         171           -14         -4         208         63         447         60100         5         3        2	ທ	-	Ģ	308	96		201	70200		7	4	۲.	007	6.1	.033	7.1	22	29.90	759.5		0.0	0
-11     -3     297     91     4     450     50100     4     2    4    007     .9     .016     71     22     29.92     760.0     170       -11     -3     214     65     2     447     50100     4     2    5    009    1    002     71     22     29.92     760.0     171       -9     -3     232     69     2     447     50100     4     2    1    002    6    010     71     22     29.92     760.0     172       -9     -3     232     69     2     447     50100     5     3    6    010     -1.1    02     29.93     760.2     171       -14     -4     225     69     2     447     60100     5     3    2    005     -1.1    019     71     22     29.93     760.2     0       -14     -4     208     63     447     60100     5     3    2    005     71     22     29.93     760.2     0	_	- 12	7	330	101		450	70120		4	7	9.	010	2	003	7.1	22	29.92	760.0		0.0	0
-18         -5         279         85         3         450         50100         4         2        5        009        1        002         71         22         29.92         760.0         171           -11         -3         214         65         2         447         50100         4         2        1        002        6        010         71         22         29.93         760.0         172           -9         -3         235         71         2         447         50100         5         3        6        010         -1,2        021         71         22         29.93         760.2         771           -14         -4         225         69         2         447         60100         5         3        2        005         +1,1        019         71         22         29.93         760.2         0           -14         -4         208         63         447         60100         5         3        2        005         +1,1        019         71         22         29.93         760.2         0	4	=======================================	ņ	297	6	4	450	50100		4		4.	007	6.	.016	7.1	22	29.92	760.0		131.8	-
-11 -3 214 65 2 447 50100 4 210026010 71 22 29.92 760.0 172 -9 -3 232 71 2 447 50100 5 36010 -1.2021 71 22 29.93 760.2 171 -14 -4 225 69 2 447 50100 5 33005 -1.1019 71 22 29.93 760.2 171 -14 -4 208 63 4 47 60100 5 32003 .5 .009 71 22 29.93 760.2 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	6	- 18	'n	279	8	က	450	50100		4	,	ت	009	-	002	7.1	22	29.92	760.0		134.3	-
-9 -3 232 71 2 447 50100 5 36010 -1.2021 71 22 29.93 760.2 171 -14 -4 225 69 2 447 50100 5 33005 -1.1019 71 22 29.93 760.2 171 -14 -4 208 63 447 60100 5 32003 .5 .009 71 22 29.93 760.2 0	S	-1-	ņ	214	65	~	447	50100		4	2	-	002	9	010	7.1	22	29.92	760.0		136.9	0
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-14 -4 208 63 447 60100 5 32003 .5 .009 71 22 29.93 760.2 0	_	- 14	4-	225	69	7	447	50100		ស	ا	ი.	005	- -	019	7.1	22	29.93	760.2		134.3	0
	_	- 14	4	208	63		447	60100		ហ	,	7	003	ت	600	7.1	22	29.93	760.2		0.0	0

CODES 43 THROUGH 45

LANDING # 615.0 NOT FOUND

LANDING # 656.0 NOT FOUND

LANDING # 656.0 NOT FOUND

LANDING # 670.0 NOT FOUND

LANDING # 722.1 NOT FOUND

LANDING # 722.1 NOT FOUND

LANDING # 723.1 NOT FOUND

LANDING # 733.0 NOT FOUND

LANDING # 733.1 NOT FOUND

LANDING NUMBER 1109 TWO CODES

LANDING NUMBER 1109 TWO CODES

### **F-18 DAY**

			LANDING	NG DATA	¥	- NODEL F-18A	18A		USS ENTERPRISE (CVN-65)	TERPR	SE (C	¥¥-65	2		_	DAY LANDINGS	INGS	SS		
LNOG	VPAF	14	VE-F1	3	*	WIND-VEL		>	VEOR	VPAMIN	z	VSP'A	<b>*</b>	KVPA	<b>≩</b>	LIFT	LIFT	WE	WEIGHT	
ġ	5				PAR.		PERP.							Z	V .dS	10	14			
	Š	N/S	\$	M/S KN	S/M	S KN	S/N	¥	s/x	×	S/M	Z Z	s/m					rBS	Š	
	~	•	*	<b>s</b> o	6 7	60	<b>б</b>	6	=	12	5	<b>±</b>	5	9	11	18	19	20	21	
1178	140	72	118	61 22	7	-	-	122	63	134	69			1.05		1.10		30554	13859	
171	138	7	116		- 2	-	-	100	5	134	69			1.03		1.99		30554	13859	
27:1	= :	۲ :	£ ;		23	~ .	- •	120	62	55	89 :			1.05		1.10	1.10	30254	13723	
11/9	2 5	8 8	9 :	57 22	-:		<b></b>	102	22	5 2	66			1.61 84		99.	9	28854	13088	
1193	3 52	8 7	2 2	25 60 22		v		116	7 09	9	8			3		- <del>-</del>	9	1007	C7/71	
1195	147	92	125		1	-	-	117	99	128	99			1.15		1.10		27754	12589	
1200	148	92	123		-	~	-	121	62	134	69			1.11		1.00		30654	13905	
1207	136	9	<b>*</b>		7	_	•	120	62	134	69			1.61		1.00		30554	13859	
1210	132	2	110		- -		•	=	21	129	99			1.02		1.10		28554	12952	
1390	157		129		<del>-</del> -	<b>.</b>	•			137	79			<b>1.</b>		. 98		31954	14494	
1397	145	۲۲ ا	112		<del>-</del> -	<b>.</b>	6	112	လ လ	136	70			1.07		. 90		31354	14222	
1402	48	9 9	6 2 3		- :		<b>6</b>	123	63	136	9 9			1.09				31354	14222	
3	80.	2 :	* * *		2:		<b>5</b> 6	/71	င္ပ င	\$ .	n 0			2:		 		30054	13936	
101	:	2 %	2 5	96 59	2 5	<b>9</b> 9	<b>D G</b>	<u> </u>	n 0	2 5	0 9			- 6		99.		10554	13850	
1407		2 2	118				9 6		n 6	2	6 9					- +		10554	1.1850	
488	65	2 2	2 2	- 60	_	· ·	•	=	2 2	5	3			3		9.1				
1489	=	<b>*</b>	116				6	13	8	133	89			1.08		96		39954	13632	
141	148	92	120		<u>-</u>	-	•	==	29	133	89			1.11		1.10		30154	13678	
1412	<u>‡</u>	*	115		5	-	-	107	55	133	68			1.08		1.00		30154	13678	
1418	142	2	117		5 13	<b>6</b>	6	119	5	129	99			1.10		1.00		28454	12967	
1419	142	2	117		2	•	•	113	<b>28</b>	129	99			1.09		96.		28554	12952	
1420	142	2	116		-	-	•	105	40	133	68			1.07		- 00		30054	13632	
1421	145	ا ا	5 5	61 26	2:	<b>∞</b> ·	•	129	9 9	5	67					- 9: 8		29054	13179	
1423	142	2 2	15				• •	196	555	130	29			1.10		1.10		28654	12997	
1424	3	7	2 2		5.	•	6	117	99	130	29			1.10		96.		28954	13134	
1425	137	92	112		_	<b>6</b>	•	105	4	128	99			1.07		1.00		27954	12680	
1427	149	1	124	•	_	<b>~</b>	•	127	65							1.10				
1428	135	69	=	_	_	~	•	108	20	136	70			1.00		8		31354	14222	
1430	25	7	113	<b>6</b> 0		∞ -	•	<b>+</b>	23	133	68			1.04		90		29954	13587	
1434	151	<b>8</b>	126		= :	<b>~</b>	•	124	4					;		9 :				
1435	147	9	122		_	~	•	125	49	136	20			1.08		1.10		31454	14268	
<b>438</b>	*	*	6		_	~	•	123	3	55	89			1.08		- 99		30354	13769	
1439	147	9	122		_	<b>~</b>	•	117	9	133	89			1.10				30354	13769	
141	40	12	124	<b>→</b> (		<b>~</b>	•	119	<b>.</b>	137	9 1			1.08		- 00		32154	14585	
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1445	151	28	126	65 25	<u>.</u>	<b>∞</b> .	•	135	69	137	9 4			1.10		9		31954	14494	
1446	<b>+</b>	*	25		_	~	9	2	ŝ	2	٩			99.		<u> </u>		\$100TO	77761	

#### NADC-91124-60

#### DEPARTMENT OF THE NAVY Naval Air Development Center Warminster, PA 18974-5000

			3	LANDING DA	ATA -	DATA – MODEL F-18A	L F-1	<b>≨</b>	٠	uss en	TERPR	ENTERPRISE (CVN-65)	SWN-6	<i>(</i> c			DAY LANDINGS	ND I NGS	SS	
2007	VPAF	u.	Υ. -	VE-FILM		WIND-VEL	-vEL		<b>X</b>	VEOR	VPAMIN	Z	V. dSA	ج.	KVPA	\$	LIFT	LIFT		WEIGHT
ġ	5				<b>a</b> ∵	PAR.	9	PERP.							Z Z	SP. A	2	7.		
	ž	K/S	₹	E/S	₹	K/S	₹	S/N	₹	S/M	ž	N/S	ž	s/m					<b>188</b>	Š
	~	n	•	60	•	7	•	0	6	=	12	<u></u>	<b>±</b>	5	91	11	18	19	<b>50</b>	21
1448	151	78	121	62	8	5	•	•	112	88	136	70			<b>- - - - - - - - - -</b>		96		31354	14222
1450	156	8	126	65	en P	5	•	•	126	65	135	69			1.16		96		30854	13995
2	147	92	117	69	9	5	•	0	122	63	135	69			1.09		1.10		31254	14177
2	151	78	12	62	ရှိ (	<del>ن</del> :	•	<b>o</b>	120	62	135	69			1.12		1.10		31054	14086
1454	* :	<b>*</b>	<b>*</b> :	6 6	8	5	<b>6</b>	•	£ :	19	<u> </u>	69					00		30454	13814
2 5	7 5	S 5	7 5	8 5	5 5	ÜÄ	9 4	<b>D</b> 6	9 7	n e	2 2	) G			 8 -				19664	13356
2 5	2 4	4 6	3 =	) E	3 5		•	•		S 5	7	6 6							19754	13050
. <u>.</u>	4	2	9	5	8 8	5 52	•	•	115	. 65	133	89			1.96		1.10		30054	13632
1460	Ξ	2	Ξ	22	3	5	•	•	11	29	133	68			1.07		1.00		29954	13587
1461	159	83	129	99	8	č	•	•	122	63	137	70			1.16		1.20		32054	14540
1462	145	75	=======================================	29	క్ర	ţ.	•	0	113	28	133	89			1.09		1.00		30054	13632
2	138	7	<b>5</b>	26	2	5	•	•	110	22	131	29			1.05		1.10		29354	13315
* (	# :	<b>*</b> :	= :	<b>8</b>	8	£ :	•	•	108	20	137	9 9			1.05		1.00		31854	14449
י פ	9	2 1	2	<b>8</b>	3	<u>.</u>	9 (	9 (	2:	9 9	5	g ;							31054	14085
/01/	7 4	2 4	2 :	R 4	3 5	<u>.</u>	<b>D G</b>	9 6	2 2	9 4	92.	) Y			= :		99.		28834	13866
1469	147	2 %	117	8 8	8	, <b>1</b>	•	) <b>C</b>	127	8 6	2 2	3 4							28554	12952
•	146	2	19	9	8	5	•	• •	117	9	135	69			1.09		1.10		30854	13995
1472	139	72	<b>6</b>	26	8	15	•	•	100	5							1.00			
n	147	76	117	2	8	5	•	•	122	63	136	70			1.08		1.30		31754	14484
1474	#	7	==	28	8	5	0	0	109	26	129	99			1.12		1.00		28454	12907
io i	152	2	122	3	2	<b>5</b>	•	•	125	<b>9</b>	135	69			1.13		1.10		30854	13995
<u>, , , , , , , , , , , , , , , , , , , </u>	3	٤ ١	23	2	<b>8</b> ;	<u>د</u> :	<b>6</b>	<b>6</b>	2	19	135	69			5.5				30854	13995
1478	?	2 8	3	20.5	9 6	<u>.</u>	<b>5</b> 1	<b>5</b> (	61.	5	129	99			1.12				28554	12952
794	10.	2 4	* *	<b>.</b>	<b>9</b>	ō ¥	) F	ч с	2 6	- 6	35	9 6			21.1				32134	14449
<u> </u>	145	5	7	. g	S	<b>5</b>	n	۰ ۵	124	, 6	136	92			1.96		99	1.00		14313
10	147	92	116	99	5	9	M	~	125	• •	135	69			1.09		1.10			14086
1486	151	78	120	62	5	9	n	8	122	3	138	71			1.09		96.		32554	14766
1487	138	7	107	55	31	9	r	8	119	61	138	71			1.00		1.00		32454	14721
1488	149	11	118	19	5	9	n	7	120	62	136	70			1.09		1.10		31754	14404
1489	151	78	120	62	3	16	n	~	<b>+</b> =	29	137	70			1.10		1.10		32154	14585
1490	150	11	13	5	5	9	n	7	127	65	134	69			1.12		1,20		30554	13859
1491	156	8	125	49	ร	16	n	7	115	29	136	70			1.1		1.20		31454	14268
1492	154	73	123	3	5	9	n	η,	<b>+</b>	29	137	70			1.12		1.10		31954	14494
1493	143	<b>7</b> i	112	80 G	5	9 :	י מ	~	120	62	135	69			1.06		1.00		30954	14041
1494	*	* 1	2	<b>2</b>	5	9 :	<b>つ</b> (	7	501	9	25	20 0			69.		9		29954	18281
1495	148	9 1	112	9 ;	<u>ج</u> :	9 :	יי	<b>7</b>	107	22	134	69			= ?		1.10		30454	13814
2	13/	2	191	ဂ္ဂ	9	ū	?	7	100	ř	2	۵			.04		. 60		29454	13368

CNDG	VPAF	<b>.</b>	VE-FI	71 CK	-	WIND-VEL	Ē		VĒ.	VEOR	VPAMIN	z	VSP'A	٠.	KVPA	≩	LIFT	LIFT	¥	WEIGHT
ġ	5				PAR.	œ.	PERP.	ď.							Z Z	V .dS	10	1		
	\$	¥	3	S/M	₹	S A	₹	N/S	ž	S/M	Z X	s/x	ž	S/M					LBS	æ
-	8	n	4	ın	•	7	€0	o	6	=	12	5.	<b>±</b>	5	16	17	<b>8</b>	10	79	21
1497	149	11	120	62	29	5	m	~	119	19	133	89			1.12		1.10		29954	13587
1496	138	7	109	26	29	15	n	N	107	55	130	29			1.06		1.00		28954	13134
1499	<del>*</del>	*	115	29	29	15	n	~	116	69	131	67			1.09		1.00		29454	13360
1566	- - - -	1	121		29	5	2	~	116	99	136	70			1.10		1.10		31554	14313
1561	147	92	122		52	13	~	_	120	62	135	69			1.09		1.00		31254	14177
1502	7	*	=	99	22	<b>±</b>	7	_	117	69	135	69			1.05		1.00		31254	14177
1563	3	<b>*</b> 1	<b>9</b> :		22	<b>*</b> :	~ (	_	127	ۍ د	135	69 1			1.07		1.00		30854	13995
1 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	2 5	2 %	2 5		76	<u> </u>	7 6		5 4 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	2 4	5 F	۶ ج			7.12				31654	14358
1507	67	2 2	122	9 60		<u> </u>	, 6		3	3	<u> </u>	2 29			70.		2 - 6	1.10	28854	13988
1568	94	2	=======================================		2	<b>±</b>	· ~	_	123	3	135	69			1.04		1.00	:	38954	14041
1512	147	92	121	62	56	13	~	_	119	19	132	68			1.1		1.00		29754	13496
1514	<del>‡</del>	*	18		56	5	~	_	114	29	130	29			<b>-</b> :		1.10		28854	13088
1515	151	82	125	79	28	13	7	_	127	65	137	70			1.10		1.10		32154	14585
1516	146	2	120		92	13	7	_	120	62	136	70			1.08		1.00		31454	14268
1518	\$	2	127		27	<b>*</b>	7	-	126	65	131	67			1.17		1.10		29254	13270
1519	145	۲ ا	120		23	<b>5</b>	~	_	120	62	130	67			= :		1.10		28954	13134
1521	159	<b>2</b> 5	7		23	2 :	~	· `	123	3	133	9			1.19		1.10		30154	13678
1522	9	<b>.</b> ;	<b>:</b>		*	72	~ <		= :	57	130	2 67			96.		9 :		28754	13843
1523		5 K	- 5	2 2	• •	ž <u>t</u>	<b>4</b> 6		77 :	2 8	2 2	9 F			. 6			9	11554	14313
1528	7	? *	121		3 2	! =	, ~		9 5	6	35	8			1.06		1.00	1.18		14041
1529	55	62	5	67	22	Ξ	~	-	122	63	135	69			1.1		1.10			14041
1531	136	2	<b>+</b>	28	22	=	8	_	108	26	131	67			1.03		1.20		29454	13360
1532	147	92	125		22	=	7	_	135	69	137	70			1.07		1.10		31954	14494
1533	142	2	120	62	77	<b>=</b> :	~	-	123	8	137	9			1.04		1.10		31954	14494
25	?	<b>*</b> 1	121		77	Ξ:	~ (	··· \	2:3	80 ;	137	9 6			<b>*</b>		91.1		32154	14585
200	101	6 k	121	8 2	3 5	ž C	7 6		<u> </u>	: 2	\$ £	2 G			5				31654	14358
1537	143	2	120		23	1 2	. ~		126	65	135	69			1.06		1.10		30854	13995
1539	146	22	123		23	12	8	-	131	67	135	69			1.08		1.10		31254	14177
1540	146	23	121	 62	22	13	7	_	120	62	132	89			1.10		1.10		29854	13542
1541	143	*	118		52	13	7	_	113	28	135	69			1.06		1.10		30954	14041
1542	140	22	115	28	23	5	7	_	116	60	135	69			1.04		1.10		31154	14131
1543	145	73	120		23	2	8	_	112	<b>28</b>	133	68			1.09		- 60	1.00	29954	13587
1544	148	92	123		22	5	7	_	117	69	135	69			1.10		1.10		30954	14041
1545	7	*	138		52	13	7	_	116	99	131	29			1.09		1.10	1.10	29354	13315
1546	9	2	121		22		~	_	117	9	134	69			1.09		1.00		38454	13814
1824	149	: 3	121	79	200	<b>*</b> :	7 (		91.0	65 65	35	e :			99.		97.1		31/34	14404
C791	200	11	CZ		53	2	7	_	/7	G	20	=			1.03		.00		16776	4000

#### NADC-91124-60

#### DEPARTMENT OF THE NAVY Naval Air Development Center Warminster, PA 18974-5000

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DAY LANDINGS

USS ENTERPRISE (CVN-65)

LANDING DATA - MODEL F-18A

¥.		Š	21	14041		14041	14131	14464	14358	13995	14041	14041	13270	13632	13814	13859	13950	13995	14585	13587	12907	13224	13134	13360	13315	1000	12987	14766	•	14358	14766	14766		14041	14041	14086	14540	14404	14404	14766	14041
WEIGHT		S81	79	30954		3445	30054	31754	31654	30854	30954	30954	29254	30054	38454	30554	30754	30854	32154	29954	28454	29154	28954	29454	29354	7 3000	28454	32554		31654	32554	32554		30954	30954	31054	32054	31754	31754	32554	30954
LIFT	<u>4</u> 4		19																																						
LIFT	10		8	1.10	99.	99.		7.20	1.00	96.	1.10	1.00	1.10	1.00	1.00	1.10	- 80	1.10	1.20	96	- 90	- 00	- 90	99.	1.00	99.		1.00	1.00	1.10	1.10	1.00	1.00	1.00	1.10	96	1.00	1.10	1.10	1.20	1.00
\$	¥ .dS		11																																						
KVPA	Z		9	1.08	,	) o c	9 5	1.13	1.08	1.06	1.12	1.09	1.10	1.06	=:	1.08	1.07	90.	<del>-</del> 99	1.04	1.05	1.12	.09	9.	1.03	:	- 4	1.06		1.08	1.06	1.09		1.05	1.09	1.06	1.05	1.05	1.09	1.08	1.07
<b>«</b>		s/m	5																																						
V. dSA		ž	=																																						
VPAMIN		s/m	£	69	ç	D (	6 9	20	2	69	69	69	67	89	69	69	69	69	9	89	99	67	67	67	67	Ç	9	25		70	7	7		69	69	69	70	70	70	7	69
Š		ž	12	135		2 :	2 5	136	136	135	135	135	131	133	134	7	134	135	137	133	129	131	130	5	5		2 0	138	}	136	138	138		135	135	135	137	136	136	138	135
VEOR		N/S	=	65	29	n v	3 6	25	9	63	29	21	61	4	63	5 8	62	21	65	45	2	2	26	57	တ္တ ဗ	9 9	3 6	62	62	<b>9</b>	62	5	61	26	61	62	5	23	7	61	89
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	e.	K/S	o	-	- •				_	_	_	-	_	-	-	-	_	_		_	-	-	-	~	~	٧.		. 6	•	0	0	0		0	•	•	0	0	•	•	0
- <b>VE</b> L	PERP	3	<b>8</b> 0	~	N 6	N 6	4 6	٧	7	7	7	8	8	8	~	8	~	~	~	~	~	<b>N</b>	<b>N</b>	<b>1</b> 3	r) •	? c	4 0	. 6	•	•	•	•		•	•	0	•	•	0	•	0
WIND-VEL	PAR.	K V	^	2	2 :	<b>:</b> :	<u>:</u> :	<u>:</u>	<b>±</b>	5	2	=	<u></u>	<b>±</b>	<b>*</b>	<b>±</b>	<b>±</b>	<b>±</b>	<del>*</del>	<b>±</b>	<b>*</b>	<b>±</b> :	<b>±</b> :	<del>د</del> :	<del>ن</del> :	2 :	: :	=	=	Ξ	=	=		Ξ	=	=	<u>=</u>	=	2	2	7
	ã	₹	•	25	2 2	> 8	9 6	<b>9 9</b>	2	22	<b>5</b> 8	<b>7</b> 0	<b>5</b> 8	27	27	21	27	27	27	27	<b>79</b>	<b>8</b>	27	2	8 8	3 2	2 6	: 2	22	22	22	77		22	22	22	77	22	23	23	23
VE-F1UM		¥	so.	62	3 :	5 5	5 4	5 2	25	5	3	62	5	80	62	5	3	20	2	57	<b>2</b>	5	29	2	<b>8</b>	8	3 2	3	62	2	5	99	62	5	2	62	62	3	65	65	62
VE.		₹	*	121	77	2 :	2 :	127	120	118	125	121	119	<u>*</u>	121	13	117	=	122	=	<u> </u>	= :	113	2	23	? :	=	125	120	125	124	129	121	119	125	121	121	122	126	127	121
<b>I</b> 5	_	M/S	n	27	2 :	C #	2 6	2 2	2	*	28	92	2	2	76	2	*	2	1	7	9	<del>ا</del> کا	2	2	2;	2	2 %	2	2	76	22	92		2	76	7.	*	*	1	11	7
VPAF	2	ž	8	146	*	?	9	55.5	1	143	151	147	145	Ξ	- - - -	145	<u> </u>	142	<b>5</b>	138	136	146	142	145	75		? ;	14	142	147	146	151		=	147	3	14.	=	149	50	<del>*</del>
ON	ġ		-	1826	182/	9791	6701	1831	1832	1833	1834	1836	1837	1838	1839	1840	1842	1843	1844	1845	1846	1847	1855	1854	1855	/091	186	2111	2112	2113	2114	2115	2116	2118	2119	2121	2122	2123	2124	2125	2126

#### NADC-91124-60

#### DEPARTMENT OF THE NAVY Naval Air Development Center Warminster, PA 18974-5000

13410 Code 6042 10 Jun 87

990	VPAF	بي	VE-	VE-FILM		WIND-VEL	VEL		3	VEOR	VPAMIN	Z	ASP.A	٠.	KVPA	≩	LIFT	LIFT	¥E	WEIGHT
€.	5				â	PAR.	PERP.	ď.							Z	V .dS	5	<b>1</b>		
	\$	X/S	₹	Ş	₹	X X	₹	R/S	Š	K/S	₹	S/M	Z	N/S					LBS	Š
-	7	n	•	•	•	^	€	o	6	=	12	5	<b>±</b>	5	16	17	8	19	70	21
2127	55	7	115	28	23	12	•	•	121	62	134	69			1.03		1.00		30554	13859
2128	144	7.	121	62	23	12	•	•	115	29	135	69			1.06		1.10		31254	14177
2129	4	76	125	Z	23	12	•	•	117	69	135	69			1.09		1.00		31154	14131
2130	149	11	126	8	23	72	•	•	125	5	137	92			1.09		1.99		31954	14494
2131	146	75	123	3	23	12	•	•	121	62	136	92			1.07		1.10		31754	14404
2133	145	2	122	3	2	12	•	•	122	63	131	29			1.1		1.10		29354	13315
2134	- - -	76	125	Z	23	12	•	•	137	70	132	89			1.12		1.10		29754	13496
2135	149	77	126	65	23	12	•	•	118	61	135	69			1.10		1.10		31254	14177
2136	142	23	119	2	23	5	•	•	121	62	133	89			1.07		1.10		30254	13723
2137	149	11	126	8	23	12	•	0	121	62	136	70			1.10		1.20		31454	14268
2139	146	75	123	3	23	12	•	•	120	62	132	89			1.1		1 20		29554	13406
2140	146	75	123	63	23	12	•	•	124	\$	136	70			1.07		1.00		31654	14358
2142	141	73	10	5	23	12	•	•	Ξ	57	134	69			1.06		1.00		30554	13859
2143	- 1 1 1	75	123	3	23	12	•	•	134	69	137	92			1.06		1.20		32154	14585
2144	140	72	117	8	23	12	•	•	120	62	136	70			1.03		96		31654	14358
2145	<del>-</del> 2	75	123	3	23	12	•	•	116	99	136	70			1.08		96		31354	14222
2146	148	26	125	79	23	12	•	•	119	19	139	72			1.06		1.00		32954	14948
2147	140	72	117	3	23	12	•	•	109	26	134	69			1.05		96.		30454	13814
2148	139	72	116	8	23	12	•	•	115	29	135	69			1.02		1.10		31254	14177
2150	146	75	123	3	23	12	•	•			137	70			1.06		1.10		31954	14494
2151	<u>‡</u>	*	120	62	<b>5</b>	12	7	_	126	65	133	89			1.08		1.28		30354	13769
2152	142	23	118	63	<b>54</b>	12	7	-	124	<b>6</b>	134	69			1.05		1.00	96	30754	13950
2153	151	28	127	8	7	12	8	_	121	62	138	7			1.09		1.20		32254	14630
2154	Ξ	22	117	2	74	12	7	-	121	62	137	92			1.03		1,20		31954	14494
2155	===	2	117	3	7	12	N	-	116	99	133	88			1.06		88.		30354	13769
2157	149	1	125	Z	<b>5¢</b>	12	7	_	109	26	134	69			=:		1.00		30554	13859
2158	151	78	127	3	<b>5</b> 4	12	7	-			138	71			1.10		1.10		32354	14676
2159	143	7	119	5	24	12	8	-	118	61	137	70			1.05		1.00		31954	14494
2161	147	78	123	3	<b>5</b>	12	~	_	119	61	133	89			1.10		1.10		30154	13678
2162	140	72	116	2	<b>5</b>	12	8	_	115	28	137	70			1.02		1.10		31954	14494
2163	140	72	116	8	<b>5</b> 4	12	7	-	Ξ	57	136	70			1.03		1.10		31454	14268

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DAY LANDINGS

USS ENTERPRISE (CVN-65)

13410 Code 6042 THEIGHT RAMP F . . น่อง - น่ 4 น่ 6 น่ 4 น่ 4 น่ 4 น่ 4 น 4 น่ 6 4 น่ 6 4 น 6 4 น่ 4 4 . น่ อ อ - น่ 4 น่ ธ น่ ม่ ม - อ น่ ม น 4 - ธ - ธ - ธ อ ธ > น อ ม WHEEL HEIGHT RAMP OVER 16.9 16.2 16.2 19.9 19.6 15.4 15.4 15.1 16.3 37 9 \$ 36 GLIDE PATH ANGLE AT Ã 33 . 073 . 055 ş 955 954 957 966 965 967 941 941 ħ 盖图 N/S FREE-FLIGHT 32 F/S 10.1 n 8 TOUCHDOWN ¥ AIRCRAFT SINKING SPEED AT Z S 28 STBO 27 Š 2 S \$ HOSE 5 23 8 ð

OVER RAMP	40		• •		., .																																
3	91																																				
OVER RAMP	7	•	, ,				- 80004									= = = = = = = = = = = = = = = = = =																					
Bw RAD	31	00	. 946. 1	96. 946. 1	. 046 . 046 . 1 859	6. 6. 6. 6. 6. 6. 6. 6. 6. 6. 6. 6. 6. 6	0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	6.00	6. 6. 6. 6. 6. 6. 6. 6. 6. 6. 6. 6. 6. 6	6. 6. 6. 6. 6. 6. 6. 6. 6. 6. 6. 6. 6. 6	6. 6. 6. 6. 6. 6. 6. 6. 6. 6. 6. 6. 6. 6	6. 6. 6. 6. 6. 6. 6. 6. 6. 6. 6. 6. 6. 6	6. 6. 6. 6. 6. 6. 6. 6. 6. 6. 6. 6. 6. 6	6. 6. 6. 6. 6. 6. 6. 6. 6. 6. 6. 6. 6. 6	0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0	9. 9. 9. 9. 9. 9. 9. 9. 9. 9. 9. 9. 9. 9	6. 6. 6. 6. 6. 6. 6. 6. 6. 6. 6. 6. 6. 6	946 946 948 948 955 955 956 958 943 943 956 958 958 958 958 958 958 958 958 958	946 946 948 948 956 956 956 958 943 943 959 959 959 959 959 959	946 946 948 948 955 955 956 958 943 943 956 959 959 959 959	946 946 948 948 955 956 956 958 943 943 956 959 959 959 959 959	946 946 948 955 955 955 955 955 955 956 957 958 959 959 959 959 959 959 959 959 959	946 946 948 948 955 955 955 955 955 955 955 95	946 946 948 948 955 955 955 955 957 970 970 970 970 970 970 970 97	9. 9. 9. 9. 9. 9. 9. 9. 9. 9. 9. 9. 9. 9	9. 9. 9. 9. 9. 9. 9. 9. 9. 9. 9. 9. 9. 9	9. 9. 9. 9. 9. 9. 9. 9. 9. 9. 9. 9. 9. 9	9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0	946 946 948 948 955 956 958 958 958 958 958 958 958 958	946 946 948 955 955 955 955 955 955 955 95	946 946 948 955 955 955 955 955 955 955 95	946 946 948 948 955 955 955 957 958 958 958 958 959 959 959 959	946 946 946 948 956 956 956 956 956 957 958 958 959 959 959 959 959 959	946 946 946 948 956 956 956 956 956 957 958 958 959 959 959 959 959 959	946 946 946 948 956 956 956 957 958 958 958 958 959 958 958 958	946 946 946 948 956 956 957 958 958 958 958 958 958 958 958
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1/S F/S 1	į	5	5	- - -	- 10 10	- n n n	- - -		5	5	5	5	5	5	5	5	5	5	5	5	5	5	5	<b>5</b>	5	5	; <del>-</del>	; ;	; ;	; ; ;	; ;	5 7.	; ;	; ;	; ; ;	5 7 2	5 7 7
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DAY LANDINGS

### DEPARTMENT OF THE NAVY Naval Air Development Center Warminster, PA 18974-5000

990			AIRCR	AIRCRAFT SIN		PEED A	KING SPEED AT TOUCHDOWN	N			GLIDE	GLIDE PATH ANGLE AT TD	NGLE /	7 0	WHEEL	MHEEL HEIGHT	HOOK HEIGHT	EIGHT	
2	NOSE	ŭ	PORT	41	ST	STBO	AVG	co.	FREE-FLIGHT	LIGHT	B-F	ž	BV	>	OVER RAMP	RAMP	OVER RAMP	SAMP.	
	5	¥	<b>5</b> /2	M/S	5/3	K K	F/S	M/S	F/S	N/S	DEG	RAD	DEC	RAD	14	3	E	3	
22	23	24	22	<b>36</b>	27	<b>58</b>	29	30	31	32	33	<b>4</b> 6	35	36	37	88	39	9	
1497	7.6	2.3	9.	7.4	7.8	4.4	7.9	4.2			2.4	.041	1.7	.030	16.3	5.0	13.5	4.1	
1498	7.9	2.4	æ. œ.	3.0	10.1	y. 1	6.6	3.0			3.0	. 053	2.9	. 050	15.9	<b>4</b> .	12.3	ъ.	
1499	8.5	5.6	10.2	3.1	9.7	<b>9</b> .	10.0	3.1			2.8	.049	2.5	.043	18.6	5.7	15.4	4.7	
500	10.3	J. 1	10.5	3.5	<b>†</b> :	3.5	- - -	3.3			J. 1	.054	2.7	.047	<del>+</del> .+	<b>4</b> .	10.9	J. J.	
1501	<b>9</b>	<b>5.8</b>	8.5	2.5	10.0		. o	. 38 . 38			2.8	.049	2.5	. 039	13.6	<del>-</del> 1	5.0	ر ا د.	
1502	12.2	3.7	12.4	ا ا	13.5	<del>-</del> -	13.0	4			3.0	. 053	n (	. 058	21.9	6.7	9.9	κ. Θ.	
2867		<b>.</b>	10.5 •	3.5	<b>-</b> •	ان دن	<u>-</u> 6	n 6			2.9	. 051 050	2.9	1651	16.7	. · ·	4.6	- r	
1585	11.1	- M	14.3	. 4	0.4	9 4	. <del>1</del>	. 4			, K	.061	3.6	.063	17.4	7 P.	14.2	, 4 , 5	
1507	6	2.9	11.2	4.6	10.9	3		4.0	10.9	J.	) ;		3.2	.055		) ;	!	2	
1508	10.9	3.3	10.3	ر ا	12.6	8.5	2.5	3.5			3.1	.055	3.2	.057	16.9	5.2	13.6	<b>+</b>	
1512	10.1	J. 7	9.6	5.9	10.4	3.2	10.0	3.0			5.6	.046	2.5	.044	14.0	4.3	11.1	4.6	
1514	9.0	5.6	6.6	3.0	6.6	3.0	6.6	3.0			3.1	.053	5.6	.046	15.0	<b>4</b> .6	12.0	3.7	
1515	9.8	J. 0	11.2	4.5	10.8	3.3	11.0	4.6			2.9	.051	2.5	.044	16.6	5.1	13.4	<b>-</b> .	
1516	10.2	J. 1	9:	3.5	13.1	<b>4</b> .	12.4	3.B			3.4	. 059	3.3	. 057	15.6	4.8	12.1	3.7	
1518	10.2	n.	= :	n :	<b>.</b> .	2.5	Ø.	J. 0			2.9	.050	4.4	140	9.9		1 <del>6</del> .1	<b>4</b> (	
1519	-	2.8	1.2	4.6	<b>19</b>	J	10.7	ы. Б.			J. J.	.058	2.5	.044	5.0	<b>9</b> .4	۲۰,	က စ	
1521	-:	4	12.2	7.7	<b>9</b> .8	J. J.	1.5	3.5			2.7	.048		.040	48.4	9. O	15.6	<b>4</b> .	
1522	2.5	4. (	13.1	<b>4</b> .	13.2	4.0	13.1	4 ·			3.7	.064	٠ ٠	. 661	5.5	o .	4.6	- r	
1525	9.4	9 4	 	. •	5. 4 5. 6		5 Y	S. 4	46.0	•	۵. ۲. ۲	. 652 972		700.	. e.	7 F	7.7.	, «	
1528	4. =	9 10	13.5	· •	11.7	, b	12.6	, 10 10	12.6	, E	- 10	.961	3.2	.056	17.5	, i,	13.8	4.2	
1529	9.6	2.9	10.7	J. J.	4.0	2.9	- 0	3.1		)	3.5	.055	7.4	.042	14.6	4.5	11.6	3.5	
1531	7.1	2.2	1.1	3.4	10.6	3.2	10.8	3.3			3.4	. 059	5.6	.046	15.1	4.6	<b>1</b> .4	3.5	
1532	12.2	3.7	12.2	3.7	11.3	4.6	1.8	3.6			2.9	. 050	2.8	.049	19.7	6.9	16.9	5.1	
1533	10.2	1.5	11.5	3.5	1.8 1.8	3.6	11.7	3.6			3.0	.052	۵. و	.052	19.3	හ. ග	16.4	လ စ (	
20.	12.8	ص د د	B. 5	<b>9</b> (	14.5	<b>+</b> •	 	4.2			- ·	2/9.	9 .	790.	20.3	7.9	7.7.	7.6	
15.00		9 K		 		) H	- o	- M			- e	946	, ,	240	5.0	. 4	12.6	9 60	
1537	10.4	2.5	13.1	4	12.2	3.7	12.9	9			. E.	.061	3.2	.057	19.3	6.0	15.9	4	
1539	6.6	9.0	1.4	3.5	11.2	4.6	11.3	3.5			3.1	.055	5.6	.046	15.6	4.8	12.5	3.8	
1540	æ.	2.6	9.5	2.8	<b>6</b>	2.7	9.1	2.8			2.8	.049	<b>5. 4</b>	. 043	14.7	4.5	11.5	3.5	
1541	13.8	4.2	13.1	4.0	13.8	4.2	13.5	<del>-</del> -			3.3	. 057	3.3	.057	20.4	6.2	17.1		
1542	12.0	3.7	12.3	3.7	<b>+</b> .=	3.5	11.9	3.6			5.6	. 946	5.8	.048	21.2	6.5	18.0		Co
1543	12.4	3.8	13.3	÷.	12.3	3.8	12.8	3.9	12.8	3.9	2.8	. 656	2.9	.051	21.6	9.9	18.7		ode
1544	<b>1.6</b>	ы Б	12.1	3.7	₩. 1.9	ъ. Ф.	12.0	3.6			4.6	. 629		.054	6.9	5.2	13.5	- ·	2 U
1545	10.7	S. S.	11.3	4.6	12.0	9.0 1	9 =	S.5	11.5	3.5	4.5	.059	ا ا -	.055	16.3	 6	13.0	<b>4</b> .	60
1546	10.7	3.5	1.5	ις (	12.1	3.7	1.8 6.4	a.6			2.9	.051	2.7	.047	17.0	2.5	9.4.	4 t	)42
1824	9.5	2.0	n.	2.8	ю ;	B. 0	9.6	2.9			2.9	959.	5.5	.040	0.0	<b>4</b> 4	12.3	٠.٠ ١	<u>}</u>
623		ر م	13.6	-	15.0	<b>4</b> .	<b>+</b> .0	<b>-</b>			3.2	900	3.5	909.	70.	7.0	0.0	· •	

13410 Code 6042 HOOK HEIGHT RAMP OVER  $\begin{array}{c} \text{$C_{1}, C_{2}, C_{3}, C_{4}, C_{5},  L WHEEL HEIGHT RAMP OVER 2 8 36 GLIDE PATH ANGLE AT 35 ₹ S 0575 BF≸ DEG 33 X/S FREE-FLIGHT 32 5 AIRCRAFT SINKING SPEED AT TOUCHDOWN ¥ 29 X/S 28 STBO 27 ¥\$ 26 <u>8</u>  $\begin{array}{c} 7.24 & -0.01 & 0$ 25 Ş 7 MOSE Ş 23 3 3

13410 Code 6042

BHW BVV DEG RAD DEG RAD
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DAT LANDINGS

USS ENIERTHISE (CVR-03)

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*	AT T0	RAD	19	021	. 003	0.000	679	.007	.131	. 642	003	. 105	660	106	600	012	. 007	082	017	. 103	007	916	012	012	065	007	600	024	.012	.031	010	.017	031	.007	.017	960.	. 038	019	010	045	9.666	.016	.059
YAW	AT	DEG	69	-1.2	7.	<b>9</b> .0	4.5	₹.	7.5	2.4	2	6.9	5.7	-6.1	'n	7	₹.	-4.7	-1.0	5.9	4.	<del>ە</del> .	7	<b>-</b> .7	-3.7	<b>†</b>	'n	<b>₹</b> . [	۲.	<b>.</b>	9.	9.	<del>1</del> 89.	₹.	-00.	5.5	2.5		9.	-2.6	0.0	œ.	4.6
į.	5	8	29	.044	052	035	035	045	056	070	075	042	054	014	072	065	966	030	040	679	063	063	056	086	010	654	965	038	059	079	051	086	. 045	963	075	091	. 077	. 059	. 677	038	005	.007	. 031
r. 9.	AT TD	DEG	28	-2.5 -	-3.6 -		-2.0 -	-2.6 -	~				-					۲.	-2.3 -	1.5	-3.6 -		-3.2 -		9		_	7			-2.9		-2.6 -		1.3	-5.2 -	-4.4	- 4.5-	+			4.1	1.8
RATE	2	RAD O	22	- 196.														.038 -1		- 649																						. 253	.042 -
ROLL RATE	AT	DEC	26	3.5	1.5.1		-5.2 -	7.3	٦.	.5.	7.7		ch.				1	2.2	<b>8</b> 0.	2.8	1					60	<b>-</b> '						_	_						5.4	-:	14.5	-2.4 -
RATE	2	SA O	55					005	600.	619							.038									094	7				.044	7			.024 -		ŧ						•
PITCH RATE	¥	DEG	45		ı			1.3	٠.											2.2		1.88			-2.2 -			∞.					J. 7	₹.	<b>+</b> .			r.		ø.	z.	8.	₹.
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N G L		RAD	51	.056	054	002	030	. 010	. 037	. 030	.010	. 033	.017		.058	.010	. 005	. 059	. 108	.054	624	.019	061	. 024	. 119	007	023	. 030	019	119	. 021	037	002	026	679	129	.016	.031	. 021	916	- 110	.084	410
۲ ۸	8	DEG	20	3.2		- - -		9.	2.1	1		ø.	6.		-3.3 -	9.	٦.	+	~	3.1	Ţ		-3.5 -		_									1.5	_		•		.2	<u>ه</u> .	+	80	80
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υ Ζ <		2	<b>5</b>	200	960	163 5	691		101	110	969	106	186		959	965	687	891	573	696	36.3	372	987	93	860	926	979	987	987	304	398	687	952	986	679	689	677	952	169	687	386 5	989	7.76
I U	8	DEG	;		į.	•	•	•	•	•	•	•	6.2		•	•	5.0	•	4.2	•	3.6	•	•	•	5.6	•	. 8.4	•	•	•	•	•	•	•	•	5.1	•	•	•	5.9	•	•	•
F 1 d		RAG G		966 5	694 5																				689 5.												4 660	•			-	_	984 4
	5	DEG	42	3.8	•	5.2 .(	5.5	8.0	1. 6.1	5.5	2.9	5.6		•	•	•	•	•	•	•	•	•	•	•	•	4.5	•	4.3	•	5.9	•	5.8	•	•	•	•	•	•	•	4.5	•	•	•
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	DEG	SA O	DEG	RAD	DEG	RAD	DEG	RAD	DEG	RAD	DEC	RAD	DEG	RAD	DEG	RAD	DEG	S.	DEG	RAD
<b>∓</b>	42	3	‡	\$\$	46	41	8	64	20	51	52	53	54	55	26	57	28	59	99	19
1448	3.6	. 963	6.5	.113		ı	1.3	023	+:	007			æ	.014 8	+	.147 -3	1.1	. 954	5.8	101
1450	3.6	. 963	5.1	. 689				. 028	4.5	.079		1	9:		5.0			035	4.7	. 082
1452	<b>6</b> .	. 086	4.3	.075		ı	9.1	028		133		J	0.0					026	2.9	.051
1453	<b>†</b> .	.677	6.3	110		,		012		009		-	9.				_	990'-	<b>4</b> .9	.112
1454	<b>4</b> .6	.080	4.7	. 082						.087			ĸ.	•				047	6.5	.113
1455	- ·	.072	5.2	. 091		-	<b>60</b>		_	037		J	Θ.					963	6.7	.117
1456	5.7	660.	٠ . م	800.			4.7	. 129		992		<b>©</b> г	ø. •				-3.6	963	•	.065
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1462	4.5	. 694	5.5	960.			-:	.019	4.0	. 676		3	0	0.000-20.3			2	091	8.6	. 150
1463	6.9	. 105	5.9	. 103		-	4.0			136			-					051	7.5	131
1464	8.9	. 103	_	.117		-	3.8			.051					•			047	<b>6</b> .4	.112
1466	3.2	.056	2.7	680			2.1			035		<b>.</b> 4	<b>.</b>					056	4.9	.112
1467	٠. و	.052	9 1	. 989				410	6.2	.168		w.	0 0 0	ı				012	æ.	416
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1472	o 1	.087	<b>.</b>	.059		1				038		7 '			· ·			049	2.7	.17
24.		221.	- 1	99.		1	• • · ·	7,042	7.0	991.		-, <b>•</b>		C00.	٠ • د			+ 10 + 10	? ·	80.
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1478	4.7	.082 -		024			<b>+</b> :			021							-3.0		4.	720.
1482	3.7	.065	_	.065		•				. 636									-1.3	023
1483	5.2	. 691		. 101		•				019		_		. 021	<b>*</b>			072	9.	.017
1484	5.7	. 689	5.5		S. S	.103 -	-	654	5.8		-3.3	058 1	-	. 619	· •			054	3.6	. 963
1485	5.0	. 987	4.7	. 082		1		024	. 5.	009		-			9			045	6.	016
1486	3.3	.058		. 989		1		019	2.5	.044		•		016 6	တ		-4.7 -	082	2.5	.044
1487	<b>+</b> : <b>+</b>	.077		.070		<b>=</b>	10.5	. 183	5.6	. 698		•		Ţ	5.3	267 -2	۲.	047	2.5	.044
<del>1</del> 488	 -	. 689	_	. 092		-				.045		•			_	007		075	6.3	.110
1489	4.5	. 079		.077		•				017		۳)		.066 -3.6	_			070		. 699
1490	5. B.	191	5.7	. 099		ı				051		•			6		-3.7	. 065		014
1491	5.8 B	161	က တ ၊	869		ľ	6	044	3.2	.056		(A			14.3		ا ھ	. 049	r.	023
1492	<b>4</b> .4	. 975	3.7	. 965			<b>+</b> !	. 024	8	.017			_		3.7	.065 -3	٠,	926	•	.031
1493	<b>4</b> .4	. 677	<b>4</b> .4	.075		, ,	2.7	.047	- 6.7	051		•			4.2	673 -4		086	3.6	. 963
1494	4.0	<b>460</b>		889		ľ		040	7	. 003		1 '			· .	4- 660	ا ا	.075	vi (	600
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1496	S.	191	5.6 0.6	. 098		-	ا. س	005 -	-2.7	047		•	ا. ا	005	۲.	.0124	1.5	. 073	9.1	010

13410 Code 6042

PITCH ANGLE ROLL ANGLE OR FF TO OR FF	ANGLE ROLL ANGLE FF TD OR	E ROLL ANGLE FF TD OR	ROLL ANGLE	ROLL ANGLE	N G L E	n E	je.		PITCH RATE AT TD		ROLL RATE AT TD	•	7. P. A.	YAW AT TD	<b>*</b> •
RAD DEG RAD DEG RAD DEG RAD DEG RAD [	RAD DEG RAD DEG RAD DEG RAD	RAD DEG RAD DEG RAD	DEG RAD DEG RAD	RAD DEG RAD	RAD		DEG	RAD	DEG	RAD	DEG	RAD DI	DEG RAD	DEG	RAD
43 44 45 46 47 48 49 50 51 52	46 47 48 49 50 51	6 47 48 49 50 51	49 50 51	50 51	51			53	\$	55	26	57 58	29	99	19
-1.2	3.1 .054 -1.2	-1.2	-1.2	-1.2	۲.	τ:						99 -4.0	070	1.7	. 030
6.2 .108 .4 .007 -2.4 -	.4 .007 -2.4 -	-2.4 -	-2.4 -	-2.4 -	۱ پ	12			_	1		031 -3.9	068	7.0	. 035
2.4 .042 1.1	2.4 .042 1.1	<u>-</u>	<u>-</u>	<u>-</u>		6			<del>-</del>		'n	.063 -2.3	040	9.9	.115
5.9 .103 .2.6 -	.2 .003 -2.6	. 903 -2.6	. 903 -2.6	-2.6	i	Ω.				.031 -5.			061	<u>-</u>	919
5.4 .894 2.5 .644 1.4	2.5 .044 1.4	.044 1.4	.044 1.4	<del>+</del> (	1.4 .024	*:				002-10.3		180 -3.9	068	2.8	.049
6.7 .60.0 - 1.6628 2.9	-1.6028 2.9	628 2.9	628 2.9	5. Y		<u>.</u>			- - 1		• .	112 -3.3	- 858 818		989.
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4.4 .077 -1.2021 5.8	-1.2021 5.8	021 5.8	021 5.8	5.8		=					8.	.014 -3.9	068	9.	.017
5.1 .689 .4 .667	5.1 .089 .4 .007	. 4 . 007	. 4 . 007	•	•	-		. 669		_		.030 -4.2	073	€.	.014
5.3 .692 .8 .014 -2.1	.8 .014 -2.1	-2.1	-2.1	-2.1	_	22			<b>+</b> .	.024-12.7		222 -4.1	072	.3	. 023
	4 2002	<b>4</b> ·	<b>4</b> ·	<b>4</b> ·	<b>*</b> .	76			5.6	.945 -4.	ы. П		065	9.0	.052
4.3 .0751	1.3 8851	3 6651	3 6651	- i	1002	32			9.	. 028	_	.002 -2.6	045	-2.0	035
5.2 .891 8.9 0.8897 -	0.0 0.0007	0.0007	0.0007	7		2 9			œ.				073	2.1	.037
5.6 .698 -1.3623 5.6 .	-1.3 623 5.6	023 5.6	023 5.6	ۍ د و		<b>8</b> 9			~ 6				044	7.	003
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5.0 150. 7.1 5.00 8.5 5.00 8.5 5.1 5.1 5.10 5.10 5.10 5.10 5.10 5.10	2.7 619 3	cto 7	cto 7	) P	100.	. <u>.</u>			; -		'		956		923
6.3 .1166019 -1.5 -	- 6 - 910 - 1.5 -	1.5	1.5	1.5	1.5026	9.			3.2				049	?	. 663
3.3 .658 5.7 .699 1.6 .617 7.2	5.7 .099 1.0 .017 7.2 .126	7 .099 1.0 .017 7.2 .126	1.9 .017 7.2 .126	7.2 .126	. 126								033	-1.5	026
6.0 .105 5.6 .098 2.1 .037 2.3 .040	5.6 .098 2.1 .037 2.3 .040	6 .098 2.1 .037 2.3 .040	2.1 .037 2.3 .040	2.3 .040	.040			. 954		038 9.6		.168 -2.6	045	თ.	.016
4.1 .072012 8.6	7. 012 8.6	9.6	9.6	9.6		99							033	-2.3	040
6.3 .110 3.9 .052 2.8	3.0 .052 2.8	2.8	2.8	2.8		<u> </u>				012 2.0			056	2.5	.044
.051 3.9 .0687012 2.6 .045	7012 2.6	012 2.6	012 2.6	2.6		ស៊ីខ			60.0	6.999 5.	<b>+</b> 0	.094 -3.5	061	κ. 4. α	400.
3 C 010 0 C 530 0 F	3. L 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.				0.0.1 1.1 1.1.1	2 -				7.02 1.30.		145 3 6	20.		
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4.1 .0723005 1.8	1.3 1.665 1.8	665 1.8	665 1.8	8,		-			1.2	1	'		066	1.2	. 621
5.2 .091 -2.7047 -4.3 -	-2.7 047 -4.3	047 -4.3	047 -4.3	7		້ຄ				_			056		019
4.6 .080 -8.9155 5.0	-8.9155 5.0	155 5.0	155 5.0	5.0		17			60	_	.2	.021 -1.8	031	<b>†</b> .	677
-2.7047 3.9	-2.7047 3.9	047 3.9	047 3.9	3.9		88				_	•	017 -1.1	019	1.9	. 033
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. +00 0.4- C00. C. 7/0. I.+ 0/0. 0.4	. +00:= 0.4= C00. C. 7/0. I.4	. +00 0.4- 000. C. 7/0. I	. +09 0.4- 000.			•		919.		999.		į	000.		
5.4 .694	1882 1.4 .824	1662 1.4 .624	1882 1.4 .824	1.4 024	•50		1		7.7	- '		1.6- /10.	1.08y	÷.	
4.8 .084 5.1 .089 2.0 .035 -1.2	5.1 .089 2.0 .035 -1.2021 1	1 .089 2.0 .035 -1.2021 1	2.0 .035 -1.2021 1	-1.2021 1	021	<del></del>	_	. 030	۲.	.012 -3.7		065 -2.9	051	n.	
4.5 .079 .8 .014 -2.9 -	.8 .014 -2.9 -	- 014 -2.9 -	- 014 -2.9 -	1 -2.9 -	ı	ñ			+. i	_	~	056 -4.0	070		\$20.
5.6 .098	1.2 .021 1.3	.021 1.3	.021 1.3	1.3	1.3 .023	ŭ			5.0	.035 -2.9	_	051 -3.0	052	6. I	016
061 2.4	-3.5061 2.4	061 2.4	061 2.4	1 2.4	2.4 .042	2			8.	-	m	.049 -3.3	058	-2.4	042

ENTERPRISE (CVN-65)

#### NADC-91124-60

### DEPARTMENT OF THE NAVY Naval Air Development Center Warminster, PA 18974-5000

SS

DAY LANDINGS

USS ENTERPRISE (CVN-65)

LANDING DATA - MODEL F-18A

10	RAD	19	072	012	98.0	9.00	600	1.003	909.	131	007	.024	.054	044	003	016	. 691	056	.044	007	. 033	. 105	. 969	1.65	+ 5 0 1	106	. 073	028	066	014	005	. 007	007	009	017	992	. 009	. 056	.028	ACA
¥	DEC	99	7	- 7		, P		, ,			+	<b>+</b> :-	3.1	-2.5		6. I			2.5	<b>+</b> :	6,	e.9		-7. 6. 0	. <del>-</del>		4.2		-3.8	۰ 1	٦.	₹.	+.1	n,	-1.0	ï	ĸ.	3.2	9.	9
5	RAD O	23	635	063					- 210 - 200	1.003	068				676					679	040				240. I	051	075	954 -		045	061	054	963		•	061	047	073	335	674
AT T	DEG	28	6) (1)	ص								i •				'n	6	ن. ا						۔ بع				· -		i ★.	'n	-	9		-	S.	7	7		•
_	RAD	57	.651 -2	7	1				200				1	082 -3.0	.038 -4.0	7	ဂ	7					? '	134 2	ĭ		1	.037 -3	.016 -2.7	7	.010 -3	7	3	7	7	7	7	7		
AT TD	DEG			•					000.	1		ı		•				ŀ				ı			ı					7117					ł			•	61	•
	RAD	26			6 -5-0				7 4 7 4 8 6		9 3.2				7	4		7	2 1.7	031 -1.5	6-12.	6-6	= '	7./	7	4	8			•			~	•	7	7	_	-10	7	*
AT TD	DEG R	55	030	.044	900	9.6	9	9.0	9.0	10.13	.019	007	012	010	028	019	031	. 028	. 042	031	<u>.</u>	0.000	028	. 623	1 60	082	.019	0.000	0.000	.047	.009	026	.014	0.000	003	096	.019	.003-	.016	
		\$	-1.7	2.5	9	) 1	. 4	,	. ·		-	<b>♥</b> .	7	9.	1.6		<u>.</u> 8	7.6	2.4	1.8	€.1	0	9 1			1.4	-	0.0	0.0	2.7	ĸ.	1.5	€.	0.0	2	-5.5	-:	7.	<u>ه</u> .	,
<b>1</b> 1	RAD.	53																																						
<b>L</b>	DEG	25																																						
	RAD	51	.056	005	106		979	240	500.	926	.042	007	.044	002	009	.054	059	.052	. 059	. 063	.157	030	.031	919	928	.024	026	122	.016	. 033	092	012	. 040	.012	.044	038	003	024	. 002	-
8	DEG	20	5.2	ان ا	-			? <b>"</b>		!	2.4		'n			3.1								ە بە	, K	· •	1.5	0		6.	-5.3		'n		'n	~	2 -	<b>+</b> :	<del>-</del> .	
	RAD	49	037 -	045 -						ı				. 030	637 -	040	.101 -3	954						. 500.	2 500 -			026 -7	005	. 885			017 2			1		<b>0</b> 52 –1	003	
5	930	48	i	9	•				•	•			'		•			1				0		. ·							_	_		i +		i G	i 1		~	,
	<b>8</b>		-2	-2	i	· ;	; c	i		? -	-1.0	4.2	7	1.7	-2.1	-2.3	'n	7.	<del>-</del>	6	<b>-</b> :	9.0	2.	•	· -	•	5.1	-1.5	i	•	9.9	7	7	i	6	<del>-</del> 5	7	m m	i	
<u> </u>	930	4																																						
	SAD D	4		_									_			_	_		_	_								_	_			_			_		_			
8		\$	. 965	101	975	. 68	3	700.		000	560	. 691	. 089	. 075	. 673	. 689	. 686	. 687	960.	.077	. 677	. 69	89	689.		. 60	. 692		. 698	. 692	. 69		. 67	. 687	660	960	. 659	.075	. 687	
	DEG	\$	3.7	5.8	7		, ,			) P?	5.7	5.2	5.1	4.0	4.2	5.1	<b>4</b> .0	5.0	5.6	<b>†</b> .	<b>+</b> .	. G	•			5.5	5.3	4.8	5.6	5.3	5.2	4.9	4.2	5.0	5.7	5.5	4.4	4.3	5.0	•
6	SA O	\$	. 682	.070	484	6	9		//0.	. 600	990	. 989	.098	. 989	. 854	. 098	. 965	. 092	660.	. 063	. 056	.079	. 689	989.	260.	660	.072	. 073	. 682	. 103	. 896	. 886	. 058	. 687	. 694	.047	. 070	960.	. 086	•
5	DEG	42	4.7	4	4				• •	. 4	3	5.1	5.6	4.6	3.1	5.6	3.7	5.3	5.7	3.6	3.2	4 · 5		- ·		5.7	7	4.2	4.7	9. 9.	5.5	4.9	3.3	5.0	4.5	7.7	<b>4</b> .0	5.5	9.4	•
		_	826	_		. a		<b>.</b>		833	. 🕶	20	_	50	•	1840	~	<b>~</b>	•	<b>.</b>	<b>.</b>	1847	1853	1854		1859	_	_	2112	<b>m</b>	_		2116		_	2121	2122	2123	2124	-

13410 Code 6042

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YAW	AT TD	RAD	19	.010	037	026	079	. 033	054	. 038	. 021	051	002	005	. 068	010	. 012	. 086	019	017	. 082	134	010	.012	. 961	028	.040	.087	.119	. 072	.127	. 164	. 049	. 138	
<b>&gt;</b>	AT	DEG	99	9.	-2.1	1.5	-4.5	9.	-3. 1	2.5	1.2	-2.9	<del>-</del>	1	ر 13.9	9.	۲.	<b>6</b> .4	- T	1.0 0.1	4.7	7.7	9.	۲.	3.5	-1.6	2.3	5.0	<b>6</b> .8	<del>-</del> -	7.3	4.6	2.8	7.9	
F. P. A.	4	Z.	29	044	047	063	023	968	044	960'-	990'-	031	054	649	030	047	033	045	058	045	035	965	030	056	017	042	. 002	687	052	042	966	054	0.000	066	
ŗ.	AT TD	DEG	28	-2.5	-2.7	-3.6	•					•	•										-1.7	-3.5	-1.0	-2.4 -			_	٠	-3.8		9.9	-3.8	
RATE	5	RAD	22		. 828 -				- 080 -					- 990'-													059	- 191 -	- 989 -	. 652 -	858 -	•	894	- 924 -	
ROLL RATE	4	DEG	26	6.1	9.1	6.9															<b>4</b> .4			-5.0 -		_		1.3	-4.6	3.0	٠	6.8	5.4	<b>+</b> :-	
RATE	10	RAD	52	.049	. 038	.035								. 038 -	•							019	.061	- 990.	005			070 1	0.000-	035	- 905 -	005	- 210.	600	
PITCH RATE	7	DEG	54	2.8	2.2	2.0	2.7	1.6			<b>.</b>		σ.		-2.2 -								3.5	3.8	1.3	<del>-</del> .	8.1	6.4	9.9	-2.0 -	L.G.	- 2.	۲.	٠.	
		RAD	53									,			•			1		1	•	1			035		•	•		,					
ш	i.	DEG	25																						-2.9 -										
Z.		ZA O	51	059	. 921	992	037	044	. 035	077	019	. 035	003	.012	044	. 094	.002	019	.007	.040	960.	028		092		106	073	.010	030		056	.010	.045	040	
<b>-</b>	8	DEG	20	4.4	1.2				6	_		2.0				5.4	Ξ.	- - -	₹.	2.3		1.9.1		-5.3	.8.	-6.1	-4.2 -	ø.	-1.7 -		-3.2 -	ø.	2.6		
R 0 L		RAD	6	072 -		. 045					•		. 954	016			.045	•				-	. 689	.045 -		012 -		.115	035 -	. 002		. 924	. 021	058 -	
	5	DEG	84	1 +	ĸ.	2.6	3 -	·			L. J	_	3.1	9	- 6		2.6		2.5		- 1.7	٠	5.1		2 -	7 -	ı	9.9		٦.	9.	<b>+</b> :-	~		
		S.	41	'				i		1											ı	,			. 105	•	•		•					1	
m		DEG	46																						6.9										
Z K		8	<b>5</b>	. 968	. 673	.113	.112	660	.084	.677	. 689	. 073	. 106	. 063	. 689	.084	. 108	. 087	.072	. 989	.073	.086		.075	869.	. 677	. 086	. 694	. 086		.075	.075	. 686	.075	
I O	ğ	DEG	‡	3.9	4.2	6.5	6.4	5.7	<b>4</b> .8	<b>+.</b>	5.1	4.2	6.1	3.6	5.7	4.8	6.2	5.0		<b>4</b> .6	4.2	6.4		4.3	5.6	4.4	6.4	5.4	e. <del>4</del>		4.3	4.3	6.4	4.3	
P		SA O	<b>5</b>		.061		_																<b>.09</b>	. 075	. 103	. 692	. 679	168	688	. 059	. 982	. 686	. 684	.068	
	5	DEG	42	4.7	3.5	3.0	<b>6</b> .	80	6.3	<b>4</b> .6	÷.5	6.7	<b>8</b> .4	3.9	6.4	<b>4</b> .8	7.2	6.0	4.2	4.5	4.5	5.3	5.4	4.3	8.8	5.3	4.5	6.2	5.1	4.6	4.7	4.6	4.8	3.9	
S C P	2		<b>=</b>	27	28	29	8	2	2	Ť,	33	36	37	39	9	42	₹	¥	<b>\$</b>	ę	4	<b>\$</b>	8	51	25	53	\$	55	57	<b>28</b>	ŝ	61	62	2163	

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DAY LANDINGS

USS ENTERPRISE (CVN-65)

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DAY LANDINGS

USS ENTERPRISE (CVN-65)

LANDING DATA - MODEL F-18A

																																					Cc	od	е	60	)42	2	
REREAD	NUMBER			7	7	7	0	-	60	-	-	_	•	-		-	0	-	0	•	6	-	-	•	0	6	0	•	0	-	•	0	-	•	•	6	0	0	-	•	-	0	6
ARR GEAR	RUNOUTS	₹	82	9.0	426.7	429.3	419.1	424.2	426.7	419.1	0.0	426.7	426.7	0.0	426.7	429.3	431.8	431.8	0.0	0.0	9.9	429.3	0.0	0.0	426.7	419.1	<b>9</b> .0	421.6	429.3	429.3	429.3	429.3	<b>9</b> .0	426.7	429.3	429.3	9.0	424.2	429.3	431.8	129.3	129.3	129.3
ARR	Ş	ĸ	2	0	168 4	169 4				165 4			168					176	0	0		169 4	0			165 4						169				169			-	•	-	•	169
ETRIC	SURE	MAN HG	80	760.2	760.2	760.2	760.2	769.2	760.2	760.2	760.2	760.2	760.2	759.7	759.7	759.7	759.7	759.7	759.7	759.7	759.7	759.7	759.7	759.7	759.7	759.7	759.7	759.7	759.7	759.7	759.7	759.7	759.7	759.7	759.7	759.7	759.7	759.7	759.7	759.7	759.7	759.7	759.7
BAROMETRIC	PRESSURE	IN HG	79	29.93	29.93	29.93	29.93	29.93	29.93	29.93	29.93	29.93	29.93	29.91	29.91	29.91	29.91	29.91	29.91	29.91	29.91	29.91	29.91	29.91	29.91	29.91	29.91	29.91	29.91	29.91	29.91	29.91	29.91	29.91	29.91	29.91	29.91	29.91	29.91	29.91	29.91	29.91	29.91
TEMP		ပ	78	21	2	21	21	51	21	7	21	71	7	23	23	23	23	23	23	23	23	23	23	23	23	23	23	23	23	23	23	23	23	23	23	23	23	23	23	23	23	23	23
-		la.	71	70	70	20	92	70	70	70	70	70	79	2	23	73	23	23	2	2	73	23	23	73	2	23	23	23	2	73	2	73	23	73	23	73	23	2	73	23	73	73	73
DECK ROLL		RAD	76	016	010	042	031	.012	. 003	. 005	014	003	. 035	005	054	. 028	030	031	012	.014	002	.014	007	007	. 007	030	012	017	002	010	. 005	021	023	021	. 003	838	.014	002	037	026	017	035	.014
DECK		DEC	75	6.1	9	-2.4	<u>-</u> 1.8	.,	?						٠. ا		-1.7			æί	7	æ	4.1	<b>†</b> .			7	1.0	;	9.1			<u>ا</u> ن	-1.2	7.	-2.5	æ.	7		<u>-1</u> .5		-2.0	æ.
DECK PITCH		<b>₽</b>	7.	002	009	003	003	903	003	007	005	005	005	002	005	003	005	003	007	003	605	003	007	003	997	007	667	005	007	997	992	005	005	0.000	009	012	667	010	009	003	005	003	007
DECK		DEC	23	-	č.	- 7	.2.	2	2	· *		ų.	٠	-	D.	. 7	ب	.2.	· •	2		.2	· •	- 2	· •	*	• •		· •	<b>+</b>	· -	ا. د	٠ ت	9.0	.55	. 7	+	. 9.	.5	2		2	*
		N/S	72	G	0	Ф	Ф	&	EO	œ	Ф	_		+	₩.	'n		'n	,	ы	n n	n		ы	'n	n.	'n	n n	n n	, ,	י י	Б	,	n		ь.	ы	, D	,	ь.		ъ	'n
SHIP	SPEED	Z Z	7	17	7	7	_	9	2	2	2	2	2	7	9	S	5	'n	S)	'n	ري د	'n	'n	S	ŝ	S	'n	S	S.	တ	S	S	S	တ	ß	S	S	S	ęs	2	S	'n	ις.
F.	CODE	_	70				·	•			•	•																															
CNDG	TYPE		69	79199	50120	50200	50120	50120	50120	50120	60200	50200	50120	70120	50120	50120	50200	50100	70100	70120	69129	50120	70100	70120	50120	50120	70120	50100	50100	50100	59199	50120	70100	50120	50200	50200	70120	50120	59120	50120	80100	59129	59200
SIDE	Š		8	567	571	267	267	571	267	571	267	571	267	572	260	551	260	572	557	573	551	260	557	573	572	560	577	511	551	557	573	572	267	551	577	260	267	567	573	511	557	572	511
WIRE	ġ		67		8	7	n	~	4	n		*	7		n	n	r	7				n			n	n		n	4	~	*	n		m	n	4		4	*	n	7	_	7
RAMP TO TD	DISTANCE	3	99	7.	67	2	79	75	93	76	92	60	67	76	33	76	72	7	5	67	88	83	99	88	67	83	<b>9</b> 6	23	8	89	8	78	72	8	75	87	70	6	95	11	22	54	69
RAMP	DIST	t	65	242	219	241	260	245	<b>1</b> 86	249	312	291	220	248	271	250	236	242	<b>700</b>	220	322	272	215	322	221	270	296	239	278	228	<b>580</b>	249	237	262	247	285	229	297	313	253	241	176	227
ENTER	NCE	3	79	-5	7	†	7	7	7	†	7	7	?	•	7	7	-7	ဟု	7	7	7	?	φ	†	۴P	7	7	7	7	†	7	†	7	†	7	ņ	7	7	†	7	†	-5	4
OFF-CENTER	DISTANCE	ב	63	ş	-	-12	=	6	9	-12	ဂ	φ	-10	7	7	ņ	q	-18	7	†	6	=	-19	-13	-15	ņ	φ	<b>9</b> 1-	F	<del>*</del>	7	114	6	-12	<b>6</b> 1	-10	-10	7	-13	6	-12	<b>\$</b>	-15
CNDC	<b>9</b>		62	1170	1171	1172	1179	1184	1193	1195	1200	1207	1210	1390	1397	1402	1403	1404	1406	1407	1408	1409	141	1412	1418	1419	1420	1421	1422	1423	1424	1425	1427	1428	1430	1434	1435	1438	1439	1441	1442	1445	1448

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DAY LANDINGS

USS ENTERPRISE (CVN-65)

LANDING DATA - MODEL F-18A

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REREAD	NUMBER			6	60	-	60	•	0	-	•	0	<b>o</b>	-	<b>6</b>	_	0	<b>5</b> 0 (	<b>S</b>	9 6	9 0	<b>9</b> 6	•	• •	. 6	0	•	•	Φ,	-	<b>o</b>	8	-	-	•	•	-	0	•	0	0	7
ARR GEAR	RUNOUTS	3	82	429.3	424.2	9.0	9.0	429.3	426.7	426.7	429.3	429.3	426.7	9	6. 6.	431.8	•	7	9.6	9.6	9.6			4	•	<b>9</b> .	431.8	0.0	6 6			429.3	9.0	<b>6</b>	<b>0</b> .0	426.7	<b>6</b> .0	431.8	424.2	426.7	429.3	429.3
\$	2	Z	8	169	167	6	0	169	168	168	169	169	168	6	•	170	6	166	9 ;	2 °	9 9	9 9	9 6	178	•	0	170	0	•	169	170	169	0	6	0	168	0	170	167	168	169	169
BAROMETRIC	PRESSURE	MA HG	80	759.7	759.7	759.7	759.7	759.7	759.7	759.7	759.7	759.7	759.7	759.7	769.2	759.7	769.2	760.2	7.00/	7.00/	7.00/	7.00/	769.2	769.2	760.2	760.2	760.2	769.7	769.7	769.7	769.7	769.7	7.69.7	760.7	760.7	760.7	760.7	761.2	761.2	761.2	761.2	761.2
BARON	PRES	N H	79	29.91	29.91	29.91	29.91	29.91	29.91	29.91	29.91	29.91	29.91	29.91	29.93	29.91	29.93	29.93	29.92	28.82	28.82	26.82	29.93	20.02	29.93	29.93	29.93	29.92	29.95	29.92	29.95	29.92	29.95	29.92	29.92	29.95	29.95	29.97	29.97	29.97	29.97	29.97
TEMP		ပ	78	22	22	22	22	22	22	22	77	52	55	22	77	22	22	77	7 6	7 8	7 8	3 6	3 6	3	2 2	22	22	7	7	7	5	7	7	7	7	7	7	22	22	22	22	22
<b>—</b>		<b>L</b> .	77	72	72	72	72	72	72	72	72	72	72	72	72	72	72	22	7 :	7 5	7 5	7 5	3 2	; 2	: 2	72	72	69	69	69	60	8	69	69	69	69	69	72	72	72	72	72
DECK ROLL		RAD	76	002	007	995	030		016	035	.017	005	. 993	. 016	035	002	.019	600	 	- e2e	9.0	2/0. I	995	621	012	049		0.000	667	1.01	. 928	•			9.666	. 023	•	•	i	005	4 1	616
DEC		DEG	75	ï	7		-1.7		6.	-2.0	<b>6</b> .		2	Ö.	-2.0	ï	- '	3.	הינ	· ;	3.5	9 0				-2.8	1.	0.0	i	1	9.	-	<b>6</b> .	9.	9.9	7.3	.7	8.	9		œ.	φ.
DECK PITCH		RAD	*	. 003	009	002	002	. 003	.007	. 663	005	005	. <b>6</b> 69			005	007				200	200	919	919	. 995	9.00	009	. 010	995	. 993	- 963	002	002	695	003	. 007	- 969	. 005	663	. 997	005	. 983
ECK		DEG	73	. 2.	ι.	<u>.</u>	<u>'</u>	7	·	7	i.	ιί I	ກຸ	. 2.	i i	٠	' *	ا ب	ن د ا	•	' ''	יי ייי		وع	י פי	9	ιύ 	9	ن		n.	' -	<u>'</u>	ن. ا	7	†	ι.	r. '	7	' ★.	ا ب	κi
	۵	S/M	72	1	l P	1	, ,	ا ا	<b>1</b>	1	1 1	n n	ן רסי	1 D	1 n	ן ו	ا 10	ו ייטי	ן יי	! つ p	ן יי	) F	) I	ו מיי	ו מי	3	1	9	! 9	ا و	9	9	9	9	9	9	9	9	9	9	9	ا و
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CNDC	TYPE		69	50120	50120	70120	70120	50120	59129	59200	50120	50200	50120	70200	69129	20200	70200	56126	92199	97190	97199	50120	78188	50120	50120	79199	58288	70120	70120	80100	50120	50120	70200	79299	70120	50120	70100	50120	50120	50120	59200	50120
SIDE	ġ		89	557	260	552	577	==	573	222	277	557	277	272	552	22	572	272	200	) i	700	7/0	573	57.2	26	573	573	277	277	277	277	572	222	57.	222	277	571	222	571	272	571	277
WIRE SIDE	ġ		67	4	+			+	4	*	~	~	4			n	•	+	•	ว	r	2		<b>1</b> 7	)		•			ימ	יח	n				~		~	n	ď	n	₹
RAME TO TD	DISTANCE	*	8	69	98	92	22	83	<b>5</b>	<b>8</b>	62	62	5	62	9	69	<b>S</b>	8	3	ر د ع	<b>S</b>	6 6	8 8	3 2	27	99	23	92	67		8	1	62	57	57	70	67	7	11	72	83	96
RAMP	DIST	E	65	293	283	312	241	292	310	294	203	<b>70</b>	9	204	297	227	214	289	3 5	/ 47	226	3 5	¥ 5	241	235	217	238	249	221	281	258	22	202	187	187	229	219	232	251	237	271	296
OFF-CENTER	DISTANCE	3	\$	7	?	7	7	ę	7	~	ņ	'n	7	†	7	Ŷ	† '		? '	7 .	? •	P	1 9	1	7	7	7	ī	7	?	7	†	ī	ģ	†	7	†	-5	†	?	?	7
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LNDG	Š		62	1448	1450	1452	1453	1454	1455	1456	1457	1459	1460	1461	1462	1463	1464	1466	1467	99	80+	24/4	1473	1474	1475	1477	1478	1482	- -	1484	1483	1486	1487	1488	1489	1490	1491	1492	1493	1494	1495	1496

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DAY LANDINGS

USS ENTERPRISE (CVN-65)

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REREAD	NUMBER			0	7	0	-	0	_	-	•	7	•	0	6	0	0	60	-	60	-	-		•	_	•	_	-	<b>S</b>	- •	•	<b>s</b> c	<b>D</b> (	<b>s</b>	-	•	60	0	•	•	•	•	0
GEAR	UTS	₹	82	424.2	431.8	419.1	9.0	431.8	9.0	431.8	<b>0</b> .0	<b>0</b> .0	424.2	431.8	426.7	429.3	429.3	429.3	9.0	426.7	426.7	426.7	426.7	426.7	426.7	426.7	129.3	431.8	126.7	5.5	0.10	429.5	2	51.8	429.3	429.3	<b>6</b>	429.3	431.8	429.3	£31.8	131.8	<b>429.3</b>
ARR GEAR	RUNOUTS	2	2	167 4	170 4	165 4	0	179 4		179 4	•							169 43	0					-	-	-	-	-	-	9/1	•					169 4				•	•	•	169 4:
TRIC	URE	NAM HG	80	761.2	761.2	761.2	761.2	761.2	761.2	761.2	761.2	761.2	761.2	761.2	761.2	761.2	761.2	761.2	761.2	761.2	761.2	761.2	761.2	761.2	761.2	761.2	761.2	761.2	761.2	7.10/	7. 10/	7.10/	7.10/	7.107	761.2	761.2	761.2	761.2	761.2	761.2	761.2	760.7	760.7
BAROMETRIC	PRESSURE	IN HG	79	29.97	29.97	29.97	29.97	29.97	29.97	29.97	29.97	29.97	29.97	29.97	29.97	29.97	29.97	29.97	29.97	29.97	29.97	29.97	29.97	29.97	29.97	29.97	29.97	29.97	29.97	78.87	78.87	78.87	28.87	29.97	29.97	29.97	29.97	29.97	29.97	29.97	29.97	29.95	29.95
TEMP		ပ	78	22	22	22	22	22	77	22	22	22	22	22	22	22	22	22	22	22	77	22	22	22	23	23	23	23	23	S	3 2	3 :	3	3 3	23	23	23	23	23	23	23	21	71
-		<b>L</b> .	11	72	72	72	72	72	72	72	72	72	72	72	72	72	72	72	72	72	72	72	72	72	2	23	2	2	2	3 ;	3 ;	?;	2	2 :	2	23	2	23	2	73	23	69	69
ROLL		8	92	. 023	010	007	. 017	.007	.012	.012	. 009	.012	.010	. 003	. 024	. 005	.017	016	.012	. 005	. 003	. 009	.010	600.	. 992	012	014	023	600	9.6	710.	799.	710.	045		. 002	012	907	010	016	012	. 028	035
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SIDE	÷		8	571	577	571	573	572	573	573	267	267	571	267	572	573	571	277	267	572	551	267	211	55	277	55	277	267	572			2	2/2	7/2	2	267	27	573	57	551	267	573	544
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<b>M</b>	018	E	8	297	253	293	214	226	317	268	227	229	243	259	248	<b>5</b> ‡	258	230	317	182	297	218	234	238	248	234	707	327	316	? :		707	107	200	27	286	7	326	253	241	257	249	269
ONTER	WCE	3	\$	7	7	†	†	7	-7	?	1	ņ	7	†	7	7	ņ	†	7	7	7	۴	۴	7	ç	7	†	7-	ī'	ę c	7 .	† '	?	† .	7	7	7	7	†	†	7	†	†
OFF-CENTER	DISTANCE	E	3	ę	†	-12	-12	ę	۴	9-	-12	<u>-</u> 5	9-	<u>-</u>	4	<u>'</u>	-15	<b>+</b>	φ	7	۴	<del>-</del>	-20	۴	<b>9</b>	†	-1 -1	ę,	7 :	י <u>מ</u>	ì :	<u>*</u> :	= :	-1z	7	-12	-10	<b>\$</b>	-13	-12	6	-12	-12
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13410 Code 6042

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REREAD	NUMBER			9	•	0	0	0	7	7	7	-	-	•	•	0	6	0	6	•	0	0	•	0	0	0	6	-	•	0	0	•	-	•	0	Φ	•	0	0	0	-	6	-
ARR GEAR	OTS	₹	82	426.7	426.7	<b>9</b> .	431.8	426.7	424.2	431.8	426.7	424.2	429.3	429.3	431.8	424.2	429.3	426.7	426.7	429.3	426.7	424.2	424.2	426.7	424.2	426.7	421.6	426.7	424.2	426.7	<b>6</b>	431.8	424.2	429.3	<b>6</b> .6	429.3	431.8	424.2	429.3	426.7	426.7	424.2	426.7
ARR	RUNOUTS	×	<b>©</b>	168 4	168 4	•	179 4	168 4	167 4	170 4						167 4	169 4		168 4				167 4		167 4					168 4				169 4	•				169 4	168 4		167 4	168 4
TRIC	SURE	¥	88	7.69.7	7.69.7	7.097	769.7	7.097	769.7	760.7	760.7	760.7	769.7	760.7	760.7	7.097	769.7	769.7	769.7	769.7	769.7	7.69.7	769.7	7.69.7	7.097	760.7	760.7	7.69.7	7.09.7	761.2	761.2	761.2	761.2	761.2		761.2	761.2	761.2	761.2	761.2	761.2	761.2	761.2
BAROMETRIC	PRESSURE	IN HG	79	29.95	29.92	29.92	29.92	29.95	29.92	29.92	29.92	29.92	29.92	29.92	29.92	29.92	29.92	29.92	29.92	29.95	29.92	29.92	29.92	29.92	29.92	29.92	29.95	29.92	29.95	29.97	29.97	29.97	29.97	29.97		29.97	29.97	29.97	29.97	29.97	29.97	29.97	29.97
TEMP		ပ	78	21	7	21	21	21	7	21	2	2	21	21	71	7	21	21	7	7	21	21	21	21	7	21	7	21	21	7	7	7	7	5		7	7	2	21	2	7	21	21
-		<b>L</b>	11	69	69	69	69	69	69	69	69	69	69	69	69	69	69	69	69	69	69	69	69	69	69	69	69	69	69	70	70	70	70	70		92	92	70	70	70	69	69	69
DECK ROLL		RAD	76	038		030				024				. 026	9.000				007	.007	005	014	016	010	037	002	012				. 993	030	. 002	037	014		021	•	. 002	•		002	030
DEC		DEC	75	-2.2		-1.7	1.0	7	-2.4	7.	1.0	<del>*</del> .	1.2	1.5	0.0	1.5	٠ •	L.	<b>†</b>	*	J. 3	1	6.	9.	-2.1	-:	7	-2.4	9.1	6. I	.5	-1.7	-	-2.1	1	φ.	-1.2	.5	-	-1.2	-2.3	-	-1.7
DECK PITCH		RAD	74	007		999	005	010	007	005	663	010	009	995	007	009	005	009	012	007	010	005	009	010	007	003	007	012	007	002	002	993	009	003	005	005	003	003	005	003	003	007	003
DECK		930	23	<b>4</b>		ا. ئ	J. 3	9.	<b>+</b> :	ا. ن	2	9.	5.	L. J	<b>+</b> .i	ا ن	ا. ن	ا. ت	7	₹.	9.	J. 3	۱ ا	9.	4.	2	<b>₹</b> .	7	<b>+</b> · ·	ï	J.	2	ر ب	2	ا.ن	J. J	2	2	J.	2	2	4.1	2
SHIP	SPEED	K/S	73	ဖ	9	ø	9	9	ø	ဖ	ø	9	9	9	9	9	9	9	9	9	ø	ø	9	9	9	9	ø	ø	ø	ø	ဖ	ø	ဖ	ဖ	•	9	9	9	9	ø	9	9	ø
		¥	7	=	=	=	=	Ξ	=	=	=	=	=	=	Ξ	Ξ	Ξ	=	=	=	=	=	=	Ξ	=	=	=	=	=	12	7	12	12	12	0	12	12	7	7	12	12	12	12
J.	3000		70																																								
LNDC	TYPE		8	50120	50100	60120	56120	50200	50120	50200	50120	50120	50200	50120	50120	50120	50120	56266	50100	58288	50120	50200	50120	59120	50120	50120	50120	50120	50200	50120	69128	50120	<b>26</b> <b>18</b> <b>18</b>	50120	50120	50120	50120	50100	50120	50200	50120	59129	50120
SIDE	Š		2	566	3	573	560	573	577	57	5	4	3	573	260	577	572	571	544	5	543	573	260	543	<b>5</b> 44	572	577	577	571	211	56 <b>6</b>	560	572	2	<b>54</b> 5	577	560	572	573	51	551	567	260
WIRE	9.		67	2	*		n		*	n	n	*	n	n	n	n	n	*	n	n	*	n	n	n	*	n	n	n	ריו	*		n	r	*		4	2	*	7	8	מי	7	n
RAMP TO TD	DISTANCE	3	8	3	8	<b>5</b>	22	72	S	2	8	8	28	3	3	ž	76	3	3	41	87	22	79	8	2	79	2	*	2	2	2	<b>5</b>	F	82	8	93	77	\$	29	7	75	3	82
	DIST	F	8	224	278	340	243	236	182	262	261	288	259	<b>708</b>	207	211	<b>52</b>	271	271	155	286	241	<b>560</b>	264	290	259	198	275	224	298	328	<b>7</b> 66	232	268	288	304	251	274	193	233	245	211	270
OFF-CENTER	DISTANCE	3	2	7	-7	7	7	7	ę	7	7	†	7	7	?	7	-7	7	†	†	7	7	7	?	7	-7	7	7	7	†	7	7	۴	7	7	'n	?	٣	†	7	-7	7	7
OFF.	018	E	3	10	۲-	†	7	-7	13	=	7	-12	Ŧ	<del>-</del> 1	=	<del>-</del> 10	-1	Ģ	-12	-12	-1	7	ĝ	9	-1	9	Ŧ	6	<b>9</b>	-12	Ŷ	٥ ا	<del>-</del> 7	ī	10	6	9	97	+1-	-12	7-	=	<u>1</u>
LNDG	<b>9</b>		62	1826	1827	1828	1829	1836	1831	1832	1833	1834	1836	1837	38.	1839	1849	1842	1843	1844	1845	1846	1847	1853	1854	1855	1857	1859	1861	2111	2112	2113	2114	2115	2116	2118	2119	2121	2122	2123	2124	2125	2126

DAY LANDINGS

ENTERPRISE (CVN-65)

13410 Code 6042

FED M/S DEG RAD DEG RAD F C IN HG MM HG 72 73 74 75 76 77 78 79 80 80 80 80 80 80 80 80 80 80 80 80 80					NO. TYPE		2021			
DEG         RAD         DEG         RAD         F         C         IN         HG         MM           73         74         75         76         77         78         79         8          1        0002        8        014         69         21         29.97         761          3        0005        8        014         69         21         29.97         761          2        0005        9        016         69         21         29.97         761          2        0005        9        016         69         21         29.97         761          2        0005        9        016         69         21         29.97         761          2        0005        1        019         69         21         29.97         761          2        0005        1        019         69         21         29.97         761          2        0005        1        019         69         21         29.97         761          2        0005        1        019         6	SPEED			بر <u>ا</u>	·	NO. NO. TYPE CODE	MO. MO. 17PC	NO. TYPE	DISTANCE NO. NO. TYPE	NO. NO. TYPE
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	12 61	_		50100	572 50100		3 572	73 3 572	241 73 3 572	-6 241 73 3 572
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0099016 69 21 29.97 7610026010 69 21 29.97 761003 .7 .012 69 21 29.97 761003 .5 .009 69 21 29.99 761009 .9 .016 69 21 29.97 7610098014 69 21 29.97 7610052003 69 21 29.97 7610092003 69 21 29.97 7610092003 69 21 29.97 7610092003 69 21 29.97 761	12 6 9.0			28288			2 572	59 2 572	194 59 2 572	-1 194 59 2 572
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8 .014 69 21 29.97	9	_		50120			2 577	76 2 577	229 76 2 577	-2 229 76 2 577
	12 63			59100			3 573	77 3 573	252 77 3 573	-2 252 77 3 573

S

DAY LANDINGS

USS ENTERPRISE (CVN-65)

# F-18 NIGHT

13410 Code 6042

WEIGHT		¥G	21	14268	13769	14313	14585	14585	14540	14540	13587	13587	13950	13769	13587	14449	14041	14313	13723	14177	13632	13587	14131	14041	13814	14131	14268	13496	14993	15402	13814	14313	13632	13134	14222	13270	14404	13134	13814	13587	13723	13451	14812
WEI		LBS	70	31454	30354	31554	32154	32154	32054	32054	29954	29954	30754	30354	29954	31854	30954	31554	30254	31254	30054	29954	31154	30954	30454	31154	31454	29754	33054	33954	30454	31554	30054	28954	31354	29254	31754	28954	30454	29954	30254	29654	32654
LIFT	<u>.</u>		19		1.00																																						
LIFT	5		<del>6</del>	1.00	1.20	1.20	96	1.10	1.10	1.20	96	1.10	96	1.10	1.00	96	1.20	1.10	96	96	96	96	1.00	1.00	1.00	1.10	1, 10	1.00	1.00	1.00	1.10	1.10	1.30	96.	96.	1.30	1.20	1.00	1.10	1.10	1.10	1.10	1.20
<b>\$</b>	۷. ط		11																																								
KVPA	Z		91	1.05	1.08	1.06	=:	<b>-</b>	1.09	1.12	1.06	1.91	1.01	1.04	1.03	66.	1.07	1.07	1.08	1.1	1.10	1.09	1.09	1.06	1.07	1.10	1.17	1.13	1.15	1.07	1.05	1.12	1.10	1.10	1.07	1.12	1.17	1.06	1.20	1.15	1.20	1.1	1.17
V.dSA		N/S	5																																								
YS.		ž	<b>±</b>																																								
VPAMIN		N/S	5	70	68	70	70	70	70	70	89	68	69	68	89	70	69	70	68	69	68	68	69	69	69	69	70	68	72	23	69	70	68	29	70	29	70	67	69	89	89	89	7
Š		Š	12	136	133	136	137	137	137	137	133	133	134	133	133	137	135	136	133	135	133	133	135	135	134	135	136	132	139	141	134	136	133	130	136	131	136	130	134	133	133	132	138
VEOR		s/m	=																																								
3		¥	6																																								
	<u>.</u>	M/S	<b>o</b>	~	~	_	n	n	n	n	~	~	~	~	7	~	7	8	7	n	n	n	n	7	8	~	8	n	n	n	n	-	-	_	_	-		-	_	-	7	7	8
-vEt	PERP	Š	€	n	*	7	ĸ	60	ĸ	40	n	n	*	*	*	*	*	*	4	80	٤O	ß	40	*	*	*	*	80	6	ĸ	ĸ	7	7	8	7	7	7	~	7	8	2	'n	n
WIND-VEL	PAR.	K/S	^	•	=	=	5	5	15	5	<b>6</b>	10	=	=	=	=	12	12	12	<b>*</b>	<b>*</b>	<b>±</b>	<b>*</b>	12	12	5	5	<b>*</b>	<u>*</u>	5	5	<b>±</b>	<b>*</b>	<b>±</b>	12	<u>*</u>	<b>*</b>	5	5	<u>*</u>	5	5	5
	•	ž	•	29	22	22	8	8	8	8	<b>50</b>	<b>50</b>	22	22	22	22	24	<b>74</b>	23	<b>58</b>	27	27	27	23	23	52	25	27	27	ఇ	8	27	27	<b>58</b>	24	27	27	<b>5</b> 6	26	27	8	36	29
VE-F1UM		K/S	10	3	3	63	63	63	62	2	62	28	29	9	20	29	62	2	62	65	62	3	62	61	62	63	69	63	8	62	21	<b>5</b>	61	29	62	62	68	80	69	65	67	62	89
¥		₹	•	123	122	123	123	123	120	124	120	115	<b>+</b>	116	115	114	120	122	121	126	120	117	120	119	128	123	135	122	33	121	110	125	119	115	121	120	35	112	134	126	130	121	132
<b>L</b>	_	K/S	n	7.	7.	73	79	79	11	79	72	8	70	7	96	9,	*	75	*	2	92	7,	2	23	*	92	82	77	83	78	72	78	2	7	2	76	82	71	82	79	82	78	3
VPAF	5	Š	8	143	<del>*</del>	145	153	153	150	<b>\$</b>	140	135	136	5	137	136	141	146	<del>+</del>	154	147	#	147	142	143	148	160	149	160	151	140	152	146	143	145	147	160	138	160	153	16	151	161
S C C	ġ		-	8393	8398	8643	9386	9369	9390	9391	9395	9396	9398	9400	9401	9406	9468	9410	9416	9417	9418	9419	9420	9424	9425	9431	9432	9435	9446	9452	9466	9510	9511	9516	9518	9521	9524	9531	9532	9535	9536	9537	9538

NIGHT LANDINGS

#### NADC-91124-60

#### DEPARTMENT OF THE NAVY Naval Air Development Center Warminster, PA 18974-5000

13410 Code 6042

WEIGHT		S KG	21	13360	14404	_	14676	13678	_	13632	_	13859	14086	14268	14540	14313	_	13950	14841	13995	_	13451	14540		13769	_	14404	14404	13950	14131	14268	14177	13814	13814	14494	_	_	Ĭ	17/61
		rBS	20	29454	31754	30454	32354	30154	30054	30054	31554	30554	31054	31454	32054	31554	29654	30754	30954	30854	30354	29654	32054	28954	30354	31754	31754	31754	30754	31154	31454	31254	30454	30454	31954	31354	29954	TOARA	24434
LIFT	<b>1</b> 4		19																	1.10																			
LIFT	đ		<b>6</b>	1.00	1.00	96.	1.10	1.20	1.10	1.20	1.00	1.20	1.00	1.00	1.00	1.10	1.20	1.00	1.88	1.10	96	1.10	1.30	96.	1.00	1.20	1.00	1.10	1.88	1.00	1.00	96.	1.60	1.00	1.10	1.30	1.30	•	
\$	. dS		17																																				
KVPA	N N		16	1.12	1.07	1.02	<b>-</b> :	1.15	1.07	1.13	1.04	1.17	1.10	1.12	1.10	1.15	1.18		1.1	1.15	1.07	-:	1.06	1.12	1.12	1.08	1.08	1.10	1.07	1.13	1.15	1.10	1.13	1.13	1.10	1.03	1.07	40	- 00
VSP.A		S/M	15																																				
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VEOR		N/S	=																																				
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	PERP.	S/M	0	8	8	-	_	-	-	-	-	-	7	7	8	7	7	7	7	7	7	7	~	8	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
WIND-VEL	_	\$	60	F)	כיי	~	~	~	74	~	8	7	m	מי	m	P	ריי	P)	m	כיי	P)	•	ניי	P)	~	8	8	7	7	~	7	~	7	~	~	~	7	·	1
×	PAR.	S/M	7	51	15	<b>*</b>	# -	<b>±</b>	<b>*</b>	<b>±</b>	<b>*</b>	<b>*</b>	5	5	_	_	-	_	5 5	15	_	_	_	15		<u>+</u>	<u>*</u>	<b>*</b>	<u>*</u>	<u>+</u>	<u>*</u>	=======================================	=======================================	-	=	10	13	•	2
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>		Z Z	•	11	5 117	169	12	12	3 115	7 12		_	•		•	_		_	•	•	•	•	_	_	_	•	_	_	-	_	121	_	_	_	_	2 119	-		-
VPAF	5	KN M/S	2	48 7	46 7	36 7	2	22	142 7;	56		_	48 76				56 86				42 73		145 75	•				51 78	• -	53 79	56 84	-	51 78	•	•	39 72		17 71	`
DON	Š	Ÿ	-	_	_	-	-	_	_	9552 1	-	_	9562 14	_	9567 1	_	_	_	_	_	_	_	_	_	_	_	9586 14	_	_	_	_	_	_	_	_	9645 13	_	•	-

NIGHT LANDINGS

USS ENIERFRISE (LVN-65)

CONTING UNIA - MADEL 1-10A

																																			CC	od e	2	60	42	•	
# 5 2 4	RAMP	3	4																																						
HOOK HEIGH	OVER RAMP	Ħ	39																																						
MHEEL HEIGHI	RAMP	3	38																																						
MEEL	OVER	E	37																																						
2	B/V	RAD	36	.043	. 030	.049	9/9	. 649	. 6	.070	.036	.679	. 048	. 054	. 065	.045	. 039	.046	999.	400.	90.0	. 60	90.	/ca.	. 649		970.	9 6	. 038	. 038	.042	. 657	990.	. 037	. 908	. 039	. 042	. 033	. 050	. 033	. 038
GLIDE PAIH ANGLE AT ID	6	DEG	35	2.5	1.7	2.8	*	2.0		6.4	2.1	4.0	2.8	3.1	3.7	5.6	2.2	5.6	ю. •	ر ا	9 i	o ,	٠ ١	٠. د.	7. R				2.5	2.5	2.4	3.2	3.8	2.1	ŧņ.	2.3	2.4	1.9	2.9	6.	2.2
	ž	RAD	34																																						
96106	<b>₩</b>	DEG	33																																						
	.IGHT	S/M	32		2.5																																				
	FREE-FLIGHT	5/2	31		₩.																																				
	<b>,</b>	S/M	30	3.0	2.1	4.0	o.	ب ه و	, d	9 0	2.5	4.5	3.5	3.3	<del>-</del>	4.6	2.9	ا ا	4.7	ا ري د و	. ·	9.	٠. د	4 ·	9	2.9	7) T	, t	9.6	2.8	3.0	3.8	4.4	2.8	1.5	2.8	3.2	2.5	3.7	2.4	2.8
	AVG A	F/S	59	9.7	6.9	11.2	17.9	11.7		16.0	7.3	14.8	10.5	16.8	13.5	11.2	9.5	7.6	15.5	12.3	10.2	13.1	14.1	9.	11.7	٠. د د	- :	7	4	0.0	10.0	12.4	14.5	9.5	5.0	9.1	10.7	8.2	12.1	7.9	9.5
	0	R/S	28	2.7	9.7	ы. Б.	2.5	٠. ر د د	, e		2.6	4.5	3.2	3.3	4.2	3.5	3.1		4. 0	ы 5.5	2.9	<b>4</b> .	÷.5	4.2	S. 6	3.2			9.6	2.7	2.8	3.6	<b>+</b> . <b>+</b>	2.2	<b>*</b> :-	2.8	4.6	5.6	3.5	2.7	5.6
) }	STBD	F/S	23	<b>8</b> 0.	6.5	11.0	7.2	12.2			9.9	4.7	10.4	10.7	13.8	1.4	10.2	8.5	₩. ÷	1.5	7.6	n	<b>9</b>	13.9	<b>8</b> 0 :	10.6	- :	· •	4	6.0	- 6	11.7	14.5	7.2	4.5	9.5	1.1	4.6	9.11	8.9	4.
	_	EK/S	<b>38</b>	3.2				4.6	·			-		•	-				<b>4</b> 1											2.8	2.5							2.1	ы. В.	2.3	3.0
A I MCKAP I	PORT	F/S	22	10.7	7.3	5.1	6.7	11.2	0 °	 	. 6	•	10.7	10.8	11.7	9.5	8. 8.	3.2	15.0	12.2	10.7	9.5		4.2	9. =		o 0	D 9		9.2	8.0	13.2	13.8	11.9	5.3	9.1	10.2	6.9	12.6	7.7	10.0
	w	S,	54	3.1				8.				4							4. W			•	•	•	•	5.9	D (							2.7	5.1	5.8	5.8	2.3	3.7	5.6	2.9
	NOSE	5	23		9.2	9.11	5.2	2.0		0.7			11.3	11.0	11.3	8.8	9.5	9.5	<b>9</b> .	2.6	<b>8</b> 0	G. 1	J. J.	3.5	<b>8</b> 0.	. s.	9.7	- 4	? <b>«</b>	7.8	6.9	4.	6.1	8.7	5.0	4.6	9.5	7.6	12.3	8.5	9.4
3	£		22	_		9643					9396	-			9466														9432 9456		9511		9518					9535	_		

NIGHT LANDINGS

## DEPARTMENT OF THE NAVY Naval Air Development Center Warminster, PA 18974-5000

9			AIRCRAFT		SINKING SPEED AT TOUCHDOWN	PEED AT	TOUCH	N		G	GLIDE PATH ANGLE AT TD	ATH A	HGLE A	0 10	WHEEL HEIGHT	EIGHT	HOOK HEIGHT	IGHT
£	2	NOSE	PORT	7	STBO	8	AVG		FREE-FLIGHT	IGHT	BHAN		B	>	OVER RAMP	AM.	OVER RAMP	d d
	F/S	N/S	<b>5</b> /2	R/S	F/S	N/S	F/S	S/M	F/S	N/S	DEG	RAD	DEC	P. P	E	3	Ħ	3
22	23	<b>5</b>	22	26	27	28	29	30	31	32	33	45	35	36	37	38	39	40
9540	9.7	2.9	10.5	3.2	6.7	2.9	10.7	3.2					2.6	.046				
9541	<b>8</b> 0.00	2.7	9.5	2.8	9.5	2.8	9.5	2.8					2.3	.040				
9544	11.3	3.4	16.7	5.1	16.1	6.4	16.4	5.0					4.6	. 989				
9546	10.0	 -	10.4	3.2	9.5	2.9	10.0	3.0					2.2	.038				
9549	12.8	G. 1	13.2	<b>4</b>	1.7	J.6	13.9	4.5					ر ا ا	.058				
900			÷ ;	بن بن بر	<b>6</b>	2.7	19.4	 					2.5	.044				
9557	. 5. 6. 6.	- 4	12.4	- m	 	. n	12.2	3.7					3.5	.057				
9558	7.9	2.4	10.4		8	2.2	9.1	2.8					2.4	.041				
9562	12.6	3.8	12.9	3.9	13.2	<b>6</b> .	13.5	<del>-</del>					3.3	.057				
9563	8.8	2.7	19.7	3.3	10.9	3.3	10.8	3.3					2.5	.044				
9567	80 ( 80 (	2.7	<b>.</b>	2.8	D	2.8	9.5	2.8					2.5	.043				
9268	6.7	5. <b>0</b>		9.0	<del>-</del> (	, i	6.7	9.6					1.7	.030				
9572	7.6	- 0	- 6	. 4	7. 6	0.7	0.0	2.0						.037				
9573	7.2	2.5	10.0	٦. ت	D.	2.8	10.1	J. 1					2.6	.045				
9574	9.6	2.8	10.2	3.1	11.0	3.3	10.6	3.5	10.6	3.2			2.2	. 038				
9276	<b>9</b>	5.9		2.8	10.5	3.2	10.3	J. 1					2.9	. 050				
9578	<b>6</b> 0 ·	2.7	10.4	3.5	9.5	2.8	ω. •	J. 6					2.3	.041				
8/08	7.5		- 1	B (	ø.	9.7		50, F					<b>*</b>	.024				
9566	10.5 7.7	. 4.	9.5	S 69	4.0	5.5 5.7	12.1 9.2	2.8					2 . 2 . 6	. <del>0</del> 36 . 036				
9585	4.6	5.9	8.8	2.7	8. 8.	5.6	8.7	2.7					2.2	.038				
9586	10.2	3.1	11.7	3.6	12.1	3.7	11.9	3.6					2.8	.049				
9588	<del>*</del> :	بر دن	7.6	<b>0</b> 0	 	4.0	10.5	3.5					2.5	.044				
200		9 0	0.7.	, e	2.5	7 .	- r						۴ ۳ ن د	909.				
9594		. e.	 	- 7. 7.7	. o.	2.6	. <del>4</del> .	. 6 . 6					2.9	. 036 . 036				
9595	19.7	3.3	12.7	8.5	14.6	4.4	13.6	<b>-</b>					3.5	.061				
9236	10.6	3.2	10.1	3.1	10.0	3.0	9.7	3.0					2.4	. 042				
9597	12.5	3.8	10.9	3.3	14.0	4.3	12.3	3.9					2.9	. 920				
9643	13.9	4.2	15.0	4.6	16.3	5.0	15.7	<b>4</b> .8					9.0	. 969				
9645	<b>2</b> .8	3.6	13.6	•	14.3	<b>4</b> .	- <del>-</del>	4.3					3.7	. 965				
9649	3.2	<b>6</b> .	න හි. අ	9 .6	4	2.3	7.9	5.4					2.1	.037				
9656	÷ :	 	. de	2.6	2.5	S. 5	5. T	4.6					7.7	848				
1005	7:-	٥.٥	ž.	4.2	13.2	<b>.</b>	- · <u>*</u>	÷.					0.0	999.				

																																					C	bc	e	60	)4:	2	
*	5	RAD	19	.148	028	.054	. 140	. 038	.012	. 965	.054	. 110	. 120	. 188	131	.073	.051	.080	. 140	. 654	. 982	. 986	059	. 204	.005	.056	.197	2/0.	38.	Caa.	3	959.	.073	919	.10	033	.010	.016	038	. 995	. 942	. 061	028
YAW	AT TD	DEG	60	8.5	9.1-	J. 7	8.0	2.2	۲.	3.7	3.1	6.3	6.9	10.8	7.5	4.2	2.9	4.6	8.0	J. 7	4.7	€.	4.5-	11.7	ij	3.2	1.3	- ·	ر. د. د	, i	٠,	<u>.</u> .	4.2		6.3	9.1	9.	o.	-2.5	r.	7.4		9.
F. P. A.	5	RAD	53	966	002	092	052	059	056	024	684	051	049	089	110	092	080	103	686	070	091	108	030	143	058	1.091	- 119	066	4.1.4 4.0.6	888	122	7/0'-	089	058	075	.040	058	. 021	. 005	030	017	072	054
Ľ.	AT TD	DEC	28	.3.8	- - -	_	-3.8	-3.4	-3.2			-2.9		-5.1		-5.3	-4.6	-5.9												ه ه								1.2			_		
ROLL RATE	5	RAD	22	. 187	.070	. 649	. 603	694	. 028		176	. 136	. 926 .					138	.113	106	021																	016					124
ROLL	Υ	DEG	26	19.7	<b>4</b> .0	2.8	7.	-5.4	9.	3.6	-	7.8	1.5	9.8	<b>®</b> .	-4.2	-1.6	-7.9	6.5	- <del>9</del>	-1.2	5.7										<b>+</b> !	9.3			30.3					80	_	89 89
PITCH RATE	10	RAD	22	0.000	. 024	. 023	092	. 082	.044	.056	106-10	. 009	0.000	.051	. 040	058	005		. 051			023	086	0.000	. 009	.010	.035-12.7		. 082		.084-10.9	00/	113				0.000				0.000	.061-11.	. 068
PITCH	¥	OEG	\$	9.9	<del>+</del> .	1.3	-5.3	4.7	2.5	3.2	-6.1	ĸ.	9.9	2.9	2.3										ιú	φ.			4.7	7.6										2.9	0.0	3.5	ر 9.
	1.	RAD	53		. 638																																						
W 	1	DEG	25		2.5																																						
z		RAD	51																																								
۲ >	8	DEG	20																																								
ROL	_	RAD	6	.010	.009	017	005	. 023	007	. 021	. 063	003	9.66	016	. 026	. 682	600.	.014	. 136	010	. 005	009	037	. 005	016	035	.010	929.	129.	9.65 6.65 6.65	6/9.	179.	023	.033	021	152	. 033	9.999	009	.037	002	.040	.044
	10	DEG	48	<b>ب</b>	'n	1.0	. S.	<b>1</b> .3	4.1	1.2		2 -	9.9	6.1	5.5	4.7	ĸ.	₩.	7.8	9.							ا بع							ص. ا	~		o.			-	ı.	2.3	2.5
		RAD	41		110	•																	•			•				•			•		•	•							
) L	9.6	DEC	9		6.3																																						
z <		<b>Z</b>	\$																																								
¥ O	8	DEG	‡																																								
P 1 4	_	RAD	\$	.075	. 106	. 063	.070	.077	.115	.070	. 075	.079	. 023	996.	. 072	. 091	<b>. 6</b> 94	. 103	.061	. 058	. 949	860.	. 106	. 687	. 092	. 986	.075	.075	7/0.	9/9		199	.094	. 979	.068	.070	. 692	. 684	. 084	. 968	. 059	.077	. 679
	5	DEG	42	4.3	<b>.</b>	3.6	4.0	<b>+</b> . <b>+</b>	9.9	4.0	4.3	<b>4</b> .5	٠. دي	ы. В.	<del>-</del>	5.2	5.4	8. 8.	3.5	3.3	2.8	5.6	6.1	5.0	5.3	o. +	<b>4</b> .	. d	•	<b>.</b>	4.	•	4.6	<b>4</b> .	9. 6.	<b>4</b> .0	5.3	<b>4</b> .8	<b>4</b> .8	3.9	4.6	<b>†</b> .	4.5
LNDG	2		ŧ	8393	8398	8643	9386	9389	9390	9391	9395	9396	9398	9400	9401	9406	9468	9410	9416	9417	9418	9419	9420	9424	9425	9431	9432	9435	9446	9452	9466	9216	9511	9516	9518	9521	9524	9531	9532	3	9536	9537	9538

13410 Code 6042

																																					C	od	e
3	2	RAD	61	. 089	.119	.033	. 883	014	044	. 194	.127	9.999	. 030	056	.112	.098	.145	021	038	077	.037	072	007	. 005	047	026	. 044	. 026	995	044	. 072	.044	. 005	016	.049	960.	. 080	.140	. 636
YAW	AT TD	DEG	99	5.1	8.9	6.	7.	8.		<del>-</del> -					4.9	9.6	8.3				2.1			۳.	-2.7	-1.5	2.5	5	٦.	-2.5	<del>-</del> :	2.5	r.	6.1	2.8	5.5	<b>4</b> .6	8	1.7
₹	5	RAD	53	045	065	105	052	051	033	161	063	.031	044	037	066	070	119	042	035	026	035	017	077	063	042	049	087	070	033	047	161	- 699	059	049	082	986	087	677	086
я. 9.	Y	DEC	58	-2.6											-3.8	-4.9		-2.4		- 5.	- 0.7-	-1.0	4.4		-2.4 -	-2.8		-4.0					-4.5-		-4.7	- 6.4	-5.0	4.	6.4
ROLL RATE	10	RAD	57				- 689	136 -										. 157		675 -	954 -	. 106 -													143 -		. 103 -	_	031 -
ROLL	<b>Y</b>	DEG	26	- 6.1-			5.1				3.5	14.9		-1.0				<b>0</b> .6				6.1		7.3	1.7			-9.6									5.9	G	80.
PITCH RATE	10	RAD	22	0.000		045				. 059				- 600 -	. 944	.059-15.1	. 673	. 003		. 619		.045	. 103	. 009	044		033 ·	. 689	014	014	.038-12.4	.040-10.	.024 -2.5	066-22.5	010		. 698		. 047
PITCH	A	DEG	54		0.0		۲.	2.0	1.8						2.5	4.6	4.5			<del>-</del> :		5.6	5.9								2.2	2.3		.8.5	9.	ņ		0.0	2.7
	£ £	RAD	53																	.024																			
ר ה	u.	DEG	52																	<b>+</b>																			
ე ჯ <b>≼</b>	£	RAD	51																																				
<b>ر</b> د	0	DEG	20																																				
8	10	RAD	49	963	. 003	.017	. 997	122	033	. 065	. 026	049	. 005	019	007	. 028	031	026	012	. 035	. 966	061	. 051	. 646	. 033	037	. 005	005	021	9.99	007	141	. 649	. 023	026	. 691	.012	059	019
	_	DEC	84	-3.6		6.	₹.	-7.0	-1.9	3.7	5.	-2.8	r.						7	7.0	3.8	-3.5	2.9	2.3	6.	-2.1	r.				<b>†</b>	- <b>8</b> .1	2.8	<del>1</del> .3	1.5	5.5	.7	4.5	
	<u>4</u> 4	RAD	41																	. 698																			
GLE	•	) DEG	46																	5.6																			
Z <	8	RAD	45																																				
C	Ö	) DEG	‡																																				
-	10	RAD .	\$	.065	.077	105	.072	.087	.680	. 682	.070	.070	.0 <b>84</b>	. 084	. 082	. 989	. 987	.687	<b>. 0</b> 94	101	. 984	. 689	.112	. 966	. 689	960.	. 698	. 686	. 691	.070	. 682	.075	.058	. 968	. 072	. 984	. 103	. 091	. 696
	<b>p</b>	DEG	42	3.7	+:+	9	<del>-</del> -	5.0	<b>+</b> .6	4.7	4.0	<b>4</b> .0	<b>*</b> .8	4.8	4.7	<b>4</b> .6	S. 0	5.0	5.4	S.8	4.8	5.1	4.9	3.8	5.1	5.5	5.6	4.6	5.5	4.0	4.7	4.3	J. J.	3.9	+:	4.8	5.9	5.2	5.5
LNDG	2		4	9548	9541	9544	9546	9549	9550	9552	9557	9558	9562	9563	9567	9568	9571	9572	9573	9574	9576	9578	9579	9586	9584	9585	9586	9588	9591	9592	9594	9595	9236	9597	9643	9645	9649	9656	9661

NIGHT LANDINGS

USS ENTERPRISE (CVN-65)

USS ENTERPRISE (CVN-65)

LANDING DATA - MODEL F-18A

DEPARTMENT OF THE NAVY Naval Air Development Center Warminster, PA 18974

																																					C	oa	le	0	04	2	
REREAD	NUMBER			\$	-	6	-	-	6	0	0	0	0	0	0	-	-	-	9	0	0	0	-	0	-	0	0	•	-	_	0	0	-	0	6	-	-	<b>©</b>	-	•	0	-	0
ARR GEAR	RUNOUTS	3	82	421.6	431.8	429.3	431.8	426.7	9.9	431.8	426.7	429.3	<b>9</b> .0	431.8	431.8	424.2	431.8	431.8	429.3	431.8	426.7	424.2	426.7	9.0	431.8	9.0	431.8	426.7	426.7	431.8	431.8	0.0	<b>0</b> .0	424.2	426.7	429.3	0.0	429.3	424.2	424.2	0.0	429.3	429.3
ARR	S.	Z	<b>∞</b>	166		169	179		0	170	168	169	0	179	170	167	170	170					168		170		-					•				169				167			169
ETRIC	SURE	MAN HG	80	759.5	759.5	761.2	759.5	759.5	759.5	759.5	759.5	759.5	759.5	759.5	759.5	759.5	759.5	759.5	759.7	759.7	759.7	759.7	759.7	759.5	759.5	759.5	759.5	759.5	759.5	759.5	759.5	759.5	759.5	760.0	760.0	760.0	760.0	760.	766.0	760.0	260	760.0	760.0
BAROMETRIC	PRESSURE	IN HG	79	29.90	29.90	29.97	29.90	29.90	29.90	29.90	29.90	29.90	29.30	29.90	29.90	29.90	29.90	29.90	29.91	29.91	29.91	29.91	29.91	29.90	29.90	29.90	29.30	29.90	29.90	29.30	29.90	29.90	29.90	29.92	29.92	29.92	29.92	29.92	29.92	29.92	29.92	29.92	29.92
TEMP		ပ	78	22	22	18	22	22	22	77	22	22	22	22	22	22	22	22	22	22	22	22	22	22	22	22	22	22	22	22	22	22	22	22	22	22	22	22	22	22	22	55	22
F		i.	77	71	7	65	7	7	7	7	7	7	2	7	7	7	7	7	7	7	7	2	7	7	7	7	7	7	7	7	7	7	7	7	7	7	7	7	7	7	7	7	7
DECK ROLL		RAD	76	.012	.012	. 009	033	005	031	016	003	600.	021	005	019	. 009	005	.012	.010	056	003	016	002	014	. 621	031	012	. 003	030	002	. 624	009	. 003	. 003	002	021	023	010	030	005	. 003	000.0	010
DEC		DEC	75	.7	.7	S.	6.	J. J.	1.8	6.1	2	ı.	-1.2	٦.	-	s.	٦.	.,	φ.	-3.2	2	9.1	7	8.	1.2	1.8	7	7	-1.7	ï	<b>+</b> .	5.5	7	۲.	ī	-1.2	1.3	9.	-1.7	. i.	4	9.0	9.1
DECK PITCH		RAD	7.	003	003	005	009	007	014	012	009	002	007	005	002	005	010	007	002	007	007	992	003	010	012	007	009	003	014	014	007	995	007	007	995	069	014	009	005	005	995	005	003
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SIDE	ġ		69	577	577	267	550	573	552	572	573	557	572	577	572	573	557	572	572	260	573	571	573	552	225	577	571	577	277	577	277	573	260	260	543	573	571	571	572	260	573	572	543
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RAMP	DIST	E	8	300	258	292	251	239	245	273	224	295	336	282	271	224	225	220	<b>700</b>	268	269	248	193	337	268	220	279	302	261	264	257	252	169	231	281	253	280	281	179	209	320	228	242
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DAY LANDINGS

USS ENTERPRISE (CM-65,

LANDING DATA - MODEL A-6

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DAY LANDINGS

USS ENTERPRISE (CVN-65,

LANDING DATA - MODEL A-6

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5.5 11.2 5.4	4.0	_	<b>.</b>		3.2	10.9	3.3			<del>-</del>	. 072	3.7	.065	19.6	6.0	14.2	4.3
2.5 7.9 2.4	7.4		4.0		2.5	- 9	2.5			2.8	.049	<b>5</b> .8	.048	13.5	<b>-</b> .	9.0	2.4
3.2 9.7 3.0 1		_	•		<b>9</b> .	6.6	<b>9</b> .0			3.7	. 964	4.5	. 059	17.3	5.3	11.7	3.6
3.0 9.3 2.8 1	2.8	_	•.		9.0	<b>9</b> .	8.8			3.5	. 062	J. 1	.054	18.1	5.5	13.4	+.
3.2 11.0 3.3 1	3.3	_	1.1		4.6	10.8	3.3			4.0	. 059	0. 0.	. <b>46</b> 2	16.9	5.2	<b>4</b> . E	3.5
5.3 9.3 2.8	2.8		6.7		9.0	S	<b>5</b> .8			3.1	. 055	0. 0.	.053	15.8	4.8	16.7	3.3
2.5 9.6 2.7 1	2.7	_	<b>.</b>		<b>6</b> .0	9.0	5.8			2.9	. 651	3.2	.056	14.1	4.3	8.3	2.5
2.9 10.6 3.2	3.2		<b>9</b> .		5.9	19.1	<del>ر</del> .			3.2	. 056	4.6	. 059	17.1	5.2	12.2	3.7
2.4 8.9 2.7	2.7		-		2.5	<b>8</b> .5	2.6	<b>8</b> . <b>8</b>	9. 9.	3.3	.058	<b>8</b> .0	.052	15.2	4.6	10.0	8.9
2.3 11.2 3.4 1	4.6	_	<b>•</b> :=		3.3	10.8	3.3			3,3	.058	3.8	990.	14.3	4.4	<u>.</u>	2.8
1.7 11.4 3.5	3.5		<b>†</b>		5.9	10.4	3.2			3,3	. 057	4.5	.059	15.6	4.0	10.4	3.2
2.6 9.0 2.7	2.7		<b>.</b>		<b>5</b> .8	<b>.</b>	2.8			4.0	. 969	3.0	.053	15.8	4.8	19.6	3.2
2.8 10.5 3.2 1	3.2	3.2 10.0	•		J. 7	10.3	٦.			3.2	. 056	J. 5	.061	18.0	S. S	12.5	S. S.
2.2 7.7 2.4	7.4	2.4 7.6	7.6		2.3	7.7	2.3			3.1	. 854	7. 9.	.045	<b>4</b> .0	4.5	9.0	7.9
1.2 11.1 3.4 1	4.6	3.4 11.0	=		3.3	10.9	J. 5			5.5	. 057	S. B	.067	15.4	4.7	10.3	 
3.0 12.6 3.8 1	3.8	3.8 11.2	11.2		4.0	11.3	4.5			3.7	<b>.064</b>	3.9	. 968	17.8	5.4	12.5	<b>8</b> 9.
1.9 9.5 2.9	2.9	2.9 9.8	8.0		O.S	9.7	2.9			3.5	999.	4.6	999	16.8	5.1	11.5	3.5
2.1 6.6 2.0	2.0	2.0 6.8	8.8		2.1	6.7	<b>7</b> .0			2.5	.043	2.3	.041	12.6	a.8	7.3	2.5
2.4 9.4 2.9 1	2.9	2.9 10.1	<b>.</b>		J. 7	Ø.	۵. د.			3.2	. 855	J. J	.058	12.9	Ø. N	7.5	2.3
2.0 7.2 2.2	2.2	2.2 7.0	7.0		2.7	7.1	7.7			2.8	.049	<b>0</b> .	. 033	16.6	5.4	11.1	4.0
6.6 2.0 6.9 2.7 9.2	2.7	2.7 9.2	9.2		<b>5.8</b>	<b>.</b>	2.7			3.0	.053	2.7	.047	15.9	4.8	<b>9</b> . E	3.3
2.4 7.5 2.3	2.3	2.3 7.3	7.3		2.2	7.4	2.3			2.7	. 048	2.0	. 035	18.2	5.5	13.2	4.0

		3	LADING DAT	1	MODEL A	Į		uss i	MEDA	USS ENTERPRISE (CVN-65)	M−65)			8	DAY LANDINGS	SOM				
		-	T U	Z <	9 1 6			<b>6</b> 2	ب د	O N V			PITCH RATE	RATE	ROLL RATE	RATE	F. P. A.	÷	YAN	
2	2		8		t			5		8	i.		¥	5	7	2	AT TA	2	AT TD	۵
	930	3	930	3	9	3	930	2	930	3	DEG	2	9	3	DEC	2	930	3	DEG	3
<b>‡</b>	7	3	\$	\$	\$	<b>\$</b>	\$	\$	8	5	25	3	\$	22	88	22	8	80	3	5
3	•	=	9.7	. 1 68	7.9	33	ī	862	-2.8	e.	r.	. 965	1.2	.021	9.9	.120 -2	-2.9 -	051	2.3	3
Ξ	7.0	22		176			7.7		<b>.</b>	•				663	0.4					623
2 2 2	• •	- 5 - 5 - 5	9. <u>e</u>	<b>8</b>			7.7	3	? -					662				052	2.3	946
75		7 7	9 -	297					-2.0	- 851			. 4	•	 -1.4.	. 924 	0.7	2 9 6 1 1 9 6 5		0 6
2	•	175	0.		10.0	.175	 8:	.026			-:	919	2.2		. 10	- 1961		658	4.6	929
7	60 t	3	- : - :	<b>Ž</b> :		•		017	-2.2	036			-:	1	~				~	038
7.5		2 2	•	5 2			7.5	2	? ?					.0/2 1. 	,	2.00.		1.055	y -	
176	9.7	2	•	175	4.0	.164	2.5	3		.012	2.7	.047	•	410	. +			963		.0.
171	4.0	147	5.9	31.		•		023	-2.4	042			9.0	9-9-9	3.5			075		.005
2		8 8 9	<b>.</b>	164		•		021	i.	. 969		1		084	5.1					. 69
<b>B</b> :	•	<b>*</b> • • • • • • • • • • • • • • • • • • •	D P					023	7.6			1		056	* ·		֡֞֝֝֝֝֜֝֝֝֝֝֝֝ ֓֓֞֞֞֞֞֞֜֞֞֜֞֜֞֞֜֞֞֩֞֩֞֜֞֞֩֞֞֩֞֞֩			1.691
<u> </u>	*	2 2	. 0	22			? ?! ! !	8 8	<del>.</del> •.	. 6				919	1 . 1 . 2	. 621		. 856.	! * * *	
<b>5</b>	8.4	.147	9.6	.168			•	.016	3.1	.054		·	_						•	968
187	7.2	126	19.7	.187			₹.	.00	о. Р	.052				٠	_					063
2 :		<u> </u>		3 3		•	r: -	026	<b>7.</b> •	. 642				. <del>.</del> .	Δ.	48 	n 1		- •	<del>0</del> 54
9 6		5		3		•		910	2.2	63.0				•		1 959 -		1,0/4	ا و او	- 687
197	9.0	8	8.2	3				- 98		.031		-	. 7			984				042
198	8.3	£ .	•••	.175				002	<b>+</b> :	. 024			e: •					-		686
2 3		<u>.</u>	• !	.157			<b>.</b>	<b>5</b>		916			2.5	_						<u>.</u>
218		25		7 5			2.2	638	5.4	. 6.66 			S. 5.	942	-2.7		, i	. 400 400 1	5 6 6 6 6	99.
217	8.2	3	•	1.00				.637	P. 7-	031			•		_			956 -		023
218	9.0	7	2.5	821		•	4	021	7.9	5. 5.			•	- 898	_			019	1.7	50
222				55		•	• • • •	<del>.</del> .		1.014		-	9 ·		) • • •	. 166 	-2.7	637	• •	
222		3		.157			*	007	2.6	945				9.00.0	_	900.0		- 940	4.	929
224	6.5	5	9.2	.161				010	3.3	.058				9.00						845
225	8.9	119	9.7	. 169		•		851	2.7	.047				. 619				051	3.8	990.
226	7.1	124	•	.157			<b>9</b> .	.028		012				.044-10.0				079	D	.130
/22		7201.	? • •	201.		•			- r	200.				900	. ·	. 010	1   2   7	809. 1	 	608
2 6			7	187				196		566			1.0	942	•			973	4	466
236		=	6.3	.162			2.5	440	-1.7	030		•	· m	014			٠	075	7.4	129
231	8.8	\$	9.2	161		•	-2.5	044	₹.	.007			•	0.000			•	031	5.4	<b>. 6</b> 94
233	n (	£ :	7.6	169			i,	. 665	 	028		T	-2.0		<b>.</b>			036	4.5	.079
234	?	.162	D.	.171			•	.012	+	007		-	60	9.000	6. 6.	999	-3.2	056	6.2	. 108

		3	LAND ING DAT	3 · · · · · ·	NOOEL A-6	4		uss e	ITERPR	USS ENTERPRISE (CVN-65)	N-65)			ð	DAY LANDINGS	INCS				
200			<b>x</b>	9 Z <	<b>.</b>			30 7	_	A N G L	ш		PITCH RATE	RATE	ROLL RATE	RATE	F. P. A.	خ ٠	YAW	_
£	2		8		Ŀ		£	•	8	~	#		¥	5	¥	Đ	AT TD	2	AT TO	و
	950	3	DEC	3	DEC	3	950	3	DEC	2	DEG	2	DEC	8	DEG	3	DEG	3	950	3
=	42	3	\$	\$	\$	<b>‡</b>	\$	6	8	5	25	S	\$	55	20	57	3	8	2	5
238	•	185		173			•	910	•	007			_	9.00	1.3	.023 -2	-2.2 -	638	3.7	. 065
236	7.6	-	10.5	35				016	4.7	. 082		7				600	-		9	689
237	•		. 8.					.003							:	-	٠		_	035
278	•		7.8		<b>6</b> .0	.120	-2.2	036	2.8	1				059		-	7.5-	-	•	068
230	•	•	B.		<b>9.</b> 0	171	•:	.017			1.2	. 021 -	ł			ese.	i 0:		-2.9 -	051
<b>3</b>	•		9.7	169			'n	<b>6</b>	. 2.	995		-,				963 L	i •:	676	≠.	.007
242	•		•	162			•	900	'n	<b>66</b>		••	• •				•	070	<del>-</del> .	. 662
25	•	•	•	8				. 963	2	. 963			<b>.</b> .				•	_		033
<b>544</b>	٠	•		3		•	_	026	ø.	.016		•	2.5		~	- 939 -		_	e: T	033
110	•		7.4	129		•	-2.3	040	2.9	. 051		-,	-		1.7.	054 -3.	Ċ	065	• •	007
419	•	•	•	8			9.	010	B. I	014			_				٠	063		010
420	•		•	191		•		021	_	016		•,			~			•		035
422	٠	•	•	200		١	- 7.5	021	9.	.033		_		•	•			Ī		019
425	•			.147			<b>+</b> :-	. 024	Ξ.						5. B.		•			. 092
426	٠				7.8	138						023 -:					٠		5.5	896
427	•			<u>\$</u>			2.8	•	. 5.	026		'n			ı		•	051	-	. 002
428	•		•	166			• •			. 002		ï	_		10.5		•	079	5.6	.045
<b>7</b>	•		•	161			<b>-</b> .			026				966.	9		_			. 075
\$	•	•	*.	<u>.</u>			9		-2.3	040		_		9.00	<b>9</b> .2		_	_		638
<b>3</b>	٠	-	•	176				967	'n	8		•		9.00	'n		_		-	838
5	•		٠	161			2.8	949.		014		ī		031	+:-		1 - T	072		014
7	•		٠	166			3.5	.961		012			-		•.			966	2.3	.040
‡	•			99				965	ŗ	. 012		•		- 110	6. T				_	014
3	٠	•		3			<del>.</del>	.031	. 0.1	010		•	9.9	6.886 -1	~	021 -4.	_		_	017
1	٠	•	.3	8		•		021	5.5	. 026					7.0.7	063 -3	_	954	_	054
<b>\$</b>	•	•		\$		•	_			. 045		••	_	.045	=	.019 -3.0	_		-	672
<del>5</del>	•		8.7	152					- 1.1	636		.,			•		_		3.B	996.
3	•		9.2	161		•	6.17	033		662		_	9.0	966.	۲.	.012	_	873	٠	966

REREAD	NUMBER			•	•	•	_	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	-	•
ARR CEAR	RUNOUTS	3	82	429.3	428.7	426.7	431.8	428.7	426.7	429.3	429.3	426.7	426.7	426.7	429.3	429.3	424.2	429.3	426.7	426.7	<b>6</b> .	431.8	428.7	428.7	424.2	426.7	426.7	429.3	429.3	429.3	429.3
\$	Ş	Z	5	169	3	5	170	3	5	169	169	5	<b>89</b>	<b>5</b>	169	169	167	169	168	<b>2</b>	•	170	168	168	167	8	<b>5</b>	169	169	169	169
ETRIC	SURE	오 로	2	763.3	763.3	763.3	763.3	763.3	763.3	763.3	763.3	763.3	760.2	760.2	760.2	769.2	760.2	769.2	760.2	769.2	768.2	761.2	761.2	761.2	761.2	761.2	761.2	761.2	761.2	761.2	761.2
BAROMETRIC	PRESSURE	N H	78	89.93	<b>8</b> .	30.05	30.05	30.02 00.00	30.05	80.02	30.05	30.05	29.93	29.83	29.83	29.93	29.93	29.93	29.93	29.93	29.83	29.87	29.97	29.87	29.87	29.97	29.97	29.97	29.97	29.97	29.97
154		ပ	28	<u>.</u>	2	2	<u>•</u>	2	<u>=</u>	2	2	2	1	1	1	7	1	1	1	1	1	17	12	1	17	12	1	17	1	1	12
=		<b>L</b> .	4	67	\$	67	67	67	67	67	67	67	62	62	62	62	62	62	62	62	62	62	62	62	62	62	62	62	62	62	62
DECK ROLL		3	76		28.	900.	002	.016	910			. 667	005	995		005	005	995	005	665	005	005	005	005	005	005			040	024	. 838
<u> </u>		DEC	22		7	•	7	œ.	œ.			₹.	7	7		7	7	<u>.</u>	J		٦.	2.1	J		. i	3			-2.3	<b>₹</b> .	2.5
DECK PITCH		3	*		<b>8</b>	007	667	003	002			900.	<b>9</b> . 999	900.		999	9.66	900.0	9.99	909.	999.	9.99	9.99	9.66	999.	900.			667	665	007
ECK		DEG	22		r;	<b>+</b> :	<b>+</b> :	2	-			•	•.	0.0		•	•	<b>6</b> .	6.9	9.0	•	0.0	6.0	9.0	•	9.6			4.	ا. د	<b>+</b>
_	B	Ş	27	7	7	7	~	~	7	7	7	7	~	7	~	~	7	~	~	7	~	~	~	~	~	'n	~	7	~	~	~
<b>E</b>	SPEED	\$	۲	*	*	*	*	•	•	*	•	*	*	*	*	4	*	*	*	4	*	*	•	*	*	*	*	*	*	*	*
3	300		2																												
8	TYPE		2	50120	56123	50120	50120	56128	56123	50120	50120		56188	56188	36198	<b>Sei 38</b>	50200	56128	50200	50120	50120	50120	50120	56288	50100	50120	50120	56126	56126	56200	56166
SIDE	₹		2	2	822	623	85	823	823	2	853	3	821	\$	820	2	821	822	828	3	2	8	2	822	821	828	822	821	2	821	2
WIRE	Š		6	n	n	~	n	~	~	n	n	*	*	*	*	n	*	7	n	n	n	*	n	4	*	n	*	~	n	n	*
5 5	ANCE	=	8	8	8	7	81	2	2	8	8	78	2	3	2	2	2	F	22	2	1	ž	5	2	5	5	3	2	87	8	23
OT OT SAMA	DISTANCE	t	2	35	264	23	286	259	275	261	35	256	282	273	278	<b>7</b>	787	252	238	265	<b>5</b> 2	<b>8</b>	265	259	<b>368</b>	<b>700</b>	<b>50</b>	225	<b>797</b>	266	317
<b>E</b>	KCE	3	3	7	7	7	7	?	7	†	?	1	7	†	۲	7	†	7	†	†	1	7	?	Ť	7	7	7	7	1	1	7
OFF-CENTER	DISTANCE	E	3	7	Ŧ	2-	Ŧ	-	Ŧ	<del>-</del>	-	7	=	<del>+</del>	7	=	<del>*</del>	ę	-12	-12	-5	7	7	-12	•	F	=	-12	-12	7	=
995	8		2	238	2	237	238	23	<b>3</b>	242	243	74	<b>9</b> :	419	<b>4</b> 2 <b>0</b>	422	425	426	427	428	<u> </u>	\$	2	5	3	\$	3	<b>11</b>	<b>4</b> 5	<del>1</del> 9	3

DAY LANDINGS

USS ENTERPRISE (CVN-65)

LANDING DATA - MODEL A-6

## **A-6 NIGHT**

	WEIGHT		S K	21	15150	15196	15150	14878	15876	15785	15105	15241	15876	15876	15/63	15422	15649	15150	14969	15422	15876	15150	15878	15876	15695	15967	16148	15105	15241	15196	19801	15468	9/961	15876	15876	15876	15831	15649	
	WE		SBJ	<b>50</b>	33400	33500	33400	32800	35000	34800	33300	33600	35000	35888	34000	34000	34500	33400	33888	34000	35999	33400	33200	3:300	34600	35200	35600	33300	33600	33500	35266	34100	99900	34000	35999	35000	34900	34500	
AND I NGS	111	<u>.</u>		<b>2</b>			;	. J							•	2			1.00				1.20			1.00										1.00		1.00	
NIGHT LANDINGS	LIA	5		₽	1.86	- - - -	1.10	9.7	99. 96.	1.00	1.10	1.00	- 1 - 1			6. 1	1.10	1.10	- . 96	<b>-</b>	96	 	97.		- 98	96.	1.10	1.00		1.10	J. 1	<b>8</b> .	8.	9. 6	1.00	000	96.	1.00	- 20
	\$	<b>∀</b> .ds		11																																			
	KVPA	Z		•	1.09	1.09	1.16	* :		1.09	1.15	<b>1</b> . <b>1</b>	<u>*</u>	1.20	9.	1.14		1.15	1.19	7.13	1.13	1.12		1.15	1.12	1.1	1.19	1.15	- 60	<del>*</del> :	2 :	1.18	9 !	7.1			1.15	1.21	77.
82)	V.dSA		K/S	ŧ.																																			
<del>√</del> (C <del></del>	Š		₹	=																																			
3518	VPAMIN		\$	5	57	57	57	ž :	ဂို ဆို	8	88	21	8	8	מ מ	3 6	5	57	56	27	8	2	ה מ	8 8	80	<b>28</b>	8	26	27	22	<b>8</b>	2	ים ה	n N	8 %	8	28	57	20
41 ERP	È		₹	7	=======================================	10	110	60	18/	112	109	=======================================	112	= = =	7 :	Ξ	Ξ	110	109	111	112	= :	2 5	112	112	133	113	109	=	110	2	Ξ:	71.	112	112	112	112	= ;	202
USS ENTERPRISE (CVN-65)	VEOR		M/S	Ξ																																			
	>		₹	•																																			
_		PERP.	Ş	•	~	~	~	N (	~ ~	~	~	~	~	~ ‹	<b>Y</b> (	٠,	· ~	~	~	~	~	~ (	٠,	٠ ~	~	~	n	ריו	r) .	<b>m</b> (	7	י מ	3 (	n ×	n	מי	n	n ,	-
NG DATA - MODEL A-6	WIND-VEL	2	₹	•	*	4	◆ ·	•	* *	*	*	*	∢ .	• •	• •	•	*	4	*	4	4	•	• <	*	*	*	80	ß	<b>S</b>	n ·	•	ימ	ימ	<b>.</b>	•	•	•	•	×
<u> </u>	MIN	P.	Ş	^	7	12	2	7	2 2	2	~	2	~	2:	2 5	2 💆	2	2	2	2	2	2:	2 =	2 2	2	2	2	2	2	2	7	2 :	2 :	5 ¥	=	<b>.</b>	9	<b>9</b> :	<u>*</u>
MTA -		•	\$	•	<b>5</b>	<b>54</b>	55	Ż.	* *	74	74	7	*	* 6	g K	3 2	23	23	22	22	23	2	3 %	2 2	23	23	2	<b>5</b> 8	78	22	74	2 5	3	2 5	3	32	32	32	17
NG NG	FILM		Ş	80	\$	Ş	3	5	, 100 m	5	22	22	3	5 5	7	3 5	3	22	3	22	22	8 :	5 5	3	2	2	2	2	9	5	3	3 5	7	5	. S	<b>4</b>	8	53	D C
	VE-F		₹	•	8	ä	3	2	2 2	8	102	≘	2	= 2		<u> </u>	5	•	<u>=</u>	=	102	8 8	2	<b>3</b>	2	2	6	2	Š	2	2	£ :		<u> </u>	6	: <b>S</b>	8		2
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	\$	-	\$	~	=	200	127	*21	122	123	126	52	128	2		126	128	126	129	126	127	22	2 5	128	125	125	125	126	120	126	127	5	2	132	120	127	129	135	125
	2005	ě		_	8	<b>\bar{2}</b>	200			9	<u>=</u>	9012	2	2 2		9 6	9621	9022	9623	9624	9625	9626	/700	9629	9636	9032	9634	9649	9046	9947	70	9657	/918		2	9113	9115	9117	3000

NICHT LANDINGS

997			AIRCRAFT	-	SINKING SPEED AT TOUCHDOWN	)EED A	T TOUCH	NMOC		Ū	GLIDE PATH ANGLE AT TD	АТН А	NGLE A	T 10	WHEEL HEIGHT	EIGHT	HOOH	HOOK HEIGHT
ş	2	NOSE	PORT	R	STBO	8	AVG	<i>(</i> 3	FREE-FLIGHT	19H		•	<b>§</b>	>	OVER R	RAMP	OVER.	OVER RAMP
	2	\$	2	Ş	2,3	\$	Ş	¥	F/S	N/S	DEC	3	DEC	8	E	3	E	3
22	23	*	23	<b>38</b>	27	28	29	8	2	32	33	*	25	38	37	80	39	<b>\$</b>
8	7.8	2.4	12.8	3.0	12.7	8.0	12.8	8.0					•	.679				
2 0 0 0 0	2 0	2.5	. e	• · ·	7.7	2.5	13.0 0.7	9 · 6					- <del>-</del>	.6/2				
9003	7.7	4.		2.9	5.0	2.9	9.5	2.8	10.3	3.1			2.7	.047				
9000		2.3	10.2	3.1	0.0	3.0	10.1	3.1					3.0	.052				
	- r		2:3		*:		5.5	- (					- (	. 67				
2	15.3	4.7	15.0	. 4	4.4.	- *	7.7	4.5					· +	. 676 . 676				
9012	10.5	3.2	11.6	3.5	10.0	3.3	11.3	4.5					3.3	.058				
200	<b>8</b> .0	2.5	7.7	2.4	8.8	2.7	9.4	2.6					2.2	.039				
5 5		8 °	ø •	, v	 	7.5	9. 0 8. 8	- 6					2.6	. 045 851				
2 2	10.2		7.3	2.2		2.5	7.2	2.5	9.7	2.9			. 60.	189.				
9019	11.7	9.0	13.2	4	12.2	3.7	12.7	8.5		) 			4.4	.078				
9621	8.3	2.5	10.4	3.2	10.5	3.2	10.4	3.2					3.6	.064				
9622	7.4	<b>-</b>	14.4	4.4	7.5	<b>+</b> •	14.5	<b>+</b> ·	,	1			G	. 988				
9623	<b>10.</b> 3		<b>10</b> .5	n :	6.7	9 O	19.1	۳ ر ا	S.	<b>5</b> .8			ا د ن	.061				
<b>729.</b>		· .	7.01		9 :	2.2	• • • •	3.2					\	. 665				
<b>96</b> 29	1. t. c	+ E	12.0	0 P	11.4	5 K	5.E	9 6					4 4 U N	. 87.9 87.5				
9627	11.7	9	7.0	2.9	5.5	3.2	10.1	. n	10.4	3.2			3.6	. 963				
9628	-	2.8	=	4.6	1.0	3.2	10.8	3.3					3.5	.061				
9029	8.1	2.5	12.2	3.7	11.8	3.6	12.0	3.7					<del>-</del> -	.071				
2	16.7	n.	12.1	7.7	4.5.	<del>-</del> (	12.8	e	•	,			4. i	.079				
729.0		0. ¥		-		- 4	 	• • •	7.4	? <u> </u>			9 . V	CC0.				
96	5.7	1.7	-	2.8	9	2.9	4.0	. 6.					4.6	.059				
9046	10.9	3.3	12.0	3.7	10.4	3.2	11.2	4.0					4.2	. 974				
9647	9.0	J. 0	9.1	2.8	<b>9</b> .1	2.8	<b>.</b>	2.8					3.0	. 052				
200	1.9	9. 9.	1.5	n.0	12.2	3.7	11.8	3.6					3.8	990.				
9657	10.1	٠, ا	10.5	3.2	<b>6</b> .5	2.8	10.1	J.,					٦.٠	. 055				
9107	7.3	2.7		2.6	16.3	 	6.7	2.7					2.9	.651				
<b>8</b> :		8 F	- 6	, r		2.7	٠. د.	8, 5						.855				
2 2 2		, ,		, w	;;	) M		, . , .					) ii	.65. 196.				
9113	4.		. 4	. 6	7.5	2.5	3	2,5	6.9	2.1			2 2	.040				
9115	5.3		11.2	4.0	10.6	3.2	=	4,0	, , ,	, , 			3.6	.062				
9117	7.5	2.3	10.3	3.1	6.6	3.0	10.1	3.1	10.2	3.1			2.7	.047				
9559	19.1	٦. -	10.7	J.	12.0	3.7	11.9	3. 8					ري 60	.067				

		3	LANDING DATA	1	MODEL A	Ģ	_	USS ENTERPRISE (CVN-65)	ERPRIS	<b>ξ</b> (ζ	-65)			ž	NIGHT LANDINGS	DINGS					
995		P 1 7	ĭ	Z	<b>.</b>			ROL	- - -	Z C	w	•	PITCH RATE	RATE	ROLL RATE	MTE	9.	خ.	YAW	*	
£	5		8		*		2		8		4		7	5	AT	ē	OT TA	2	AT TD	2	
	930	3	930	2	DEC	3	DEG	3	DEG	3	DEC	2	DEC	3	DEG	2	DEG	2	DEC	3	
<b>∓</b>	7	2	‡	\$	\$	14	\$	<b>6</b>	95	5	25	3	\$	22	26	57	88	28	9	5	
*	9.7	99					•	.014				7	7	.073	€0.	.014 -2	•	.045	2.3	.040	
198	9.0	5. 5.				•	2	. 003				-	ĸ.	. 926	<u>-</u>		*	042	4.7	. 682	
9992		<b>Ξ</b>					1.6	. 028				*	<b>e</b>	. 984			۲.	647	5.3	.092	
5000		162		_	.7.	8	2.3	. 040		7	2.1	637 4	۲.	.082	•			030	4.6	.059	
		3 5					۲. ر د د	.030				ī	ا دې چ	. 416. . 716.	6 ¢	935 -2 928 -3	<b>.</b> -	1.049 1.954		. I.S.	
•		3					•	8						710	•		. ^	- 965	- 7	012	
1	4.0	112					•	.00				•	•	9.99	•		•	635	۲. ۲.	.054	
2012	9.6	58				Υ	.7	. 065				•	•			<b>659</b> -3		966	۱. و	014	
513	9.0	154				•	2.6	. 845				6	•		-3.9		-	072	<del>-</del>	.019	
519	7.2	126					1.2	. 921				80	<b>10</b> .	191.	 6.1	986 -3				860.	
7190	6.2	99						. 005				•	ø.	.129 -4	•			•		049	
818	7.7	134		~	6.6	154		. 966		7	2.3	949 3	•	_	j.		-1.2 -	921	J. 1	.054	
2 2		117						. 838				7	ø.	963 5	<b>-</b> .		•	026	3.7	. 965	
100		7				Ī		023				i		002			•	- 635	÷.	.072	
9622		157		•				<b>10</b> .		•				014			•	<b>9</b> 35	. u	960.	
9623		3			7.5	121		.017		-	- -	919 9					•			124	
\$2 <b>6</b>		<u>,</u>				1	)    -	. 628				•	B •	- 999.9			•	) <del>0 (</del>	* •	//0:	
3626		7 5					- r	. C. C.				ř	ı			949	4 19		- en	+ o	
7627		8		_	9.8	156	2.1	637				<b>612</b> 2			1			99.	2.3	. 040	
9058		\$		•				919			•	 	1						-1.2	021	
9629		124					_	.019					7.						•	410.	
9636		134						669					n	•	ω.		-3.5	•	5.3	092	
9632	•	.157		-	•	.157 -		031		7.7		024 0	9.9				ا نہ	803	i,	200.	
<b>X</b>		5 :						.651				7 `	ة 1	•			. •	e4\		1631	
		<u> </u>					ا د د	CZ9.				• •		000.	٥ ٦			906		- 6	
7		124				•		6.6				•				•	-			035	
25		3						916				•	•	•		968 -2	•		- 20	896	
9657		3				Ī	8	021				•	•			-	n		•	016	
9107		908				•		016					7		1	026 -2	₹.	042		115	
9169		129				•		012				•					•	628		. 617	
111		99				1	•	031				-	۲.	. 030 -				061		145	
1112		164				ī	*	024					-	. 689			~			968	
1113		152		_	8.9	145 -1	<b>.</b>	031		ī	<del></del>	024 -2	ı.	044	• •	-	<del>-</del> 1		-7.5	13 	
9115		143		•				030		•		1	ا ئ ا	005	<b>80</b> (	51 -3	i,		9.0	.052	
117	7.5	13.		, ~	7.7	134		633		ī	.i e:T	- 833 -		012	<b>B</b> •	<b>9</b> 35 –:	 		e ,	631	
9559	12.2	213					J. J	.058				Đ	6.6	9.000	i :	. e19	ا ۳	- 686 -	1.1	. 13 <b>4</b>	

		1	ATAG CATONA	-		7		S VY	1	100	INC ENTERROPIEE (CALLES)	3			ā	5	SOUTHWAY TOOL	•			
		5	<b>3</b>	•	3	į		3	5	214	2	?			Ž	<u> </u>		^			
200	47	OFF-CENTER	RAMP TO TO	50 51	WIRE	SIDE	997	2	SHIP		DECK PITCH	11CH	DECK ROLL	שנו	TDP	•	BAROMETRIC	rRIC	<b>A</b>	ARR CEAR	REREAD
Š	0151	DISTANCE	DIST	DISTANCE	9	€.	TYPE	<b>300</b>	<b>SPEED</b>	8							PRESSURE	Æ	\$	RUNOUTS	NUMBER
	E	*	<b>L</b>	2					\$	Ş	DEG	8	DEC	3	<b>L</b>	Ü	N K	至	Z	₹	
2	2	3	2	2	6	2	8	2	2	27	22	*	73	8	12	28	82	8	5	82	
3	7	1	231	2		828			40	17		600	-	662	3	=	29.96	761.0	•	6	•
900	-12	4	3	2		2			10			600	-	992	4		29.96	761.0	•		•
9992	-12	1	262	8		821			6	n	'n	. 989	_	662	<b>3</b>		29.96	761.0	•	•	•
500	-12	†	239	2	~	90	86286		8	ה י		. 969	-	002	5		29.96	761.0	100	406.4	•
900	7	7	247	22	<b>*</b> :	821	59200		<b>n</b>	, ,		. 999	-	002	<b>3</b>		29.96	761.0		406.4	•
	<b>-</b> :	? .	2	۲.	ימ	826	56286		ומו	י יי		. 669		002	<b>*</b> :		29.96	761.0		451.8	<b>•</b> (
	<b>:</b>	† '	2	₽ (	2		92190		n •		٠.	. 689.	! - !	799	;		29.95	9.5	20	429.3	<b>5</b> (
	* *	1 1	525 276	5 2	4	270	97198		n k	) )		20 G	1 1	7997	<b>.</b>	2 =	20.82	) (a) (b) (b) (c) (c) (c) (c) (c) (c) (c) (c) (c) (c	9	73 e.e	<b>5</b> 6
	2 5	7	֓֞֞֝֟֝֓֞֝֓֓֓֞֝֟֝֓֓֓֓֞֟	5 2	• •		20.00		n e	) r	י האים			2007	5 3		20.80	7		128.5	•
	2 2	? 1	1 5	\$ 5	P P7	7 2	50120		o e	יי נ		700	1 1	- 982	5 2		29.86	761.0		429.3	₽ €
	4 6	7		? ;	•	2	10120		•		_		_	99.	2		20.00	759.5		428.7	•
	? 9	? ?	3 5	. 2	10	32	20170 20170		M			500		992	4		29.96	781.0		428.7	•
9	9	' ?	279	2	•	100	66120		n	۱ م		. 963		010	4		29.96	761.0		•	•
9021	-12	1	275	3	*	90	50120		n	~	7	. 993		010	<b>5</b>		29.96	761.0	169 4	429.3	•
9622	-18	4	269	82	*	100	56126		n	7	7	. 963		919	4		29.96	761.0	167	424.2	-
9623	1	7	327	2	*	821	80120		n	~	ä	. 963	9.1	010	<b>5</b>		29.96	761.0		424.2	•
9624	-12	1	277	3	*	9	<b>50100</b>		n	~	7	. 663	9 1	010	<b>*</b>		29.96	761.0		429.3	•
<b>D6</b> 25	-	7	<b>5</b> ‡	*	n	820	50120		n	~	7	. 003		010	79		29.86	761.0		431.8	•
9026	-12	†	249	2	<b>n</b>	826	50120		<b>m</b>	~	7	. 663	-	<del>0</del> 16	<b>3</b>		29.86	761.0		429.3	•
9027	• •	?	241	2	<b>N</b> (	821	50120		n	~	ų.	. 663	ю (	010	<b>.</b>		29.96	761.0		429.3	•
8628 8628	7:	7		2	י מ	į	50120		יו מי	N 6	i e	200	D 4	919	<b>.</b>	2:	29.96	761.0	69	429.3	•
	? ?	7		: \$	,	2 6	78128		) P	, ,	i	50.			4		20.00	788.7			•
9632	1	7	8	2	2	2	86196		n	۰ م	! ~!	. 903		010	3		29.90	759.5	7 67	431.8	•
9634	•	7	236	72	8	820	50120		n	~	7.	. 003	9.	010	*	₽	29.95	769.7		429.3	•
9646	-29	4	220	67	8	961	50120		n	~	7	. 963	9.1	010	<b>4</b>		29.95	7.69.7		428.7	-
9646	<del>*</del>	Ť	285	6	4	820	50120		n	~	ĸ	. 993			2		29.95	769.7		426.7	•
9847	7	7	3	2	4	ē	50120		n	~		. 002	_	9.00	40		29.95	769.7		424.2	•
9653	7	7	ž	2	n	826	20200		n	~	' -	002		002	<b>3</b>		29.95	769.7		426.7	•
9057	9	7	313	8	*	828	<b>Sei ee</b>		r	7	_			002	3		29.95	769.7		426.7	•
9107	7	7	268	8	n	8	50100		n	7	9.0			040	3		29.91	759.7	170	431.8	•
9160	4	7	Š	ž		821	76188		"	7				030	53		29.91	759.7	•	<b>6</b>	•
911	7	7	298	5		820	70100		n	7	r S	999		. 030	3		29.91	759.7		<b>.</b>	•
9112	Ŧ	7	221	67	~	821	50100		n	7	٠ <del>٠</del>	997	7	012	2		29.91	759.7		426.7	•
9113	<del>+</del>	†	<b>528</b>	78	N	8	80.08		n	7	\ <del>\</del> .	997		002	2		29.91	759.7		431.8	-
9115	<b>*</b>	†	275	ž	*	826	<b>30100</b>		n	7	ا. ا			002	63		29.91	759.7		426.7	•
9117	-13	ę,	248	76	~	90	80120		n	~			-2.6 -	945	<b>9</b>	2	29.91	759.7		431.8	-
9559	7	7	<b>3</b> 2	1	~	8	50200		40	י י		005	œ.	.016	Ξ		9.93	769.2	166	421.6	•

## A-7 DAY

	WEIGHT		2	23		11266	11402	11266	11085	11175		10858	11130	11311	10812	10/67	10812	16456	100/0	10722	10858	10495	16949	10767	11402	16490	11357	10540		11175	10812	11221	19941	ונונו	11221	11221	10767		76511	11402
	WE		SS	<b>50</b>		24837	25137	24837	24437	24637		23937	24537	24937	23837	23737	23837	23837	24137	23637	23937	23137	24137	23737	25137	2313/	25037	23237		24637	23837	24737	22137	24937	24737	24737	23737	-	/5057	25137
INGS	LIFT	4		<del>c</del>															<b>B</b>																					
DAY LANDINGS	LIFT	5		<b>5</b>	8.	1.20	<b>8</b> .	8 :		1.28	1.10	1.10	1.10	<b>8</b>	1.10	1.18 1.18	<b>2</b> .	<b>2</b> 3	- <del>-</del>	6	- 1	1.99	1.99	1.10	8	1.28		1.10	<b>-</b>	- 19	<b>8</b>	<b>8</b>	1.10	9.	- 10	- 1	1.10	 8 .	9 .	1.00
	\$	<b>V</b> .ds		11																																				
	KAPA	Z		5		. e.	96.	1.67	. 65	1.05		<b>+</b> :-	1.03	90.	1.06	. 08	4 6	1.12	59.	1.97	.08	1.08	1.19	1.07	1.07	CB -	1.05	1.08		1.18	1.10	- .05	. 98	. es	1.07	1.12	1.03	,	99.	1.07
ž	V.dSA		K/S	5																																				
USS ENTERPRISE (CVN-65.)	S		Š	<b>±</b>																																				
RISE	VPAMIN		¥	5		2	<b>F</b> i	9 6	2 6	79		69	2	7	6	5	8	2	9 6	9	69	68	69	69	7	3	3 5	8		9	69	70	67	7	2	70	69	i	ς ξ	22
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uss e	VEOR		Ş	=	8	8	24	<u>د</u> د	3 2	2	8	5	2	9	57	Š i	2	8	3 2	9	2	22	8	3	2 :	ი <u>მ</u>	9	9	9	3	9	8	57		20	5	20	5	70	S 55
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		_	3	LANDING DATA - MODEL A-7E	1 2	MODEL	¥.74		د	USS ENTERPRISE (CVN-65)	TERPR	1SE (1	9 <del>-</del>   €	õ			DAY LANDINGS	NDINGS			
9	MA		VE-F1	3		WIND-VEL	VEL		¥.	VEOR	VPAMIN	Z	V.dSA	<b>.</b> <	<b>₹</b>	\$	LIFT	LIFT	WE	WEIGHT	
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USS ENTERPRISE (CVN-65)  VEOR VPAMIN VSP'A KVPA KV LIFT LIFT  MIN SP'A TO FF
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		3	LANDING DATA	MTA - I	- MODEL A-7E	F-7E	5	SS ENTE	USS ENTERPRISE (CNN-65)	(CM-6	ñ			DAY U	DAY LANDINGS			
			AIRCR	AFT SI	MKING S	AFT SINKING SPEED AT TOUCHDONN	TOUCH	Neg			CLIDE PATH ANGLE AT TD	PATH · A	NGLE A	5	WHEEL HEIGHT	HEIGHT	ноок нетсит	T S
£	NOSE	¥	2	F.	S	STBO	AVG		FREE-FLIGHT	IGHT	8 1		Š	>	OVER RAMP	RAMP	OVER RALP	<b>S</b>
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22	22	*	22	2	22	28	2	2	ñ	32	3	*	S	36	37	8	8	\$
~	15.0	<b>.</b>	÷.	4.5	14.0	4.5	14.8	4.5		. •	3.9	. 669		.672	18.8	5.7	15.5	4.7
<b>+</b> (	13.5	+.	13.0	• •	12.6	9.0	12.8	9.5			2.7	.064		.064	13.2	<b>+</b> ·	6.7	3.0
~ «				7 T	• • • • • • • • • • • • • • • • • • •	4 4 0 4	7 <del>7</del> .5	+ + + +			B ^	. 967 96. 4	• r	. e69	<del>6</del> 6 4 6	e e		<b>+</b> •
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=	12.7	9.0	13.1	•	12.9	9.0	13.0	•		. •	•	.070	8.0	990	19.5	9.0	10.1	4:0
=	13.2	•	12.5	8.P	12.1	3.7	12.3	2.7			• •	. 676	3.5	. 061	13.3	<del>-</del> :	<b>6</b> .	8°
2 :	• · ·	4. 8.	7.7	4.	15.0	4.0	9.4.	4. 8.			න (	968	ب 100 ا	.967	4.6		15.2	4.
2:	22.	•	2.5	ų,	12.1	•	B. +	•			۳. <del>د</del>	.062		.062	9.7	4.0		4
<u> </u>	12.0	) W	12.0		2.5		13.7	. d		•		9/6		96.	7.6.	. • • •	7. <b>6</b>	, .
•	12.7	9.0	13.9	7	12.5	3.0	13.2	•			9 69	969	, n	.963	16.8	5.1	13.4	-
2	14.4	+:	15.2	•	14.0	*.	4.9	4.5		•	4.2	.074	9.0	998	17.9	8.5	14.8	4.5
2	12.2	2.7	12.5	<b>8</b> .0	12.5	8.8	12.5	80 · 00			4.0	.060	•	.059	23.0	7.0	19.7	
ī	1.2	4.7	12.0	7.7	- :	, ,		n .	•	•	Ø •	. e51	<b>.</b>	. 656	15.0 1.00	<b>4</b> .	12.6	, ,
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<b>5</b>	13.0	•:	14.0	4.3	12.9	3.0	12.7	3.9		•	4.0	.059	3.3	.058	17.5	5.3	4.4	7
22	11.0	3.5	1.6	S. 55	<b>.</b>	<b>3.3</b>	11.3	4.4			4.5	. 059		.052	16.9	5.2	13.8	4.2
2	13.3	<b>.</b>	13.8	4.5	13.7	4.2	13.8	4.2			8.5	. 969		.065	19.8	•	16.5	80
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8	= .e	. e	±	3.0	•:	4.0	+:=	3.5			4.2	.074		.058	21.5	9.	1.00	8.
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3 3	13.7	7	12.4	, N	12.5	, N	12.6	, m		• •		. 663	) IO	. 661	20.7		17.3	8
5	=	4.0	=	3.1	:	J. 7	19.7	J. 7			2.9	.051		.042	13.2	<b>•</b> .	10.0	
3	12.7	<b>6.</b>	14.0	4.5	13.5	<b>+</b> :	14.1	4.3		•	3.8	990	8.8	. 968	18.3		14.9	4.0
ĝ	<b>1.8</b>	0. 0.	12.3	<b>9</b>	12.3	7.7	12.3	7.7			S. 3	929	<b>.</b>	999	15.7	<b>4</b> .	12.3	2
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5	7.1	2.5	<b>+</b> .=	3.5	•:	4.6	11.2	4.6		•	3.2	. 056	2.9	.051	16.0	4.0	12.4	ы В.
25	1.8 6.1	3.6	1.4	3.5	<b>+</b> .=	S.5	1.4	3.5		•	3.3	.057	٠. د د	.054	17.0	5.2	13.8	4.2
3	15.7	<b>4</b> .0	14.5	<b>†</b> .	14.3	4.0	4.4	<b>+</b> .		•	6.0	.067	ر 10.00	990	9.0	5.3	14.5	7

AIRCRAFT SINKING SPEED AT TOUCHDOWN  NOSE PORT STBD AVG FREE-FLIGHT BHW BVV  NA/S F/S M/S F/S M/S F/S M/S DEG RAD DEG RAD	CRAFT SINKING SPEED AT TOUCHDONN PORT STBD AVG FREE-FLIGHT M/S F/S M/S F/S M/S	STBO AVG FREE-FLIGHT  F/S M/S F/S M/S F/S M/S	FREE-FLIGHT S F/S M/S	FREE-FLIGHT S F/S M/S	FREE-FLIGHT S F/S M/S	_	_	GLIDE PATH ANGLE AT TD  BHM BVV  DEG RAD DEG RAD	PATH ANGLE AT TD  # BVV  RAD DEG RAD	MGLE AT TD BW DEG RAD	5 5 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8		WHEEL HEIGH OVER RAMP	WHEEL HEIGHT OVER RAMP FT M	HOOK HEIGHT OVER RAMP FT N	EIGHT RAMP
F/S M/S F/S M/S F/S M/S F/S M/S DEG RAD 25 26 27 28 29 39 31 32 33 34	M/S F/S M/S F/S M/S F/S M/S DEG RAD 26 27 28 29 39 31 32 33 34	M/S F/S M/S F/S M/S DEG RAD 28 29 30 31 32 33 34	F/S M/S F/S M/S DEG RAD 29 30 31 32 33 34	M/S F/S M/S DEG RAD 30 31 32 33 34	F/S M/S DEG RAD 31 32 33 34	M/S DEG RAD 32 33 34	DEG RAD 33 34	<b>3</b> \$		35		<b>3</b> %	E A	<b>3</b> g	t 8	<b>z ę</b>
2.0 9.4 2.9 2.5	2.0 9.4 2.9 2.5	2.0 9.4 2.9 2.5	2.9	2.9	9.7	•	•	•	.043 2.	6 P	4.	.042	13.9	4.4	**	3.2
5.6 10.0 5.2 10.7 5.5 10.6 5.2 5.2 5.5 5.6 5.6 5.6 5.6 5.6 5.6 5.6 5.6 5.6	3.5 10.6 5.2 5.2 5.5 5.6 5.6 5.6 5.6 5.6 5.6 5.6 5.6 5.6	3.5 10.6 5.2 5.2 5.5 5.6 5.6 5.6 5.6 5.6 5.6 5.6 5.6 5.6	. 5.0 4.0	. 5.0 4.0		• •	• •	• •	.838 J.	י ה	<b>.</b> •	.052	17.3		13.0	. 4 . 4
3.1	3.1	3.1	3.1	3.1	•	•	•	•	.057 2	~	•	.048	19.6	0.9	16.0	4.0
. 4.0 a.1 a.2	. 4.0 a.1 a.2	. 4.0 a.1 a.2	. 7.0	. 7.0	3.7	•	•	•	. 965	<b>"</b>	•	.052	17.7	4.0	- · · · ·	4. W.
4.5	4.2 14.7 4.5 4.1 .071	4.2 14.7 4.5 4.1 .071	4.5	4.5	4.1 .071	1.00.	1.00.	1.00.		י מ		.062			4.5	<b>7.</b> 7
10.1 5.0 2.1 1.1 1.4 10.4 10.1 1.1 1.2 1.2 1.1 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0	3.1 3.1 654 3.1 654	3.1 3.1 654 3.1 654	3.1 3.1 654 3.1 654	3.1 3.1 654 3.1 654	5.5 4.0 4.0					<b>4</b> ~	. 6 . 6	.045	15.6	o <b>⇔</b>	12.4	, so
3.4 .059	3.6 16.1 3.1 11.0 3.3	3.4 .059	3.4 .059	3.4 .059	3.4 .059					2	•	.053	1.91	0.4	12.9	3.0
4.3 13.8 4.2 13.9 4.2	4.3 13.8 4.2 13.9 4.2	4.2 13.9 4.2	4.2 .074	4.2 .074	4.2 .074	4.2 .074	4.2 .074			*	<b>6</b> .	690	18.2		14.7	4.9
4.6 6.6 6.6 10.5 12.1 5.7 5.7 5.64	4.6 6.6 6.6 10.5 12.1 5.7 5.7 5.64	3.0 10.5 3.2 12.1 3.7 3.7 .064	3.2 12.1 3.7 3.7 .864	3.2 12.1 3.7 3.7 .864	3.7 3.7 .064	3.7 3.7 .064	3.7 .064			N P		.051	20.4	<b>6</b>		- e
					200. 0.4 W. 1	0.00 0.00 0.00 0.00	9.0	2. e. 4 . e. 6	698			.002	20.5		1.5.	4
4.0 12.3 3.7 12.7 3.9 3.7	4.0 12.3 3.7 12.7 3.9 3.7	3.7 12.7 3.9 3.7	3, 4, 9	3, 4, 9	3.7 .064	3.7 .064	3.7 .064	3.7 .064	.064		3.6	.064	6.9	8.0	15.7	4.0
12.4 5.8 12.4 5.8 12.4 5.8 5.7	1 3.8 12.4 3.8 12.4 3.8 3.7	4 3.8 12.4 3.8 3.7	4 3.8 3.7	4 3.8 3.7	3.7				. 965		3.5	.061	16.1	4.0	12.5	3.8
3 11.1 3.4 10.1 3.1 10.6 3.2	3.4 10.1 3.1 10.6 3.2	3.1 10.6 3.2	3.2	3.2	8.N	_	_	_	996		2.7	.054	15.3	4.7	11.8	9.0 0.0
0.4 10.0 0.2 10.0 0.0	0.4 10.0 0.2 10.0 0.0	3.2 16.6 5.3	77.7	77.7		_	_	_	. 658 678			. 655	15.3	<b>.</b> .	1.0	n .
3 10.6 3.2 10.4 3.2 10.5 3.2 3.2 3.2	4.2 10.4 4.0 10.2 4.0 4.2 4.2 4.2 4.2 4.2 4.2 4.2 4.2 4.2 4.2	4.2 10.8 4.0 4.2 4.2 4.2 4.2	- 0. m	- 0. m	- 27				.055		2.7	.047	13.3	. <del>.</del>	10.	u
10.1 3.1 10.4 3.2 10.3	3.1 10.4 3.2 10.3 3.1 3.2	3.2 10.3 3.1 3.2	3 3.1 3.2	3 3.1 3.2	3.2	3.2 .056	3.2 .056	3.2 .056	. 056		3.0	.052	18.7	5.7	15.1	4.6
5 13.4 4.1 12.7 3.9 13.1 4.6 5.9	4.1 12.7 3.9 13.1 4.0	8,0 6.4 1.05 6.0 (1)	6.0 (1)	6.0 (1)	6, 1)				.969		ا ا ا	.063	21.7	<b>6</b>		S. 6
D 4	0.6 12.5 0.6 12.4 0.6 0.7 v.	3.0 12.4 5.0 5.7 4.4 4.4 4.4 4.4 4.4 4.4 4.4 4.4 4.	. 7.0	. 7.0		•	•	•	.054		ر د د د	.066	9.6	9.4	13.8	D 4
3,2 10,9 3,4 10,5 3,2	3,2 10,9 3,4 10,5 3,2	3,4 10,5 3,2 3,5	10 m	10 m	. 10 10		3.5	3.5 .061	961		2.7	.048	16.3	8	13.1	4
2.8 9.1 2.8 9.2 2.8 9.4 2.9 3.7	2.8 9.1 2.8 9.2 2.8 9.4 2.9 3.7	2.8 9.2 2.8 9.4 2.9 3.7	2.8 9.4 2.9 3.7	2.8 9.4 2.9 3.7	9.4 2.9 3.7	2.9 3.7	3.7	3.7 .064	.064		2.7	.047	15.9	4.0	12.2	2.7
4.1 12.4 3.8 13.0 4.0 3.7	4.1 12.4 3.8 13.0 4.0 3.7	3.8 13.0 4.0 3.7	. 4.0	. 4.0	3.7				. 964		3.6	. 963	17.5	5.3	14.0	4.3
4.2 12.5 3.8 13.2	4.2 12.5 3.8 13.2 4.8	4.0 13.2 4.0 0.1	4.0	4.0	4.0	•	•	•	990		N.N	.057	15.0	<b>4</b> .6	12.1	3.7
. 6.6 6.6 5.8 6.7 6.6 6.6 6.6 6.6 6.6 6.6 6.6 6.6 6.6	G. 6.6 2.6 6.7 G. 6	2.6 9.7 4.0	. e.b	. e.b	•:	•	•	•	.053		7.7	146	14.7	4. 10.	4.1.	
S.6 11.9 S.6 11.9	G.6 17.9 G.6 17.9 G.6	3.6 11.9 3.6	. 6.6	. 6.6					964		4.6	. 659	17.3		13.0	4.5
. 6.60 6.60 6.60 6.60 6.60 6.60 6.60 6.	7.8 18.8 5.8 5.8 5.8				<b>9</b>	•	•	•	.963		2.6	949	9.0	æ ·	16.3	
2.6 9.2 2.6 9.2 2.6	2.6 9.2 2.6 9.2 2.6	2.6 9.2 2.8 5.2	2.6	2.6	3.2	•	•	•	922		2.7	.047	2. 2. i	4.2	10.7	3.2
. 6.4	. 0.4 10.0 0.1 10.1 0.1 0.1 0.0 1 0.1 0.1 0.1	. 0.4	. 0.4 . 0.4	. 6.4		•	•	•	698	•••	<b>8</b> . 7	.030	17.3		14.2	4.
3.4. 10.6 3.2 50.8 3.3 5.1 5.54 5.4 5.4 5.4 5.4 5.4 5.4 5.4 5.4 5.	43.4 10.6 4.2 10.8 4.4 4.4 4.4 5.4 5.4 5.4 5.4 5.4 5.4 5.4	3.2 16.8 3.3	3.3	3.3	3.1 .054	.954	.954	.954		-,	<b>6</b>	.052	÷.	4.5	÷.	ر د د
. 4.0 4.1 4.1 4.1 6.1 6.0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	. 4.0 4.1 4.1 4.1 6.1 6.0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	. 4.0 4.4 4.6 4.6	. 4.0 4.0 4.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5	. 4.0 4.0 4.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5	**************************************	•	•	•	. 059		<b>9</b>	.052	15.2	4.	11.7	o n
3.1 11.3 3.5	5.5 10.2 5.1 11.3 5.5	3.1 11.3 3.5	3.5	3.5	. 2.2	•	•	•	625		n :	. 658	4.8	4. 0.	4.1.	
5.5 10.1 5.1 10.1 5.1		. 6.1 16.1 0.1 0.1 0.1 0.1 0.1 0.1 0.1 0.1 0.1 0	. 6.0	. 6.0	•	•	•	•	.052		91	.053	18.9	<b>.</b>	12.9	ю. О
. C.S. 8.8 G.B G.B C.S.	. C.S. 8.8 G.B G.B C.S.	3.0 9.9 3.9 2.7	3.0	3.0	•	•	•	•	.047		2.7	.047	16.7		13.2	<del>.</del> 0
3 3.7 12.3 3.8 3.8	3.8 12.3 3.7 12.3 3.8 3.8	. 3.7 12.9 5.8			10.1				.067		υ.	.961	7.7	4. c	11.5	U. 0
5.9 12.1 5.7 12.4 5.8	5.9 12.1 5.7 12.4 5.8	3.7 12.4 5.8	. 8.70 8.70 T	. 8.70 8.70 T	. 8.0	<b>.</b>	<b>.</b>	<b>.</b>	.067		٠. ا	. 055	20.1		9.9	
5.2 9.6 2.9 9.4 2.9 9.4 2.9 5.1 .054	2.9 9.4 2.9 9.4 2.9 5.1	8.4 Z.8 8.4 Z.9 J.1 .654	Z.8 8.4 Z.9 J.1 .054	4.4 Z.9 J.1 .054	Z.9 5.1 654	924	459. 1.0	5.1 .05¢	.054		2.5	. 444	16.7	 	13.5	<b>-</b>

		5	LANDING B	ATA -	data — model a-7e	-7E	Š	SS ENTE	USS ENTERPRISE (CVN-65)	(C8	<u> </u>			DAY U	DAY LANDINGS			
995			AIRCR	IS TAN	CRAFT SINKING SPEED AT TOUCHDOWN	PEED A	T TOUCH	NOC			GLIDE	GLIDE PATH ANGLE AT TD	NCLE A	5	WHEEL	WHEEL HEIGHT	HOOK HEIGH	#E16#
2	NOSE	SE	2	PORT	Ţ	STBO	AK	(9	FREE-FLIGHT	LIGHT	<b>8</b>	*	PA PA	>	OVER RAMP	RAMP	OVER	OVER RAMP
	2	\$	٤	Ş	2	Ş	2	Ş	5/2	K/S	DEC	3	DEG	3	E	3	E	_
22	23	24	23	26	27	28	28	8	5	32	33	z	33	38	37	8	99	₹
112	14.1	4.4	13.9	4.2	13.5	÷.	13.7	4.2			<del>-</del>	.072	3.7	<b>.</b>	16.8	5.1	13.6	*
121	9.9	2.6	7.8	2.4	7.8	2.4	7.8	2.4			2.8	.048	2.1	. 637	14.7	4.5	11.2	~
124	5.0	ب ا	<b>6</b> .9	2.7	<b>8</b>	5.6	7.0	2.7	6.7	3.0		!	2.4	. 042	,	•	;	
126	10 4 10 P	7.7	• •	, ,	<b>.</b>	9 e					2.7	.047	2.G	.959	0.0 0.0 0.0	<b>4</b> •	<b>9</b>	n (
3 =	12.7	7 0	13.8	÷.2	12.6	, K	13.2	•					4.4 .5.5	.058	R.7			4
=	10.7	3.3	10.0	3.1	8.6	9.0	0.0	3.0			3.3	.057	2.7	.047	15.7	4.8	12.4	n
145	12.4	3.8	12.9	3.8	13.9	4.2	13.4	<del>-</del> :			3.7	.064	3.5	. 962	20.0	6.1	17.0	40
147	12.3	7.7	= .	3.0	•.	3.0	10.0	J. 5			,		2.9	. 051				
<b>9</b>	12.7	<b>6</b>	13.1	•	5.0	4.5	13.4	<b>-</b> !			<b>9</b> .9	.052	3.2	.056	18.2	بر در د	15.2	◀ ·
2	12.8	9	13.0	4.	÷.	4.	<u>+</u>	<b>.</b>				.067	۵. د	.064	17.5		14.2	♥ (
151	9 · •	4 r	9.6	•	5.5	•	5.6	10 C			4 . 6 .	.879 653	<b>*</b> . •	. 683	23.0	<b>9</b> . •	4.6.	י מ
7 5		; •	? =			; •		, r				944	, ,	948	. ¥	; <b>•</b>	2 :	7 6
3 3	-	) P)			•	, n		) P)			, c	951	2.8	949	. 4	4	1.9	) F)
200	10.2	3.1	•	2.8	0	9.	8	2.9			2.9	.051	2.5	.043	4.3	4	-	, m
157	0.0	 	4.0	2.9		2.8	5.0	2.8			2.8	.048	2.3	. 039	15.8	4.8	12.7	~
<b>5</b> 5	1.5	J.5	10.6	3.5	1.0	3.5	1.1	4.4			5.6	.046	2.8	.049	13.7	4.2	10.4	n
9	12.8	8.5	13.2	4.0	13.1	<b>4</b> .	13.2	•			3.8	990.	3.6	.063	19.4	G	16.1	*
5	13.4	7	12.8	0.0	12.4	۵. ا	12.6	D. D			2.8	.048	5.9	.051	18.7	5.7	15.5	*
162	<del>*</del> •	<b>*</b> (	13.7	÷ ;	12.8	ص د د	13.4 2.4	<del>4</del> (			۵. و و	.063	<b>+</b> •	929	17.1	2.5	2.0	<b>*</b> *
3 5		, r		, r		9.7		0 F			3 P	9 6	, c	5 t d	9.0	• •		າ ◀
<u> </u>	1.5	, u		'n	12.1	, b	12.0	, n			. r.	. 965	, 6	.053	. 6. 6. 6.			t <b>4</b>
166	11.3	3.5	12.2	3.7	11.5	3.5	12.0	3.7			4.6	.059	3.2	. 055	7:1	4.3	10.7	n
167		3.5	<b>+</b> :-	J. 5	12.1	3.7	1.8	3.6			3.5	.062	3.0	.053	14.8	4.5	11.2	n
2	- 5			2.7	<b>6</b>	6 6 6	e :	2.7			n. n.	.057	4.6	.042	9.5	eo •	15.4	<b>4</b> F
	2 .			7.7		, .					7.6	6.6	, r	2 6 6	) K	•		> ◀
2.5		9	10.2		0	2.7	9.	2.9			3.1	.054	2.5	.043	16.5	9.0	12.9	· 12
173	10.3	7.0	10.0	3.1	9.7	8°.	6.6	3.0			2.5	. 944	2.2	.039	13.8	4.2	10.7	n
175	13.4	<del>*</del>	12.9	3.0	1.8	3.8	12.4	3.8			3.7	.064	3.3	. 057	19.1	5.8	15.8	4
178	12.9	3.9	13.2	•	12.1	3.7	12.6	3.8			3.5	. 062	3.5	.061	17.4	5.3	<u>+</u>	*
10	1.7	8.0 9.0	13.2	<b>4</b>	12.9	<b>0</b> (	13.1	<b>4</b> .0			0.0 1	.064	3.7	.064	5.6	<b>4</b> .	12.2	י מי
182	- (	2.8	B) (	9	D	2.7	4.	2.9			n.	.057	2.7	.047	15.7	4 ·	12.3	? '
2	1.2	٠ •	9. e.	7	7	8 ·	16.5	2.5			- 6	409.	B . C	949	÷	÷ •	12.0	? •
D :	. o	? <b>●</b>		o. ►	9.9		7. E	÷ r	6	,	, v	. 63.1 848	2.5 4.0	941	16.6 1.5	 	4.6	+ 17
6	1. 5		12.2		1 -	, 10 , 10				?		2	4	929		•		•
13	10.2	. <del>.</del> .	. 60	3.0	10.5	3.2	10.1	3.1			3.5	. 969	5.8	.051	15.2	4.0	11.9	n

205			AIRCR	AFI	SINKING SPEED AT TOUCHDOWN	) EEO A	T TOUCH	N			GLIDE	GLIDE PATH ANGLE AT	NGLE A	01 10	WHEEL	HEIGHT	HOOK HEIGHT	HO!!
2	NOSE	SE	8	×	STBO	8	AVG	(5	FREE-FLIGHT	IGHT.	<b>8</b>	*	Š	>	OVER	RAMP	OVER RAMP	3
	2	Ş	٤	\$	5	¥	٤/٤	Ş	5/3	K K	DEG	3	DEG	3	E	*	E	3
23	22	54	23	2	27	28	29	2	31	32	z	ż	33	38	37	8	8	\$
=	10.8	3.3	10.2	3.1	10.2	7.7	10.2	1.1			3.0	.052	2.6	.046	16.3	5.6	12.8	
195	11.0	3.0	10.0	3.3	10.0	3.2	10.7	3.3			3.4	. 059	4.2	.042	17.5	5.3	14.3	•
2	=	7.7	10.7	3.3	10.0	J. 7	10.4	3.2			3.0	. 053	2.8	. 049	13.7	4.5	10.6	'n
ž	16.7	3.5	10.4	3.2	9.0	2.9	 	3.1			3.4	. 059	2.7	949	15.6	4.8	12.4	'n
207	5.0	2.8	9.5	2.8	•	2.7	9.1	2.8			2.5	.044	2.8	. 045	15.3	4.7	11.9	2
<b>1</b>	8.7	7.6	10.2	3.1	8.8	3.0	10.0	3.1			3.2	. 055	2.8	.050	15.0	<b>4</b> .6	11.7	3.0
<b>2</b>	12.0	3.7	13.3	<b>•</b> :	13.6		13.4	+:+			3.5	. 969	G. 9	.067	16.9	5.2	13.5	*
210	19.8	J. 7	=:	4.0	<b>→</b> .	3.2	10.7	3.3			3.3	.058	3.2	. 055	15.8	<b>4</b> .0	12.4	2.0
212	<b>.</b>	2.5	4.6	7.6	7.8	4.4	<b>.</b> .	2.5	9.0	5.6	3.0	. 052	2.5	.038	13.4	<b>+</b> .1	<b>6</b> .	'n
215	16.9	3.3	5	2.8	0.0	3.0	9.7	3.0			3.1	. 053	4.0	. 059	14.8	4.5	<b>+</b> .=	2
Ş	11.2	4.5	6.3	2.5	0.0	٠. د.	<b>8</b> .0	3.0			2.1	. 037	2.3	. 039	11.7	3.6	8.7	7
3	12.9	3.0	1.6	3.5	12.2	3.7	#. 6.	S.0			3.2	. 055	2.8	949	13.8	4.5	10.8	'n
3	₽. ₽.	9.P	13.4	<b>+</b> :	12.4	3.8	12.9	a.5			3.7	. 063	4.6	. 059	18.0	5.5	14.9	<del>*</del>
3	<b>*</b> .	 	-:	<b>e</b> :	4.7	7.7	<b>6. 4</b>	1.5			2.8	. 049	<b>+</b> .	. 025	8.0	2.4	4.2	_
3	#. E	3.5	<b>.</b>	7.8	9.5	2.9	<b>8</b> .0	9.P			2.5	. 044	7.4	.041	10.8	3.3	7.4	~
672	19.2	٠. ۲.	<b>+</b> .=	3.3	<b>8</b> .8	1.8	11.0	4.6			3.5	. 060	4.6	. 060	10.1	3.1	<b>9</b> .9	7.
9	14. <b>0</b>	4.4	12.0	0.	<u>-</u>	4.0	11.5	3.5			3.9	.068	3.2	.056	14.3	<b>+</b> .+	10.6	'n
86	13.5	+:	12.7	0. 0.	13.0	<b>.</b>	12.8	3.9			3.5	. 961	3.1	.054	18.3	5.6	14.8	*
<b>6</b> 0	12.9	8. 8.	13.8	4.2	12.2	3.7	13.0	<b>•</b> .•			3.7	. 065	3.3	.058	17.9	5.5	14.4	+
669	13.0	•:	13.1	•.	13.1	4.0	13.1	<b>•</b> · •			3.3	.057	3.3	.058	16.5	5.0	13.3	÷
7	13.1	•.	<b>1</b> .8	3.0	<b>6</b> .E	a.6	1.9	3.6			4.9	.679	3.1	. 055	16.0	4.9	12.6	'n
11	12.0	3.7	13.2	•:	7.7	4.3	13.6	4.2			4.6	. 059	ъ. В.	.067	18.9	5.8	15.6	+
712	14.2	4.4	13.8	4.2	13.6	<b>-</b> .	13.7	4.2			3.7	. 965	3.0	. 968	17.0	5.2	13.7	*
714	5.0	2.8	12.7	3.0	12.1	3.7	12.4	3.8			3.2	.055	3.5	.062	14.6	4.5	11.2	'n
715	10.3	3.1	<b>19.</b> 3	3.1	•	3.0	19.1	3.1	10.1	٠. ۲.	2.9	.050	5.8	.051	13.6	<del>-</del> -	10.2	'n
716	12.0	3.7	12.2	3.7	12.7	a.	12.5	3.8			3.6	. 063	<b>4</b> .	.070	15.0	4.6	11.7	'n
720	#. 	0. 0.	<b>+</b> :=	3.5	<b>10.0</b>	3.3	=======================================	4.6			3.0	.052	4.6	. 060	14.9	4.5	1.0 1.0	n
726	3.0	1.2	=:	4.5	14.5	<b>+</b> .	13.6	<del>-</del>			3.8	.067	3.9	.069	11.7	9.0 9.0	4.8	7.
<b>465</b>	13.4	<del>-</del> :	=:-	3.4	11.5	ъ.	1.3	4.6			3.6	. 063	J. 0	. 053	1.5	3.5	9.0	, 7
4051	7.3	7.7	7.5	2.3	7.3	2.5	7.4	2.5			2.0	. 035	<b>6</b> :	. 032	±.8	3.6	8.2	2.
4633	14.7	4.5	<u>-:</u>	4.3	13.8	4.2	13.9	4.5			3.4	.060	3.7	.064	13.9	4.2	10.7	n

	<b>&gt;</b>	AT TO	3	5	. 963	101	.023	e16	014		028	.019	. 635	.052	966	9.	771.	026	059	012	.016	995	679.	989		.023	. 963	626 63	1.0	. 673	.026	021	005	- 965	038	.036	. 023	017	. 049
	YAW	AT	DEC	2	~:	5.8	r. (	P 6	0	۳.	9.	-	7. 9.	o.	ر ا	9 9	. I	5	4.5	7	<b>.</b>		4. c	, ,		1.3	. O.	7.	• •	7	1.5	-1.2	ا. ن	7.7	-2.2	7.7		<del>0</del> : <del>1</del>	2.8
	F. P. A.	AT TO	3	<u>8</u>	056	049	947	40. 40. 40. 40. 40. 40. 40. 40. 40. 40.	- 049	052	040	056	- 658	999.	929	600.	900	051	038	054	063	- 959	1.965	975	961	061	686	075	9.4	947	-, 966	056	047	044	042	052	651	965	070
	ı.	7	DEG	80	-3.2	-2.8	-2.7	- °	-2.8	-3.0	-2.3	7.5	ان ا	ا ا	7.7	? ?	9 6	-2.9	-2.2	-3.1	ار ا	4.1	7.7	? 1	5.5	-3.5	9. T	7'	ה ה	-2.7	<b>8</b> .5	-3.2	-2.7	-2.5	-2.4	ر ا ا	-2.9	-3.7	9.4
DINGS	ROLL RATE	5	\$	22	. 042	. 654	- 103	2007						9.9	183	900	115				. 691		216			600	038	9.0	240				.679	134	.073	16 5.53	.051	. 805	. 033
DAY LANDINGS	BOLL	A	DEG	20	2.4		G	- ^	. •	3.1	_	+	• • •	<b>.</b>	1 <del>0</del> .5		, , «			19.9	5.2	•	12.4			•	~			- <del>-</del>	'n	8.9	÷.5	<b>8</b>	4.2	ب ب ب	5.6	r.	1.9
۵	PITCH RATE	5	3	93	.017	.037	.024	1.040. CA.	410	.636	•	-				. e				.017	. 669	028	646	500	2.5	.012	.024	. 633		. 68	040	410	. 030	. 631	.651	965	919	.045	.084
	PITCH	AT	DEC	<b>8</b>	<b>.</b>	2.1		0.7 7	, <b>e</b>		- -	<b>n</b>		ri e	9 1	٠,			*	<b>9</b> .	ĸ.	• •	2.3	n =	. <del>.</del>		<b>+</b> :	o. (	? ;	· •	'n	<b>8</b> 0	1.7	8.	6. 10.	ן ני			<b>4</b> .8
		<u> </u>	3	S				•					•		•	•	•	617				•									•						•		
W-65)	w L	<b>L</b>	DEG	22														•	:																				
uss enterprise (cvn–65)	υ ×	8	2	5	066	. 003	- 689	919	619	. 667	631	.002	.033	<b>698</b>	. e38	979	700	7	.047	.002	. 068	. 040	073	9. e	963	. 995	.677	600	99.6	642	021	.054	. 863	.054	919	017	.963	.037	.045
NTERPR	<u>ب</u>	•	DEG	8	6.5	~		ָ װְ	٠.	*	9.7	<del>-</del> .	•			^	7 7	•	2.7	<del>-</del> .	3.9	2.3	7	· -	_		<b>+</b> .	e.	D	; <	. ~	J.,	~	ر ا	_	6 ¢		2.1	5.6
USS E	8	2	3	<b>\$</b>				3	_	624	024	030							045	054	017	030	550	7/0.			016	666	070				014	019	<del>0</del> 1		. 621	636	003
		<b>,-</b>	DEC	\$	2	-	<b>.</b>	7.5	•	+.7	4.7	-1.7			ر د د	-7.	- 0		-2.6	5.1	_		9.9	- 0	-2.6	*				, ,		-1.6	<b>®</b> .			6 6 7	: 2	1.7	2
A-7E		<u>u</u>	3	+														154																					
MODEL A-7E	GLE	•	DEC	\$														•	)																				
ATA -	*	8	3	\$	 82	. 159	.147	<u> </u>	3	54	. 129	\$	35	3			771	*	173	131	40.	2	. 175	7 5	3	131	.175	90	70.	2	<u>=</u>	168	. 161	74.	154	5 5	188	1.38	.157
LANDING DATA	Z C F	•	930	‡	7.9	-	4.0		8.5	8.3	7.4	4.6	<b>6</b>	<b>.</b>	÷ •				0.0	7.5	7.7	7.9	• ·	? •	9.7	7.5	• •	6.7			4	9.0	9.5	9.5			10.2	7.9	9.6
3	•	2	2	2	3.	. 162	.126	<u> </u>	. 152	.166	. 129	-	2	<b>3</b>	. 152		3 5	157	7	119	35.	. 152	= :		25	138	.166	<b>*</b>	• 77.	3	55	161	<del>-</del>	*	*	178	187	.147	. 699
		-	050	42	7.6		7.2		6.7	8.5	7.4	Ø. 0	<b>6</b>	7.9		- ·		•	7.7	6.8	7.6	7.0	- 1	. v	. 0	7.0	6.5	<b>6</b>			7.9	9.2		7.7	4	<u> </u>	10.7	4.0	5.7
	200	2		<b>‡</b>	7	<b>*</b> 1	<b>~</b> (	<b>0</b>	. =	=	12	2	<b>*</b> !	5	2 :	2 9	? =	2 :	12	7	22	29	2	3 =	5 25	3	ま	2	3 5	5 5	8	7	Ŧ	42	<b>.</b>	\$ \$	3 5	22	53

RAD         DEG         RAD <th></th>	
56         RAD         DEG         RAD	<b>10</b> OR FF 10
9.6         51         52         53         56         57         58         59         69           -1.6         -0.07         -1.6         -0.07         -1.6         -0.07         -1.6         -0.07         -1.6         -0.07         -1.6         -1.7         -0.07	DEG RAD DEG RAD DEG RAD DEG
6.6         6.0 <th>42 45 46 47 46 49</th>	42 45 46 47 46 49
4.7         -082         2.2         -038         4.6         -066         1.2           4.2         -073         -0.1         -065         3.5         .061         -3.5         -061         -4.6         -2.6         -4.6         -2.6         -4.6         -2.6         -6.6         -2.7         -065         3.5         .061         -3.4         -065         -1.1         -066         -1.2         -066         -3.4         -065         -1.2         -066         -3.1         -066         -3.1         -066         -3.1         -067         -3.4         -065         -1.2         -068         -3.4         -068         -3.4         -068         -1.2         -068         -3.4         -068         -1.2         -068         -3.4         -068         -1.2         -068         -1.2         -068         -1.2         -068         -1.2         -068         -1.2         -068         -1.2         -068         -1.2         -068         -1.2         -068         -1.2         -068         -1.2         -068         -1.2         -068         -1.2         -068         -1.2         -068         -1.2         -068         -1.2         -068         -1.2         -068         -1.2         -1.2	
4.2         .073        065         3.5         .061        5        061        5        061        5        061        5        061        5        061        054        061        054        061        054        061        064	.113 8.2 .143
1.3         .023         -1.1        019         2.1         .037         -3.5        061         -2.5        061         -1.0         -035         -3.1        064         1.0         -035         -3.1        064         1.0         -035         -3.1        064         1.0         -035         -3.1        065         -3.1        065         -3.1        065         -3.2        061         1.2        065         -3.1        053        061         -2.3        061         1.3         -3.5        061         -2.3        061         1.3         -3.5        061         -2.3        061         1.3         -3.5        061         -2.3        061         1.4         -2.5        061         -2.3        061         -2.3        061         -2.3        061         -2.3        061         -2.3        061         -2.3        061         -2.3        061         -2.3        061         -2.3        061         -2.3        061         -2.3        061         -2.3        061         -2.3        061         -2.3        061         -2.3        061         -2.3        061         -2.3        061	- 1.7 - 10.1 .176 - 1.7 -
3.4         .059         2.9         .051         .3         .065         -3.1         .065         -3.1         .065         -3.1         .065         -3.1         .065         -3.1         .065         -3.1         .065         -3.1         .065         -3.1         .065         -3.5         -061         -3.5         -3.5         -1.2         .061         -3.2         -4.6         14.3         .259         -2.6         -0.45         -7         -7         -1.6         -3.3         -3.5         -661         -2.7         -661         -2.7         -661         -2.7         -661         -2.7         -661         -2.7         -661         -2.7         -661         -2.7         -661         -2.7         -661         -2.7         -661         -2.7         -661         -2.7         -661         -2.7         -661         -2.7         -661         -2.7         -661         -2.7         -661         -2.7         -661         -2.7         -661         -2.7         -661         -2.7         -662         -2.7         -662         -2.7         -662         -2.7         -662         -2.7         -662         -2.7         -662         -2.7         -662         -2.7         -662         -2.7 </td <td>7. 168 10.3 .180</td>	7. 168 10.3 .180
2.4         .042         -3.1        054         2.0         .035         -3.4        059         1.2           -1.6        023        040         -3.5         .061         1.9         -033         -4.1        052        052        040         -3.5        061         -2.3        040         -3.5        061         -2.5        045         -7.7         -7.7         -7.5        061         -7.2         -7.7         -7.7         -7.5         -7.6         -7.7	.3 .197 9.9 .173002
100210021002100220102	.145 6.8 .119
-1.6028	5 9.4 .164 -2.6
	.120 8.4 .147 -2.8
	.146 8.1 .141 -2.2
1.4       .024       .2       .069       5.1       .069       8.0       .140       -5.5      061       1.6         1.3       .023       1.9       .033       12.7       .222       -4.9      070       2.8         -4.1       -002       1.9       .033       12.7       .222       -4.9      070       2.8         1.6       .026       2.1       .037       -7.9       -082       -3.5       -083       -2.2         2.4       .042       -1.7       -030       3.6       .063       -2.9       -085       -2.2         2.4       .042       -1.8       -034       -3.5       -085       -2.2       -2.0         3.5       .065       -1.15       -7       -0.16       -0.24       -0.65       -1.7       -2.2       -2.2       -0.05       -0.16       -1.7       -0.10       -0.10       -0.5       -1.7       -0.10       -0.10       -0.5       -0.5       -1.7       -0.10       -0.2       -0.6       -1.7       -0.10       -0.10       -0.5       -0.5       -1.7       -0.2       -0.2       -0.2       -0.2       -0.2       -0.2       -0.2       -0.2       -0.2       -0.2	.157 8.7 .152 0.0
1.3 . 023 1.9 . 033 12.7 . 222 -4.0070 2.8 -4.0010 8.6 . 150 -4.5079 -2.9051 -4.0 1.5 . 023 1.9 . 033 4.7 . 082 -3.9063 -2.2 2.4 . 042 -1.7 . 034 3.6 . 063 -2.9051 -2.2 2.4 . 042 -1.7 . 030 3.6 . 063 -2.9051 -2.2 1.3 . 063 -1.7 . 030 3.6 . 063 -2.9051 -2.2 1.4 . 042 -1.7 . 030 3.6 . 063 -2.9051 -2.0 1.5 . 023 -1.4 . 024 . 9 . 016 -3.8065 -1.7 3.0 . 052 -1.4 . 024 . 9 . 016 -3.8065 -1.7 3.0 . 052 -1.6 . 028 -2.7 . 047 -4.00700 2.2 . 036 -1.7 . 030 2.4 . 042 -4.4077 4.2 2.3 . 040 -1.8 . 028 2.0 . 033 -3.5061 1.5 2.3 . 040 -1.9016 8.8 . 154 -3.7065 -1.4 3.5 . 061 -3.9016 8.8 . 154 -3.7065 -1.4 3.5 . 061 -3.9016 -3.9063 -3.1 1.9 . 033 -033 -031 -3.5061 -3.9063 -0.8 3.7 . 065 -1.7 . 047 -2.2 . 003 -3.7063 -0.8 3.7 . 065 -1.8 . 031 -3.5061 -3.9063 -0.8 3.7 . 065 -1.9 . 031 -3.5061 -3.9063 -0.8 3.7 . 065 -1.9 . 033 -3.5 -0.9 -3.5 -0.9 -0.9 -3.9 3.8 . 040 -2.2 -0.0 -2.3 -0.0 -2.3 -0.0 -3.5 -0.0 -0.0 -3.9 3.9 . 052 -1.9 . 052 -1.9 . 053 -3.6 -0.0 -3.9 3.1 . 054 -2.2 . 058 -3.8 -0.0 -0.0 -3.9 3.2 . 056 -1.9 . 055 -3.9 -0.0 -3.9 3.3 . 057 -1.9 . 055 -3.9 -0.0 -3.9 -0.0 -3.9 3.4 . 007 -1.8 . 051 -3.9 -0.0 -3.9 -0.0 -3.9 3.7 . 065 -1.9 . 052 -3.9 -0.0 -3.9 -0.0 -3.9 3.8 . 061 -3.9 -0.0 -3.9 -0.0 -3.9 -0.0 -3.9 3.9 . 062 -3.0 -3.0 -3.0 -3.0 -3.0 -3.0 -3.9 3.1 . 054 -3.2 . 056 -1.9 -0.0 -3.9 3.2 . 056 -1.9 -0.0 -3.9 -0.0 -3.9 3.3 . 061 -3.9 -0.0 -3.9 -0.0 -3.9 3.4 . 062 -3.9 -0.0 -3.9 -0.0 -3.9 3.7 . 065 -3.0 -3.0 -3.0 -3.0 -3.0 -3.0 -3.0 3.8 . 061 -3.9 -0.0 -3.9 -0.0 -3.9 3.9 . 061 -3.0 -3.0 -3.0 -3.0 -3.0 -3.0 3.1 . 052 -3.0 -3.0 -3.0 -3.0 -3.0 -3.0 3.2 . 061 -3.0 -3.0 -3.0 -3.0 -3.0 3.3 . 061 -3.0 -3.0 -3.0 -3.0 -3.0 3.4 . 062 -3.0 -3.0 -3.0 -3.0 -3.0 3.7 . 065 -3.0 -3.0 -3.0 -3.0 -3.0 3.8 . 061 -3.0 -3.0 -3.0 -3.0 -3.0 3.9 . 061 -3.0 -3.0 -3.0 -3.0 -3.0 3.1 . 062 -3.0 -3.0 -3.0 -3.0 -3.0 3.2 . 061 -3.0 -3.0 -3.0 3.3 . 061 -3.0 -3.0 -3.0 -3.0 3.4 . 062 -3.0 -3.0 -3.0 -3.0 3.7 . 062 -3.0 -3.0 -3.0 -3.0 3.8 . 061 -3.0 -3.0 -3.0 -3.0 3.8 . 06	. 206 9.9 . 173 12.9 . 225 -1.1 -
60106010701010023110272009200920092009202730053006300630063007400700700	.103 7.4 .129
-4.1072 -4.1072 -4.20.09 -4.20.09 -4.30.09 -4.30.09 -4.40.02 -4.40.02 -4.50.09 -4.50.09 -4.50.09 -4.61.50.03 -4.61.50.03 -4.70.03 -4.80.03 -4.90.06 -4.00	.143 7.2 .126 -1.6
5        009         2.1         .037        3        065         -2.2           1.6         .026         7.1         .124         7.6         .133        055         2.2           2.4         .042         -1.7        036         3.6         .063         -2.9        051         -2.9           1.5         .023         -1.4         .024         .9         .016         -3.3        065         -1.7           4.3         .075         -1.6         .024         .9         .016         -3.6         -1.7           4.3         .075         -1.6         .024         -4.9        086         -1.7         .067         -1.9          96         .055         -1.7         .021         -3.7        065         -1.7        07         -4.2          96         .055         .1         .062         1.4         -0.4        07         4.2           2.2         .038         1.4         .024         -4.9        063         -1.4           2.3         .046         .052         2.4         -042         -4.9        060         -1.4           2.3         .046	1.7- 861. 9.7 181.
1.6         .026         7.1         .124         7.6         .135         -5.3        058         2.2           2.4         .042         -1.7        039         3.6         .063         -2.9        051        5           3.         .065         -1.15         .7         .012         -2.4        042         -2.9           4.         .052         -1.6        026         -2.7        047         -4.9        066         -1.7           4.         .052         -1.6        026         -2.7        047         -4.9        066         -1.9           4.         .052         -1.6        026         -3.6        069         -1.0           2.         .036         -1.7         .021         -3.6        063         -7           2.         .036         -1.7         .024         -4.4        070         -1.1           2.         .036         -1.7         .036         2.4         -042         -4.4        070         -1.4           2.         .036         -1.6         -1.7         .036         2.4         -042         -4.4        070         -1.4           <	.145 9.6 .1662.5
2.4       .042       -1.7      030       3.6       .063      051      2.9         1.3       .065       -1.15       .7       .012       -2.4      042       -2.0         3.0       .052       -1.6      056       -1.7      067       -1.6      067       -1.6         4.3       .052       -1.6      028       -2.7      047       -1.0       -1.0       -1.0        9      016       2.2       .038       1.4       .024       -4.0      070       -1.1         2.2       .036       1.7       .030       2.4       .042       -4.4      077       4.2         2.2       .038       1.4       .024       -4.0      070       2.1         2.2       .038       1.4       .042       -4.4      077       4.2         2.3       .040      036       2.4       .042       -4.4      077       4.2         2.3       .040      036       2.4       .042       -4.4      077       4.2         2.3       .040      036       2.4       .042       -4.4      077       4.2         2.3	- 7 166
.3       .005       -6.6      115       .7       .012       -2.4      042       -2.0         3.0       .052       -1.6      024       .9       .016       -3.8      065       -1.7         4.3       .075       +6      024       .9       -016       -3.8      065       -1.9        9      016       1.2       .024      95       -3.6      070       2.1         2.2       .036       1.7       .036       2.4       .042       -4.4      070       2.1         2.2       .038       1.4       .024       -4.6      070       2.1         2.2       .038       1.4       .024       -4.4      077       4.2         2.2       .038       1.4       .024       -4.4      077       4.2         3.5       .061       2.6       2.6       .035       -3.5      061       11.5         2.3       .061       9.6       1.6       -1.4      077       4.2         2.5      061       9.6       1.6       -1.4      077       4.2         2.5      061       9.6       1.6       -1.7	. 202 10.7 .187
1.3       .023       1.4       .024       .916       -3.8      966       -1.6      028       -2.7      047       -4.0      070       -8       -1.6      028       -2.7      045       -4.0      070       -1.6      028       -2.7      045       -4.0      070       -1.0	.147 7.6 .133 -2.0
3.6       .852       -1.6       -828       -2.7       -847       -4.6       -879       -1.6       -1.6       -878       -4.9       -879       -1.9       -4.9       -879       -1.9       -1.9       -4.9       -1.9	5.1-
-4.9       -0.0	. 164 16.2 . 178
-4.9       -686       2.2       -636       -7.4       -676       2.1         2.2       -636       1.7       -696       2.4       -674       -677       4.2         2.3       -646       -1.6       -686       2.4       -674       -677       4.2         2.3       -646       -1.6       -686       -1.6       -3.7       -665       -1.4       -         -2.9       -651       -616       8.6       -1.6       -3.7       -665       -1.4       -         -2.9       -651       -616       8.6       -1.6       -3.7       -665       -1.4       -         -2.9       -651       -616       8.6       -1.6       -3.7       -665       -1.4       -         -2.9       -651       -616       8.6       -1.6       -3.7       -665       -1.4       -         -2.9       -651       -652       -1.6       -3.7       -665       -1.4       -       -       -       -665       -1.4       -       -       -665       -1.4       -       -       -1.4       -       -       -665       -1.4       -       -       -       -       -       -       <	445 45 4
2.2       .038       1.7       .090       2.4       .042       -4.4      077       4.2         2.3       .040      9      016       0.8      154      055       -1.4          2.3       .040      9      016       0.8      154      055       -1.4          -2.9      051       .057      051       .037       -4.1      065       -1.4          -2.7      047       2.7       .047      2      003      1      005       -1.4          -1.9      033       4.7       .047      2      003      1      005       -1.4          1.9      033       4.7       .082      4      001      03      068       4.0         1.9      033       1.8       .061      061      068      068       4.0         3.7       .065       3.1       .054       2.2       .003      061      068       4.0         3.7       .065       3.9      061      061      061      068      068      068      068      068	
3.0       .052       .1       .002       1.6       .035       .3.5      061       154       .3.7      065       -1.4          3.5       .061       .061       .061       .061      067 <td>134 7.8 .136 -1.5</td>	134 7.8 .136 -1.5
2.3       .040      9      016       0.0       .154      055       -1.4         3.5       .061       9.6       .168       -3.0      052       -1.4         -2.9      057       .047       .2.7       .047       -1.2       .065       .7         -1.9      083       .9       .016       -1.1      003       .7       .016       -1.9      066       .7         5.0       .087       4.7       .082       -1.4      061       -1.8      065       .7         5.0       .087       4.7       .082       -1.4      061       -1.8      066       7.4         1.9       .033       1.8       .031       -3.5      061       -3.9      068       4.0         3.7       .065       .7       .012       1.9       .033       -3.6      068       4.0         1.5       .026       .7       .012       1.9       .033       -3.6      063       6.8        9       .026       .7       .012       1.9       .033      053      053      053      053      054      053      054      053 <t< td=""><td>.194 10.5 .1153 11.3 .197</td></t<>	.194 10.5 .1153 11.3 .197
3.5      061       9.6      052       -1.4         -2.9      051      037       -4.1      072       2.2         -2.7      047       2.7       .047      2      063      3.7      065      7         -1.9      053      9       .016       -1.1      019       -4.9      065      7         5.0       .087       4.7       .082       -4.7      061       -3.9      068       3.1       4.4         1.5       .065       3.1       .054       2.2       .008       -3.8      068       4.3         1.5       .065       3.1       .054       2.2       .033       -3.5      068       7.4         1.5       .065       3.7       .042       3.2       .003       -3.5      063       6.8      053       4.3        9      0       <	.152 9.1
-2.9      651       .2       .063       2.1       .063       -4.1      072       2.2         -2.7      047      2      063       -3.7      065       .7         -1.9      053       4.7       .082       -4.9      086       3.1         5.0       .067       4.7       .082       -4.9      068       4.0         3.7       .065       3.1       .054       2.2       .081       -3.9      068       4.0         4       .065       3.1       .054       2.2       .033       -3.5      063       6.8        9      0	.134 6.3 .110 -2.3
-2.7047	.164 9.1 .159 -1.6
-1.9      633       .9       -616       -4.9       -686       3.1         5.6       .687       4.7       .682       -4      607       -1.8      631       4.4         1.9       .633       -3.5      661       -3.9      668       4.6         3.7       .665       3.1       .654       2.2       .938       -3.8      668       7.4         1.5       .626       .7       .912       1.9       .933       -3.5       6.8       7.3      663       6.8        9      616      2      693       -3.2       .963       -3.5      693       -4.3      7      617       -3.9      651       5.5      653      8      653      8      653      8      663       3.9      8      663       3.9      8      653      8      642       3.9      8      663       3.9      4      659      8      663       3.9      4      659      8      6       3.6      6       3.6      6       3.6      6      6       3.6      6      6       3.9      8      6	. 120 8.9 .155 1.3
5.6       .087       4.7       .082      4      087       -1.8      631       4.4         1.9       .033       1.8       .031       -3.9      063       4.0         3.7       .065       2.2       .038       -3.9      068       4.0         1.5       .026       .7       .012       1.9       .033       -3.8      066       7.3        9       .066       .9      5      099       -2.9      053       4.3         2.7       .047       3.8       .066       .8       .012       -2.4      042       3.9         -4.3      075       2.3       .040       5.2       .091       -3.4      059       2.4         3.9       .055       2.3       .040       5.2       .091       -3.4      065       2.4         3.9       .055       -3.8      065       -3.8      066       3.0	. 169 10.1 . 176
1.9 .033	.124 8.4 .147 2.0
3.7 .065 3.1 .054 2.2 .036 -3.8 .066 7.4 1.5 .026 .7 .002 1.9 .033 -3.6 .065 0.8 6.8 1.5 .026 .7 .002 1.9 .033 -3.6 .065 0.8 6.8 1.0 .003 4.3 4.3 1.6 .007 1.6 .00850092 1.051 5.5 2.7 .0047 3.8 .0668 .014 -2.4042 3.9 2.8075 2.3 .049 5.2 .091 -3.4059 2.4 3.0055 -3.8065 3.0051 2.3005 -3.8066 3.0005	6.9 .120 -1.5
1.5 .026 .7 .012 1.9 .033 -3.6 .063 6.8 4 607 1.6 608 .3.2 636 -1.9 933 4.3 4 607 1.6 628 5 609 2 631 5.5 2.7 647 3.8 666 8 614 -2.4 642 3.9 2.3 649 2.3 648 5.2 691 -3.4 659 2.4 3.6 675 2.3 648 5.2 691 -3.4 659 2.4 3.6 655 3 655 3.6 655 3.0	.112 8.4
1.9     1.0     1.2     1.00     3.2     .056     1.9     1.05     4.3       2.7     .007     1.6     .028     1.5     1.009     2.9     1.051     5.5       2.7     .004     3.8     .066     .8     .014     2.4     1.042     3.9       2.8     .049     .7     .012     -3.4     1.059     1.8       4.3     1.075     2.3     .040     5.2     .091     -3.4     1.059     2.4       3.0     .052     4.2     .073     .3     .005     -3.8     1.066     3.0	. 159 9.7
2.7     .067     1.6     .028    5    009     -2.9    051     5.5       2.7     .047     3.8     .066     .8     .014     -2.4    042     3.9       2.8     .049     .7     .012     -3.4    059    8     -       -4.3    075     2.3     .040     5.2     .091     -3.4    059     2.4       3.0     .052     4.2     .073     .3     .005     -3.8    066     3.0	. 152 9.1
2.7 .847 3.8 .866 .8 .814 -2.4842 3.9 2.8 .849 -2.3849 .7 .812 -3.485984.3875 2.3 .848 5.2 .891 -3.4859 2.4 3.8 .852 4.2 .873 3.805 -3.8866 3.8	4. 136 7.8 .136
2.8 .049 -2.3040 .7 .012 -3.405984.3075 2.3 .040 5.2 .091 -3.4059 2.4 . 3.0 .052 4.2 .073 .3 .005 -3.8066 3.0 .	.133 10.2 .178 -1.6 -
3.9 .052 4.2 .073 .3 .005 -3.8066 3.0 .	.186 7.7 .134
3.0 .052 4.2 .073 .3 .005 -3.8066 3.0	7.7 .134 -2.1
	.120 8.5 .148 6.0

	3	LANDING DATA	ı	MODEL A-7E	-76		USS ENTERPRISE (CVN-65)	ERPRI	SE (CV	<del>(</del> 62)			DAY	DAY LANDINGS	SQ.				
	P	I O	Z V	n n			ROL	٠	Σ Ω	Lu	۵.	PITCH RATE		ROLL RATE	ATE	F. P. A.	٠	YAW	
2	•	8	_	•		2		8		14		AT TO	_	AT TO	_	OT TA	۵	AT TD	٥
DEG	3	DEC	2	DEG	3	DEG	8	DEC	SAD O	DEG	8	DEC	3	DEG	3	DEC	3	DEG	3
	\$	‡	<b>5</b>	<b>\$</b>	4	\$	40	20	2	22	53	<b>3</b>	22	26	57	<b>5</b>	23	2	5
_	.13		22		'	-2.4 -		2.8	949		7	i +	. 059 2	2.9	.051 -2		935	. 5.5	961
<b></b> .		10.2	92	,					.031					i		-	982		669
٠. د د	2		:	10.4	181	 - 4	854	•		-2.1 -	<del>0</del> 54 3								<b>8</b> 38
	35	•				   •   •	. 617 7 6 6	ا م ب	. <b>99</b> 2		ار 10 -		066 1	• ·	.024 -3.8 095 -1 0		966 	6. c	628
	12.		3		•				3		7					•		9.0	.052
	.127		. 155		ſ			-2.2 -	038		2.7				7				9.99
	.136	9.9	. 110		1			, L	619		7	١						2.5	.044
			•		ı	_		ı	į		4.0							1 <b>6</b> .0	. 175
			.126		•		1	6 6	031		-7.0				087 -3.7		965	<b>4</b> (	. 667
					ſ	ו פּ פּ	866 - 844		. 628		, . , .		1.000 -3.5		000	; (	e/2 - 982	, s	9. 8. 8. 8. 8. 8. 8. 8. 8. 8. 8. 8. 8. 8.
		•	.157		1	ı			026		9 6				879	•			
		8.8	154		•				049							2			.058
		•	. 140						636		_				1	-		3.0	.052
		•	.157		T				061		5.0		•						. 665
		- •			i		020		<b>)</b>		N •	7.7	6.2 8.3		9.07 449. I		700.		949. 978
		0.0	8 2			•		- G	163		- 1	. 1						2.0	. 035
		8.7	. 152		1	•			.021		ં તં		~						667
		8.2	.143		•				.026		<del>-</del>								.079
		7.0	.152		T				- 689		•		. e16 . s	~ -	.091	٠,	063		023
_			? =		,	2.7.	070.		602 6.37		- 1		- 616 -2.1		2.637 -3.5 5.637 -3.5			2.1	. 037
_			159		ı	1		- 10	010							•		. 🕳	. 967
			.176		T	•	•		689		•	· -		_	101 3.6			_	024
_			<b>2</b>						.051		- '				7	_		2.8	.651
7.7	126	- 0	8C -		•	- ' ' <del>-</del>	012 -2 024	6.7 6.7	1.051 AAA			· ·	.838 /	9.4	77	_	e/2 - 956	<b>D C</b>	. 032 010
		S .	2		•	ا ءه خ			940		•							2.7	. 047
		•	142		ī		•	ı	410		i <del>-</del>								021
_		4.0	.147		ſ		_		. 030		₹				.149 -2	i +	042		007
_	118	8.5	. 148		ı	1 7.7	677		.010		<del>-</del>				.147 -2.6				9.00
_	25.	-	. 159						. 091		-2.0								014
_	÷ :	9.7	19:		1	_		1.2	.021		•			<b>.</b>	7				. 636
_	. 145	9.5	191		ı				416		_			<b>40</b> I	7		•		019
8.2	.143	8.5	143	•		<b>.</b>			.026					5.7	S- 660.	ï	<del>0</del> 56		007
<u>.</u>	164	8. S	. 166	r.	. 162	- (	002	í Ť	007	• •	.624 -3.2		056 5		7.		072	 	. <del>0</del> 21
	÷.		;		T.	Ŋ.			3		_				1.	i Be	9/9	? r	. 623
_	. 158		. 140		ľ	- 2.1	637 -1	 ◆	624		•	N	.ee3 -5.	i 7	. 189.	i D	999	•	. 612

		3	LANDING DATA	1	MODEL A-7E	7.		uss	ENTER	USS ENTERPRISE (CVN-65)	;9-₩-)	3			Ď	DAY LANDINGS	INGS				
3		P 1 4	HOL	2 2	n n			œ	0 6	<b>x</b>	G L E		1	PITCH RATE	ATE	ROLL RATE	MTE	r.	F. P. A.	YAW	
2	5		8		4			5		8		<b>1</b>		AT TD	۵	AT TD	٩	AT TD	5	AT TD	2
	DEG	3	DEC	3	930	3	DEG	9 <b>X</b>		DEG R	<b>8</b>	DEG R	SZ.	DEC	3	OEG	3	DEG	8	DEC	2
<b>∓</b>	7	\$	‡	ŧ.	<b>\$</b>	47	\$	49	80	55	25	53		24	22	28	22	8	20	99	5
100				.176		•	4.	824	•	910.			7		944	-			668	9.9	9.00
5 6 5	- 7	141	7 0	<u> </u>					7 7	. 635	·^		6 1		. 168 	6 4 6 4	1994	9. Y	<b>0</b> 52 - <b>0</b> 61	4. <b>«</b>	799.
201				<del>-</del>		•	2.5	056		939			5.3							-1.2	021
202				. 169			٠. د	885	•		•		•	•				- 4.5-			637
į				150			<b>†</b> ·	667	8.9		•		7.					•		n	058
2 6				108			+ o	007		C00			ا ن د		2- 200	-2.8 		2.5.	. 646. I	2.0	049
212		-			10.5	183		.026	: ï	092	7.5	.026	8					- 10	. 963		916
215							2	.005	•	035			*	•					963	8.7	.117
629				.141			3.7	. 065	۳.	. 916			<b>÷</b>	_	_	_	-	7.7	073	0. 0.	. 033
2				. 126			7	002	ï	016	_		2.8		,	1		*	059	.2	003
645				126			=	.019	+	. 689	•		5.0	<b>.</b>		~			054	4.0	. 986
3		-		.211		•	7	072	, ,	<b>†60</b>	<b>.</b>		6	٠,	_				<b>9</b> 61	ų.	600
672				. 162 162			4.4	. 642	4	419.	- ~		-	_	931	5.0	. 1986 1. 1.	7.7		ດ່ອ	101
999				175			~	. 993	6	.112	. ~		4.8	_				•	656	2.7	.047
<b>8</b> 9				. 166			2	003	9.	9.99	•		4			•		•	673	5.5	960.
694				. 162			7	012	4	. 686	<b></b>		•			12.7		•	058	<b>+</b> . <b>+</b>	.677
600				3			<b>†</b>	007		•	_		-2.3	•				ø	668	5.8	.051
<b>*</b> :							? •	80. 8	2.	. 691	_ ^		4. A		. 982 - 999	6 - 6 - 1 -	016 -3		963 	4 4 - 4	.072
712				145			?	- 993		416			2.5		949	•		ب د	-,045	7.7	134
714				991.			3.0	.063	_	710.			9.9	•		3.0			682	8.8	15
715					9.2	161	J. 3	.023	•	. 667	7 1.3	. 023					.047 -2	'n	044	5.3	. 692
716				.145			S. 0	. 052	4	. 982	~		•				052 -1	'n	023	5.1	.089
720				.155				.012	Ξ	.019	•		3.5		. 961	<b>.</b>		٥.	103	4.0	. 164
726				136			1.7	. 636			~		7.7	•	075-13.	_	-	•	049	<b>4</b> .4	.075
1929				99 :			2.2	.038	~	_			7.5		1	•	052 -3	•	052	J.,	. 654
199		-		.202			2.5	.038	7	028	<b>.</b>		i	i n	_	e :		•	- 679		024
3				356			Ď.	9.	#. •	. 986	<b>.</b>		'n	Da	. 109.	?	949	-3.2	056 -	7.7	003

	REREAD	NUMBER			•	7	•	N <b>G</b>	۰ م	•	•	8	•	N (	<b>.</b>	<b>D</b> (	v «	•	•	•	~	8	- (	<b>D</b> (	<b>-</b>	-	_	- (	• •	4 @	•	-	-	<b>-</b>	•	•	<b>o</b> (	~	<b>.</b>	Þ
			3	82	•	•	•	e e	9 9	9.0	9.	0.0	•	9.0	<b>.</b>	9.6		0.0	9.0	9.0	9.9	9.9	6.0	9 G	9 6	0.0	9.0	<b>.</b>	e		0.0	9.0	9.9	0.0	•	<b>6</b> .6	<b>9</b> .0	6. 6.	e (	Þ.
	APR CEAR	RUNOUTS	N.		•	•					•	•	•	9 ·	D (	P 6	P 6			•	•			D (					D 9	) G		•	•	•		-	<b>6</b>	B (		D D
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	BAROMETRIC	PRESSURE	子	2															763.5	763.5	763.5	763.5	763.5	763.5	763.5	763.5	763.5	763.5	763.5	763.5	763.5	763.5	763.5	763.5	765.8	765.8	765.8	765.8	765.8	65.0
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FLUDG FLAP SHIP DECK PITCH DECK ROLL TEMP F C III																		
FIANCE NO. NO. TYPE CODE SPEED  MAYS DEC RAD DEC RAD F C IN  1	RAME TO 1	_	SIDE		3	풄		ECK P.	<u>₹</u>	DECK	POLL	10	•	BAROMETRIC	TRIC	8	APR CEAR	REREAD
MAYS         DEG         RAD         DEG         RAD         DEG         RAD         DEG         RAD         PA         71         72         73         74         75         76         77         76           86         2         1         22         2         1         -002         -1         -005         59         15           73         2         233         50120         4         2         -1         -002         -1         -005         59         15           84         4         234         50120         4         2         -1         -002         -1         -005         59         15         60         15         100         59         15         15         100         59         15         15         15         15         15         15         15         16         15         16         16         16         16         16         16         16         16         16         16         16         16         16         16         15         16         16         16         16         16         16         16         16         16         16         16         16         16 </th <th>DISTANCE</th> <th></th> <th>Š</th> <th>TYPE</th> <th><b>300</b></th> <th><b>3</b>8</th> <th>8</th> <th></th> <th></th> <th></th> <th></th> <th></th> <th></th> <th>PRESSURE</th> <th>URE</th> <th>\$</th> <th>RUNOUTS</th> <th>NUMBER</th>	DISTANCE		Š	TYPE	<b>300</b>	<b>3</b> 8	8							PRESSURE	URE	\$	RUNOUTS	NUMBER
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91         4         245         59123         5        4        967         -1.4        924         61         16           73         2         237         59126         5         3        2        963        9        916         61         16           73         2         237         59126         5         3        5        969         -1.1        919         61         16           83         2         2        963         -1.1        919         61         16           77         3         251         59126         5         3        2        963         -1.1        919         61         16           84         4         234         59126         5         3        3        960         -1.1        919         61         16           84         4         234         59126         5         3        3        960         -1.1        919         61         16           84         4         234         59126         5         3        7        962         -1.1        919         61         16 </td <td></td> <td>_</td> <td>245</td> <td>60123</td> <td></td> <td>'n</td> <td>n</td> <td></td> <td></td> <td></td> <td></td> <td>69</td> <td></td> <td>30.06</td> <td>763.5</td> <td></td> <td>429.3</td> <td>•</td>		_	245	60123		'n	n					69		30.06	763.5		429.3	•
73         2 251         56106         5         3         -2        063        9        016         61         16           72         2 237         56126         5         3        2        069         -1.1        016         61         16           73         2 245         56123         5         3        2        069         -1.1        016         61         16           77         3 245         56123         5         3        2        063         -1.4        024         61         16           84         4 234         56126         5         3        3        062         -1.4        024         61         16           84         4 234         56126         5         3        1        062         -1.1        019         61         16           84         4 234         56126         5         3        1        062         -1.1        019         61         16           84         4 234         56126         5         3        1        062         -1.1        062         -1.1        016         61         16<	-	<b>*</b>	245	50123		8	i n	•			. 024	5		30.08	763.5		431.8	-
84       2       237       56126       5       3      5      609       -1,1      619       61       16         73       2       2.34       56126       5       3      6      619       61       16         76       3       2.54       56123       5       3      6      619       61       16         87       4       234       56123       5       3      7      602       -1,1      619       61       16         84       4       234       56126       5       3      7      602       -1,1      619       61       16         84       4       234       56126       5       3      7      602       -1,1      619       61       16         84       4       234       56126       5       3      7      612      619       61       16         84       4       234       56126       5       3      7      612      619       61       16         84       4       234       56126       5       3      7      612       62       17		n -	251	<b>50108</b>		5	i i				.016	5		30.06	763.5		429.3	-
72       2.34       50120       5       3       -5       -009       -1,1       -019       61       16         73       2.25       50120       5       3       -6       -010       -1,2       -021       61       16         77       3       251       50123       5       3       -2       -005       -1,1       -019       61       16         84       4       251       50120       5       3       -1       -005       -1,1       -019       61       16         84       4       251       50120       5       3       -1       -002       -1,1       -019       61       16         84       4       251       50120       5       3       -1       -002       -1,1       -019       61       16         84       4       251       50100       4       2       -1       -002       -1       -014       61       16         84       4       251       50100       4       2       -1       -002       -1       -014       61       16       16       16       16       16       16       16       16       16		7	237	50120		6	n					5		30.06	763.5		429.3	_
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87       4       234       596120       5       3       -1       -1095       -1       -1045       61       16         84       4       231       59620       5       3       -1       -1095       -1       -1049       61       16         84       4       231       596120       5       3       -1       -1095       -1       -1049       61       16       17       16       2       17       16       2       17       16       2       17       16       2       17       16       2       17       16       2       17       16       2       17       16       2       17       16       2       17       16       2       17       16       2       17       16       2       17       16       2       17 <td></td> <td>n :</td> <td>243</td> <td>50123</td> <td></td> <td><b>6</b>0 1</td> <td>i D</td> <td></td> <td></td> <td></td> <td>9.5</td> <td><b>5</b> :</td> <td></td> <td>9.00</td> <td>763.5</td> <td>9</td> <td>429.3</td> <td>- (</td>		n :	243	50123		<b>6</b> 0 1	i D				9.5	<b>5</b> :		9.00	763.5	9	429.3	- (
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## **EA-6 DAY**

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5. Mol. W/S         INI         SP-AR.         MIN         SP-A         TD         FF           5. Mol. W/S         INI         W/S         INI         I/S         II	VPAF VE-FI	VE-F1	Æ-F1		3	*	N-ONI	ᇳ		VEOR	\$	NIW.	Ş	٧.	KVPA	≩	LIFE			IGHT
6         7         8         10         14         15         16         17         18         19         20           25         13         4         2         10         11         12         13         14         15         16         17         18         19         24           25         13         4         2         137         76         168         178         19         24         11           26         13         4         2         137         76         168         168         24437         111           26         13         5         3         137         76         168         178         18         24         22         24437         111           26         13         5         3         135         69         168         168         24137         18           24         12         13         67         168         168         168         24137         18           24         12         13         67         168         168         179         18         18         18         24         18         18         24         18	2					Ž	<b>.:</b>	PER							Z		5	<b>F</b>		
25         13         4         15         14         15         16         17         18         24           25         13         4         2         134         78         1.85         1.85         1.86         1.86         1.86         24437           26         13         5         3         135         68         1.86         1.86         1.86         24437           26         13         5         3         135         68         1.86         1.86         24337           26         13         5         3         135         68         1.86         1.86         24337           26         13         6         1.81         1.86         24337           26         13         6         1.81         1.86         24337           26         13         6         1.86         1.86         24337           26         13         6         1.86         1.86         24337           26         13         6         1.86         1.86         24337           26         13         13         6         1.16         24337           26         13	1 NO1 S/71 NO1	5	-	-								Ş	₹	s/x					8	X
25         13         4         2         136         76         1.61         .96         24437           26         13         4         2         134         69         1.65         1.26         24437           26         13         5         3         135         69         1.66         1.16         24137           26         13         5         3         135         69         1.66         1.66         24137           26         13         5         3         135         69         1.61         24137           24         12         4         2         135         69         1.61         1.66         23137           24         12         4         2         135         69         1.60         24437           24         12         4         2         135         69         1.60         24437           24         12         4         2         135         69         1.60         24437           25         13         4         2         135         69         1.60         24437           26         13         4         2         135 <th>+</th> <th>•</th> <th>+</th> <th>-,</th> <th>r</th> <th></th> <th>_</th> <th>•</th> <th>_</th> <th></th> <th></th> <th>5</th> <th><b>±</b></th> <th>ž.</th> <th><b>e</b></th> <th>11</th> <th>5</th> <th><u>.</u></th> <th><b>50</b></th> <th>21</th>	+	•	+	-,	r		_	•	_			5	<b>±</b>	ž.	<b>e</b>	11	5	<u>.</u>	<b>50</b>	21
25         13         4         2         134         78         1,65         1,26         24637           26         13         5         134         69         1,63         1,16         24137           26         13         5         3         135         69         1,66         1,26         24637           26         13         5         3         135         69         1,66         1,69         24137           26         13         5         135         68         1,61         1,69         25137           24         12         4         2         135         69         1,69         25137           24         12         4         2         135         69         1,69         24137           24         12         4         2         135         69         1,69         24137           24         12         4         2         135         69         1,69         2437           26         13         6         1,69         1,69         2437         2437           26         13         6         1,14         1,16         1,13         2437	71 113	1 113 5	5			22	n	•	8		5	92			1.0		Š	_	24437	11665
26         13         5         3         134         69         1,65         1,26         2,83,7           26         13         5         3         135         69         1,69         1,10         24137           26         13         5         3         135         69         1,69         2,6137           26         13         63         1,61         1,69         2,5137           24         12         132         68         1,61         1,69         2,5137           24         12         135         69         1,61         1,69         2,5137           24         12         135         69         1,61         1,69         2,5137           24         12         135         69         1,69         1,19         2,5137           26         13         67         1,69         1,19         1,19         2,5137           26         13         67         1,69         1,19         1,19         2,5137           26         13         69         1,19         1,19         1,19         2,5137           26         13         4         2         1,35         69	43 74 118 6	118 6	• •			2	~	•	8		137				1.05		- 8	_	24637	11175
26         13         76         .89         1.00         24837           26         13         69         1.00         24137           26         13         69         1.00         25137           26         13         69         1.00         25137           26         12         69         1.00         25137           26         13         69         1.01         1.00         25137           26         12         69         1.01         26137           26         13         69         1.01         26137           26         13         69         1.01         1.00         25137           26         13         66         1.03         1.00         21437           26         13         66         1.03         1.00         22437           26         13         66         1.03         1.00         22437           26         13         67         1.00         2137           27         13         69         1.00         2437           28         13         63         1.00         1.00         2437           28	73 116	3 T T T T	<b>3</b> (			2	n	<b>.</b>	n		2	_			1.05		1.20	_	23837	10812
26         13         5         3         135         69         1,10         24137           26         13         5         3         135         68         1,90         1,10         24137           26         12         13         68         1,91         1,96         23137           26         12         13         68         1,91         1,96         23137           26         12         13         68         1,91         1,96         23137           26         13         68         1,93         1,16         2437           26         13         68         1,16         1,16         2437           26         13         66         1,16         1,16         2437           26         13         13         66         1,16         2437           26         13         13         66         1,16         2437           26         13         13         66         1,16         2437           26         13         13         67         1,16         2437           27         13         13         69         1,16         2437	36 76 116 55		in i			- · 2 :	<b>,</b>	<b>د</b> د	<b>છ</b> 1		137				66.		1.98		24837	11266
24         12         6         1.06         256.77           24         12         4         2         112         66         1.01         1.06         24.137           24         12         4         2         113         67         1.03         1.10         226.37           24         12         4         2         135         68         1.03         1.10         226.37           24         12         12         66         1.03         1.10         226.37           26         13         5         3         125         66         1.03         1.10         226.37           26         13         5         3         126         66         1.03         1.10         226.37           26         13         5         3         126         66         1.03         1.10         226.37           26         13         12         66         1.03         1.10         24.137           26         13         12         66         1.03         1.10         24.137           27         13         13         67         1.93         1.10         24.137	72 113		7 in			 8 =	<b>7</b> -	n u	n =		5 5						9 .		24137	18949
24         12         4         2         132         68         .98         1.00         23137           24         12         4         2         132         68         1.01         .90         23137           24         12         4         2         131         67         1.03         1.10         22637           26         13         5         3         123         66         1.10         1.10         22637           26         13         5         3         123         66         1.10         1.10         22637           26         13         5         3         123         66         1.10         1.10         22637           26         13         6         1.10         1.10         24137         22637           26         13         6         1.10         1.10         24137         22637           26         13         6         1.10         1.10         24137         22637         24537           26         13         6         1.10         1.10         24137         24537         24537         24537           26         13         4	68 167	167					) P1	, ru	. P		3 5				96				25837	11357
24         12         4         2         135         69         1.01         .99         23137           24         12         4         2         135         69         1.01         1.00         24137           24         12         4         2         132         66         1.03         1.10         22637           26         13         5         3         128         66         1.06         1.00         21437           26         13         5         3         128         66         1.06         21437           26         13         6         1.10         1.00         24337           26         13         6         1.10         1.00         24337           26         13         6         1.00         24337           27         13         6         1.00         24337           28         13         13         6         1.00         24337           29         13         4         2         136         1.00         24337           29         13         4         2         136         1.00         24337           29	96 165	163 5	ι. S			- *	~	•	. ~		132	_			86		2	_	23137	10495
24         12         4         2         135         69         .97         1.00         24137           24         12         4         2         131         67         1.03         1.10         22637           26         13         5         3         128         66         1.00         1.10         22637           26         13         5         3         128         66         1.00         1.10         22637           26         13         5         3         127         69         1.00         21437           26         13         6         1.10         1.00         24137           26         13         6         1.10         1.00         24137           26         13         6         1.10         1.10         24137           26         13         6         1.00         1.10         24137           26         13         6         1.00         1.10         24137           26         13         6         1.00         1.10         24137           26         13         7         1.00         1.00         24537           26 <th>62 110</th> <th>3 116 5</th> <th></th> <th></th> <th>-</th> <th>- 2</th> <th>7</th> <th>•</th> <th>~</th> <th></th> <th>132</th> <th>_</th> <th></th> <th></th> <th>1.01</th> <th></th> <th>96.</th> <th>_</th> <th>23137</th> <th>16495</th>	62 110	3 116 5			-	- 2	7	•	~		132	_			1.01		96.	_	23137	16495
24         12         4         2         131         67         1.63         1.16         22637           26         13         5         3         126         66         1.10         1.16         22637           26         13         5         3         128         66         1.10         1.10         22637           26         13         5         3         128         66         1.10         1.00         22637           26         13         5         3         128         66         1.10         1.00         22637           26         13         5         3         135         69         1.00         24137           24         12         135         69         1.00         1.00         22637           24         12         135         69         1.00         1.00         22637           24         12         135         69         1.00         1.00         22637           25         13         4         2         136         70         1.00         1.00         22637           25         13         4         2         136         70	67 107	7 167 5	5	-7		- 2	~	··	2		135				.97		1.00	_	24137	10949
24         12         4         2         132         66         1.00         1.10         22837           26         13         5         3         131         67         1.06         1.00         22437           26         13         5         3         132         66         1.00         1.00         22437           26         13         5         3         128         66         1.00         1.00         22437           26         13         5         3         128         69         1.00         24137           26         13         4         2         135         69         1.00         24137           24         12         4         2         135         69         1.00         24137           24         12         13         67         1.05         1.00         24137           25         13         4         2         136         70         1.00         24337           25         13         4         2         136         70         1.00         24537           25         13         4         2         136         70         1.0	69 110	9 110 5	•			_	8	···	~		131				1.03		1.10		22637	10268
26         13         5         3         128         66         110         110         21437           26         13         5         3         128         66         1.06         1.06         21437           26         13         5         3         127         65         1.10         1.06         21437           26         13         5         3         135         69         1.14         1.10         22437           24         12         4         2         135         69         1.00         2437           24         12         4         2         135         69         1.00         24537           24         12         4         2         135         69         1.00         24537           25         13         4         2         135         69         1.00         24537           25         13         4         2         135         69         1.00         24537           25         13         4         2         135         70         1.00         24537           25         13         4         2         135         70	36 70 112 5	112 5	2	~		- *	7	•	~		132				1.03		1.10		22837	10359
28         13         67         1,06         1,06         22637           28         13         65         1,10         1,00         21437           26         13         5         3         128         66         1,10         1,00         21437           26         13         5         3         135         69         1,10         1,10         24137           24         12         135         69         1,00         24137 <td< th=""><th>72 114</th><th>2 114 5</th><th>4</th><th>•</th><th></th><th>~ %</th><th>n</th><th>'n</th><th>n</th><th></th><th>128</th><th></th><th></th><th></th><th>1.10</th><th></th><th>1.10</th><th>_</th><th>21437</th><th>9724</th></td<>	72 114	2 114 5	4	•		~ %	n	'n	n		128				1.10		1.10	_	21437	9724
28         13         5         3         128         66         1.16         1.09         21437           26         13         5         3         128         66         1.16         1.09         24137           26         13         4         2         135         69         1.16         24137           24         12         4         2         135         69         1.09         1.16         24137           24         12         4         2         135         69         1.09         1.16         24337           24         12         13         69         1.09         1.20         24437           24         12         13         69         1.09         1.20         24337           25         13         4         2         136         70         1.00         1.00         24537           25         13         4         2         136         70         1.00         1.00         24537           25         13         4         2         136         70         1.00         1.00         24537           25         13         4         2	71 112	12 5	<b>6</b> 0	~ `		- 2	n	•n	n		131				1.06		- 9	_	22637	10268
26         13         5         3         127         65         1.16         1.19         24137           26         13         6         1.14         1.19         24137           26         13         6         1.06         1.19         24137           24         12         135         69         1.06         24637           24         12         135         69         1.06         24637           24         12         135         69         1.09         1.36         24137           25         13         4         2         136         70         1.09         1.09         24537           25         13         4         2         136         70         1.09         1.00         24537           25         13         4         2         136         70         1.00         24537           25         13         4         2         136         70         1.00         24337           25         13         4         2         136         71         1.00         24337           25         13         4         2         136         71	67 105	201	io io	<b>x</b> !		۰ ب	n	ທ	<b>.</b>		128				1.03		- 00		21437	9724
25         13         69         1.14         1.19         24137           26         13         69         1.14         1.19         24137           24         12         135         69         1.00         24137           24         12         135         69         1.00         24537           24         12         135         69         1.00         24537           25         13         4         2         136         70         1.00         24537           25         13         4         2         136         70         1.00         24537           25         13         4         2         136         70         1.00         24537           25         13         4         2         136         70         1.00         24537           25         13         4         2         136         70         1.00         24537           25         13         4         2         136         71         1.00         24537           25         13         4         2         136         71         1.00         24537           25	72 114	***	<b>+</b> 9			- · 2:	י מ	י מ	י מ		127						<b>8</b> .		21137	9288
24         12         4         2         135         69         1.06         1.16         2337           24         12         4         2         135         69         1.06         1.16         24537           25         13         4         2         136         76         1.99         1.26         24537           25         13         4         2         136         76         1.99         1.06         24537           25         13         4         2         136         76         1.99         1.06         24537           25         13         4         2         136         76         1.09         1.00         24537           25         13         4         2         136         76         1.06         1.00         24537           25         13         4         2         136         77         1.06         24537           25         13         4         2         138         71         1.06         24937           25         13         4         2         138         71         1.06         24937           25         13	821 99	- •		X:		- · e :	<b>?</b> •	. ·	<b>.</b>		2				<u>*</u> ;				7413/	24894
24         12         4         2         137         76         1.65         1.69         24537           24         12         4         2         131         67         1.99         1.20         24137           25         13         4         2         135         69         1.09         1.20         24137           25         13         4         2         136         70         1.09         1.09         24537           25         13         4         2         136         70         1.09         1.09         24537           25         13         4         2         136         70         1.09         1.09         24537           25         13         4         2         136         71         1.06         24537           25         13         4         2         138         71         1.06         24537           33         17         6         3         138         71         1.06         24537           35         16         6         3         138         71         1.06         24537           35         16         6         3<			) <del>-</del>	٤,		3 2	, c	• •			135						1.00		23937	18858
24         12         4         2         131         67         .99         1.36         22737           25         13         4         2         135         69         1.09         1.26         24137           25         13         4         2         136         70         1.09         1.00         24537           25         13         4         2         136         70         1.00         1.00         24537           25         13         4         2         136         70         1.00         1.00         24537           25         13         4         2         136         71         1.00         24537           25         13         4         2         136         71         1.00         24537           33         17         6         3         138         71         1.00         24537           35         16         6         3         138         71         1.00         24537           35         16         6         3         138         71         1.00         26937           35         16         6         3         138 <th>7</th> <th>-</th> <th></th> <th>=</th> <th></th> <th>- *</th> <th>. ~</th> <th>•</th> <th>. ~</th> <th></th> <th>137</th> <th></th> <th></th> <th></th> <th>1.05</th> <th></th> <th>-</th> <th>_</th> <th>24637</th> <th>11175</th>	7	-		=		- *	. ~	•	. ~		137				1.05		-	_	24637	11175
25         13         4         2         135         69         1.09         1.26         24537           25         13         4         2         136         70         1.03         1.06         24537           25         13         4         2         136         70         1.09         24537           25         13         4         2         136         70         1.09         1.09         24537           25         13         4         2         136         71         1.06         2437           25         13         4         2         136         71         1.06         2437           33         17         6         3         138         71         1.29         .96         2437           33         17         6         3         138         71         1.06         .96         2437           35         16         6         3         138         71         1.06         .96         2437           35         16         6         3         138         71         1.06         .96         24537           32         16         6	99	_	υ 10	X		- 2	7	•	~		131				66.		1.30		22737	10314
25     13     4     2     136     76     1.63     1.69     24537       25     13     4     2     135     76     1.69     1.69     24537       25     13     4     2     136     76     1.69     1.69     24537       25     13     4     2     136     76     1.69     1.69     2437       25     13     4     2     136     71     1.66     39     2437       33     17     6     3     138     71     1.29     39     2437       35     16     6     3     138     71     1.64     39     24837       25     13     4     2     138     71     1.64     39     24837       35     16     6     3     138     71     1.64     39     24837       35     16     6     3     138     71     1.16     1.39     24537       35     16     6     3     138     71     1.16     1.39     24537       35     16     6     3     134     69     1.69     23137       35     16     6     3     134     6	76 122 (	_	8	2		ت ت	~	···	~		135				1.09		1.20	_	24137	10949
25         13         4         2         136         76         .99         1.06         24537           25         13         4         2         136         6         1.00         1.00         22037           25         13         4         2         136         7         1.00         1.00         22137           25         13         4         2         136         71         1.00         2337           33         17         6         3         138         71         1.29         .90         24937           33         17         6         3         138         71         1.29         .90         24937           35         16         6         3         138         71         1.00         24937           25         13         4         2         138         71         1.00         24937           35         16         6         3         138         71         1.00         24937           35         16         6         3         138         71         1.10         25137           32         16         6         3         135		9 :		3		- ເຂ	<b>n</b>	•	~		136				1.03		<b>6</b> .	_	24537	11130
25     13     4     2     136     70     1.00     1.00     22137       25     13     4     2     130     67     1.00     1.00     22137       25     13     4     2     136     71     1.00     20337       33     17     6     3     136     71     1.29     .90     24937       35     16     6     3     137     70     1.00     24837       35     16     6     3     138     71     1.00     24837       35     16     6     3     138     71     1.10     1.10     24837       32     16     6     3     138     71     1.10     1.10     24537       32     16     6     3     135     70     1.10     1.30     24537       32     16     6     3     135     69     1.00     23137       32     16     6     3     134     69     1.00     23537       31     16     5     3     134     69     1.00     23137       32     16     6     3     135     68     1.00     23137       32	35 69 11 <b>6</b> 117 117 117 117 117 117 117 117 117 11	- •	•	ō.		 2 ±	n =	• •	~ .		136				6.				24537	11130
25       13       4       2       130       67       1.06       22137         25       13       4       2       135       68       .96       2337         33       17       6       3       136       71       1.29       .96       25137         32       16       6       3       137       70       1.06       24837         25       13       4       2       138       71       1.04       .96       24837         32       16       6       3       138       71       1.10       1.10       25137         32       16       6       3       135       79       1.11       1.20       24537         32       16       6       3       135       69       1.06       23137         32       16       6       3       134       69       1.06       23537         32       16       6       3       134       69       1.06       23537         31       16       5       3       135       68       1.06       23137         32       16       6       3       135       69	2	-				•	) P7	•			136				8		-		24337	110.39
25         13         4         2         133         68         .96         1.00         23337           33         17         6         3         136         71         1.06         .90         25137           33         17         6         3         136         71         1.29         .90         24937           32         16         6         3         138         71         1.04         .90         24937           32         16         6         3         138         71         1.10         1.10         25137           32         16         6         3         136         79         1.11         1.20         24537           32         16         6         3         135         69         1.14         1.20         24537           32         16         6         3         134         69         1.09         1.09         23137           32         16         6         3         134         69         1.09         23137           31         16         5         3         135         68         1.09         23137           32         1		2	9	: 3		_	n	•	. ~		5				.03		1.1	_	22137	10041
33         17         6         3         138         71         1.06         .96         25137           33         17         6         3         136         71         1.29         .96         24937           32         16         6         3         136         71         1.04         .96         24837           32         16         6         3         136         71         1.10         1.10         25137           32         16         6         3         135         69         1.14         1.20         24537           32         16         6         3         132         68         1.09         1.09         24537           32         16         6         3         134         69         1.09         23137           32         16         5         3         134         69         1.09         2357           31         16         5         3         135         68         1.09         23137           32         16         6         3         135         69         24137           32         16         5         3         135		7 165	ω 	X	~	-	n	···	8		55				86.		1.00	_	23337	10586
33     17     6     3     136     71     1.29     .96     24837       32     16     6     3     137     76     1.64     .96     24837       25     13     4     2     136     71     1.16     1.16     25137       32     16     6     3     135     69     1.16     1.36     24537       32     16     6     3     132     68     1.69     23137       32     16     6     3     134     69     1.69     23137       31     16     5     3     135     68     1.69     23137       31     16     5     3     135     68     1.69     1.19     23137       32     16     6     3     135     68     1.69     23137       32     16     6     3     135     68     1.69     23137       32     16     6     3     135     68     1.99     24137	76 114 5	#=	<del>.</del>	×		_	7	•	n		138	•			1.06		<b>8</b> 6.	_	25137	11402
32     16     6     3     137     70     1.02     1.06     24837       25     13     4     2     136     71     1.04     .90     25837       32     16     6     3     136     70     1.10     1.10     24537       32     16     6     3     135     69     1.09     24537       32     16     6     3     134     69     1.09     23137       31     16     5     3     135     68     1.09     1.00     23537       31     16     5     3     135     68     1.09     1.10     23137       32     16     6     3     135     68     1.09     23137       32     16     6     3     135     68     1.09     23137		± =	т •	2	~; -	2	7	•	•		138	•			1.29		86.	_	24937	11311
25     13     4     2     136     71     1.64     .96     25637       32     16     6     3     136     79     1.16     1.36     25137       32     16     6     3     135     69     1.69     24537       32     16     6     3     132     68     1.69     1.69     23137       32     16     6     3     134     69     1.69     23137       31     16     5     3     135     68     1.69     23137       32     16     6     3     135     69     24137	72 166	20 T	9	*	~7 ·	_	•	•	n		137	•			1.02		- - -	_	24837	11266
32     16     6     3     136     76     1.16     1.19     25137       32     16     6     3     135     69     1.14     1.20     24137       32     16     6     3     132     68     1.69     1.69     23137       32     16     6     3     134     69     1.69     1.90     23537       31     16     5     3     132     68     1.69     1.19     23137       32     16     6     3     135     69     24137		118		=		_	<b>m</b>	•	~		50	-			<b>.</b>		8	_	25037	11357
32 16 6 3     136 70     1.16     1.30     24537       32 16 6 3     135 69     1.14     1.20     24137       32 16 6 3     134 69     1.09     1.00     23137       31 16 5 3     132 68     1.09     1.00     23637       31 16 5 3     135 69     1.09     23137       32 16 6 3     135 69     .99     24137	_	_	• •	:2		~ ~	•	•	n		138						1.10	_	25137	11402
32 16 6 3     135 69     1.14     1.20     24137       32 16 6 3     134 69     1.09     1.09     23137       32 16 6 3     132 68     1.05     1.09     23537       31 16 5 3     132 68     1.09     1.10     23137       32 16 6 3     135 69     .99     24137	2	_	- 9. :	<b>ä</b> '		۔ ا	•	•	m.		136				1.18		4.38		24537	11130
32 16 6 3     132 68     1.09     1.09     23137       32 16 6 3     134 69     1.05     1.09     23637       31 16 5 3     132 68     1.09     1.10     23137       32 16 6 3     135 69     .99     24137	- 28	_	- N	8		- 2	•	•	n		135				<b>*</b> :-		1.20	_	24137	10949
32 16     6     3     134 69     1.05     1.09     23637       31 16     5     3     132 68     1.09     1.10     23137       32 16     6     3     135 69     .99     24137		_	~	×		-	•	•	•		132	_			1.09		1.00		23137	10495
31 16 5 3 132 68 1.09 1.19 23137 1 32 16 6 3 135 69 .99 .99 .24137	40 72 108	20 E	9	*		2	•	<b>•</b>	n		134				1.05		1.00		23637	10722
32 16 6 3 135 69 . 99 . 99 . 24137	45 75 114	<b>*</b>	<b>+</b>	ភ		_ ·	•	<b>.</b>	n		132				1.09		1.19		23137	10495
	_	162	<u></u>	2		~	•	•	n		135				66.		86.		24137	16949

			3	ING DATA - MODEL A-7E	1	HODEL	A-7E		5	USS ENT	DRPR IS	ENTERPRISE (CVN-65	Š	_		-	Z I CHI	NICHT LANDINGS	4.5	
995	VPAF	١.	7	3	_	WIND-VEL	<b>1</b> 3		VEOR	œ	VPAMIN		V. dSA		KAPA A	₹	LIFT	111	₩ #	WEIGHT
8	2				PA.	æ	<b>6</b>	ď							Z	<b>∢</b> 85	5	1		
	₹	\$	\$	<u> </u>	_ ₹	Ş	-	- \$	2	<u> </u>	₹ 2	κ κ	<u>₹</u>	Ş					8	æ
-	~	n	•	so.	•		•	•	•	=	2	5	+	5	5	11	5	2	<b>50</b>	5
50 100	152	2	=		3	17	•	n			25.	2			<u>+</u>		<b>8</b> .		23437	10631
80.0	7	2	102		32	16	•	~			120	32			=:		-:		19137	8681
9110	130	72	107		32	9	•	2			_	22			. 96		<b>8</b>		22737	10314
9114	=	2	2		32	9	•	n			_	69		•	. 85		8		23537	10676
9116	3	20	121	62	32	9	•	2			132 (	2			. 15		1.20		23137	10495
9120	<u>\$</u>	11	118		32	9	•	n			_	65			1.12		<b>-</b>		23637	10722
9121	<b>‡</b>	7	112	-	22	•	•	n			_	2		•	99.		-:		24137	10949
9124	2	8	3		22	•	•	2			_	50			8.		1.1		24137	10949
9125	#	7	112		22	2	•	•			_	2		•	90.		1.20		24137	10949
57.0	122	3	2		3	17	•	n			_	22		•	<u>.</u>		1.38		19137	8681
9132	33	8	3		32	9	•	n			_	<b>9</b> 2			1.02		<b>8</b> .		23137	10495
9137	129	\$	6		32	9	•	n			_	₽			.97		1.30		23137	10495
1410	3	3	=		22	•	•	n			_	8		•	. 63		- 8		21937	9951
9147	149	11	115		z	17	•	n			Ĭ	23		•	1.15		1.10		22137	18641
9189	161	3	128		2	17	•	n			•	=		•	.16		1.10		25037	11357
1919	142	2	2		2	17	•	n			Ī	8		•	. 95		1.1		24137	10949
9192	2	89	=	25	2	17	•	2			•				86.		1.00		24637	11175
9227	151	92	117		ž	17	n	~			_	22			1.15		1.10		22937	10404

		3	a Selection	ATA - 1	LANDING DATA - NODEL A-7E	-7E	5	SS ENTE	USS ENTERPRISE (CVN-65)	(CVF-6:	3			NICHT L	NICHT LANDINGS			
99			AIRCR	AFT SII	AFT SINKING SPEED AT TOUCHDOWN	`£® ∧ì	T TOUCH	N N		•	GLIDE PATH ANGLE AT TD	ATH A	HOLE A	T T0	WHEEL HEIGHT	EIGHT	HOOK HEIGHT	19H
2	NOSE	M	2	Ę	STBO	<b>&amp;</b>	AVC		FREE-FLIGHT	IGHT		-	<b>8</b>	>	OVER RAMP	•	OVER RAMP	ş
	Ę	\$	٤	\$	٤	\$	5,	\$	2	K K	DEG	3	DEC	8	E	3	E	3
22	23	*	ង	<b>5</b> 2	27	28	73	8	5	32	23	*	SS	36	37	8	39	\$
1504	16.2	•	16.5	•	17.4	5.3	16.9	5.2					5.3	.092				
25.00	13.8	4.2	13.3	•:	13.1	•:	13.2	•.					4.0	. 969				
8	17.0	5.5	14.9	4.5	15.4	4.7	15.1	<b>.</b>						.081				
9642	12.5	7.7	5.2	• •	12.8	o :	12.e	÷ ;						.073				
? ;	13.4	, <del>,</del>	13.6	, <del>4</del>	13.5	o →	12.5	o →						926				
9045	13.6	4.2	12.0	0.0	13.1	4	±.	4.3						.081				
97 68	•.•	٠. د.	<b>.</b>	2.8	<b>6</b> .	3.0	<b>9</b> .5	2.9						.052				
8708	10.3	3.5	13.1	•.	14.5	<b>+</b> .	13.8	4.2						.074				
9636	12.6	8. N	* :	3.5	10.7	n.,	9.6	3.2						.058				
	14.2	? .	5.6	7.7	?:		• ·	7.						.073				
7000	• •	) K	2 -	, L	13.5	, v	 	٠ ٢ ٢ ٢					? r	. e. de				
9655	2.1	•	15.0	•	2.5	÷	7.7	4						873				
9626	12.2	3.7	13.9	4.2	13.2	•	13.5	<b>.</b>						.074				
8658	12.4	3.0	11.5	3.3	12.0	a.6	<del>+</del> :=	3.5						. 858				
9659	n. 0	2.8	10.2	2.1	11.2	4.6	1.1	4.6						.049				
90	7.1	7.5	<b>9.</b> /	7	12.5	<b>m</b> .		بر در						.964				
		5. •	7.2	7 7	4.	1.7		o						. 932				
200	5.6	• •	1.2.1	, r	- «	, c	. <b>.</b>						7 F	. 600. 7.7.				
898	9.0	3.2	10.0	3.5		9	•	. r						.047				
1296	12.6	8.0	7.=	3.5	÷.	3.5	10.9	J. 2						.054				
9673	12.1	3.7	<b>+</b> :=	J.5	1.4	3.5	<b>+</b> :=	3.3						. 060				
<b>8</b> 27 4 5 1 5 1 5 1 5 1 5 1 5 1 5 1 5 1 5 1 5	e. :	4. 4 6. 4	15.0	4 4 6 4	# <u>*</u>	4. 4 8: 6	a :	6.4 6.5					• .	.077				
9679	13.5	+	14.2	4	13.5	-	13.8	4.5						.073				
9996	9.0	2.8	9.7	3.0	9.7	9. 9.	<b>6</b>	3.0						.054				
9663	10.2	3.1	₽.	7.0	9.9	3.3	9.0	3.3						.055				
9884	12.8	<b>0</b> .	4.4	<b>4</b> (	15.8	<b>4</b> (	5.5	<b>4.</b> 7						.057				
000	B (			7:7		7.7		7.7						.40.				
9988	= 	4.6	13.6	÷ :	12.4	ю. О	13.1	<del>4</del> .						.059				
8988	<b>+</b> •			. c	9	7.7	<u>ه</u> و	B . C						220.				
0000		, ,	7.1	, r		4		7.7					, ,	. 651				
2007			10	2.6	9.0	3.2	8	9.0						.045				
918	9.0	5.6	9.7	9.0	6.0	2.8	9.5	5.8						.043				
9101	14.0	¥.4	15.6	4.7	14.2	4.3	14.9	4.5					4.2	. 974				
9102	10.3	<del>د</del> . ا	8.8	2.7	10.3	J.	4.6	2.9					2.8	.049				
9163		2.8	8.7	2.6	D.0	2.8	<b>.</b>	2.7					2.9	.051				

F/S M/* DEG RAD DEG RAD FT M FT M 31 32 33 34 35 36 37 38 39 40 2.7 .047 2.8 .049 3.4 .060 2.4 .042 2.7 .047 2.6 .065 2.7 .047 2.6 .065 2.7 .047 2.6 .065 2.7 .047 2.6 .065 2.7 .047 2.6 .065 2.7 .047 2.6 .065 2.7 .047 2.6 .065 2.7 .047 2.6 .065 3.9 .067 3.9 .067 3.9 .067 3.1 .069 3.1 .060 3.4 .060	LANDING DATA - MODEL A-7E USS ENTERPRISE (CVN-65)  AIRCRAFT SINKING SPEED AT TOUCHDOWN  GL  NOSE PORT STBD AVG FREE-FLIGHT	LANDING DAIA - MODEL A-7E AIRCRAFT SINKING SPEED AT TOUC PORT ST80 A	AT TOUC	AT TOUC	AT TOUC	AT TOUC	TOUCHDOMN AVG			ERPRISE (CVN FREE-FLIGHT	(§ 150 ± 15	GLIDE P	PATH /	S) NIG GLIDE PATH ANGLE AT TD BHW BVV	NICHT T TO	NIGHT LANDINGS TO WHEEL H OVER R	ANDINGS WHEEL HEIGHT OVER RAAP	HOOK HEIGHT OVER RAMP	EIGHT
32 33 34 35 36 37 38 39 39 39 32 33 34 35 36 37 38 39 39 39 39 34 35 36 37 38 39 39 39 39 39 34 36 34 36 39 34 36 8	F/S W/S F/S W/S F/S W/S F/S	F/S 14/S F/S 14/S	M/S F/S M/S	F/S N/S	F/S N/S		5,		Ş	5,	Š	930	2	DEC	3	E	3	E	3
2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	23 24 25 26 27 26 29	25 26 27 28	26 27 28	27 28	28		23		2	ñ	32	33	ħ	25	36	37	38	39	\$
	11.2 3.4	10.3 3.1 11.2 3.4	3.1 11.2 3.4	11.2 3.4	4.8		11.1		4.5					2.7	.647				
2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	<b>9.9</b>	9.8 3.0 9.0 2.7	3.0 9.0 2.7	9.0 2.7	2.7	_	4.0		2.9					2.8	. 049				
8 4 4 V 8 V 8 8 8 V 8 8 V 4 V 4	3.2 11.6 3.5 9.9 3.0	11.6 3.5 9.9 3.0	3.5 9.9 3.0	9.9 3.0	3.0	_	10.8		3.3					5.8	.051				
2 4 4 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	4.4 4.4 4.4 4.4 6.4 6.4	14.6 4.4 14.4 4.4	4.4 4.4 4.4	14.4 4.4	<b>+.</b>	_	14.5		+.+					3.8	990.				
4 7 8 7 8 8 7 8 7 4 7 8 8 7 8 8 7 8 8 7 8 8 7 8 8 7 8 8 7 8 8 7 8 8 7	3.9 15.1 4.0 12.3 3.7	13.1 4.0 12.3 3.7	4.0 12.3 3.7	12.3 3.7	2.7	_	12.7		3.0					4.6	999				
2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	3.2 10.5 3.2 9.8 3.0	10.5 3.2 9.8 3.0	3.2 9.8 3.0	9.8	0.0	_	19.1		3.1					7.4	.042				
8.7.9.9.9.9.9.9.9.9.9.9.9.9.9.9.9.9.9.9.	2.6 10.4 3.2 9.9 3.0	10.4 3.2 9.9 3.0	3.2 9.9 3.0	9.0 3.0	9.0	_	10.2		3.1					2.7	.047				
2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	3.9 13.5 4.1 11.4 3.5	13.5 4.1 11.4 3.5	4.1 11.4 3.5	11.4 3.5	3.5		12.5		3.8					3.6	.063				
2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	3.1 10.2 3.1 10.3 3.1	10.2 3.1 10.3 3.1	3.1 10.3 3.1	10.3 3.1	2.7		10.3		3.1					2.7	.047				
9. 9. 4. 4. 4. 4. 4. 4. 4. 4. 4. 4. 4. 4. 4.	2.9 7.2 2.2 7.3 2.2	7.2 2.2 7.3 2.2	2.2 7.3 2.2	7.3 2.2	2.2		7.2		2.2					5.6	.045				
2, 2, 2, 2, 2, 2, 2, 2, 2, 2, 2, 2, 2, 2	3.9 13.3 4.1 12.5 3.8	13.3 4.1 12.5 3.8	4.1 12.5 3.8	12.5 3.8	3.8	_	12.9		3.0					3.8	. 967				
2.2.2.4.5.0 5.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4	2.9 7.0 2.1 8.7 2.6	7.0 2.1 8.7 2.6	2.1 8.7 2.6	8.7 2.6	2.6		7.9		2.4					5.8	.045				
- 2 2 2 - 5 5 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	2.8 8.4 2.6 7.9 2.4	8.4 2.6 7.9 2.4	2.6 7.9 2.4	7.9 2.4	2.4	_	₩.		2.5					2.7	.047				
2.2.2.5.5.5.5.5.5.5.5.5.5.5.5.5.5.5.5.5	2.6 7.9 2.4 8.0 2.4 7.9	7.9 2.4 8.0 2.4 7.9	2.4 6.0 2.4 7.9	8.0 2.4 7.9	2.4 7.9	1 7.9			4:					<b>9</b> .	. 029				
4.4.4	2.9 9.5 2.9 16.2 3.1 9.8	9.5 2.9 16.2 3.1 9.8	2.9 10.2 3.1 9.8	10.2 3.1 9.8	3.1 9.8	8.0	•	٠,	•					2.5	.044				
4.6	2.1 8.3 2.5 8.5 2.6	8.3 2.5 8.5 2.6	2.5 8.5 2.6	8.5 2.6	2.6	_	4.0		2.5					7.4	. 042				
4.6	2.7 6.9 2.1 5.7 1.7	6.9 2.1 5.7 1.7	2.1 5.7 1.7	5.7 1.7	1.7	_	6.3		<b>6</b> .					1.7	. 030				
	4.1 14.5 4.4 12.8 3.9	14.5 4.4 12.8 3.9	4.4 12.8 3.9	G. 20	G. 20	_	13.6		4.2					4.6	.060				

		3	LANDING DATA	1	NODEL A-7E	37:		USS ENTERPRISE (CVN-65)	ERPRIS	پر پر	<del>-6</del> 5)			N	NIGHT LANDINGS	DINGS				
			×	2	<b></b>			ROL	LAN	C C	ш	۵	PITCH RATE		ROLL RATE	ATE	F. P. A.	÷	YAW	
2	₽	_	8		14		2		8		<b>L</b>		AT TD	٥	AT TO	٥	AT TO	٥	AT TO	6
	950	2	DEG	3	DEC	3	DEG	8	DEG	8	930	8	DEC	3	DEC	3	DEC	2	DEC	8
<b>∓</b>	4	2	‡	\$	9	41	\$	\$	<b>8</b>	31	25	53	24	22	26	57	<b>8</b>	88	2	5
9631	5.0	<u>.</u>				,		662				7-	-2.4	042 -7		1	.2	673	7.0	.122
9633	_	.124				•	1.0.1	010				7							7.8	.133
9638		<del>-</del> :				•		8						•					c	<u> </u>
7 90	- «	5				īī		228.1				I		504 -2- 504	ا س	4.4. 678. - 842.		/ G		. 1.56 875 875
1100		.147				- 44		938				-7	-	035					5.0	869
9043		.115				_		. 619				7		019-17.3		302 -5.3			8.8	.154
9 5 6 5	•	<u>.</u>				ï		042				~ .		.835 -6.1					<b>†</b> •	.147
		<u> </u>				· ī		. 926 				n <b>◄</b>	. €	9.01-050-1 9.01-080-1	_	- 196 - 2.9 - 646 - 4.8		1.00.1	0 17	118
9651		22				7		654				1	•	863 -6.3					7.7	.124
9052		136				_		.023				7	-						7.4	. 129
9654		181						919.				-2.	_	035 2	7				5.0	.087
0000 0000 0000	9.6	22.				7 '	1   	075				ł		.963 11.	n e	.201 -4.3		075	• •	122
900		3 2						. 916				· 7		623			-		3.7	965
9629		185				~,		.056				P		105 -1.7					5.9	. 103
9966		.216				_		. 824				ı		014-15.8	_				9.9	. 140
9961		- - -				. •	i nr	. <b>.</b>				•	6.6	_	• •				4. s	.679
2002	12.0	200				· T	•	628				n		.005 14.	- v:	253 .4	-	<del>6</del> 90.	- v.	.026
8908		÷.				1		886				S.			•	.201 -1.	+		2.6	.045
9671		.079				•		016				•					-		2.5	14.
9673	7.7	<u> </u>				• '	 	967					İ	- 619	i.	985 -3.8 828 -3.8		052	4.6	486.
9677		126				1		075				ī <b>-</b>	•	- ~	; <u>,</u>		<b>.</b> .0		. 7	936
9679		 64						.014				1		10	+	.094 -1.2	١		2.6	.045
9996	7.2	.126				•	•	009				7			- (		٠. ن	•	- ( - (	919
7886		124					• • • •	. 924 				1	7.7	000 - 070	P. 4	4./- /IN.	<b>.</b> .	128 	» ·	
9884		166				í		200				1		- 694 - 1.			-		. t.	.129
9996		145				_		.024				9		115 7.			•		D. 0	.162
6996		. 195				ī		019				•		1		9652.	•		4.6	.059
8002		. 155				•		. 963				1			<b>6</b> 0 1		ю.		7.5	.038
9696		.124				γ'		066				ī'	1	<b>9</b> 33 2.	٠.					868.
1696		. : :				í		1.000 0.000 0.000				? <b>6</b>	. 6	000	, 0 K	0.71 245. 063 15.0		587	 	200
919		136				7	•	026				۱٦		_					S.	. 961
9162		.117				ī		024				7		.045 -9.2				_	10.1	.176
9103	7.7	÷2.				•		005				-	1.3	. 623 🛧	î 8, †	084 -2.3	•	040	5.5	960.

		3	LANDING DAT,	TA - IK	A - MODEL A-7E	37-	_	USS ENTERPRISE (CVN-65)	(ERPR 1	ξε (CM	£63			Ž	SH	NIGHT LANDINGS				
200		P 1 4	X U	ANGL				ROLL		ANGLE	w	•	PITCH RATE	RATE	ROLL RATE	RATE	F. P. A.	خ خ	YAW	
2	5		8				5		8		i.		7	5	¥	Ę	AT TA	٤	OT TA	_
	9	3	93	3	DEG	3	DEC	2	DEC	3	DEC	2	DEC	3	DEC	3	DEG	3	DEC	3
<b>=</b>	42	\$	‡	\$	9	41	\$	<b>\$</b>	8	51	22	53	\$	22	8	57	80	20		5
200	6.3	= :						.021									•	054		.073
3168	8.8	. 155				•	8	<b>•</b> 14				~		1	_		•			101.
=======================================		118						.012				7	1.0.1	_		.236 -	-3.8 -		6.9	.120
9114	5	.113				'	1	.017				_		.028	1.2					.072
9116	7.9	5. 5.				•		.024				ī	٠					014		.045
120	-	201						.023				_					-			.176
1121	•	.157				•		992				7	•				•	059		110
1124	8.5	3.				1		150				7		617	16.7			017		.047
1125	6.	.173						017										070		.136
325	•••	.175				•		995				•	6.9			. 967		094		.152
1132	6.7	. 152				•		919				•		662				063		.127
1137	7.4	. 129						710				•		110		. 225		. 679	•	. 621
1141	8.0	.155				F		617				_		. 023	œ.	.016		079		.113
1147	5	.113				·	-	916				4		. 042						.143
9169	7.1	.124				Ī		865				ı		. 962		- 860°-	-9.1	106		. 021
191	7.3	.127				•	-	002					<b>⋆</b>			030 -	ا. ا			100
1192	5.0	==				•	-	965					8.4	.147	9.7	. 169 -	-5.2 -	691		.126
1227	6.7	. 152				T	-2.4	042				a	۲.		3.1	. 229 -	4.7			.051

	REREAD	NUMBER			•	•	•	<b>.</b>	•	•	•	•	•	<b>D G</b>	•	-	•	•	•	•	•	<b>D</b> •	- •	•	-	•	•	•	•	•	•	•	•	-	•	•	•	•	
	ARR GEAR	RUNOUTS	8	82	429.3	431.8	429.3	429.3	44.3	429.3	426.7	429.3	429.3	478.S	431.8	431.8	431.8	431.8	429.3	434.3	424.2		428.5	0.0	429.3	• •	7.474	429.3	•	431.8	429.3	429.3	•	431.8	•	431.8	429.3	431.8	
	<b>A</b>	\$	Z	5	169	170	5	2 0 0 2 0 0 2 0 0 3 0 0 3 0 0 4 0 0 4 0 0 5 0 5	12	169	<b>5</b>	69	169	200	178	170	170	170	169	17	167	9	1 0 0	•	169	• ;	) ·					169	•	170	•	170	169	170	
S	BAROMETRIC	PRESSURE	\$	8	769.7	768.7	769.7	760.7	769.7	769.7	760.7	7.09.7	769.7	7.00.	769.7	769.7	769.7	769.7	768.7	769.7	769.7	760.7	769.7	7.69.7	760.7	769.7	769.7	769.7	759.7	759.7	759.7	759.7	759.7	759.7	759.7	759.7	759.7	759.7	
NIGHT LANDINGS	BARON	PRES	N H	79	29.95	29.95	29.95	29.93	29.95	29.95	29.95	29.95	29.95	CR . 67	29.95	29.95	29.95	29.95	29.82	29.95	29.95	29.95	29.93 29.95	29.95	29.95	29.95	28.83	29.95	29.91			29.91	29.91	29.91	29.91	29.91	29.91	29.91	
<u>x</u>	TEM		ပ	78	5	2	<b>9</b> 9	D =	. <del>.</del>	2	2	<b>E</b>	<b>₽</b> 9	2 :	9 5	2	2	2	5	5	₽ :	D (	20 60	19	2	<b>9</b> (	D .	2 5	2	2	2	13	<b>£</b>	17	17	17	17	1	
			-	77	2	2	<b>3</b> :	<b>3</b>	\$	2	\$	\$	\$	\$ 3	5 6	\$	\$	\$	<b>5</b>	\$	\$	\$		2	\$	<b>3</b> :	\$ 3	4	2	3	2	_			_	_	_	3	
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USS ENTERPRISE (CVN-65)	DECK PITCH		8	*	. 863	. 003	. 963 2	500	. 963	.003	002	9.00	9.000	200-	1.002	602	002	002	002	002	002	002	002	002	002	002	7997	662	992	007	005	607	010	002	003	007	999	003	
<u>ن</u> س	OECK		DEC	2	~	4	ų,	i c	: ~	~	-	0.	e. •			-	7	7	7	-	- ·	- ·		7	7	- ·			7	<b>*</b> :	J.	<b>+</b> .		7	2	<b>4</b> .	s.	2	
PR IS	_	SPEED	K K	72	8	~	~	7	۱ ۲	~	~	~	~ (	N (	4 0	۱ ۸	~	~	~	~	~	~	7	~	~	<b>~</b>	N 6	٠,		n	m	n	n	~	N	~	~	~	
DNTE	풄		Ş	7	n	n	<b>7</b> )	יא מ	2	2	n	<b>17</b>	י מ	? •	) P	· •	n	n	n	n	<b>1</b>	י מ	2	n	n	ומ	? F	מי נ	6	'n	S	Ю	80	*	*	*	*	4	
SS	\$	300		7																																			
	20	3		2	50120	50100	50120	56128 56128	50120	50120	50120	50120	50120		58286	50100	50200	56186	20790	20200	59120	66136	50120 50100	60123	50120	69120		50.00	50120	<b>Se 186</b>	50200	<b>36188</b>	66126	58286	70120	56186	50120	56128	
7.5	SIDE	Š		2	245	231	242	251	25.	245	231	253	242	5 5	2 2 2	251	235	253	235	253	235	245	235	245	253	245	î i	25.5	243	234	235	231	237	237	245	243	251	245	
MODEL A-7E	WIRE	ě		67	•	2	М.	+ -	- 17	*	n	•	<b>*</b> •	·	ว ◀	n	7	•	*	-	4	•	N 17	ľ	n	•	• •	) P	1	~	*	4		7		n	4	~	
6	_	ANCE	=	2	5	3	2	<b>ž</b> 5	۶,	20	28	5	2	8 8	8 8	25	2	87	8	3	<b>5</b>	<b>Ž</b> i	2 2	ž	92	8	5 5	2	92	72	e S	81	Ē	2	8	11	=	71	
LANDING DATA	RAMP TO TI	DISTANCE	E	2	266	272	228	20 E	259	283	255	=	276	5 52	, o c	246	276	285	200	175	297	910	243 266	8	248	316		273	256	237	===	286	Š	238	321	253	98	232	
3	OFF-CENTER	DISTANCE	3	3	7	7	? '	7 7	۱7	7	7	7	7.	1 1	7 7	4	?	?	7	7	†	7:	? 1	7	9	7	7 9	1 7	7	?	T	7	ī	†	7	†	7	7	
	9615	0151	E	3	7	7	<b>T</b> '	? 4	•	-	=	4	7 :	71-	7	- 1	•	•	7	Ŧ	-12	7	9 <del>4</del>	7	-13	۴ '	ì	P =	7	?	7	7	1	-12	Ŧ	-12	~	15	
	99	ě		62	200	5633	96.38	778	3	9645	96 64 64	840	9626		9634	9655	9626	8988	9059	9998	9061	200	C 990	2671	9673	9674	120	8498	2882	1998	9685	9996	8998	9695	9696	2698	9010	9101	

		3	LANDING DATA	ı	NODEL A-7E	H-7E		USS E	NTER	PR IS	USS ENTERPRISE (CVN-65)	(59→			Z	IGHT	NICHT LANDINGS	40			
ğ	OFF-CENTER	DATER	RAMP TO	ot 01	WIRE	SIDE	3	3	SHIP		DECK PITCH	H2TICH	DECK	ROLL	Ħ	184	BAROMETRIC	IRIC	<b>A8</b>	ARR GEAR	REREAD
9.	DISTANCE	WCE	DISTANC	ANCE	₹.	₹	TYPE	300E	SPEED	8							PRESSURE	æ	RUNOUTS	VIS	NUMBER
	t	3	E	2					\$	K/S	DEC	3	DEG	3	L.	ပ	N HG	£ ₹	Z	3	
62	3	•	3	8	67	2	8	2	7	72	23	2	22	76	11	28	79	8	5	82	
5	1	T	298	=	4	251	56266		n	~	φ.	889	ιú	600	63	17	29.91	759.7	-	31.8	•
3	4	7	211	3	~	231	50120		n	~	•	995	ø.	910	Ş	1	29.91	759.7	169 4	29.3	•
•	7	7	287	87	*	251	56128		n	7	· 6.	009	₹.	.007	53	17	29.91	759.7	-	29.3	•
==	7	7	362	85	*	245	50120		n	7	•	012	<b>6</b> , 1	014	3	1	29.91	759.7	•	429.3	•
116	ş	7	266	8	n	245	50120		n	7	-	002	-1.2	021	63	17	29.91	759.7	170 4	31.8	•
120	4	-	328	2		237	70123		n	7	. S.	009	۲.	.012	63	17	29.91	759.7	•	0.0	•
121	=	7	<b>\$</b>	5		243	76128		n	~	+:	907	<b>9</b> .	.033	3	1	29.91	759.7	•	0.0	•
124	91-	?	247	73	n	235	50120		n			009	4	. 003	63	17	29.91	759.7	178 4	31.8	•
125	Ŷ	7	310	š	*	237	50120		n	7	• •	007	₩,	. <del>0</del> 14	63	17	29.91	759.7	-	29.3	•
36	-12	†	184	90	-	235	50120		~		. 2.	003	พ์	600.	63	1	29.91	759.7	179 4	431.8	•
132	7	7	314	9	*	243	56128		n	7		007	7	012	3	7	29.91	759.7	-	29.3	•
137	-13	7	213	\$	7	237	56123		4	7	- 2.	993	<b>9</b> .	. 028	3	17	29.91	759.7	-	31.8	•
=	=	?	276	4	*	243	50100		*	7	-	002	1.2	. 021	63	17	29.91	759.7	-	29.3	•
147	4	7	242	7.	n	237	50123		4	~	. 7.	012	6,1	016	63	17	29.91	759.7	-	31.8	•
189	q	7	<b>50</b> 2	3		201	70120		n	7	-	002	-	002	63	17	29.91	759.7	•	9.0	•
191	۴	7	269	82		235	50120		n		.2.	003	5.1	009	63	17	29.91	759.7	•	0.0	•
192	?	7	292	2		201	58288		n	7	4.	007	_	019	63	17	29.91	759.7	169 4	429.3	•
227	<del>+</del> <del>-</del>	1	217	90	8	201	50120		n	7		669	7.	. 003	3	1	29.91	759.7	169	29.3	-

	WEIGHT		8	21	17464	17237	17146	16692	16783	16692	16511	18598	18235	18598	17963	17690	17464	1/91/	17282	20049	17328	17509		17.12R	17191	18734	18280	18325	18325	18144	18008	18325	17826	17554	,	18235	17418	17464	16919	) •
	WEI		LBS	20	38500	38000	37800	36800	37000	36800	36400	41000	40200	41000	39600	39868	38588	20000	38100	44200	38200	38600	6076	38288	37900	41300	40300	40400	40400	40000	39700	40400	39300	38700		40200	38400	38288	37800	
INGS	LIFT	11		19								1.10													1.00				•	2										
DAY LANDINGS	LIFT	5		18	1.00	96.	1.00	 8 .	99.	96	1.20	1.00	1.10	- - - -	- 60	1.20	6. 6		96	1.10	1.10	96	9.		1.10	1.19	1.20	<b>1</b> .	91.1	- 6	1.00	1.10	1.00	1.19	1.10	90	1.10	96.	9 6	) ) •
	\$	<b>∀</b> . <b>∀</b>		17																																				
	KVPA	Z Z		5	1.1	1.06	1.02	9: 9	91.1 1 A7	1.09	1.24	1.12	1.15	<b>-</b> . <b>-</b>	1.16	7.13	99.	20.		1.03	1.09	1.10	,	7	= =	1.10	1.23	1.12	 	- 1	1.15	<b>-</b> :	1.18	1.23	;	= :	= :	1.10	<b>=</b> =	
55)	V.dSA		N/S	55																																				
(CVIÈ)	ΙSΑ		ž	<b>±</b>																																				
RISE	VPAMIN		M/S	5	19	99	69	8	2 6	8	29	62	62	62	5	6	5	5 6	9	65	69	5	į	- 6	9	3	62	62	79	2 2	62	62	61	61	;	62	- 6	19	9 6	) }
NTERPI	Š		₹	12	118	117	117	135	113	115	=	121	120	121	119	118	9 :	2 5	11.5	126	117	118	:		= 1	122	120	121	5 5	128	120	121	119	18		120	118	118	116	:
USS ENTERPRISE (CVN-65)	VEOR		N/S	=	3	3	41	22	8 C	8	8	26	28	57	8	26	2 5	9 Y	8	19	88	20	25	8 8	4	25	62	55	÷ 5	7 5	22	5	26	9 :	2	51	57	4	2 2	)
	>		ž	6	103	103	9	Ξ	168	6	13	168	112	10	8	109		5 6	6	119	=======================================	97	102	5	95	102	121	107	95	3 =	102	66	109	117	103	90	100	6	187	)
•		PERP.	K/S	0.	-	-	-			-	-	-	-	-	-	<b>-</b> .	- ,		- 6	6	•	•	•	<b>9 6</b>	•	•	-	<b>-</b> .	- •	- 6	. ~	-	-	-	-	_	-	-		•
יי די	WIND-VEL	Ω.	₹	<b>6</b> 0	8	~	7	~	7	۰ ۵	~	8	8	7	7	N (	N (	7 6	4 6	•	•	•	•	<b>D G</b>	•	•	7	8	<b>7</b>	4 P	, m	8	8	7	7	7	N 1	7	N 0	•
300%	WIN	PAR.	Ş	^	12	12	12	= :	2 5	! =	=	=	=	2	2	2	<u> </u>	= =	=	=	=	2	2 :	3 5	<del>5</del>	5	2	2 :	<b>:</b> :	<u> </u>	5	<b>*</b>	<u>*</u>	<b>±</b> :	* :	*	<b>±</b> :	<b>±</b> :	<b>*</b>	•
DATA MODEL EA-6			₹	•	23	23	23	22	3 8	2 2	22	22	22	22	52	52	77	3 5	3 2	22	22	52	22	3 5	88	۶	<b>5</b>	<b>5</b> 8	8 8	3 8	3	<b>58</b>	<b>58</b>	<b>58</b>	28	78	<b>58</b>	28	% %	;
LANDING (	VE-FILM		Ş	40	8	25	64	<b>3</b> :	3 2	3	62	39	8	Š	8	20	<u>,</u>	3 2	<b>3</b>	56	8	S	3 :	8 2	3 5	53	3	9	2	5 2	8	55	<b>8</b>	<b>6</b>	3	20	25	25	3 6	\$
3	<u>Κ</u>		\$	•	5	=	8	5	\$ 5	<u> </u>	120	114	116	=	+	109	20	<u> </u>	Ξ	100	106	194	2	<b>B E</b>	<b>2</b>	2	122	6	9	2 2	101	106	113	118	<b>1</b>	90	102	102	<b>\$</b> 6	
	VPAF	5	Ş	7	67	<b>3</b>				2		•	•						8 8		99		8 :						<b>P</b> :		2			•		_	_	_	<b>8</b> 8	
		•	\$	~	13.	124	Ξ	127	2 5	126	7	136	55	139	ř	40	721		3 2	50	128	129	<u> </u>	2 5	3 3	¥	7	ř	92	3 3	137	ņ	141	1.5	n i	ž	130	<u>بر</u>	132	į
		Š		-	1173	1174	1175	1178		1187	2	1191	1194	1196	1197	1201	1202	207	1206	1208	1211	1432	1436		158	1471	1712	1713	17.	1716	1718	1719	1720	1721	1722	1723	1727	1728	12.5	5

	돐		ă	12	16874		16375	18507	18416	18416	18598	17554	18144	17826	18598	18235	18235	17509	17328	16602
	WEIGHT		CBS	<b>50</b>	37200		36100	40800	40600	40600	41000	38766	40000	39300	41000	40200	46266	38600	38200	36699
SUNCS	LIFT	<u> </u>		19					1.10				1.00							
DAY LANDINGS	LIM	5		č	1.00	8.	1.88	1.20	1.10	1.20	8.	1.00	1.00	96	96.	8.	1.00	1.00	1.00	96
	\$	٠ کو:		11																
	KVPA	Z		16	1.21		1.14	1.20	1.15	1.20	1.15	1.19	1.19	1.15	1.16	1.15	<del>*</del> :-	1.09	1.08	1.15
65)	V.dSA		K/S	5																
USS ENTERPRISE (CVN-65,	Š		₹	=																
RISE	VPAMIN		M/S	5	99		29	62	62	62	62	6	62	5	62	62	62	61	69	20
NTERP	\$		\$	12	116		114	121	121	121	121	118	120	119	121	120	120	118	117	15
a ssn	VEOR		K K	=	52	<b>4</b>	3	99	8	5	26	8	50	26	99 98	58 8	55	4	53	26
	>		ž	•	102	8	103	117	97	118	109	109	8	168	112	113	106	105	103	169
•		PERP.	X/S	<b>9</b>	n	n	n	n	n	n	n	n	n	'n	n	n	-	7	-	-
1. EA-6	WIND-VEL	2	₹	₩	•	•	•	•	•	•	•	•	•	•	•	•	8	n	7	7
	NI M	PAR.	Ş	^	5	<b>9</b>	16	9	9	•	9	9	•	•	•	9	<b>:</b>	5	<b>±</b>	12
NG DATA - MODEL		•	₹	•	32	32	32	32	32	32	32	32	32	32	32	32	27	53	27	23
	411A		Ş	60	26	5	5	8	8	8	8	8	57	3	21	8	21	2	2	26
100	VE-F		Š	*	-		8	-	-	•	•	-	•	•	•	•	•	•		•
	VPAF	٤	Ş	~	2		-							•		•				_
	5	•	\$	7	7	5	131	<u> </u>	Š	Ť	<u></u>	+	ž	5	ž	3	13.	125	12	5
	S C C	ż		-	1736	1737	1739	1742	1743	1745	1748	1749	1751	1752	1755	1756	1841	1858	1860	4180

ноок неіснт	OVER RAMP	3	9	3.5	3.6	2.9	9.n	3.5	. ·	3.2	8.8	£.4								3.3		. u		2.6	2.5	8.7 2.9	2 2	2.1	3.5	3.5	2.4	4.2	9.0	4.5	5.5	7.0	7.5
¥00±	8	E	82	11.6	11.7	6.6	3. G	11.5		9.0	10.9	7.	9.6	15.6	4.5	=	9.6	6	7.6	10.7	8.	6. 6	9 60	8	eo (	• •	7.	6.8	11.6	= :	7.8	13.9	16.2	14.7			5.0
WHEEL HEIGHT	OVER RAMP	3	82	5.2	5.4	4.7	D. +	5.7	7 0	. 4 . 0	5.1	6.9	4.5	6.5	4. K	5.5	4.5	4.7	7.7	5.2	4.5	5.7	4	4.5	4. W.		÷	3.9	5.3	5.4	4.2	B. G	6.9	6.3	9.0	e n	0.0
WHEEL	OVER	E	33	17.1	17.8	15.5	<b>19</b>	17.2	2 5	16.9	16.8	19.6	14.6	21.3	15.2	17.0	14.7	15.4		16.9	14.8	6.9	15.6	14.8	7.	6.25	13.5	12.8	17.5	17.6	13.7	19.0	22.5	20.7	7.:	» · ·	9.0
AT TD	AS M	8	80	.846	. 968	.051	. 056	646 646	. 6	. 052	.052	.050	.042	. 968	940.	. 965	. 035	.059	946	.071	.056	.054	.047	.064	1964	.04/	.024	.045	.053	.047	.048	.051	.961	. 059	.053	. a	629
ANGLE	ĬO.	DEG	SS	2.6	3.9	2.9	3.2	7 ° 6	) -	. b	3.0	2.9	7.4	ი ი	9.7	, r	2.0	4 6	, c	4	3.5	n (	2.7	3.6	8. 8.	, c	÷	5.6	<del>د</del> .	2.7	2.8	5.8	3.5	4.6	0. 1.0	ა . ა .	7.0
GLIDE PATH ANGLE AT TD		8	Ř	.047	. 053	. 043	. 648	949	070	. 969	.056	. 854	. 048	. 658	5. 6. 6	. 651	. 045	.056	740.	.061	. 963	. 961	. 050	.067	. 986	. e.	646	.049	.051	. 657	. 055	. 961	. 965	. 054	.058	0.40 0.40	7 6
GLIDE	<b>&amp;</b>	DEG	S	2.7	J.	2.5	2.0	2 °	, c	4. 4.	3.2	3.1	2.8		ر اه و	. 6.	5.6	3.2	, ,	3.5	3.6	ا ا ا	2.8	g. B	<b>6.</b> 4	7 F	2.3	2.8	2.9	3.5	3.5	ا ا	3.7	3.1	بى دى د	, v	p .
	LIGHT	M/S	32								3.2												3.0				1.9										
	FREE-FLICHT	F/S	31								10.4												8.8				6.2										
NHOO	v	K/S	30	2.8	4.6	2.7	٠. د .	6 6 7		, w	3.2	3.3	2.8	4. 0.	5) K	, w	2.4	6. u	ر د د	+	3.0		6.6	3.7	<b>4</b> .0	2.5	9.	2.8	4.6	2.9	J	3.7	3.8	3.7	6 F		
SINKING SPEED AT TOUCHDOWN	AVG	5/5	29	9.3	11.3	8.9	1 <b>9</b> .9	 		. <del>.</del> .	4.0	9.6	- 6	<del>.</del> .	÷ •	, r)	o.	<b>e</b> j (	ء د	· <del>*</del>	<b>.</b>	 	4.0	1.7	•	<u> </u>	. 2	9.1	n	4	9.5	2.2	2.5	2.2	9.6	D (	7.5
PEED A'	_	K/S								_	-	Ξ	•	÷.	Ø =	: 2	7	= :	9 0	5	Ø,	<b>6</b> 0		12	14.6	9 0		O)	1.3	ò	-	7	=	_	•	_	
S N	M	3	28	2.8	4.5	2.5	ا ا ا	5.5	- 0	. t.	3.1		•		2.9		_			_	_	4.6		_	4.8 14.		·	_	_	2.8	_	3.8 12	3.6	3.7	9.0	٠ • •	9 6
Ŷ	STBO	۲. ۲.	27 28	9.2 2.8	11.1 3.4	8.2 2.5	10.8 3.3	8.3	- 6.0	5 5.5	2 3.1	8 3.3 1	2.4	4 (	5 Y	, w	2.4	3.5	, c	•	3.0	4. e	9 6	3.7	<b>4</b> .	, c	2.7	2.7	4.6	2.8	J. 0.	8. 8.	3.6	3.7	10.0 3.0		8.7 2.8
-					3.5 11.1 3.4		_	2.7 8.3 2.5		11.5 3.5 1	10.2 3.1	16.8 3.3 1	8.9 2.4	14.6 4.5	41. 7 7.9	12.5 3.8	7.8 2.4	10.4 3.2	8.8 2.2 7.0	13.0 4.0	9.7 3.0	1.2 3.4	9.7 3.0	12.3 3.7	15.7 4.8	9.4 2.9	7.0 2.1	8.8 2.7	11.1 3.4	9.3 2.8	9.7 3.0 1	12.5 3.8 1	11.9 3.6 1	12.1 3.7 1	9.6	7) CE	, .
AIRCRAFT SINKIN	PORT STB0	5	27		11.5 3.5 11.1 3.4		_			11.5 3.5 1	10.2 3.1	8 3.3 10.8 3.3 1	2.9 8.9 2.4	6 4.1 14.6 4.5	2.8 9.5 2.9	12.5 3.8	2.5 7.8 2.4	4.2 10.4 3.2	3.6 8.6 2.0	4.2 13.0 4.0	3.6 9.7 3.6	3.1 11.2 3.4	2.8 9.7 3.8	3.7 12.3 3.7 1	8 4.5 15.7 4.8 1	2.5 8.4 2.9	7.0 2.1	3.1 8.8 2.7	4.6 11.1 3.4	9.3 2.8	9.7 3.0 1	12.5 3.8 1	11.9 3.6 1	12.1 3.7 1	9.6	7) CE	, .
-	PORT	M/S F/S	26 27		.5 11.8 3.5 11.1 3.4		_			11.5 3.5 1	10.2 3.1	8 3.3 10.8 3.3 1	2.9 8.9 2.4	6 4.1 14.6 4.5	2.8 9.5 2.9	2 3.7 12.5 3.8	5 8.3 2.5 7.8 2.4	7 13.9 4.2 10.4 3.2	3.6 8.6 2.0	13.7 4.2 13.0 4.0	9.9 3.0 9.7 3.0	1.2 3.4	9.1 2.8 9.7 4.6	12.2 3.7 12.3 3.7 1	4.5 15.7 4.8	11.4 5.5 8.4 2.8	1.8 7.9 2.1	16.1 3.1 8.8 2.7	11.4 3.5 11.1 3.4	9.5 2.9 9.3 2.8	10.8 3.3 9.7 3.6 1	11.8 3.6 12.5 3.8 1	13.1 4.0 11.9 3.6 1	12.3 3.7 12.1 3.7 1	9.6	12.6 5.7 40.8	, .
-		F/S M/S F/S	25 26 27		1.8 .5 11.5 3.5 11.1 3.4		_			11.5 3.5 1	10.2 3.1	8 3.3 10.8 3.3 1	2.9 8.9 2.4	6 4.1 14.6 4.5	2.8 9.5 2.9	2 3.7 12.5 3.8	3 .5 8.3 2.5 7.8 2.4	2.7 13.9 4.2 10.4 5.2	0.0 8.0 7.0 8.0 7.0 8.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0	1.2 13.7 4.2 13.0 4.0	3.2 9.9 3.0 9.7 3.0	.7 10.2 3.1 11.2 3.4	9.1 2.8 9.7 4.6	4.0 12.2 3.7 12.3 3.7 1	3.3 14.6 4.5 15.7 4.8 1	7.0 7.4 7.5 6.4 2.6	1.9 5.9 1.8 7.9 2.1	2.4 10.1 3.1 8.8 2.7	1.5 11.4 3.5 11.1 3.4	3.1 9.5 2.9 9.3 2.8	2.1 10.8 3.3 9.7 3.0 1	11.8 3.6 12.5 3.8 1	1.7 13.1 4.0 11.9 3.6 1	3.5 12.5 3.7 12.1 3.7 1	. d 19.0 d.1 10.0	.6 12.6 5.7 9.8	7.8 2.4 8.7

DAY LANDINGS

USS ENTERPRISE (CVN-65)

LANDING DATA - MODEL EA-6

		3	LANDING D	DATA -	MODEL	ទ ភ	>	USS ENTE	ENTERPRISE (CNN-65)	9- ₹ ()	ତ୍ରି			DAY L	DAY LANDINGS			
8			AIRCR		MK ING	NT SINKING SPEED AT TOUCHDOWN	T TOUCH	N			GLIDE	PATH A	GLIDE PATH ANGLE AT TD	5	WHEEL	HEIGHT	ноок нетснт	IGHT
2	2	MOSE	ğ	¥	w	STBO	Y.C	ø	FREE-FLIGHT	IGHT	<b>B</b> +46	<b>*</b>	<b>₩</b>	>	OVER	RAMP	OVER R	RAMP
	53	Ş	2	Ş	5,5	R/S	£/\$	M/S	F/S	S/M	DEC	2	DEG	<b>3</b>	E	3	E	3
22	23	77	22	<b>38</b>	17	28	28	8	ñ	32	23	*	જ	36	33	88	80	<b>\$</b>
1736		6.	10.3	3.1	8.	d.0	10.1	J. 1			3.2	. 056	2.8	. 648	16.7	5.1	16.8	3.3
1737	6.3	<del>-</del>	=:	3.3	10.2	3.1	10.8	3.3			2.9	. 050	3.2	.055	16.1	<b>6</b> .4	9.7	3.0
1739	10.8	3.3	9.5	2.8	10.5	3.2	9.7	3. <b>0</b>			3.5	.061	3.0	. 053	15.6	<b>4</b> .8	<b>9</b> .3	2.8
1742	4.6	•	12.7	g. 5	12.9	3.9	12.8	3.8			4.5	. 679	3.6	. 063	12.9	3.9	<b>6</b> .8	2.1
175	7.8	7.4	7.3	2.2	7.3	2.5	7.3	2.2	7.7	2.3	2.2	. 038	<b>.</b> .	.628	14.8	4.5	69 90	2.7
1745	9.9	2.1	¥.:	3.5	10.4	3.2	10.9	3.3			3.3	. 058	2.6	.045	18.5	5.6	13.2	4.0
1748	8.2	2.5	-	2.8	5.0	2.8	9.5	2.8			9.1	. 033	2.3	. 640	12.3	3.7	6.4	1.9
1749	3.9	1.2	7.9	2.4	8.8	2.7	8.6	5.6			2.7	.047	2.3	.040	14.6	4.5	8.7	2.7
1751	4.0	2.5	4.9	2.0	7.4	2.3	6.9	2.1	6.9	2.1	2.3	.040	<b>6</b> .	.032	13.4	<del>-</del>	7.5	2.3
1752	<b>•</b> :	ij	9.0	3.2	16.7	3.3	10.7	3.3			3.3	. 058	4.6	. 060	14.5	<b>+</b> .+	8.2	2.5
1755	3.0	œ.	12.5	3.8	<b>+</b> .=	3.5	12.0	3.6			3.1	. 054	4.6	.059	12.7	g.5	<b>6</b> .8	2.1
1756	10.0	3.0	13.2	<b>4</b> .	1.6	3.5	12.4	3.8			3.2	. 055	3.7	.064	14.2	4.3	. <del>0</del>	2.5
1841	2.8	'n	12.1	3.7	12.7	3.9	12.4	3.B			3.3	. 058	4.6	. 060	14.8	4.5	9.5	2.8
1858	<b>+</b> .+	1.3	1.6	J. 3	<b>.</b>	3.3	11.2	4.0			3.0	. 053	3.3	. 058	16.5	5.0	10.1	٦. ٦.
1866	7.4	۲.	13.0	4.0	10.6	3.2	1.8	3.6			3.5	.062	3.7	. 965	17.3	5.3	11.0	4.5
4186	7.9	2.4	1.8	3.6	12.0	3.7	11.9	3.6			2.8	.049	4.6	. 059	15.8	<b>4</b> .8	10.2	3.1

		3	LANDING DATA	1	NODEL EA-6	۴		uss ev	TERPRI	USS ENTERPRISE (CVN-65)	N-65)			<b>6</b>	DAY LANDINGS	INGS				
995		d	Ξ U	Z Z	T.			ROL	٠,	A N G L	w	•	PITCH RATE	<b>W</b> TE	ROLL RATE	<b>W</b> TE	۳. و	₹.	YAW	
9	2		8		4		5	_	క		1		¥	5	AT 1	5	AT TD	ē	AT TO	P
	DEG	2	DEC	3	DEC	2	DEC	8	DEG	8	DEG	3	DEG	3	DEG	3	DEG	3	DEG	3
7	42	2	‡	\$	9	41	<b>\$</b>	49	20	51	22	53	54	22	26	22	88	29		5
1173	5.0	162 1	•.	.192			9.	.028	2.3	. 848		•	*	.677		.023 -	-3.2 -	056	<b>9</b> .	.070
1174	10.9		12.9	. 225		•	•			. 059		7	-2.2		2.8		-	028	2.4	.042
1175	11.1	•	-	.232		1		•		026		•			. 0.			058	4.6	. 686
1178	5.3	162	3.4	.234						.052		<b>4</b> )		.087	6.			058	•	002
1381	.:.	7 7 7	• •	.202		t I	-2.5	1.044	7.7.	1.038 1.058				999.00		. 629.	-2.5 - 4.5	1.040 1.040	o. •	.068
2 2			, r	250								, (4			_				. 17	. 665
200		•	0.0	173		ſ			-	054		<b>F</b> )		•				056		016
1191	10.5	_	2.0	.269 11		. 192 -				- 990.	<del>-</del>	019			2.5			051		.016
1194	9.0	_	6.7	.187			n	_		993		P3 ·	3.6		•		~			410
1196	٠.	_	<b>*.</b>	.199		T				. 038		•					· - :			037
1197	9.0	_	9.0	.185		ſ	~	ı		061		7								.058
1201	13.3	- '	a :	.208		•			ν,	169.				i			~ (			04 4 6 6 6
1202		500	* * * •	216		I	ب د	410.	• •	//0.			9 7.0 9 7.0		. 1 0 00	. 628. I	7.7	1.658 1.858	٠. <del>د</del>	. 026 120
3 5	•		. d	78.		ı			 	. a.		•				000		25.		191
1206	•		9	202			7.7			679					· -:		. 🕶	042	9	. 986
1200	-	-	2.0	209		1			•	051		•	0	9.000 -:	ŧ		ED	990	4.5	.679
1211	12.9	_	2.8	.223		ſ	1.7			007		9					•	044	3.5	.061
1432	= •:=	-	12.7	. 222			2.0		10	028		_					6		<b>.</b>	.017
1436	11.7	204 1	1.7	.204						.087		•	9.9						•	044
1440	12.3	_	7.7	.216		ı				023		•	ıŭ i		ui (			961		.092
1451		2 2	n e					<b>9</b> 51	- - -	919		9	` `'	- BCB.	Ņ 4	1.629	֓֞֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜		? • • •	911. 874
147	•			777	•		. 4	•	• 65	900	•		•	900	- 0				5.7	666
1712		-	•	181			8.9			*			)	.042-11.9			•	051	2.1	.037
1713	12.5	-	3.3	.232			-:	.002	۲.	. 003			'n		10.5		_	012		9.000
1714	12.4	_	7.0	.208						669							n 1		<b>4</b> .0	.084
1715	6.9		9.0	.227 11	.5	. 201			9.	.028	9.1	919 5			, 4,6			9/9	2.g	040 0 1
1716		- •	9.0	.225			2.6	. 645 5 45	2.3 •	949			* 6	. 024 053	_ ~	1 100.	- «		7.7	/CO.
0171			+	017.		1	ה ה		- «	6.6		, •		900	2 17			979	6	191
1728				202					2.1	.037					5.1		6	052	*	.077
1721	٠.	•	8	154			4:		5.4	. 694		۳,		•		.059 -1	*		2.7	.047
1722	11.3	-	2.5	.218		ı	_	- 710		091		-			6.9				. 2.1	023
1723	•	_	2.4	.216			-			. 002		•		0.000			•		2.3	. 949
1727	14.2	248 1	<b>6.</b> ★	.260				•		042		F) '						961	4.5	.073
1728	•	192	- ( • (	.246		•				012		7`					<b>6</b> 4	028	D) +	816.
1731	6. 6	5 5 5		. 168 89 6		•	- 7. 8.6			.087		<b>,</b>	6 6 6 6	999.99	-2.9 		-2.6	645 676	- r	689.
1/32	6.9	28.	4.0	. 203				- 999.9		740.		,			2			2/2	;	400.

	AYA	OT TA	D DEG RAD	68 61	4.7	1.2 .021	2.5	9.	6.5	9.4	2.9	2	6	-	4	12.4	·	4.7	·	
	F. P. A.	AT TD	DEG RAD	58 59	-3.6063	.1 .019		-	•	.9 833			-	5 - 644	Ť	•				
SONIO	ROLL RATE	5	<b>3</b>	57	•	.038	143 -5.5		663 -3.6	.689	021 -2	865 -2	- 1691 -	005 -2.5	105 -1					•
DAY LANDINGS	ROLL	¥	DEG	26	6.	2.5	8.2	-1.3												
9	PITCH RATE	5	SAD .	88		002														
	PITC	Υ	930 0	5		-	_	2.5	<b>.</b>	3.2					*.		7			
^		F F	8	55					002				023							
CVN-65	u	_	050	52					-				1.3							
USS ENTERPRISE (CVN-65)	ANGLE	8	G RAD	5	410.	. 662	. 024	. 196	. 019	. 624	863	996	.019	9.00	.040	047	. 082	686	100	
ENTERP	0 1 1	•	D DEG	80	<b>5</b> 0	-			-					0.0		•		•		
uss	<b>&amp;</b>	10	DEG RAD	6	042	052	. 651		1.003	.00	.012	. 628	014	030	044	.044	.024	. 658	017	
			<b>8</b> 40	\$	-2.4	7.0	2.9			J.		<b>9</b> .	_	1.7	-2.5	2.5	<b>+</b>	3.3	-	
3	la l	1	DEG R	47					. 206				.213							
- MODEL	0		<b>2</b>	4	.211	_		_	8. = 1.8	_	_	_	12.2	••		_	_	_	_	
DATA .	- -	8	DEG	\$																
LANDING DATA	P 1 T C		<b>3</b>	\$	1 12.1															
ב	۵	2	DEC 18	4.	¥5.					•	-			•	Ĭ	·	Ť	Ī		
			8	- 42	8.8											•	•		-	
	200	3		Ŧ	1736	173	1736	1742	7	17	174	1749	1751	1752	1755	1756	184	1858	1864	

#### NADC-91124-60

	REREAD	NUMBER			-	•	•	•	9 6	-	•	•	•	•	- (	<b>5</b> (	9 0	9 6	•	•	-	-	•	<b>6</b> •	-	•	•	<b>.</b>		•	8	-	•	•	•	•	<b>.</b>	- «	• •
	ARR GEAR	RUNOUTS	3	83	419.1	424.2	426.7	419.1	428.5	429.3	431.8	426.7	<b>9</b> .	431.8	9.9	426.7	424.2	431.8	426.7	419.1	428.7	<b>6</b>	9.6	429.3	426.7	429.3	431.8	424.2	420.7	429.3	424.2	428.7	426.7	426.7	428.7	424.2	424.2	7.474	424.2
	<b>F</b>	\$	Z	5	:65	167	8	165	178	169	170	\$	•	170	• ;	9 5	9	178	8	165	<b>168</b>	•	•	169	8	169	170	167	9 9	169	167	168	<del>2</del>	168	<u>8</u>	167	167	2	167
	BAROMETRIC	SURE	<b>₽</b>	8	760.2	760.2	769.2	760.2	760.2	760.2	760.2	760.2	760.2	760.2	760.2	760.2	7.00/	769.2	760.2	769.2	769.2	759.7	759.7	759.7	759.7	769.2	769.0	760.6	769.0	760.0	760.0	760.0	760.0	760.0	760.0	760.0	760.0	160.0	760.0
DAY LANDINGS	BARON	PRESSURE	Z Z	2	29.93	29.93	29.93	29.93	29.93	29.93	29.93	29.93	29.93	29.93	29.93	29.93	28.82	29.93	29.93	29.93	29.93	29.91	29.91	29.91	29.91	29.93	29.92	29.92	20.07	29.92	29.92	29.92	29.92	29.82	29.92	29.92	29.92	78.87	29.82
DAY L	<b>J</b>		ပ	78	21	77	7	2 2	2 2	5	5	5	5	5	5 5	5 3	5 5	7 5	7	7	7	23	23	3 5	7 2	22	77	2 2	3 6	2	22	22	22	77	2	22	2 2	7 8	22 22
_	F		<u>.                                    </u>	11	70	29	9	2 6	9 6	92	79	96	9	<b>e</b> i	<b>6</b> 1	9 9	<b>9</b> 9	2 6	2	70	96	2	2	2 5	2 2	72	7	<b>F</b> i	7	7	7	7	7	7	7	7	<b>F</b> i	= ;	7.7
	C ROLL		3	78	667	030	<b>.</b> 014	002	619. 619.	.002	016	. 003			•		8.0	1.016	. 026	•							.019	986.		.005	.019	005	.017	999	.002	010	002	219	.002
	DECK		DEG	22	4.	-1.7	€.	- ·	- 9	:	6.1	7	4.1		ī		֡֝֜֝֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֡֓֓֓֓֓֡֓֓֡	1 1	5.	7	6. I	<b>†</b>		•	1 1			e e	ا ذ		_	•	<b>-</b>	9.0	<del>-</del> .		- '	` '	ņ <del>-</del>
USS ENTERPRISE (CVN-65)	DECK PITCH		8	7.	005	. 002	- 993	- 995	1 68	992	995	002	005	665	885	005	983	1.00	. 993	003	865	005	999	005	600	995	667	- 669	ee.	- 693	009	005	995	010	010	603	995	C00.	669 665
SE (C	DECK		DEC	22	J	-	-,2		7 5	7	7	7	7	 		7		7 4	7	7	ا. د	ا. د	<b>6</b>	ا ا	y 15		<b>†</b>	ا دن			5		ا. ن		9.	5.	ا ا	ا ن ر	i i i i
RPR I	SHIP	SPEED	¥S	72	•	0	<b>O</b>	<b>o</b> (	O 60	•	•	80	•	€ 1	<b>6</b> 0 (	<b>6</b>		o ≪	^	~	7	n	r)	י ני	) b)	7	8	~	7 6	۰ ۵	*	*	*	*	*	4	∢ •	٠.	+ +
			Ž	7	17	17	1	2	9 9	5	5	5	5	5	5	2	2 :		2 22	2	2	60	<b>S</b>	<b>.</b>	D 40	10	n	י ניו	? "	<b>*</b> 7	<b>*</b>	•	7	7	7	7	۲ ۱	- 1	- ^
nes	3	300 300		70																																			
	3	TYPE		8	50200	50100	50100	58280	8 8	50128	50100	50120	66128	<b>36</b> 188	60 60 60 60 60 60 60 60 60 60 60 60 60 6	50120	20200	20.00	50200	59100	50100	70120	70120	59120	36156 86126	56266	59299	50120	97196	50200	59120	50120	50200	50120	50120	50120	59120	50120	56166 56120
<b>5</b>	SIDE	Š		2	3	116	<b>±</b>	8	2 4	5	919	8	910	8	9	8		2 8	9 6	5	913	8	8	2 8		Ē	500	25	2	10	55	919	<b>*</b>	963	913	60	913		963 913
MODEL	WIRE	Š		6	•	•	•	m ·	4 M	. ~	~	7		~	•	<b>%</b> :	n •	•	<b>*</b>	*	7		•	r) r	3 8	*	~	N 1	<b>,</b>	1 12	2	n	~	*		*	n ·	•	+ 10
ı	50 TO	ANCE	3	2	3	87	3	<b>F</b> 3	12	3	3	11	87	2	2	<b>0</b>	3 8	3 %	? ?	2	72	*	2	<b>*</b>	6 <b>2</b>	20	\$	3 ;	2 %	2 2	82	8	8	2	\$	7	3	2 3	<b>8</b> 7
LANDING DATA	3	DISTAN	E	2	273	286	273	251	2 2	224	214	252	287	236	293	226	5 5	3 2	228	282	236	244	223	<b>5</b> 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	25	181	147	98	2 5	239	269	265	213	248	276	9	173	272	768 769 769
3	OFF-CENTER	DISTANCE	ফা	3	7	~	7	<b>?</b> ·	1 1	7	7	7	7	?	7	7	7 '	? 7	•	?	†	†	7	† •	, w	7	7	7	ត្ ។	17	7	9	7	7	7	†	†	7 '	77
	7	018	E	2	7	n	7	<b>9</b> 9	7 7	1	7-	• •	7	-	•	٠ ا	?:	7	•	7	<del>*</del>	-12	7	<b>;</b> :		7	9	= :	<u> </u>	4	†	-17	7	7	٩	13	<b>+</b> '	? '	7 =
	200	ĕ		62	1173	1174	1175	1178		1187	2	1191	181	200	1197	1201	782	2 4	1206	1200	1211	1432	1436	• • •	1458	1471	1712	1713	*	1716	1718	1719	1720	1721	1722	1723	1727	1728	1731

		3	LANDING DATA	1	MODEL EA-6	9 3		USS E	N 1530	RISE	USS ENTERPRISE (CVN-65)	<b>⊙</b>			Š	3	DAY LANDINGS					
8	OFF	OFF-CENTER	3	TO TO	WIRE	SIDE	3	3	SHIP	_	ОЕСК РІТСН		DECK 39	אסרר	154	Δ.	BAROMETRIC	'RIC	ARR	ARR CEAR	REREAD	
ġ	DIST	DISTANCE	DISI	DISTANCE	3	Š	TYPE	<b>800</b>	SPEED	۵							PRESSURE	RE	RUNOUTS	UTS	NUMBER	
	E	3	E	3					₹ 3	N/S	DEG RV	PA0	DEC	2	L.	S	IN HG	E H	Z	3		
62	3	3	2	2	19	2	8	92	7 17	7 27	73 74	75		92	11	82	79	80	5	82		
35	=	7	33	11	•	10	56 60 60 60 60 60 60 60 60 60 60 60 60 60		10	4 2	4007	·	8014	416	=	7	9.92	760.0	167 4	24.2	•	
737	<b>=</b>	?	220	2		518	<b>8</b> 1 <b>8</b> 0		<b>5</b> 0	3 - 5	5 889	•	9 916	316	=		29.92	760.0			•	
2	4	7	223	2	n	913	<b>39299</b>		'n	i n	3 005		.4 007	797			9.92	760.0	176 4	31.8	•	
742	-12	T	<u>.</u>	\$		2	66126		'n	32	2 963	5	•	. 667			9.92	760.0		6	• •	
?	7	1	263	3	n	910	80120		'n	'n	7012	29	-	316 7	:		9.92	766.8	168 4	78.7	,	
3	7	7	25	2	*	963	50120		'n	L. 1	7012	2		112 7	-		9.92	760.0		26.7	• •	
3	7	7	278	85	*	3	50120		'n	9.1	6 010	•	, ,	. 995	=		9.92	768.8	169		• •	
25	7	?	259	2	n	918	50200		'n	i i	Ċ	7		010	-		9.92	760.0			- •	
25	-12	†	282	2	n	3	86126		'n	5 2	3 965	5 -1.0	i	17 7	-	22 2	9.92	769.9	168 4	7 2	٠.	
727	5	ę	237	22	n	919	56126		'n	3	99.00			128 7	-		9.92	769.9	-		. 6	
755	<b>9</b>	7	<b>36</b> 2	<b>6</b> 2	n	913	50120		'n	1	3 995			92 7	-		26.6	769.9			• •	
756	<b>e</b>	4	223	3	n	913	56126		'n		-	1	_	24 7	-		20.0	769.9			-	
140	-5	7	<b>50</b> 8	3	2	96	50120	•	=	ì	-		_	_	80		6	769.7			- 6	
35	•	7	238	2	r	26	56266		-	1								7.637			9 6	
9	7	1	200		,	3	80120		•								) i	100.1		7.47	9	
3	•	•	,	2 ;	יי		97190		_	:	- 600	6. 1.0	6 028	_	69	7	9.95	7.097	-	۲. 9. ⊑	0	
B	3	?	247	e	מ	993	50120	_	~ •	``.  -	3005		96	916 7	9	2	29.93	769.2	169 43	429.3	•	

# **EA-6 NIGHT**

		2		NG DAT	TA - 1	4G DATA – MODEL EA-6	<b>9</b>		USS E	uss enterprise (CVN-65)	1SE (	¥. C <b>N</b> F-€	3		-	NIGHT LANDINGS	ANDINGS		
OM	VPAF		VE-F	3	-	WIND-VEL	ដ		VEOR	AP.	VPAMIN	V.dSA		KVPA	\$	LIFT	LIFT	WE	WEIGHT
ě	5				PAR.	نه	PERP.							Z	٧.	5	4		
	3	¥	2	Ş	2	¥	KN K/S	χ Σ	S/N -	₹	N/S	X	N/S					<b>S8</b> 1	8
_	7	n	•	<b>S</b>	•	7	•	5	=	12	5	<b>±</b>	15	9	17	5	6	20	52
9445	132	2	8	3	27 1	±	<b>10</b>			121	62		-	. 69		1.10		46866	18597
9450	148	76	- ' - '	5	8	<u></u>	10.4 10.1			119	5			1.24		1.10		39500	17917
9451 9454	3 3	2 2	2:	3 5	3	٠. د	n :			124	<b>*</b>		🔻	.07		 	1.20	42900	19459
9456	2	. E	- <b>-</b>	2 6	 3	2 10	0 10 G C			123	2 3		. —	<u> </u>		1.26		42999	19651
9461	=======================================	_	=	57	8	n	5			116	99		_	1.21		1.00		37600	17855
2468	129		8	2	2	5	<b>S</b>			120	62		-	1.07		1.00		40000	18144
9476	167	-	5	2	9	<u>د</u>	ر در			<b>*</b>	29			. 47		1.20		35900	16284
9478	137	_	6	20	8	<u>so</u> :	n :			120	62			<b>*</b> :		1.20		49999	18144
40	137	_		2	8	<u> </u>	n :			13	5		-	5.		1.20		39400	17872
9486	5	_	-	2 :	9	<u>د</u>	<b>.</b>			121	62			60 1		8		41000	18598
	5	- '	., .	2 :	<b>5</b>	<u> </u>	80 ( 80 (			121	62		- ,	60.		<b>1</b> .1		40200	18371
9489		•		2 :	۳ چ	<u> </u>	n (			119	<b>.</b>			٠ ت		- 10 - 10		39166	17736
9640		- 1	7.0	7 :	9	Ω !	91			120	62		- '	9 :		99.		40000	18144
9491		_	19	2 5	- ·	n u	r) r			118	19		- •	= 5		 6 (		38500	17464
767		•	9 1	2 :	9 (	<u>.</u>	n (			2	9		_ (	9 .		96.		37800	17146
764	7 1	: :	<u> </u>	<b>?</b> :	72	•	7			121	29			2:		9.		41000	18598
101	_	- •	0 6		76	<u>•</u> •	 , c			121	70		-	2 6		9 6		40000	18144
9498		_	2			5	- c			120	2 6		_			5 -		40000	18144
1499		_	12	2		2	2 2			121	62		_	.1.		96		40700	18462
9502	137	_	<b>.</b>	22	27 1	*	2			120	62		_	<u></u>		1.00	1.00	39900	18099
9503	135	_	2		27 1	<b>*</b>	7			118	5		_	<u>+</u>		1.20		38800	17600
503	7	_	97		27 1	<b>+</b>	7			120	62		-	. 12		- 90		39800	18053
9298	26	_	8		27	<u>*</u>	7			117	99			. 16		1.10		37900	17191
9512		_	12		27	<u>*</u>	7			121	62		-	5		1.30		40200	18371
9515		_	- -	× :	27	+	7			121	62		_	2		. 30		41666	18598
9517		68 68 68 68	9	Š.	24 1	7	7			122	63		_	8		8		41300	18734
9519		-	<b>*</b>		27	+	7			122	63		_	9		1.10		41600	18870
9520		_	77		28	<u>+</u> ·	7			123	63		_	 5		- 10		42300	19187
9226		_	12		28	<u>*</u>	- 7			116	9		_	. 20		1.20	1.20	37700	17101
9539	136 6	_	9		<b>9</b>	<u>.</u>	2			121	62		_	-12		- 10		40500	18371
3543		_	-, 9	<b>9</b>	27 1	<b>+</b>	7			121	62		_	=		1.00		41000	18598
9548		_	95		27 1	<b>+</b>	7			123	63		_	.07		- 90.		42300	19187
551	_	_	97	ŭ	27 1	<b>+</b>	7			123	63		_	9		1.20		41866	18960
9266	139	72 10	80 80	<b>8</b>	8	<b>5</b> 0	3			121	62		_	. 15		1.00		40500	18371
9220		_	~	<b>9</b>	28 -	رم م	2			119	61		_	19		1.10		39200	17781

		3	LANDING DATA	_	- NODEL EA-6	<b>9</b>	3	S ENTE	USS ENTERPRISE (CVN-65)	(cvr−6;	2			NICHT LANDINGS	ANDINGS			
90			AIRCRAF	_	KING S	PEED A1	SINKING SPEED AT TOUCHDOWN	N O		J	3017s	GLIDE PATH ANGLE AT TD	ICLE A		WHEEL HEIGHT	:1GHT	ноок нетсят	IGHT
2	MOSE	SE	PORT	R	ST	STBO	AVC	••	FREE-FLIGHT	IGHT	8		8	>	OVER R	RAMP	OVER RALLP	<b>8</b>
	2	Ş	٤	Ş	<b>5</b> /2	\$	<b>5</b> /2	M/S	F/S	N/S	930	3	DEG	2	E	3	E	3
22	23	24	25	<b>38</b>	22	28	59	80	2	32	33	#	35	36	37	82	39	6
445	4.5	4.	10.8	<b>5</b> .5	10.8	3.3	10.8	3.3					3.2	. 056				
456	<b>9</b> .	7.4	7.2	2.2	8.7	2.7	8.2	2.5					6.1	.034				
451	7.9	7.4	<b>9</b> .0	2.8	<b>9</b> .0	2.4	<b>9</b> .	2.7	8.7	2.6				. 055				
<b>1</b> 2 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	8 -	9 4 k	4.5	% • •	٠ ن ن	4 . 4 .	8.2 2.2	% <b>4</b>					9 °	. <b>6</b> 35				
101	8.8	2.5		, n	1.8	9	. E	9 69						. 656				
168	7.1	7.5	8.2	2.5	6.5	7.6	8.5	2.6						.042				
1476	9.7	2.9	4.0	2.6	<b>6</b> .9	2.1	8.0	2.4					•	.027				
3478	5.8	- -	11.6	3.5	19.1	3.1	10.9	3.3						. 046				
484	4.2	1.3	13.6	<del>-</del>	9.6	3.2	12.3	3.8						. 058				
1486	•.	<b>9</b> .	12.5	3.8	12.0	3.6	12.4	3.8					3.6	. 063				
466	2.7	•	9.5	2.8	<b>.</b>	2.7	<b>.</b>	<b>5</b> .8						. 048				
489	5.4	9.	8. 8.	<b>9</b> .	8. 8.	<b>.</b>	6.2	6.						. 028				
1496	<del>-</del> -	1.3	1.6	J.5	12.7	3.9	12.2	3.7						. 062				
1491	10.4	3.5	10.3	٠. ۲.	6.7	J. 0	6.6	J. 0						.054				
1492	8.S	<b>5.</b>	7.4	2.3	7.2	2.5	<b>6</b> .9	2.1						. 039				
493	<b>.</b>	ņ	7.3	2.5	7.6	2.3	7.5	2.3						.03;				
1494	11.9	3.0	1.8	3.6	12.3	3.7	12.5	3.8						. 055				
1495	J. 7	œ.	1.5	3.5	1.6	3.5	1.8	3.6						. 055				
1498	4.0	•	8.3	2.5	9.7	3. <del>0</del>	9.5	2.8					2.5	.043				
499	11.7	٠ ا	11.7	ر م	<b>e</b> .	ر ا	=.a							. 054				
205	• •	- 5	<del>7</del> .4	<b>4</b> (	2.5	4.6	12.8		13.3	<b>4</b> . <b>0</b>			ب م. م	.062				
200	7.0	- (		;;		* •	· •	;;						140.				
		.,		) 4	• •		0 Y							0 4 4 0 4 4				
512	•		7.7		7		ec.							22.6				
513	12.3	10	12.4	10	11.8		12.1	3.7						956				
1517	7.9	2.4	-	4.6	4.	2.9	10.3	J. 1						944				
519	5.5	1.7	12.6	3.8	11.0	3.4	11.8	3.6						.054				
1520	12.6	S. 50	14.0	4.3	13.6	<del>-</del> :+	13.8	4.5					4.0	. 969				
1526	3.8	1.2	4.6	1.6	<b>8</b> .8	2.1	5.7	1.7	6.1	4.9				.022				
1530	۲.	ij	14.1	4.3	12.4	3.8	12.3	3.8					3.2	.057				
543	5.5	1.7	8.5	2.6	7.6	2.3	8.0	2.2					2.5	. 044				
348	8.6	<b>5.0</b>	9.7	3.0	<b>8</b> .3	2.5	9.S	5.9						.047				
1551	<b>4</b> .	<b>o</b> :	9.0	2	8.2	2.5	<b>8</b> .1	2.5					2.5	. 038				
2566	<b>8</b> 0 ·	2.7	<b>8</b>	e,	ص ص	9. 9.	<b>6</b> 0 1	9 9					2.8	.048				
9570	<b>4</b> .0		B.	2.1	<b>8</b> .7	2.6	7.7	2.3					6. -	.034				

		3	LANDING DAT	<	- NODEL EA-6	3		Š	S ENTE	RPRIS	USS ENTERPRISE (CVN-65)	-65)			Z	IGHT L	NICHT LANDINGS				
200		- I	Σ U	Z <	6 L E			Œ	ROLL	<b>z</b> <	اد ن ع	ш		PITCH RATE	RATE	POLL	ROLL RATE	r.	F. P. A.	YAW	_
2	2	6	8		•	4		5		8		i.		¥	5	¥	5	AT TD	5	AT TD	۾
	DEG	3	DEC	3	DEC	3		DEG	8	DEC	3	DEG	\$	DEC	3	DEG	<b>8</b>	DEG	8	DEG	3
Ŧ	7	3	\$	\$	<b>\$</b>	41	\$	49		80	51	25	53	\$	22	28	22	80	28	99	19
9445	12.7	. 222					ī	'	32									-5.7	- 689	ø.	.120
9456	<b>8</b> .	.155							25		•		•			် ရာ ရ	-		073		.196
9451 9454	2.0	76 T			12.3	.215	4.7. 4.4.	042	2 2		ī	0.[-	970	. n.	. 658.	2 . 2 . 3 .	.839. .858.	0	686 968	• •	129
9456	<u> </u>	.246					- 6	. 633	; z							19.5			965	2.2	.038
9461	8.7	.152					•		<b>e</b> :					3.2	.056	<u>.</u>		,	082	9.0 0	.052
9468	e '	.208					 	. 623	ខ្ល					ب و و	625	• • • <u>•</u>	1007		988	ه د د	. 016 7.0
9478	11.2	. 1.					*		; <u>c</u>						802	.0			698	5.4	.079
9484	9.	. 208					5.3	1	82							13.4		6.7	986		009
9486	10.6	. 185					-2.6	ı	ž.						0.00	ø. ;		<b>+</b> 1	059		049
9488	12.1	.211						.012	2 2					<u>-</u> :	.019	ا . ا			699	4.5	.073
9489	5:	. 201					, c	. 859	929					7.4	2/9.	ر اه ده اه ده	- 200. - 201	֓֜֜֜֜֜֜֜֜֝֜֜֜֜֓֓֓֓֜֜֜֜֜֓֓֓֓֜֜֜֜֜֓֓֓֓֓֜֜֜֜֓֓֓֡֓֡֓֜֜֜֜֡֓֡֓֡֡֡֓֡֓֜֡֡֡֡֓֜֝֡֡֡֜֝֡֜֜֡֡֡֡֡֡֜֝֜֜֡֡֜֝֜֜֜֝֡֜֜֝֡	1.003	٠: ر	4. d
949	20.5	183					2 .0	6	935										. 963		. 0.5
9492	8.	13					2.9	.051	: 5									-5.3 -	692	•	007
9493	8.0	171.					<b>æ</b> .	410.	<u>*</u>					•		-1.2		- -: T	072	<del>+</del> .	.024
9494	8.6	.150					5.0	. 987	37						.017	. <del>.</del>		<b>.</b>	084	2.8	.049
9495	12.1	.211						.026	9 :				1			α.		ار د د	054		.028
0 0 <b>7</b> 0	- P	3 5					7. 6	921	5 5					ر 10.0	. 949. 9.999.9	- w	. 663	, r	1.682 1.082	 	
9562	12.5	.218			12.7	. 222	•	ı	9		_	6.	- 710.			16.2		~	038		051
9503	9.5	. 166					-2.9		<u>=</u>					6.3					070		017
9595	8	.155					0. 0.		37					<b>.</b> ;		•			636		939
9598	6.7 7.8	.117					E .		2 5					4. 6	181	9 9	e1e - 133 -	- 2.5	058 058	5 0	063
9513	1	194					1.2		2 2										051	8.0	996
9517	80	<del>-</del>					5.4		*						. 005	9.5			.012		042
9519	9.0	. 168					2.2		82					3.7	. 065	8.2			.035		9.00
9550	7.8	136						002	92					4.0					092	. S	148
9526	<b>9</b>	. 168 			10.3	. 180	Ī	059	<u></u>		7	٠.5	068		.122		063	0.7	136	19.2	178
900	<b>.</b>	5:					<b>.</b>	999.	999					7 E		0 0			1.803	·	
		. 8					7 17	. 603	3 17					, 10 , 10		13.0			679		. 633
9551		- -						. 023	2							60	014 -		035	4.6	. 059
9266	9.7	. 169					-	ġ	992					0.0	0.00	_	012 -	~	091	8.2	143
9570	10.2	.178					<b>+</b>	ë	24					7.5	.131-10.	_	176 -	5.1	689	1.7	. 030

	3	CANDING DATA	1	MODEL EA-6	<b>9</b>		USS E	USS ENTERPRISE (CVN-65)	RISE	₹)	-65)			Z	IGH THE	NIGHT LANDINGS	'n			
	OFF-CENTER		RAMP TO TD	WIRE	WIRE SIDE	997	3	SHIP		DECK PITCH	11CH	DECK ROLL	POLL	10	15.49	BAROMETRIC	TRIC	\$	APR CEAR	REREAD
ä	DISTANCE	DISTANCE	ANCE	€.	Š	TYPE	300E	SPEED	A							PRESSURE	URE	2	RUNOUTS	NUMBER
E	3	E	×					a Z	S/N	DEC	3	DEG	3	4	ပ	IN HG	¥	Z	8	
3	2	\$	9	67	8	9	7	7 17	. 22	22	7.	22	76	12	78	79	88	<b>8</b>	82	
-	-7	261	2	n	418	56126		7	l +	, 1	965		.031	7	22	29.90	759.5	171	434.3	•
7	7	276	82	*	913	50200		_	1	+	667		005	7	77	29.90	759.5		426 7	-
÷	7	251	1	7	8	<b>36</b> 1 <b>88</b>		7	+		. 003		.010	7	22	29.90	759.5		426.7	•
7	ų,	780	2	*	<b>8</b>	20200		7	i +	5.	. 998		003	7	22	29.80	759.5		429.3	•
<b>*</b> :	† '	227	2 ;	~	8	50200		_	í T		. 993		.992	۲ i	22	29.98	759.5	89	426.7	•
2:	? •	5 5 5 5 7	<b>5</b> !	•	513	78128		•	í <b>→</b> •		897		621	F #	2 2	29.90	759.5		• •	•
<u>-</u> :	? •	25	3 3	7	<b>1</b> 5	56200		<b>~</b> r	i • •	ا د د	. 969		021	ς;	2 2	29.98	759.5		431.8	<b>6</b> (
2	? 1	3 5	3 5	• (		99796		<b>-</b> r	i   • •	! • •	/ ee ·	ų.		< ;	3 8	98.82	U. 80.	20 0	428.5	<b>D</b> 6
* *	1 1	326	<b>à 2</b>	N C	8	97195		· r	i 1	6 e	4 6		C20.	< F	3 5	28.82	750.0		428.5 428.5	Ð -
2 2	7	266	3 2	٠	2 6	8 6 6		. ~	i   • <b>→</b>	, I	9 6		023	: =	3 2	28.82	759.5		6.6	- <b>-</b>
: =	†	<b>5</b>	3	44	2	50120		. ~	` i	ا. د د د	995		600	: =	52	29.90	759.5	170	431.8	. •
9	?	252	11	n	903	50200		7	Ĭ <b>+</b>	+.	967	<b>+</b> :-	.024	71	22	29.99	759.5	169	429.3	•
7	1	259	2	*	2	50120		7	i +	ن. 1	- 969	₹.	. 007	7		29.90	759.5	169	429.3	-
•	•	S.	102		8	60200		_	ľ	~	003	J. 10.	. 995	<b>.</b>		29.90	759.5	0	9.9	•
7	7 -	321	8		2 3	50200		٠,	i + c	~ •	. 993 5 5	ų.	999	<b>-</b>	3 5	29.90	759.5	<b>6</b>	<b>6</b>	<b>6</b>
= =	7 1	27.0	2 8		9	70.00		٠ ٦	1 C	  -	996	· «	. e		3 6	78.67	759.0	9 6	9 6	9 6
- 6	٩	222	: 2	8	919	50200		+	. I	) (၁)	010		. 992	: =	1 ;	29.92	769.0	167	424.2	۰ ۸
100	ရ	233	7	n	416	50200		+	1		009	ĸ.	. 669	71	77	29.92	760.0		429.3	-
9	7	333	101		905	66128		4	7	ان ا	005		002	7		29.92	760.0	0	<b>9</b> .	0
-100	47	<b>528</b>	92	7	919	80120		+	7	+ •	007		012	7		29.92	769.9		426.7	7
7	†	224	2	8	<del>5</del>	56166		•	7	†	007	6.1	016	7	22	29.82	760.0		429.3	•
ø	-7	<b>5</b>	22	7	86	<b>50200</b>		*	1	.7 -	012		003	7	22	29.82	769.0		429.3	9
7	1	228	69	8	993	50120		4	1 7	- 7.	012		662	7	77	29.90	759.5		431.8	-
P	7	<u>5</u>	22	~	996	<b>Se 188</b>		*	7	_	012	9.1	010	7	22	29.90	759.5	<b>168</b>	428.7	•
97	4	159	\$	7	913	50120		*	7	ı. I	009		. 023	7	22	29.90	759.5		428.7	-
-12	-	<b>7</b> 00	5	*	P 96	56266		*	1	.7	012	-	002	7		29.82	769.0		426.7	-
=	·	192	8	8	913	50120		4	1	! ♥.	007		019	7		29.92	760.0	168	426.7	<b>-</b>
-		277	*		993	60120		*	ر د	.2	003	-1.7 -	030	7		29.92	760.0		<b>.</b>	0
7	-	259	2	~	992	56186		4	7	٠ ا	609		662	7	22	29.82	760.0		429.3	-
5	-	101	3	~	5	50200		*	1		012		009	7		29.82	760.0	168	426.7	•
٩		261	2		996	70120		*	7	0.0	9.00		012	7		29.92	760.0		<b>9</b> .0	•
۴	-	265	5	n	996	20200		n	i n	۱ ♦	007		9.666	7	<b>5</b> 5	29.93	760.2		424.2	•
*		285	87	n	993	50120		ر د	i I	1 + 1	007	-1.7 -	030	<b>7</b> i		29.93	769.2	169	429.3	•
2	7	297	5		993	66126		n.	i n	i.	. 995		. 997	<b>F</b> i	22	29.93	760.2		<b>9.</b>	<b>o</b> •
٩	7	258	8	*	905	50200		60	i n	¹ ★.	. 997	2	003	7		29.93	760.2	167	424.2	•

			KG	21		n	<u>.</u>	• •	· <del>·</del>	2	n.	<b>+</b> (	0 £		, io	ŭ	7	ຄັ	<b>+</b>	<b>±</b> !	2 ◀	• <u>•</u>	· <b>6</b> 0	ıΩ	יפי	<b>.</b>	i e	Ņ	Ģ	<u>,</u>	Ņ,	<b>+</b> (	ē.	<b>.</b>	<u>*</u> 1		t s	- 1	. 🛧
	WEIGHT		×	~		19713	20802	19759	20394	20802	19623	19864	205/5	10701	20575	19532	19577	19305	19214	20394	19214	70394	19078	19895	19033	19858	18716	18942	18942	19577	19532	19864	19858	19850	+995L	19713	12161	10577	19864
	*		LBS	20		43460	45860	44806	44960	45860	43260	43660	45560	43460	45360	43060	43160	42560	42360	44960	44/66	44969	42969	43860	41960	43760	41260	41760	41769	43160	43060	43660	43760	43760	43556	43468	42100	41160	43660
INGS	LIFT	FF		19																																,	99.		
DAY LANDINGS	LIFT	5		<b>5</b>	1.20	- - - - -	 8 .	90	1.00	1.99	. 90		9. 0		. 6	96.	89	96.	1.00	1.10	 5 6		1.00	.80	96.	 80	99.	96.	98.	1.10	8.	8	- 10		99.	9 6	9 6	9 0	96.
_	≩	٧. م		11	;	1.29	1.26	1.33	1.30	1.37	1.24	1.21	1.32	 	1.32	1.23	1.27	1.24	1.25	1.19	1.23 80 80	1.26	1.28	1.28	1.20	1.22	1.22	1.30	1.26	1.27	1.25	1.22	 	1.25	9	1.25		3.5	1.21
	KVPA	Z Z		16																																			
ž	V.dSA		N/S	5	;	<b>;</b> !	<b>4</b>	} <b>1</b>	<b>.</b> 5	<b>\$</b>	‡	‡ :	Q *	; ;	. <del>1</del>	‡	‡	‡	‡	<del>ر</del> د ن	ç <b>२</b>	5.	‡	‡	‡	‡!	<u> </u>	5	5	‡	‡	‡ :	‡ :	<b>;</b> ;	::	:	;	; ;	‡
USS ENTERPRISE (CVN-62,	8		호	<b>±</b>	•	8	e e	8	88	88	86	98	20 K	8	8	96	88	82	82	80 7	) «	8	8	86	82	86	, g	8	\$	86	86	8	98	8	9 6	88	6 8	3 4	98
PRISE	VPAMIN		N/S	5																																			
ENTER			N X	1 12	10	<b>س</b> ا	~ #	, i		•	•	~ 4				_	_	s S	~	<b>~</b> .				••	<b>.</b>	~ -	. ~			<b></b>	~	<u>~</u>		•		· .			
uss	VEOR		KN W/S	16	69	•	91 47	7	•	96 4	. •	•	20 40			84 43	4	*		83 43	84 40			90 46	•	81 42			•	•	•		•		•	88 46	•		98
			N/S		-	-				6	<b>19</b>	<b>=</b>		. «		E	7	<b>6</b> 0	<b>.</b>	<b>.</b>	» «			6	<b>.</b>	-		60	6		<b>6</b> 0	<b>.</b>	<b>o</b> n (	o (	<b>.</b>	10 P			. 80
E-20	Æ	PERP.	Z.	•	7	~	~ ~	٠,	. 4	7	7	N (	N 6		. ~	~	8	~	~	N (	4 6			~	<b>7</b>	~ .	۱ ۲۷	'n	7	N (	~	N (	<b>N</b> (	N (	N (	N 6	٦ ,	4 6	
~ MODEL E-20	WIND-VEL	PAR.	Ş	7	12	<u>.</u>	2:	3 🕏	2	13	5	2 :	2 =		: 2	13	13	5	<b>1</b>	2;	2 💆	2 12	<b>5</b>	5	<b>P</b> :	2:	3 12	5	13	<b>5</b>	<b>5</b> i	2 :	2 !	2:	2:	2:	2 :	2 5	<u> </u>
DATA -		ā	₹	•	23	53	5 5	2 5	22	22	52	52	υ <b>κ</b>	, ,	23	22	22	22	23	52	, K	2 52	22	22	52	52	2 2	22	22	23	22	8	ខ្ល	20	8 8	2 2	g K	3 ¢	22 22
CANDING D	VE-FILM		Ş	60	3	<b>‡</b> :	<b>\$</b>	7 9	\$	<b>\$</b>	7	<b>;</b> ;	<b>;</b> ;	<b>?</b>	: <table-cell-rows></table-cell-rows>	7	7	7	4	<b>;</b> ;	<b>†</b> 2	; ;	7	‡	<b>6</b> 2	7 9	4	‡	42	7	7	4	<b>\$</b> :	7:	ů á	<b>7</b>	? ?	; ;	Ŧ
3	Š K		2	*	3		6	_	2	8	95	8 7	5 \$	3 2	5	9	2	5	5	2 8	8 2	8	3	8	76	<b>=</b>	7 82	2	82	*	97			2 :	6	6	0 a	9 4	8 6
	VPAF	2	<b>S</b>	2			22.58			_	107 55	8	0 Y 4	7		106 55		•		3	2			_	•,	96		110 57				96 55	13 58	88		197	00 CB		2 4 2 2
	SON	Š.	\$	_	•		1986	-	_	_	•		1966		•	•-	_	_	_	- 1	7007	•	•	_	_	2008		_	-	•-	_	-	_	- 1	- '			- •	2034 10
	Í	-		-	- ;	= :	5 5	- 5	2	2	5	<u> </u>	~ 2	. 0	5	2	2	5	7	2 2	7 6	3 6	2	26	2	26	28	2	2	3	26	2	7	2	2	2 2	ž	, ,	26

995			AIRCRAFT	••	KING S	PEED A	SINKING SPEED AT TOUCHDOWN	N			GLIDE PATH ANGLE AT TD	PATH A	NGLE A	T 10	WHEEL HEIGHT	1EIGHT	HOOK HEIGHT	IGHT
£	NOSE	SE	PORT	7	S	STBO	AKG	<b>.</b>	FREE-FLIGHT	IGHT	<b>8</b>		8	>	OVER RAMP	de la contra	OVER RAMP	ANP.
	5	Ş	2	Ş	Ş	¥	5,5	N/S	£/\$	M/S	DEG	2	DEC	2	E	3	E	*
2	22	<b>5</b>	22	<b>38</b>	27	28	53	95	5	32	z	z	35	36	37	82	39	\$
3	5.0	2.8	8.8	2.7	<b>8</b>	2.7	9.6	5.9				.072	<b>4</b> .6	.679	18.2	5.5	15.4	4.7
1978	3.7	=	<b>9</b> .	<b>9</b> .	7.9	7.4	<b>8</b> 9.	2.7		. •	3.5	999	3.7	. 964	18.1	5.5	12.4	3.8
98	<b>9</b> .0	о. Р	12.7	a. B.	•.	o. 0	5.5	3.5		Ť	3.5	.061	4.4	.075	19.0	S. 8	13.6	4.2
1981	<b>†</b>	7	4.9	7.0	<b>8</b>	2.5	7.0	2.1			2.5	110	5.6	.045	13.3	<del>-</del> :	7.2	2.5
25	4.	1.7	8.5	2.5	9.0	2.4	7.9	7.4			5.6	940	2.8	.048	16.5	 •	T	4.6
3	6.7	7.0	<b>.</b>	5.8	0	5.6	<b>.</b>	2.7		•		.055	J. J	.058	18.6	5.7	12.8	a. n
2865	٠. د د	7.5		n. e	<b>9</b> .0	n	<b>4.6</b>	3.5		•	- r	. 672	ب د د	.064	20.9	<b>4</b> •	5. s	<b>↓</b> . ¢
		· ·		) (			7.01	- ·		•	? r	95.4	- 4	7/0.		•		7 ·
) S		- c	. e	7 F		, c	7. 8	7.7			2 0	957		948	5.0	, e	. v.	. 4 . 6
98	7.0	2.1	8,3	2.5	8.5	2.6	4.	2.6			2.8	948	3.7	964	16.1	4	7.0	9.0
1996	-	"	8.1	2.5	7.5	2.3	7.8	7.4			3.5	.055	2.9	.051	16.2	6.	10.4	3.2
1992	<b>.</b>	'n	5.3	9.	5.6	1.7	5.5	1.7			3.1	.054	2.0	. 036	16.3	5.0	10.8	3.3
1993	7.2	2.5	9.	7.4	9.3	5.6	8.3	2.5			8.	.031	3.1	. 054	14.4	<b>+.</b>	8.5	9.8
1994	4.7	<b>*</b> :	7.4	2.5	7.3	2.5	7.1	2.1			2.2	.038	2.8	.048	13.1	<b>4</b> . <b>0</b>	<b>.</b> .	2.5
1999	9.9	<b>7.</b>	7.3	2.5	7.2	2.5	7.2	2.5			2.5	.039	2.8	.049	12.9	g. E	7.3	2.2
<b>786</b>		<u>.</u>	4.7	<b>+</b>	4.6	<b>9</b> .	<b>6</b> .	5.			5.9	.051	2.5	.039	e. =	٠. ا	<b>.</b>	æ.
2	S. 6	<b>.</b>		2.5	<b>60</b>	2.7	7.8	7.4			4.6	969	6. 6.	.053	<b>8</b> .6	5.7	12.3	ຄ. ຄ.
Z <b>66</b> Z	D (	2.1		2.5	1 0	2.5	<b>5</b> •	2.7				900	5.2 2.2	.055	9. ¥	<b>*</b> •	. e. c	2.5
	, d					• •	. €	0.7 •			 	200	7.4	829.	. ¥			9 6
200	8.8		5.5	1.7	9.0	2.1	. 6	2.1			9.6	951	2.5	.043	13.2	4	7.3	2.5
2000	5.2	9.		2.8	6.5	2.0	7.9	2.4			1.7	.029	3.0	.053	10.2	3.1	4.7	4
2007	8.7	2.6	9.5	5.8	7.9	2.4	8.5	2.6			2.5	.043	3.7	. 964	15.9	4.8	<b>†</b> .	5.9
2002	4.7	<b>+</b> :	8.7	5.6	5.0	<b>.</b>	6.3	6.			2.3	949	2.2	. 038	13.1	<b>6</b> .4	7.6	2.3
2000	<b>6.</b>	£.	9.0	1.7	<b>6</b> .0	-	J. 1	<b>•</b>			2.5	.038	1.2	.020	1.5	ب ا ا	5.7	1.7
	<b>D</b>	7.7	B. 6	? .		7.4		N (			- 1	929	, ,	.067	7.5.	<del>,</del> ,		/:
2012			 	 	4.7	2.5	2.0 1.7	, ,			 	5.6		944	7.21	F 01	- a	2.1
2019	8.0	-	7.2	7.7	4.7	<b>+</b> :	9.	<b>*</b>			9.5	952	2.4	.042	4.4	4.4	0.6	2.7
202	9.0	=		2.8	11.7	3.6	10.3	3.1			2.5	944	3.9	. 969	14.2	<b>4</b> .3	7.9	7.4
2024	7.1	2.1	<b>8</b> .8	2.1	7.2	2.5	6.9	2.1			2.6	945	2.7	.047	17.0	5.2	1.1	4.6
2025	5. 0.	<b>.</b>	7.8	2.4	<b>9</b> .7	<b>.</b>	7.3	2.2			2.7	948	2.7	.047	17.3	5.3	1.5	u.5
2026	5.5	<b>9</b> .	7.5	2.3	<b>6</b>	<b>.</b>		2.0			9.0	.045	2.5	.044	15.4	4.7	<b>6</b>	5.0
2027	<b>6</b>	2.7	7.3	7.7	7.8	4.6	7.3	7.5			4.5	146	2.5	.044	9.5	4. m	10.4	3.5
2029		2 9 (	1 <b>6</b> .5	2.5	, 0	2.5	9 ·	2.7	•		9 0	040		.863		<b>.</b> .		, c
285	, ,	7.	× •	? ·	- 0		- ·		2.2	9.	9. C	934	٠ ر ۲ رو	.028 010	12.8		D	- ''
2621	7.0.7	<u>.</u> .	- •	- (	, ,	D 7	Þ. ć	- r		•		***	 	, e c	5.0	7.7	- r	, c
3	• •		o (	» c	7.	÷ •	9.7	7.0			0.4	240	0 0	- 50	+ · ·		. 6	, c
1007	P.	7.1	7:	7.7	9.	.,	?			•	?	) 1	•	200	<u>;</u>	-		-

DAY LANDINGS

USS ENTERPRISE (CWI-65)

LANDING DATA - MODEL E-20

200			AIRCRAFT	S	KING :	MKING SPEED AT TOUCHDOMN	T TOUCH	N			GLIDE	GLIDE PATH ANGLE AT TD	WGLE A	0T T	WHEEL	MEEL HEIGHT	HOOK HEIGHT	EIGHT
2	MOSE	SE	8	PORT	'n	STBO	AVG	ø	FREE-FLIGHT	LIGHT		<b>2</b>	6	<b>A</b>	OVER RAMP	RAMP	OVER RAMP	RAMP
	2	Ş	£	\$	2	Ş	53	K K	F/S	S/M	930	8	DEG	3	E	3	E	3
8	23	*	23	26	27	28	53	8	ñ	32	33	ņ	35	36	33	88	39	40
2635	3.5	=	3.6	-	J. 7	ø.	2.6	€0.			3.0	.052	1.2	.620	15.6	<b>*</b>	10.2	3.1
2658	<b>.</b>	ņ	. c	2.8	8.2	2.5	<b>6</b> .0	2.7			2.0	. 035	3.6	. 062	12.5	3.8	6.2	9.1
2639	<b>.</b>	5.	6.0	2.1	7.6	2.3	7.2	2.5			<b>5.0</b>	. 034	2.9	.051	11.3	4.8	5.8	1.8
7 7 7	S.	<b>.</b>	<b>0</b> .0	2.1	7.0	2.1	7.0	2.1			2.1	. 036	5.6	.045	13.4	4.1	7.3	2.2
2	7.7	- !	<b>6</b>	2.1	7.6	2.3	7.3	2.5			5.6	.046	2.8	. 049	14.2	4.3	8.6	2.8
2042	ر د د	7.7	7.	2.1	<b>4</b> .	7.0	6.7	7. 9.			ا د ن	.961	2.5	.044	18.4	9. <b>0</b>	13.1	<b>6</b> .4
200	• - • •			- c	- 7	6 6 7	8 8 4	6 7 8			ان د . د	.054 44	4. c	. 64.	16.1 1.0	<b>4</b> 4	- <del>-</del> -	n.,
2132	4		-	; r;		9 6	10.4	3.2			;		4	690	2	n •		?
2141	8.3	2.5	8	o.n	7.6	2.3	8.7	5.6			2.7	.048	4.6	.059	17.5	5.3	1.0	4.6
2149	5. •	 5.	<b>†</b> .	2.0	2.5	۲.	4.3	r	8.8	2.1	5.9	.050	<b>+</b> .	. 024	17.4	5.3	10.9	u.5
2371	7.4	2.2	8.7	2.7	10.8	3.3	9.6	2.9			2.2	. 038	3.7	. 065	13.4	<b>+</b> .4	8.2	2.5
2372	<b>8</b>	2.7	10.3	3.2	8.5	<b>5.8</b>	6.6	2.7			2.7	.048	3.2	.057	16.6	5.1	=:-	4.6
2376	<b>7</b> .	2.1	7.3	7.5	7.1	2.5	7.5	2.5			2.9	. 656	2.8	.048	17.9	s. S	12.4	а. В
2377	7.6	2.3	<b>.</b>	5.5	13.7	4.5	9.0	ا ا			2.7	.047	4. D.	.076	14.7	4. R.	<b>8</b> 0.0	2.6
23/8	- ·	2.5	- (	7.0		2.8	D) (	7.7			, id	949	o .	199.		<b>.</b>		8.0 0.0
			9 1	0 r			7:/	7.7			7.7	. 648	9 F		3.5	4.2	- 0	2.5
000		- <b>·</b>			•	÷ (	• •							949		•	:	•
2383	 			2.2		1.7	9.4	- 6	2.6	1.9	 	. 600		979	1. 4.		• •	• <i>•</i>
2364	9.5	2.8		3.	4	6.	10.0	9.	<u>:</u>	:	6,0	.053	÷	.072	19.1	. RO	13.6	. 4
2385	10.0	3. •	10.5	3.2		2.8	9.6	2.9			2.7	.048	3.8	990.	13.8	4.2	8.0	2.5
2386	9.5	5.6	4.0	7.6	8.5	2.6	<b>4</b> .	2.6					4.5	. 969				
2387	3.5	<b>6</b> .	3.7	=	4.0	1.7	<b>4</b> .	<b>+</b> .			2.4	. 042	2.1	. 037	10.5	3.2	4.8	<b>†:</b>
2368	<b>+</b> 1		4.	<b>+</b> (	7.4	2.3	6.2	6.6			9 :0	.045	4.4	140	<b>10.</b>	3.2	<b>4</b> .	5.5
2368		7 6		, v	0.	2. c		9 10			7.7	. 040 0.	* 0	. 608 749	4. <del>4</del> . 4	÷ •	9 C	50 C
2301		¥.		-		9 -					) F	45.	4	942	13.0	. 4		
2392			7.0	2.1	7.7	2.3	7.3	2.2			2.7	948	2.5	944	1.5	3.5	S.	. 6
2393	9.1	2.5	•.	2.7	7.3	2.5	7.7	2.3	8.5	5.6	2.8	.049	2.8	. 050	17.3	5.3	11.7	3.6
2394	<b>3.6</b>	1.7	<b>9</b> . <b>7</b>	2.0	7.0	2.1	6.7	2.0			2.2	.038	5.8	.051	12.3	3.7	6.1	9.1
2396	6.8	2.1	7.3	7.5		2.5	7.7	2.3			2.8	.049	3.2	. 055	16.2	<b>6.</b>	10.2	3.1
2402		5.6	٠. د	7.5	7.4	2.5	 	7.7			2.1	.038	7.4	.042	<b>+.</b> +	4.4	<b>9</b> .	7.4
2404		5.6	7.1	2.5	0.	7.7	7.5	2.3			9.	.046	5.8	. 656	16.4	•	9.9	ы. Б
2	<b>8</b>	- (	۵. و	- (		<b>.</b>	 	- ·			2.5	. 638	<b>6</b> .	.034	13.8 8.5	4.2	7.9	2.4
2406	10 t	2.6	10 F	2.7	10.5	3.5	6.7	5.6			6. c	.051	ا ا ق	.062		n. •	÷ •	, 5 5 5
	0. T	- «	p	۲. د د د	? <b>•</b>	o •		2.6			8. F	949.	7.7	848	 	+ u	÷ ;	9 e
4 6 3 6		1.7	. e.	==	, to		0.0 0.7				r.	PC9.		. 926	<u>.</u>	0	5.4	D. ?

RAD         DEG         RAD         RAD         RAD         RAD         RAD         RAD         RAD         RAD         RAD <th>LANDING DATA - ME</th> <th>1 2</th> <th>1 2</th> <th></th> <th>MODEL E-20 6 1 F</th> <th>ģ</th> <th></th> <th>BOIL ANGLE</th> <th>-</th> <th>  </th> <th><b>L</b>ai</th> <th>0.</th> <th>PITCH RATE</th> <th>ra ATE</th> <th>DAT CANDINGS</th> <th>RATE</th> <th><u>د</u></th> <th><b>4</b></th> <th>***</th> <th></th>	LANDING DATA - ME	1 2	1 2		MODEL E-20 6 1 F	ģ		BOIL ANGLE	-	  	<b>L</b> ai	0.	PITCH RATE	ra ATE	DAT CANDINGS	RATE	<u>د</u>	<b>4</b>	***	
RAD         DEG         RAD         RAD <th></th> <th></th> <th></th> <th>FF TD</th> <th></th> <th></th> <th></th> <th></th> <th>O</th> <th>5 E</th> <th>ل</th> <th>•</th> <th>. IV</th> <th></th> <th>7</th> <th>1 P</th> <th>. ¥</th> <th>·ρ</th> <th>¥ .</th> <th>. e</th>				FF TD					O	5 E	ل	•	. IV		7	1 P	. ¥	·ρ	¥ .	. e
52 53 54 55 56 57 58 59 60  3.7	DEG RAD DEG RAD DEG RAD DEG RAD I	DEG RAD DEG RAD DEG RAD	LO DEG RAD DEG RAD	RAD DEG RAD	DEG RAD	3		_	DEC	3	DEG	2	DEC	2	DEG	8	DEG	8	DEC	3
3.7	42 43 44 45 46 47 48 49 50	45 46 47 48 49	46 47 48 49	47 48 49	48	\$		2	_	2	25	53	54	22	8	22	88	28	8	5
-2.7047 5.3 .0924007 3.2 -2.3040 8.2143 -2.10373 -1.6040 8.2143 -2.1049 4.2 -1.3065 1.9 .033 -2.3040 3.1 -2.2038 -2.3040 -1.80313 -0.0 0.000 -4.0070 -3.0040 3.1 -1.1002 5.60102038 -2.6 -1.1002 5.60102038 -2.6 -1.2002 5.60111002 -3.1 -1.3002 1.80312047 2.0 -1.3002 1.80312047 2.0 -1.3002 1.80312047 2.0 -1.3002 1.80312047 2.0 -1.3002 1.80312047 2.0 -1.3002 1.80312047 2.0 -1.3002 1.80312047 2.0 -1.3002 1.80312047 2.0 -1.3002 1.80312047 2.0 -1.4002 1.80312047 2.0 -1.5006 1.40021 1019 0.0 -1.5006 1.4024 -2.2091 1.7 -1.6006 1.7 -1.4024 -2.7047 2.0 -1.6006 1.7 -1.4024 -2.7075 1.2 -1.7006 1.7 -1.4024 -2.7075 1.2 -1.8007 1.3 -002 -3.1 -002 -3.1007 1.3 -1.9009 -2.7047 -2.7047 3.3 -1.0009 -2.7047 -2.7047 3.3 -1.0009 -2.7008 -3.1056 -3.1056 -3.1009 -3	- 9 810. 6. 700.	6 6 610	6 6 610					-	ı	072		מי						. 938	2.7	.047
-2.3040 8.2 .143 -2.10373 -1.5040 8.2 .143 -2.1049 4.2 -1.5005660103040 3.1 -2.2035 -2.3046 -1.80313 -2.2035 -2.3046 -1.80313 -0.0 0.0004 0070 -3.0052 3.2 -1.1002 5.6 .101 2.2 .038 -3.1 -1.2002 5.6 .101 2.2 .038 -3.1 -1.3002 1.8 .0318014 3.0 -1.3002 1.8 .0318014 3.0 -1.3002 1.8 .0318014 3.0 -1.3002 1.8 .0318014 3.0 -1.3002 1.8 .0311019 1.7 -1.3002 1.8 .0311019 1.7 -1.3002 1.8 .0033044 1.3 -1.4002 1.8 .0311019 1.7 -1.5006 1.4024 -5.2091 4.4 -1.6008 2.9005 -2.2035 -1.8 -1.6008 2.9005 -2.2035 -1.8 -1.7008 2.9005 -1.1019 1.7 -1.8001 2.4024 -2.5045 2.4 -1.9008 2.9005 -1.1019 1.7 -1.9008 2.9005 -1.1019 1.7 -1.9008 2.9005 -1.1019 1.7 -1.9008 2.9005 -1.1019 1.7 -1.9009 2.9005 -1.1019 1.7 -1.9009 2.9005 -1.1007 1.3 -1.0000 -2.7047 -2.7047 3.3 -1.0000 -2.9001 -2.7047 3.5 -1.0000 -2.9001 -2.7047 3.5	. 134 8.1 . 141	.1 .141	.1 .002	.002	.002	.002		÷.		. 080		7					_	.007		.056
6010 -6.4112 -4.0070 -4.2  -1.50266 -010 -2.8049 -4.2  -2.2038 -2.3040 -1.80313  -0.0 0.0006010 2.2038 -2.6  -1.1002 5.81011002 -3.1  -1.2002 1.80312044 1.3  -1.3002 1.80312044 1.3  -1.4002 1.80312044 1.3  -1.5002 1.80313044 1.3  -1.5002 1.80312044 1.3  -1.5002 1.80312044 1.3  -1.5002 1.80312044 1.3  -1.5002 1.80312044 1.3  -1.5002 1.80312044 1.3  -1.5002 1.80312044 1.3  -1.6000 1.4024 -5.2044 1.3  -1.8001000 2.9051 -1.4024 2.0  -1.9000 2.9051 -1.4024 2.0  -1.0000 2.9051 -1.4024 2.0  -1.0000 2.9051 -1.4024 2.0  -1.0000 2.9051 -1.4024 2.0  -1.0000 3.1054 -4.3055 1.3  -1.0000 3.1054 -2.50440  -1.0000 -2.7047 -2.7047 3.3  -1.0017 -1.4024 -6.2001 -2.7  -1.0000 -2.0051 -2.7  -1.0000 -2.0001 -2.7  -1.0000 -2.0 -001 -2.7  -1.0000 -2.0 -001 -2.7  -1.0000 -2.0 -001 -2.7  -1.0000 -2.0 -001 -2.7  -1.0000 -2.0 -001 -2.7  -1.0000 -2.0 -001 -2.7  -1.0000 -2.0 -001 -2.7  -1.0000 -2.0 -001 -2.7  -1.0 -000 -0000 -2.0 -001 -2.7  -1.0 -000 -0000 -2.0 -001 -2.7  -1.0 -000 -0000 -2.0 -001 -2	117 7.3 .127 0.0 0	3 .127 6.0 0	0.0	•	•	•	9.000	3	I 	.016		7						.037	•	065
-1.3 - 0.05	9 .138 10.1 .176 3.0	1 .176 3.0 .052 1	3.0 .052 1	. 652	. 652	. 652	_	<b>.</b>		.031		, ,		•				979	4.5	. 673
-2.2038 - 2.3040 - 1.80313  e.e e.eee	0 <	. 150		•	•	•	200	- ?	ı	. 002		ī '		. 500 070	0 0			940	7 F	545
6.0 6.000 -4.0 -070 -3.0 -0552 3.2 6.0 6.000 -6. 010 2.2 -038 -2.6 -1.1 -002 5.8 -101 -1 -002 -3.1 -1.3 -0055 -7 -012 -2.7 -047 2.0 -1.3 -0052 1.8 -031 -18 -014 1.3 6.0 6.000 -1.4 -024 -5.2 -0041 4.4 -1.3 -025 1.8 -031 -1.2 -021 2.1 -2.3 -025 -3.2 -026 -2.3 -040 0.0 -2.3 -025 -3.2 -025 -3.2 -026 -1.1 -1.3 -025 -3.2 -025 -2.3 -040 0.0 -2.3 -025 -3.2 -025 -3.3 -040 0.0 -2.3 -025 -3.2 -025 -3.3 -040 0.0 -2.3 -025 -3.2 -025 -3.3 -040 0.0 -2.3 -025 -3.2 -025 -3.3 -040 0.0 -2.3 -025 -3.2 -025 -3.3 -045 -1.1 -1.8 -031 -7.1 -124 -2.6 -045 2.0 -2.9 0.00 0.000 7.3 127 -2.6 -045 2.0 -2.9 0.00 0.000 7.3 127 -2.6 -045 2.0 -2.9 0.00 0.000 7.3 127 -2.6 -045 2.0 -2.9 0.000 0.000 0.1 128 -1.10 1.0 -2.1 0.000 0.000 0.1 128 -1.0 -2.1 0.000 0.000 0.1 128 -1.0 -2.1 0.000 0.000 0.1 120 1.2 -021 -2.0 -2.1 0.000 0.000 0.1 0.000 0.1 0.000 0.1 -2.1 0.000 0.2 -001 0.2 -005 0.1 -2.1 0.000 0.2 -001 0.2 -005 0.1 -2.1 0.000 0.2 -001 0.2 -005 0.1 -2.1 0.000 0.2 -001 0.2 -005 0.1 -2.1 0.000 0.2 -001 0.2 -005 0.1 -2.1 0.000 0.2 -001 0.2 -005 0.1 -2.1 0.000 0.2 -001 0.2 -005 0.1 -2.1 0.000 0.2 -005 0.1 0.1 -2.1 0.000 0.2 -005 0.1 0.1 -2.1 0.000 0.2 -005 0.1 0.1 -2.1 0.000 0.2 -005 0.1 0.1 -2.1 0.000 0.2 -005 0.1 0.1 -2.1 0.000 0.2 -005 0.1 0.1 -2.1 0.000 0.2 -005 0.1 0.1 -2.1 0.000 0.2 -005 0	126 6.8 .119 3.7	6.8 .119 3.7 .865 4	3.7 .065 4	. 965	. 965	. 965	*			.679		-2			:			.031		. 99.
0.0 0.000 .6 .010 2.2 .038 2.2 .011 1.002 2.3.1 1.002 2.3.1 1.002 2.3.1 1.002 2.3.1 1.002 2.3.1 1.002 2.3.1 1.002 2.3.1 1.002 1.3 1.3 1.002 1.3 1.3 1.3 1.3 1.3 1.3 1.3 1.3 1.3 1.3	.163 16.5 .183 2.4 .642 2	10.5 .183 2.4 .042	183 2.4 .042	. 942	. 942	. 942		2.2		.038		•					•			. 656
1002 5.8 .101 .1 .002 -5.130057012 -2.7047 2.01002 1.8 .0318014 1.30 0 0.000 -1.4024 -5.2004 1.4 -1.3023 1.8 .03112021 2.13023 1.8 .031 -1.2021 2.13025 -3.2056 2.3040 0.05009 -3.2056 2.3040 0.05009 -3.0055 2.2038 -1.33056 8.8 .154 -1.1019 1.7 -1.8056 8.8 .154 -1.1019 1.7 -1.8056 8.8 .154 -1.1019 1.7 -1.9 0.00 0.000 2.9 .051 -1.4024 2.0 -0.0 0.000 7.3 .127 -2.6045 2.4 -0.0 0.000 7.3 .127 -2.6045 2.0 -0.0 0.000 8.7 .152 -1.2056 2.3 -1.8 .001 2.4 .059 -4.5079 6.7 -1.9 0.00 0.000 -2003 -1.2056 2.3 -1.0 0.000 -2003 -1.2051 -2.0 -0.0 0.000 -2003 -1.2051 -2.0 -0.0 0.000 -2003 -3.4059 -3.4059 1.3 -1.0 0.017 -1.4 -024 -2.50440 -0.0 0.000 -2.7 -047 2.7059 -1.0 -0.0 0.000 -2.7 -047 2.7059 -1.0 -0.0 0.000 -2.7 -091 -3.2056 -1.0 -0.0 0.000 -2.7 -091 -3.2056 -1.0 -0.0 0.000 -2.9 -051 -2.7047 3.5	9.136 7.7 .134 -3.5	7.7 .134 -3.5	134 -3.5				. 961 .5	ń		. 969		•	_	900	٠.					045
38027812 -2.7847 2.8  -1.1802 1.8 .8318914 3.8  -1.3802 1.8 .8318914 3.8  -1.3802 1.8 .8318914 3.8  -1.3802 1.8 .8318914 3.8  -1.38024 .897 -1.1919 9.8  -1.5809385628562848 9.8  -1.580938563848 9.8  -1.680371242848 9.8  -1.883171242848 9.17  -1.883171242845 2.4  -1.980228981824 2.8  -1.980228981824 2.8  -1.980238024875 1.3  -1.9802918562856 2.3  -1.98029999999999	5.5 .896 -1.6 631 -4	5.5 8.6	4-1.6 031 -4	1.031	1.031	1.031	1	4.2	ı	. 073		1	· 	902						. 854
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### E-2 DAY

1   C   A   N   G   E	3	LANDING DATA	ŧ	MODEL E	E-20		uss em	TERPRI	USS ENTERPRISE (CWN-65)	N-65)			8	DAY LANDINGS	INGS				
Fr   Fr   Fr   Fr   Fr   Fr   Fr   Fr	-		Z	W					Z	w	**	TCH	RATE	ROLL	RATE	<del>ر</del> .	₹	×	•
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45         46         49         59         51         52         54         55         56         57         58         59         68           1192         -1.2         -844         -1.3         -862         -1.4         -824         -1.5         -823         -1.6         -828         -1.7         -1.9         -823         -1.6         -828         -1.9         -823         -1.1         -823         -1.1         -823         -1.1         -823         -1.1         -823         -1.1         -823         -1.1         -823         -1.1         -823         -1.1         -823         -1.1         -823         -1.1         -823 </th <th></th> <th>930</th> <th>3</th> <th>930</th> <th>3</th> <th>DEG</th> <th>3</th> <th>DEC</th> <th>8</th> <th>DEG</th> <th>8</th> <th>DEG</th> <th>3</th> <th>DEG</th> <th>3</th> <th>DEC</th> <th>3</th> <th>DEC</th> <th>3</th>		930	3	930	3	DEG	3	DEC	8	DEG	8	DEG	3	DEG	3	DEC	3	DEC	3
148		\$	\$	\$	<b>†</b>	\$	\$	8	5	25	23	Š	85	26	57	88	20	9	5
182		•	#		•	-	<b>1</b>	-	. 985		•	_				•	. 028	2.3	.023
159	-		. 192		1		•		.024		1						. 628		. 669
181   1.6   .028			.150			ĸ.			. 969		7		1				. 033		014
152			181			9.		*	. 044		_						.070		.052
124			.152						. 995		1		ł	' +			. 072	2.2	. 038
134			.124						· 014		_			6			. 054	<b>5.0</b>	. 635
134   1.1			126			<b>-</b>			. 037		ī '			<b>+</b> (			. 965	2.1	.037
1.85   11.1   194     1.862     1.8			<u>*</u>						. 033		_	•				_	.676	J. J	. 658
1.   1.   1.   1.   1.   1.   1.   1.	-	•				- •	. 662		•		T <b>°</b>	_					.052	G .	. 103
8.4         147         -27         -847         -5         -899         1.5         -26         8.0         140         -4         -897         -2           8.4         147         -27         -847         -5         -899         1.5         -26         8.0         140         -4         -897         -2         -899         -2         -899         -6         -899         -7         -2         -897         -2         -899         -7         -2         -897         -2         -899	-		)	-		ŗ, r	• •	•		,							0.40	• •	809.
8.4 144		9 7	- <del>5</del>	:	<u> </u>	. <del>.</del>	•				) to:	9 6	. 916 -	ı			. 852	9.0	616
8.2         :143         .2         :063         .2         :063         .2         :063         .2         :063         .2         :063         .2         :063         .2         :063         .2         :063         .2         :063         .2         :063         .2         :063         .2         :063         .2         :064         .2         :084         .0         :086         .0         :086         .2         :084         .2         :084         .2         :084         .2         :084         .2         :084         .2         :084         .2         :084         .2 <th>2</th> <td>4.0</td> <td>147</td> <td></td> <td>•</td> <td></td> <td>-</td> <td>1</td> <td>600</td> <td></td> <td>-</td> <td></td> <td>.026</td> <td></td> <td></td> <td></td> <td>. 997</td> <td>7</td> <td></td>	2	4.0	147		•		-	1	600		-		.026				. 997	7	
1.0         1.6         1.7 <th></th> <td>8.2</td> <td>24.</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>. 663</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>•</td> <td></td> <td>. 961</td> <td></td> <td>. 689</td>		8.2	24.						. 663						•		. 961		. 689
8.0         140         -4.0         -6.00         -4.0         -6.00         -4.0         -6.00         -4.0         -6.00         -6.0         <			176				.628	ĸ.	600.		7	•	. 689-11	,			. 986	6.3	110
9.2         10.0         1.0 <th>=</th> <td>•</td> <td><b>?</b> :</td> <td></td> <td>•</td> <td></td> <td>•</td> <td>ı</td> <td>. 667</td> <td></td> <td>•</td> <td>1</td> <td></td> <td></td> <td></td> <td></td> <td>929</td> <td>4.5</td> <td>.073</td>	=	•	<b>?</b> :		•		•	ı	. 667		•	1					929	4.5	.073
19.3         1189         2.8         .049         2.8         .049         2.8         .049         2.8         .049         2.8         .049         1.1         .019         5.1         .089         -1.7        039         .2         .089         -1.7        039         .2         .089         -1.7        039         .1         .089         -1.7        039         .1         .089         -1.7        039         .1         .089         -1.7        039         .089         -1.7        039         .089         -1.9         .089         -1.1        019         5.1         .089         -1.7        039         .099         -1.8        083         .0         .0        052        0<	124	7.6	<u>.</u>						. 623		•						4 6		
8.3 .145 7.9 .136 .4 .667 1.9 .633 .6 .616 1.1 .619 5.1 .689 -1.7636 .9 .9 .9 .9 .157	3	10.3	8			2.8			.049		- 6	6					.023		
9.9         .14         .3         .995 -2.3        949         -1.1        019         3.4         .959 -3.6        965        9        958         9.9        958         9.9        958         9.9        958         9.9        958         9.9        958         9.9        958         9.9        958         9.9        958         9.9        958         9.9        958         9.9        958         9.9        958         9.9        958         9.9        968        969 <th>•</th> <td>8.3</td> <td>•</td> <td>7.9</td> <td></td> <td>₹.</td> <td></td> <td></td> <td>.033</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>. 636</td> <td>œ.</td> <td>916</td>	•	8.3	•	7.9		₹.			.033								. 636	œ.	916
1.57 1.2 .021 1.0 .017 2.3 .046 3.2 .056 -3.3058 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.	3	•	<b>?</b>			r.		ı	.040		7	•			. 659		. 963	٦.	. 002
	3	•	.157				. 621	•	.017		<b>4</b>				.056	ı	. 958		9.00
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152 153 154 155 155 156 157 158 158 158 158 158 158 158 158 158 158		?!	791.						. 614		•				169.		9 t 6	o .	
162 1 1.2 1.3	2 5		141			? M			. 58. 58.		- 6						275	9 G	200
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1555669 5.1 .689 2.9 .651 -2.1637 -1.6628 2.6 .148 9.3 .162 2.1 .637 -7612 2.9 .651 0.0 0.066 2.2 .638 -4.8684 5.5 .185 .185 .4 .667 -3.3658 0.0 0.066 -1.6028 -5.2691 4.7 .185 .197 .2.2038 -3.2656 2.1 0.0 0.066 -2.0035 -1.3623 1.8 .195 .195 .196 .2038 -3.2656 3.1 .2 .669 -2.0035 -1.3665 3.1 .156 .18	57	+.0	<u>\$</u>			۲.			.014		4			ı			.045		. 686
. 145 9.3 . 162 2.1 637 7 612 2.9 651 0.0 0.060 2.2 638 -4.8 684 5.5 . 185	\$	8.8	. <u>1</u> 55						. 689		4		•	ı			. 028	<b>5.6</b>	.045
. 185 4	\$	8.5	 84 	9.3		2.1		ţ		2.9	.051	9.0					. 884	5.5	960.
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8 .171   1.6 .025   1.1 .019   0.0 0.000   6.2   .105   4.4   .077   5.5	3	۵ ( ا	<u> </u>			<b>»</b> (			109.		•		369.				.663	::	5 6
8 .154		D (	<u> </u>						81 <b>8</b> .		<b>9</b>		1 999:	•			//0:		080
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7.5 13.5 - 1.0 - 1	2 :	• •			1							ŀ	110.				774	) <b>~</b>	120
		?	701.						++0.							i c		•	67.0

Fig.   May   D   TO   MIRE SIDE   LUGG   SSEED   FIG.			3	LANDING BATA -	_	NODEL	E-20		uss i	2	RPR 15	USS ENTERPRISE (CWN-65)	N-65)			•	۲ خ	DAY LANDINGS				
Fig.	8	Ş	BATER	2	57 57	WIRE	SIDE		3	돐	٩	DECK	PITCH	DECK	ROLL	16	9	BAROME	TRIC	AR	GEAR.	REREAD
Fig.   Name   Color		<b>DIST</b>	<b>ACE</b>	DIST	ANCE	€.		TYPE	80E	8	83							PRESS	URE	\$	STUC	NUMBER
44         65         66         67         68         76         71         72         73         74         75         76         77         76         77         78         76<		t	*	t	3					\$	K/S	DEG	8	DEG	3	la.		IN HG	¥ ¥	Z	3	
2 210         64         1         4 50100         4 2   <		3	3	2	3	67	2	2	70	7	72	22	74	72	92	11	78	79	88	5	82	
24         84         3 346         56126         12         6         -1         -083         -2         -083         67         19         96         75         18         76         18         76         18         76         18         76         75         18         76         75         18         76         18         76         18         76         76         18         76         76         18         76		*	1	210	Z	-	*	56166		*	8	89.	669	4.1	.007	99	5	30.06	763.5	9	9.	-
-3 280 73 344 7020 12 6 -1 -002 17 19 30 02 762.5 0 1   -2 284 87 3 347 7020 12 6 -1 -002 17 19 30 02 772.5 0   -2 284 87 3 347 7020 12 6 -1 -002 14 19 2   -2 284 87 3 347 7010 12 6 -1 -002 14 19 2   -2 284 73 7010 12 6 -1 -002 14 19 2   -2 284 73 7010 12 6 -1 -002 14 19 2   -2 284 73 7010 12 6 -1 -002 14 19 2   -2 284 73 7010 12 6 -1 -002 14 19 2   -2 284 73 7010 12 6 -1 -002 14 19 2   -2 285 77   -2 287 78 3 346 7010 12 6 -1 -002 14 19 2   -2 287 78 3 346 7010 12 6 -1 -002 14 19 2   -2 287 78 3 346 7010 12 6 -1 -002 14 19 2   -2 287 78 3 346 7010 12 6 -1 -002 14 19 2   -2 287 78 3 346 7010 12 6 -1 -002 14 19 2   -2 287 78 3 346 7010 12 6 -1 -002 19 2   -2 287 78 3 346 7010 12 6 -1 -002 19 2   -2 287 78 3 347 7010 12 6 -1 -002 19 2   -2 287 78 3 348 7010 14 17 -1 -021 10 10 10 10 10 10 10 10 10 10 10 10 10		9	?	274	3	n	3	50120		12	•	7	.003	2	. 993	29	19	30.02	762.5	-	126.7	-
-3 229 78 344 78289 12 6 -3 -065 16 17 19 30-02 782.5 0 -2 284 17 19 30-02 782.5 0 -2 284 17 19 30-02 782.5 0 -2 284 17 19 30-02 782.5 0 -2 284 17 19 30-02 782.5 0 -2 284 17 19 30-02 782.5 0 -2 284 17 19 30-02 782.5 0 -2 284 17 19 30-02 782.5 0 -2 284 17 19 30-02 782.5 0 -2 284 17 19 10-02 14 -024 17 19 30-02 782.5 0 -2 284 17 19 10-02 14 -024 17 19 30-02 782.5 0 -2 284 17 19 10-02 14 -024 17 19 30-02 782.5 10 -2 284 17 19 10-02 14 -024 17 19 30-02 782.5 10 -2 284 17 19 10-02 14 -024 17 19 30-02 782.5 10 -2 284 17 19 10-02 14 -024 17 19 30-02 782.5 10 -2 284 18 10-02 14 17 10-02 14 -024 17 19 30-02 782.5 10 -2 284 17 19 10-02 14 17 10-02 14 -024 17 19 30-02 782.5 10 -2 284 17 19 10-02 14 17 10-02 14 -024 17 19 30-02 782.5 10 -2 284 17 19 30-02 14 17 10-02 14		7	?	266	2		3	70120		72	•	-:	002	1.7	. 030	29	<del>5</del>	30.02	762.5	•	9.9	•
-2 284	•	<u>=</u> '	7	228	2		3	78286		2	•	ا. د	995	é.	919	67	6 :	30.02	762.5	<b>6</b>	9.0	•
2. 25.3         77         3.34         72.00         1.5         6.1         6.00         1.5         6.1         6.00         1.5         6.1         1.00         1.0		7 "	7 (		2	•	3	78188		2 5			. 98.	- 4	. 662	2 6	2 9	38.82	762.5	•	9.9	•
25         355         99         344         7020         12         6-1         -002         1.4         -024         67         19         30.02         762.5         9           258         79         344         7020         12         6-1         -002         -1.4         -004         67         19         30.02         762.5         6           258         79         344         5010         12         6-1         -002         -1.4         67         19         30.02         762.5         6           257         78         30         344         5010         11         60.0         67         19         30.02         762.5         16           257         78         344         5010         14         7-4         -004         -1.2         -021         60         70         20 <th< td=""><td></td><td>P <b>4</b>7</td><td>7 ?</td><td>5 5</td><td>76</td><td>3</td><td>Š</td><td>70200</td><td></td><td>7 2</td><td>o <b>«</b></td><td>- <b>«</b></td><td>799.</td><td>P ~</td><td>90.5</td><td>67</td><td>2 0</td><td>30.02</td><td>762.5</td><td>8</td><td>0.07</td><td></td></th<>		P <b>4</b> 7	7 ?	5 5	76	3	Š	70200		7 2	o <b>«</b>	- <b>«</b>	799.	P ~	90.5	67	2 0	30.02	762.5	8	0.07	
256         79         341         70100         12         6 - 1         - 002         - 1, 4 - 024         67         19         30.02         762.55         18.9           -3         259         79         3,44         50100         12         6 - 15         - 009         - 1, 4 - 004         67         19         30.02         762.55         18.9           -3         259         79         3,44         50100         12         6 - 1, 5 - 003         - 1, 6 - 004         67         19         30.02         762.55         18.9           -2         23         78         3,44         50100         14         7 - 0.         0.00         70         21         30.02         762.51         18.9           -2         23         78         50100         14         7 - 0.         0.00         70         21         30.02         76.25         18.9         76.25         18.9           -2         23         77         341         50100         14         7 - 2         -003         70         21         30.02         76.25         18.9           -2         24         77         24         26         70         21         30.02		7	7	325	: 2		3	78286		2	•	- 6	002		.024	6	6	30.02	762.5	•	0.0	~
-3         259         79         3         3.06         50100         12         6         -3         -0.09         -4         -0.07         19         30.02         762.5         169           -3         254         90         4         344         50100         12         6         -1         -0.05         -1         -0.05         -1         -0.1         -0.1         -0.1         -0.1         -0.1         -0.1         -0.1         -0.1         -0.1         -0.1         -0.1         -0.1         -0.1         -0.1         -0.1         -0.1         -0.1         -0.2         -0.1         -0.2         -0.2         -0.1         -0.2		51.	†	258	2		7	70100		7	•	7	002	_	. 024	67	0	30.02	762.5	•	0.0	•
-3 224 99 4 344 55190 12 6 .1 .002 0.0 0.00 67 19 30.02 762.5 189 -2 258 89 342 70120 12 6 1005 -0.03 70 19 30.02 762.5 189 -2 2313 95 344 50120 14 74007 -1.2021 70 21 30.02 762.5 189 -2 231 95 344 50100 14 71002 -1.02 70 21 30.02 762.5 169 -2 231 95 344 50100 14 71002 1.4 .024 70 21 30.02 762.5 169 -1 234 71 2 344 50100 14 71002 1.4 .024 70 21 30.02 762.5 169 -1 234 71 2 344 50100 14 71002 1.4 .024 70 21 30.02 762.5 169 -1 234 71 2 344 50100 14 71002 1.4 .024 70 21 30.02 762.5 169 -1 234 71 2 344 50100 14 71002 1.4 .024 70 21 30.02 762.5 169 -1 234 71 2 344 50100 14 71002 1.4 .024 70 21 30.02 762.5 169 -1 234 71 2 344 50100 14 71002 1.4 .024 70 21 30.02 762.5 169 -1 234 71 2 344 50100 14 71002 1.4 .024 70 21 30.02 762.5 169 -1 234 71 2 344 50100 14 71002 1.4 .024 70 21 30.02 762.5 169 -1 234 71 2 344 50100 14 71002 1.4 .024 70 21 30.02 762.5 169 -1 234 71 2 344 50100 14 71002 1.4 .024 70 21 30.02 762.5 169 -1 234 71 2 344 50100 14 71002 1.4 .024 70 21 30.02 762.5 169 -1 234 71 2 344 50100 14 71002 1.4 .004 70 21 30.02 762.5 169 -1 234 71 2 344 50100 14 71002 1.4 .004 70 21 30.02 762.5 169 -1 234 71 2 344 50100 14 71002 1.4 .004 70 21 30.02 762.5 169 -1 234 71 2 344 50100 14 71002 1.4 .004 70 21 30.02 762.5 169 -1 234 71 2 344 50100 14 71002 1.4 .004 70 21 30.02 762.5 169 -1 234 71 2 344 50100 14 71002 1.4 .004 70 21 30.02 762.5 169 -1 234 71 2 344 50100 14 71002 1.4 .004 70 21 30.02 762.5 169 -1 234 71 2 344 50100 14 71002 1.4 .004 70 21 30.02 762.5 169 -1 234 71 2 344 50100 14 71002 1.4 .004 70 21 30.02 762.5 169 -1 234 71 2 344 50200 14 71002 1.4 .004 70 21 30.02 762.5 169 -1 234 71 2 344 50200 14 71002 1.1 .002 70 21 30.02 762.5 169 -1 234 71 2 344 50200 14 71002 1.1 .002 70 21 30.02 762.5 169 -1 234 71 2 344 50200 14 71002 1.1 .002 70 21 30.02 762.5 169 -1 234 71 2 344 50200 14 7 71002 1.1 .002 70 21 30.02 762.5 169 -1 234 71 2 344 50		9	?	259	2	n	336	50100		7	•	5.1	999	_	.007	67	19	39.92	762.5	•	129.3	•
-6         228         69         342         78120         12         63         -865        6        6         14         7 0.0        6        6         14         3 0.0         762.5         16           -3         313         36120         14         7 0.0        6        6         13         20         27.5         18           -3         274         84         341         58120         14         71        602         71         21         30.02         762.5         169           -2         251         37         341         58120         14         72         -603         14         .024         70         21         30.02         762.5         169           -1         234         5100         14         72         -603         14         .024         70         21         30.02         762.5         169           -1         234         5100         14         72         -603         14         72         -605         14         72         -605         14         72         -605         14         72         -605         14         72         -605		<u>•</u>	?	294	2	*	ž	50100		12	•	-	. 662		. 909	67	19	30.02	762.5		129.3	•
2         257         78         3 346         59126         14         7         0.0         0.000         -13         -023         76         21         30.02         762.5         168           -2         213         85         3.41         50120         14         7         -1         -002         76         21         30.02         762.5         169           -2         234         50120         14         7         -2         -003         14         024         76         21         30.02         762.5         169           -2         266         63         2         344         50100         14         7         -2         -003         14         002         76.2         169           -1         234         50100         14         7         -2         -005         76         21         30.02         762.5         168           -3         246         75         5         -005         14         7         -2         -005         76         21         30.02         762.5         168           -3         246         35         34         50100         14         7         -1		-19	۴	228	8		342	70120		12	•	D. 1	865		.014	67	<b>6</b>	30.02	762.5		9.0	-
-2         313         95         342         70120         14         7         -4         -007         -1         -021         70         21         30         22         762.5         169           -2         274         84         50100         14         7         -1         -002         -1         -024         70         21         30         22         762.5         169           -2         206         63         2         342         50200         14         7         -1         -002         70         21         30         2         762.5         169           -1         234         77         344         50100         14         7         -2         -005         11         024         70         21         30         2         30         20         762.5         168           -1         234         50100         14         7         -1         -005         11         02         21         30         2         30         2         30         2         30         2         30         2         30         2         30         2         30         2         30         2		4	7	257	78	n	326	59129		<b>±</b>	7	9.0	9.99		.023	9	7	30.02	762.5	-	129.3	_
-3         274         844         3 341         58186         14         7         -1         -802         -1         -802         76         21         39-82         762.5         168           -2         251         77         341         58186         14         7         -2         -803         14         -824         76         21         39-82         762.5         168           -1         234         71         2         344         56186         14         7         -2         -865         76         21         39-82         762.5         169           -3         245         75         346         56186         14         7         -3         -865         76         21         30-82         762.5         169           -3         246         347         56186         14         7         -3         -865         76         21         30-82         762.5         167           -3         246         347         56186         14         7         -1         -862         -1         30-82         762.5         167           -3         248         347         56186         14		7	7	27	<b>S</b>	1	342	70120		<b>±</b>	<b>~</b>	<b>+</b> ·	007		. 021	9	21	30.02	762.5		0.	•
251         77         3 341         30120         14         7         2         1403         14         1024         70         21         30:02         70:25         160           1         234         71         2         342         30120         14         7         2         -003         14         02         70         21         30:02         70:25         160           3         245         75         345         30100         14         7         -0         03         10         21         30:02         70:25         163           -3         276         84         3 341         30100         14         7         -1         -005         -1         00         70         21         30:02         70:25         167           -3         276         84         3 341         30200         14         7         -1         -002         -1         00         20	1	•	7	274	3 !	י מ	7	50100		<b>±</b> ;	<b>~</b> (	- (	002		.002	<b>6</b> 5	7	30.02	762.5	-	129.3	•
- 2 256		ę.	7 0	25	:3	n (	<del>,</del> ;	58128		<b>:</b> :	<b>~</b> 1		993 505	* •	.024	9 9	5 5	39.62	762.5	-	7.921	<b>9</b> 6
-3         245         75         3 336         59196         14         7         -3         -695         3 965         70         21         30         27         762.5         167           -3         245         75         3 336         59196         14         7         -4         -697         1.1         1619         76         21         30.02         762.5         162           -3         276         84         3 34         56206         14         7         -1         -602         -3         -665         70         21         30.02         762.5         163           -5         194         59         4         344         50106         14         7         -1         -602         -1         -003         70         21         30.02         762.5         167           -2         291         69         4         344         50106         14         7         -1         -002         -1         -002         70         21         30.02         762.5         167           -2         20         60         70         1         70         20         30         21         30         22		P 7	<b>Y</b> 7	<b>8</b> 2	3 5	<b>,</b>	3	2070C		: :	- 1	<b>7</b> F	5 4	<u>.</u>	500	9 6	- c	30.02	762.5		7.00	•
-3         276         84         3 341         5626         14         7         -4         -607         1.1         1619         76         21         30.62         762.5         162           -3         276         84         3 341         5626         14         7         -1         -602         .3         -665         76         21         30.62         762.5         167           -5         184         56         24         50100         14         7         -1         -602         -5         -609         76         21         30.62         762.5         167           -3         201         60         4         34         50100         14         7         -1         -602         -5         -609         76         21         30.62         762.5         167           -3         201         60         60         60         60         60         76         21         30.62         762.5         168           -4         210         67         76         60         60         60         76         76         21         30.62         762.5         168           -4         210	•	7	- <b>"</b> ?	245	: 22	4 17		Se : es		<u> </u>	. ~		1,000	- 17	995	2 2	3 2	30.02	762.5		124.2	• •
-3         278         85         337         70100         14         7         -1         -002         .3         .005         76         21         30.02         762.5         167           -5         184         58         337         70100         14         7         -1         -002         -1         003         76         21         30.02         762.5         167           -3         276         84         334         50100         14         7         -1         -002         -1.5         -009         76         21         30.02         762.5         167           -3         271         67         23         50100         14         7         -1         -002         -1.5         -009         76         21         30.02         762.5         167           -4         213         85         344         60200         14         7         -1         -002         -1.5         -003         21         30.02         762.5         168           -4         213         85         344         60200         14         7         -1         -002         -1.5         -003         762.5         168 <td>ı</td> <td>· =</td> <td>7</td> <td>276</td> <td>3</td> <td>· 17</td> <td>7</td> <td>50200</td> <td></td> <td><b>±</b></td> <td>. ~</td> <td>+</td> <td>007</td> <td>: -</td> <td>919</td> <td>2</td> <td>; <del>7</del></td> <td>39.92</td> <td>762.5</td> <td></td> <td>126.7</td> <td>•</td>	ı	· =	7	276	3	· 17	7	50200		<b>±</b>	. ~	+	007	: -	919	2	; <del>7</del>	39.92	762.5		126.7	•
-5         194         59         2         342         5620         14         7         -1         -662         1.4         0.64         70         21         30.02         762.5         167           -3         276         64         334         59100         14         7         -1         -662         -5         -696         70         21         30.02         762.5         167           -3         291         80         4         344         59100         14         7         -1         -692         -5         -693         16         0.24         70         21         30.02         762.5         167           -2         229         70         2         344         59200         14         7         -693         2.5         -644         70         21         30.02         762.5         168           -4         219         67         2         347         59100         14         7         -693         -693         70         21         30.02         762.5         168           -4         219         67         67         690         690         10         690         10         70	1	=	7	278	2		32	70100		=	~	-	002	'n	.005	70	7	39.92	762.5		<b>.</b>	•
-3         276         64         337         78100         14         7         -1         -002         1.4         024         70         21         30.02         762.5         167           -3         291         89         4         344         50100         14         7         -1         -002         -5         -009         70         21         30.02         762.5         167           -2         229         70         2         344         50200         14         7         -6         -603         21         30.02         762.5         168           -4         219         65         2         344         60200         14         7         -6         600         19         21         30.02         762.5         168           -4         219         65         600         10         600         10         600         10         21         30.02         762.5         168           -5         240         7         6         600         10         600         70         21         30.02         762.5         168           -6         341         500         14         7         <	1	2	ę	184	8	7	342	58288		<b>±</b>	1	ا. د	005	1.5	. 969	70	7	30.02	762.5	-	124.2	_
-3         291         89         4         344         50100         14         7         -1         -002        5         -009         70         21         30,02         762.5         167           -3         221         67         2         337         56200         14         7        6        603         2.5        644         70         21         30,02         762.5         168           -4         219         67         2         344         56100         14         7        6         0.605         19         0.605         70         21         30,02         762.5         168           -4         219         67         2         345         56100         14         7        6         0.606         1.9        607         70         21         30,02         762.5         168           -2         243         74         3         341         56100         14         7        6         0.606         -1.8         -031         70         21         30.02         762.5         168           -4         240         73         56200         14         7        2 <t< td=""><td>ı</td><td>•</td><td>7</td><td>276</td><td>3</td><td></td><td>3</td><td>79196</td><td></td><td><b>±</b></td><td>~</td><td>-</td><td>002</td><td><b>→</b>:</td><td>.024</td><td>9</td><td>5</td><td>30.02</td><td>762.5</td><td></td><td>0.0</td><td>•</td></t<>	ı	•	7	276	3		3	79196		<b>±</b>	~	-	002	<b>→</b> :	.024	9	5	30.02	762.5		0.0	•
3         221         67         2         337         59280         14         7        6963         1.6         .928         79         2         344         59280         14         7        693         2.5         .044         70         2         344         602.5         16         7        695         2.5         .044         70         2         344         602.5         16         7        695         16         17         0.0         17         0.0         0.00         1.6         1.7         0.0         0.00         1.8         0.31         70         21         30.02         762.5         162           -2         229         70         2         345         50100         14         7           17         2         100         100         100          100	•	•	7	2	8	•	3	50		<b>±</b>	_	- 1	992		600	9 1	5	30.02	762.5	-	24.2	•
-2         2.29         78         2.34         60200         14         7         -3         -605         7         2.3         -607         7         2.3         -607         7         2.3         -605         7         2.3         -605         7         -605         -7         -605         -7         -605         -7         -7         -7         -606         -7         -605         -7         -7         -7         -7         -606         -7         -7         -7         -7         -7         -606         -7	ı	<u>.</u>	? '	22	6	~ •	3	28288		<b>*</b> :	۱ م	ر ا	600.	- (	.028	2 5	2 5	39.92	762.5		7.92.	<b>.</b>
-4         219         67         2         342         56100         14         7         0.0         0.000         1.9         0.33         70         21         30.02         762.5         168           -2         243         74         3         341         50100         14         7         -4         -007         1.8         0.31         70         21         30.02         762.5         168           -4         240         73         2         337         50100         14         7         -6.00         -1.8         -031         70         21         30.02         762.5         168           -4         240         73         2         337         50100         14         7        2        005         .7         .012         70         21         30.02         762.5         168           -4         280         86         4         342         50100         14         7        1        002         .2         .003         762.5         168           -4         271         83         34         50100         14         7        1        002         .1        003		) <u>"</u>	7 1		<b>.</b>	4	3	2070E		: :	- 1	y r			64.4	2 5	3 5	30.02	782.5			4 <b>C</b>
-3         244         74         3         341         56166         14         7         -4         -607         1.8         .631         70         21         30.02         762.5         168           -2         229         76         237         56166         14         7         -6.66         -1.8         -631         70         21         30.02         762.5         168           -4         246         73         2         337         56166         14         7        2        665         .7         .012         70         21         30.02         762.5         168           -4         286         86         4         342         56166         14         7        2        665         .2         .063         70         21         30.02         762.5         168           -4         271         83         3         344         56166         14         7        1        062         .2         .063         70         21         30.02         762.5         168           -3         286         86         4         344         56206         14         7        5        0	- 1	1	1	218	6	8	342	50100		<b>_</b>		0.0	999	-	.033	70	7	39.92	762.5	-	124.2	•
-2         229         70         2         337         50100         14         7         0.00         -1.8         -0.31         70         21         30.02         762.5         168           -4         240         73         2         337         50200         14         7         005           1         7         005           1         30.02         762.5         167          167         005           30.02         762.5         167          167         005         007         70         21         30.02         762.5         167          167  <		•	7	245	7	n	77	50100		*	~	+	007		.031	70	7	30.02	762.5	•	128.7	•
4         246         73         2         337         5626         14         7		ņ	7	229	2	8	23	<b>3618</b>		<b>±</b>	7	9.0	0.000		.031	70	21	30.02	762.5	-	126.7	~
4         289         86         4         342         50100         14         7        2        003        4        007         70         21         30.02         762.5         166           -1         294         90         341         70100         14         7        1        002        2         .003         70         21         30.02         762.5         167           -3         286         68         4         341         50200         14         7        1        002        3        005         70         21         30.02         762.5         168           -3         275         64         4         342         50200         14         7        1        002         .1         .002         70         21         30.02         762.5         168           -5         246         75         2         337         50200         14         7        2        003         .3         .002         70         21         30.02         762.5         168           -4         243         74         50200         14         7        2        003	1	5	†	248	2	N	23	58288		<b>±</b>	7	ا. د	005		.012	70	7	39.62	762.5		124.2	•
-1 294 96 341 70100 14 710022 .003 70 21 30.02 762.5 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	•	<b>*</b>	†	288	2	*	345	56166		<b>±</b>	7	2	003	١	.007	70	7	30.02	762.5		121.6	•
-4     271     83     344     58186     14     7     -1    082    3    085     70     21     30.82     762.5     167       -3     288     85     4     341     58286     14     7    3    085     .1     .082     70     21     30.82     762.5     168       -3     275     84     4     342     58286     14     7    1    082     .1     .082     70     21     30.82     762.5     168       -4     245     74     2     344     58286     14     7    2    803     .3     .085     70     21     30.92     762.5     169       -3     318     97     342     68186     14     7     .2     .803    6    016     70     21     30.92     762.5     8		?	T	<b>787</b>	2		7	70100		<b>±</b>	^	-	002		. 003	70	21	30.02	762.5		0.0	•
-3     286     88     4     341     50200     14     7    3    065     .1     .002     70     21     30.02     762.5     166       -3     275     84     4     342     50200     14     7    1    062     .1     .002     70     21     30.02     762.5     168       -5     246     75     2     337     50200     14     7    5    069     1.4     .024     70     21     30.02     762.5     169       -4     243     74     2     344     50200     14     7    2    063     .3     .005     70     21     30.02     762.5     169       -3     318     97     342     60100     14     7     .2     .063    6    010     70     21     30.02     762.5     9	•	51.	†	172	3	n	344	50106		<b>±</b>	7	-	002	1.3	. 905	70	71	30.02	762.5		124.2	~
-3 275 84 4 342 58286 14 71882 .1 .882 78 21 38.82 762.5 168   -5 246 75 2 337 58286 14 75889 1.4 .824 78 21 38.82 762.5 168   -4 243 74 2 344 58286 14 72883 .3 .885 78 21 38.82 762.5 169   -3 318 97 342 68188 14 7 .2 .8836818 78 21 38.82 762.5 8	ı	÷	7	288	20	*	3	<b>20200</b>		<b>±</b>	7	L. J	005		. 002	70	21	30.02	762.5	-	121.6	•
-5 246 75 2 337 50200 14 75009 1.4 .024 70 21 30.02 762.5 166 -4 243 74 2 344 50200 14 72003 .3 .005 70 21 30.02 762.5 169 -5 318 97 342 60100 14 7 .2 .0036010 70 21 30.02 762.5 0		•	7	275	2	*	342	28286		<b>±</b>	^	-	002	Ξ.	. 002	70	21	30.02	762.5	-	121.6	-
-4 243 74 2 344 50200 14 72803 .3 .805 70 21 30.02 762.5 169 -3 318 97 342 60100 14 7 .2 .0036010 70 21 30.02 762.5 0	ı	5	Ŷ	246	22	~	337	20200		<b>±</b>	7	ا ب	009	4.	. 024	9	7	39.92	762.5	-	121.6	•
-3 318 97 342 60160 14 7 .2 .6036010 70 21 30.02 762.5 0		12	†	243	7	8	446	<b>26566</b>		<b>+</b>	^	2	003	ı.	. 993	92	7	39.92	762.5		129.3	•
		e î	7	318	97		342	69166		<b>±</b>	7	7	. 003	9.1	.010	92	7	30.62	762.5		•	•

REREAD	NUMBER			•	•	•	•	•	-	-	•	_	•	-	•	-	-		-	•	7	-	-	•	-	7	-	•	-	•	-	-	•		-	•	•		•	•	-	. <b>_</b>
Ž	ПS	₹	82	131.8	126.7	426.7	6.7	129.3	126.7	126.7	129.3	21.6	128.7	424.2	126.7	129.3	126.7	129.3	124.2	126.7	126.7	431.8	124.2	129.3	126.7	129.3	129.3	129.3	126.7	129.3	124.2	126.7	424.2	126.7	126.7	126.7	424.2	424.2	126.7	129.3	129.3	129.3
ARR GEAR	RUNOUTS	Z	<b>.</b>	70 43	54	68 42	68 42	69 42	68 42	•	•	•	•	•	•	•	•	69 42	•	68 42	68 42	70 43	67 42	69 42	68 42	69 42	69 42	59 42	•	•	•	•	67,42	•	68 42	68 42	67 42	67 42	-	•	•	•
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BAROMETRIC	PRESSURE	¥ ¥	8	761.	761.	761.7	761.	761.	761.	761.	761.	761.2	761.2	761.2	769.7	769.7	769.7	769.7	769.7	769.7	769.7	769.7	769.7	769.7	769.7	769.7	769.7	760.7	769.7	769.7	769.7	769.7	769.7	769.7	769.7	769.7	769.7	769.7	769.7	769.7	769.7	761.
BARO	PRES	H H	78	29.99	29.99	29.99	29.89	29.88	29.99	29.99	29.97	29.97	29.97	29.97	29.92	29.92	29.92	29.95	29.92	29.95	29.95	29.95	29.92	29.95	29.95	29.92	29.95	29.92	29.95	29.92	29.95	29.92	29.82	29.95	29.95	29.95	29.95	29.95	29.95	29.95	29.95	29.99
TDAP		ပ	78	23	23	23	2	23	23	2	7	7	7	5	77	22	22	22	22	22	22	22	22	22	22	22	22	22	22	22	22	22	22	22	22	22	22	22	22	77	22	12
F		•	11	2	2	2	2	73	2	2	92	69	69	69	7	7	7	7	7	7	7	7	7	7	7	7	7	7	Ξ	7	7	71	7	7	7	7	7	7	7	7	7	2
POLL		3	76	019	. 669	016	. 669	916.	88.		- 969	010	012	010	. 007	.007	. 669	. 005	. 005	002	. 667	. 003	005	662	9.99	9.66	. 992	863	662	9.666	. 662	B. 999	. 002	. 005	002	9.99	9.99	9.000	.003	.002	992	.007
DECK ROLL		DEG	75		'n	- 6	'n	œ,	j	'n	. 5.	- 9 -		9.1	₹.		ņ	'n	r.		₹.	7	- 5.1	•	9.9		_	2 -		9.9	Ξ.	7.00		ņ		9.9		9.9	~	-	-	*
10H		<b>8</b>	74	- 605	005	002	005	005	9.66	967	995	003			9.00	963	900.	9.999	9.99	. 993	002	. 003	0.000	. 002	0.000	005	.005	992	900.	600.	002	967	003	.003	002	010	993	002	999.	. 002	993	.002
DECK PITCH		DEC	22	_	L)	·	i	i	6	í +	i n		i D	i D	6	i i	•		6		i -		9		•	'n		i -	6		_	i +	1		i	9		, ,	6	_		· ·
30				•	i	i -	i	i	•	i	i	1	i	i	•	i	6	•	•	_	i	•••	•	•	6	i	_	i	•	-; -	i	i	i -	-	i	•	1	i	6		_	i
SEE	SPEED	S/N T	72	~	~	~	_	•	•	•	~	~	~	•	=	=	=	5	5	- 1	10	=	- 10	10	=	5	5	- 19	=	=	5	=	=	=	=	=	-	19	5	10	19	, <b>6</b> 0
2	3000	\$	17 97	¥	ï	=	-	Ξ	_	_	=	=	ï	=	22	7	7	7	*	7	ñ	20	20	*	7	Ä	8	Ä	<b>50</b>	*	6	=	~	~	~	7	*	7	20	×	7	; <b>2</b>
				•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•		•	•	•	•	•	•	•	•	•	•	•	•	•	•	. 6
DON'T	TYPE		2	50100	59198	50120	50200	2000 S	50100	50120	2020	50120	50120	50120	<b>20200</b>	26168	50120	56266	20.02	50120	50200	58286	80120	50120	58288	59120	59129	5620	56128	56128	50200	59120	80200	56126	56266	50100	50120	50200	50100	50100	50200	50120
3018	Š		2	ž	ጀ	3	ž	3	342	2	ž	Ĭ	Ž	ž	3	ž	3	ij	2	35	¥	3	ž	33	342	3	ጀ	3	342	3	ž	Ī	ž	7	ž	2	23	3	¥	345	337	Ħ
WIRE	Š		67	n	~	~	7	N	"	~	4	2	~	N	~	n	n	N	n	8	~	n	~	n	~	~	~	~	~	~	N	N	N	n	~	N	n	n	~	~	8	18
6	3	3	2	2	=	=	2	*	82	22	2	2	8	22	2	74	3	23	z	2	7	82	2	8	67	3	2	22	7	*	57	3	82	3	74	89	1	8	3	2	2	8
RAME TO TO	DISTANCE	-	3	n	80	~	•	~	•	50	•	<b>+</b>	_	•	•	n	7	•	•	_	~	•	_	n	_	•	7	•	~	n	•	n	_	_	•	•	8	~	•	_	4	. a
		E	•	<b>36</b>	26	<b>5</b> 6	28	7	28	23	27	<b>5</b> 8	<b>78</b>	27	26	ž	27	23	23	7	23	2	7	28	22	9	5	17	2	ž	₽	16	22	27	<b>*</b>	22	25	26	2	23	28	179
OFF-CENTER	DISTANCE	3	3	1	1	?	-2	?	?	?	7	ę	?	7	7	ņ	?	7	ņ	7	1	ş	7	?	?	7	Ŷ	1	9	7	1	ę	?	7	1	7	1	7	ş	1	1	ΨŶ
Q T	910	E	3	-12	-12	9	7	7	7	• •	F	-15	Ŧ	7	7	-17	7	19	<u>-</u>	-13	-12	13	ę	?	<b>e</b>	-12	<b>9</b> 1	-12	<del>-</del> 1	7	13	18	<b>•</b>	7	-13	<del>-</del>	+	9	-12	+	113	10
200	ġ		2	2635	2038	2639	2040	ž	2042	2043	2117	2132	2141	2149	2371	2372	2376	2377	2378	2379	2380	2361	2363	2384	2365	2386	2387	2388	2389	2396	2391	2382	2393	2394	2396	2402	2404	2405	2406	2407	2468	4638

# E-2 NIGHT

VE-FILM  NN M/S NN  NN M/S NN  14 5 6  14 5 6  14 2 29  14 2 29  14 2 29  14 2 29  14 2 29  15 45 22  16 45 28  16 45 28  17 45 28  17 45 28  18 4	M/S M/S 7 7 7 111 115 115 115 115 115 115 115 1	EL	VEOR 10 11 11 11 11 11 11 11 11 11 11 11 11	VPAMIN KN M/S 12 13	* - **********	A	MIN 16	ν		FF 19	WEI LBS	WEIGHT
₹ a \$\$4±43\$\$		<b>5</b>					,	7. 1.23 1.23 1.23 1.23 1.23 1.24 1.34	8 8 8 6 6		LBS	ģ
₹ ° \$\$\$±\$\$\$							<del>5</del>	7 1 22 1 23 1 23 1 24 1 24 1 25 1 25 1 25 1 25 1 25 1 25 1 25 1 25	±	<del>6</del>	LBS	ÿ
n 22222322	~~~~~~~~				· · · · · · · · · · · · · · · · · · ·		<b>5</b>	7	£	9	20	!
\$\$4243\$\$	= 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5				8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8			222222222222222222222222222222222222222				23
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2	<u> </u>	80000000000000			8			222222222222222222222222222222222222222			43360	19668
<b>+ 4 3 <b>4 4 + 4</b></b>	<u> </u>				83 88 88 88 89 89 88			22 22 23 24 24 25 25 25 25 25 25 25 25 25 25 25 25 25	88. 86		45660	20711
234823	4 4 4 4 E 4				88 88 88 89 89 88			1.23 1.24 1.24 1.35 1.36	98. 1. 1. 98.		44568	20212
3 4 3 2 2	****				8 8 8 8 8 8 8 8			1.22 1.22 1.42 1.43 1.32	9		45868	20802
\$ \$ ± \$	* * * * *				8 8 8 8			1.22		i	40860	19695
\$ ± \$	<u> </u>				8 8 8 7 8			1.22	1.20	- 3 <del>0</del>	43060	19532
÷ 4	2 2				8 8	• • • •		1.24	 80 :	- 60	43760	19850
7	7	~~~~			88	•		1.24 1.38 1.32	- 00		44760	20303
!!	•				•	‡		1.36	96		45360	20575
<b>3</b> :	<b>*</b> :				88			1.38	<b>6</b> 6.		43360	19668
<b>\$</b>	<b>±</b> :				80	7		1.32	- 60		42660	19351
	2				87	45			<b>8</b> .	- 90	44369	20122
3 43 28	<b>*</b> ;				88	‡ :		1.29	 60 :		43560	19759
\$ ;	<b>*</b> !	- (			98	‡ :		 	1.10		43668	19804
29 47 29	2 ;	7 F			6	<b>\$</b> :		80. 1	8.		43950	19946
<b>;</b> 9	ŭ f	7 C			0 4	; ;		<u>.</u> .	- +	90	41860	1040
	2 #				8	7		75.			42760	19396
z	=	1			88	‡		1.12	1.00		43560	19759
96 46 28	<b>±</b>	2			88	‡		1.39	1.20		42560	19305
2	<b>*</b>	2			86	‡		1.22	1.00		43760	19850
87 45 28	<b>±</b>	1			85	‡		1.35	1.00		42360	19214
	<b>*</b>	2			82	‡		1.30	1.00		42760	19396
42	=	7			8	‡		1.20	<b>8</b> 6.		43160	19577
41	=	7			82	‡		1.34	1.30	1.30	41900	19006
95 49 21	_	7			88	‡		1.35	1.00		43360	19668
7	_	-			8	‡		1.24	96.		42400	19233
•	12	-			86	‡		1.18	8.		43160	19577
7	=	-			86	‡		1.21	1.00		43660	19864
7	12	7			87	45		1.23	96.		43960	19940
9 41 22	=	2 1			88	‡		1.18	1.00		43060	19532
3	=	2 1			86	‡		1.23	96		43860	19895
	0	2 1			86	‡		1.27	1.20		43660	19864
87 45 21	Ξ	2			86	‡		1.26	1.10		43260	19623
	Ξ	2 1			86	‡		1.26	1.00		43260	19623
5 44 22	=	2			86	‡		1.24	1.00		43660	19864
	12	7			85	‡		1.28	1.30		42460	19260
3 43 23	12	7			85	‡		1.25	1.30		42460	19260
8 40 23	_				80	1		1 20	9		42050	19078

WEIGHT		ă	21	19033	19532	19895	19668	18489	19864	19351	19351	19577	19441	19033	19033	19305	19214	19124	18942	19895	19895	19864	19759	21165	19668	19713	20984	19169	19351	19441	20167	19532	19169	19396	18897	19895	19214	19487	18988	19668	19351	20621	19532
AE.		<b>18</b>	<b>50</b>	41960	43968	43860	43360	40760	43660	42660	42660	43160	42860	41960	41960	42560	42360	42160	41760	43860	43860	43660	43560	46660	43360	43460	46260	42260	42660	42860	44469	43969	42269	42760	41660	43860	42360	42960	41860	43360	42660	45460	43060
LIFT	<b>1</b> 1		19																		1.00																						
LIFT	2		8	88.	1.20	1.00	<b>9</b> 5.	1.20	1.10	96	96.	96	1.00	86.	1.10	. 99	1.00	- - -	1.00	1.10	1.00	- 96.	1.30	96.	1.20	96.	1.29	1.00	1.20	<b>8</b>	95	1.19	1.10	1.60	<b>8</b> 6.	1.10	1.00	1.10	1.00	1.20	1.00	96.	96.
\$	<b>∀</b> %		11	1.25	1.28	1.15	1.19	1.27	1.31	1.19	1.32	1.24	1.23	1.28	- 18	1.25	1.24	1.26	1.29	1.27	1.21	1.25	1.20	1.12	1.25	1.16	1.28	1.29	1.26	1.26	1.25	.38	1.28	1.27	1.22	1.30	<del>-</del>	1.22	1.23	1.29	1.33	1.19	1.16
KWPA	Z		9																																								
V.dSA		R/S	5	‡	‡	‡	‡	<b>\$</b>	‡	‡	‡	‡	‡	‡	‡ :	‡	‡	‡	43	‡	‡	‡	‡	46	‡	‡	46	‡	‡	<b>‡</b> !	<b>.</b>	‡	‡	‡	<b>.</b>	‡	‡	‡	4	ŧ	‡	5	‡
Š		ž	<b>±</b>	85	96	98	86	83	86	82	82	86	86	82	92	82	82	82	84	86	86	86	86	83	86	86	83	8	8	98	84	8	82	82	84	98	82	86	8	86	82	88	86
VPAMIN		M/S	13																																								
>		Ž	12																																								
VEOR		K/S	=																																								
		Ž	9																																								
	PERP.	N/S	•	-	-	-	-	-	-	-	•	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	<b>-</b> -	-	_	-	-	<b>,</b>	-	-	-	-
WIND-VEL	•	\$	40	~	7	~	7	7	~	7	8	7	~	~	N (	7	a	~	7	7	7	~	8	7	7	~	7	~	~	~	N	N .	~	~	7	~	~	7	7	~	7	~	8
*I	₽.	¥	7	12	5	12	•	7	_	7	12	7	2	7	2	7	_	_	_	_	_	7	Ξ	=	=	Ξ	=	=	=	= :		=	<del>-</del>	=	=	Ξ	Ξ	Ξ	=	=	=	=	=
		₹	•	23	26	23	₽	23	23	23	2	23	2	23	23	23	23	23	23	23	23	23	22	22	22	22	2	2	22	22	22	77	77	22	22	2	2	22	22	22	22	22	22
VE-FI UA		Ş	80	42	7	8	3	3	<b>\$</b>	7	\$	3	7	‡	3	?	3	Ç	‡	\$	42	‡	42	\$	‡	7	\$	\$	\$	‡ :	÷.	4	<b>4</b>	\$	42	41	2	4	42	9	47	4	6
V.		Ž	*	82	87	76	2	3	2	2	2	2	97		7	Ď	2	<b>*</b>	8	8	97	8	82	2	8	78	3	2	2	2	94		84	87	5	5	8	83	87	8	8	3	1
5	_	Ş	n	3	8	2	25	3	3	25	3	S	3	Š	5	9	S	50	8	21	ž	ş	3	જ	8	2	28	2	8	8	Š	2	<b>26</b>	8	3	3	62	\$	3	57	50	ž	2
VPAF	5	₹	~	50	168	8	102	106	=======================================	102	113	9	103	2	2	-	106	107	100	-	105	<u>5</u>	101	8	<u>5</u>	<b>8</b>	=======================================		107	107	2	=	<b>6</b>	109	100	112	120	105	101	=======================================	114	105	8
	9.		-	9996	9667	8669	9672	9673	9676	9696	500	9682	200	9683	900	960	8898	9696	9692	9693	9694	9695	8696	6696	9701	9702	9763	9766	9707	84/6	9718	9712	9713	2117	9718	9720	9721	9723	9724	9726	9727	9729	9730

NIGHT LANDINGS

USS ENTERPRISE (CVN-65)

LANDING DATA - MODEL E-20

	HOOK HEIGHT	OVER RAME	3	49																																
		8	<b>t</b>	39																																
DINGS	WHEEL HEIGHT	OVER RAMP	<b>⊼</b>	7 38																																
NIGHT LANDINGS		Ò	RAD FT	36 37	.039	.054	7967	9/9	. 671	.059	.073	.044	951	109.	.064	.059	. 083	.074	920	.054	.046	949.	.055	.050	. 656 649	.076	.054	.073	.033	.056	, t	288.	759	.011	.028	-
	HCLE AT	8	DEG	33	2.3		-	) <del>+</del>		4.0												5 K			5.6								0 -		•	9
	GLIDE PATH ANGLE AT TD	ŧ	8	*																																
(65)	GLIDE	<b>8</b> 4	DEG	33																																
USS ENTERPRISE (CVN-65)		FREE-FLIGHT	M/S	32					3.6	2.9				4.7				3.1						2.7												
ERPRIS		FREE-	F/S	2					11.7	ທ. ຜ			6	9.00				10.3						<b>6</b> 0												
uss ent	HDOM	AVG	K/S	8	1.9	2.5	5.6	3.5	3.5	9 .	. n	2.4	7.0	2.3 4.0	4.7 3.7	2.9	3.8	ю. С	6.7	2.7	2.0	2.5	2.5	9 :0	2.7	3.2	2.4	3.2	٠. دن	, v	7.7	2	. <del>.</del>		<b>+</b>	2.4
	AT TOUC	•	<b>F/S</b>	29	6.5	8.5	4.	11.5	11.6	0) 4 0) 0	10.8	7.9	10 G	7 0	10.4	9.6	12.5	6.6	7 17	8.8	9 1	):\ 	4.0	<b>6</b>	9.6	10.4	7.7	10.4	4.0	<b>6</b>	7.7	12.4	, e	2 2	4.	7.7
E-2C	SINKING SPEED AT TOUCHDOWN	STBO	S¥	28	E	2.6	9.6	0 Y	3.5		y	2.5	9.6	2.5	- n	2.8	3.9	2.7	2 .0	2.5	E (	 	2.1	2.4	2.1	3.1	2.5	9.5	1.7	6 6 7	2.7	• •	 	; r?	. <del></del>	2.0
- MODEL E-20	INKING	•,	2	27	50. S			_		- 1	_			. v	9	D. 00	12.7	<b>8</b> 0 0	7.7		SO I		9.0	7.0	, v , v						9 (		- C	<b>,</b> –	4.0	9.9
	AIRCRAFT S	PORT	<b>X</b>	<b>56</b>	2.3	2.0	4.5	B 61.	3.6	2. c	A. 10.	2.5	2.6	, v v	3.2		3.2	4.6	. o	2.6	2.4	7 6	2.8	2.7	2.0	3.2	2.2	3.3	1.2	2.5	 	.,		7.	1.3	2.6
LANDING DATA	AIR	-	5,5	25	7.7	9	7.7	12.7	_	9 1	. =	8.3	9 0	2.6	16.5			= •	. 6			) K			. w						•	_	, v	. 4		0.00
-		NOSE	\$	24	2.3	-	7.0							7.0		~		9.6	, c		- 1				2.6			<b>F</b> )		- •	- •	- •			1.2	2.8
		-	7/5	23	7.7	*	◆ (	9.4	_	0 1					2.4			•							* *			_						4.0		9.2
	9	2		22	8696	9599		9662	266	700	3	9669	9612	2000	96 13	9617	9619	9620	9623	9624	9625	9626	9628	2	9631	3	9641	9646	9647	9648	9659	9653	9655 9653	9663	9664	9665

99			AIRCRAFT		SINKING SPEED AT TOUCHDOWN	PEED A	T TOUCH	NAOQ			GLIDE PATH ANGLE AT TD	PATH A	NGLE A	1 10	WHEEL HEIGHT	EIGHT	ноок нетсит	EIGHT
2	MOSE	ň	PORT	<b></b>	STBO	£	AVG		FREE-FLIGHT	IGHT	BHA	•	8	>	OVER R	RAMP	OVER RAMP	RAMP
	ž.	Ş	2	Ş	٤	¥\$	5	\$	F/S	K/S	DEC	8	DEG	3	E	*	t	*
22	23	<b>34</b>	ន	56	23	28	58	90	5	32	33	<b>4</b> 5	<b>8</b>	36	37	82	39	\$
9996	7.9	4.7	7.2	2.2	9.3	2.8	8.1	2.5					3.1	.055				
9667	<b>9</b> . <del>4</del>	<b>+</b> :	7.7	7.7	5.5	1.7	9.9	7.0					2.6	.046				
8996	9.5	2.8	<b>*</b> :	5.8	9.0	2.9	7.6	5.8					3.9	. 968				
9672	<del>-</del> :	1.2	6.2	<b>.</b>	8.6	0. 0.	8.3	2.5					J.,	. 954				
9673	6.2	<b>6</b> .	8.8	2.7	7.0	2.1	7.9	2.4					3.0	.053				
9676	5.7	1.7	7.5	2.3	<b>6</b>		e0 :	2.7					J.	.055				
<b>8</b> 5 6	ا ا ا	- c	6. ¢	4 °	7. K	4 4 5	e	., c					3.5 4.5	.057 858				
9682	1.3	. n	2.0	•	12.1	3.5	12.8	, N					. r	989				
9683	<b>9</b> .	7.6	6.3	2.5	6.2	6.	7.2	2.2					2.8	.049				
9665	6.4	5.5	10.2	3.1	8.5	2.6	9.8	2.9					3.7	. 964				
9696	<b>.</b>	•	12.1	3.7	10.3	J. 7	10.9	3.3					4.6	.081				
9696	<b>9</b> .9	<b>.</b>	8.5	2.8	10.7	ر ا	6. G	9.P					4.0	.070				
8888	4.0	<b>.</b> . (	<b>.</b>	9 1	7.5	2.3	<b>6</b>	<b>7</b> .4					5.9	.050				
	0 Y	7.7		, c	, c	2. ¢	N 6	9 r					n «	199.				
9693	6.2	9	6.5	2.0	7.2	2.2	6	2.5					2.7	948				
1696	7.5	2.3	-	2.5	<b>8</b>	2.6	4.0	2.6	8.5	5.6			4.6	.059				
9695	9.9	7.4	6.3	2.5	10.1	3.1	9.6	2.7					4.6	. 059				
8696	<b>.</b>	i.	2.1	•	n, 0	2.8	4.9	2.8					5.6	.045				
8698		<b>D</b>	5.7	1.7	 	<u>د</u> د	<b>6</b>	2.1					 	. 055				
9761	9 F	::	÷ •	÷ •	2.7	•	8 · G							919				
20/0	, r.	9		. 6			- 6	. 6					. 6	.035				
9706	4.2	7.2	7.3	2.2	8.2	6	8.1	2.5					 	.054				
9707	9.9	<b>5.0</b>	7.1	2.2	8.5	5.6	8.5	5.6					4.5	. 059				
9769	<b>9</b> .0	<b>5.0</b>	<b>+</b> :=	3.5	13.8	4.2	12.5	3.B					4.8	.084				
9710	 	6	1.0 0.1	4.	9.9	N :	10.8	n, n					4.2	.073				
9712		2.5	- 10. - 10.		12.6	<b>10</b>	s:						5.5	.679				
9713	<b>9</b> .	2. 9.	. ·	9 .		1.7	- 1						2.5	. e.s				
9717	<b>4</b> 1					9.	÷.	<b>*</b> :						.032				
9718	 	2.2		7.7	÷ •	÷ •	, ,						2.5	.044				
97/A	- r	•		•	0 d			9.4					, . 0 •	¥9.				
9723		- K	) G	. 6		2.5	7.6	. 6					- r	557				
9724	7.8	2.4	8.7	2.7	0	n	-	2.8					9.5	.967				
9726	6.2	1.9	5.3	1.6	4.9	7.0	5.9	1.8					2.1	.037				
9727	8.7	2.6	10.2	3.1	<b>8</b>	5.6	4.6	5.8					3.3	.057				
9729	<b>.</b>	2.7	<b>0</b>	2.7	9.0	2.7	<b>6</b> .	2.7					3.7	. 964				
9736	13.7	4.2	12.1	3.7	13.8	4.2	12.6	ы. В.					5.6	. 898				

		3	LANDING DATA	1	MODEL E-	E-20		uss da	TERPRI	USS ENTERPRISE (CVN-65)	N-65)			Ĭ	NICHT LANDINGS	DINGS				
997		-	I	Z Z	T.			ROL	٠	N G L	w	-	PITCH RATE	RATE	ROLL RATE	<b>W</b> TE	9.	÷	YAW	•
2	Ę		8		9.6		2	_	8		i.		AT TD	2	AT TD	2	AT TO	2	AT TD	2
	DEC	3	DEC	3	930	3	DEC	3	DEC	8	DEG	8	DEC	\$	DEG	8	DEG	3	DEG	3
7	7	2	<b>‡</b>	\$	9	47	<b>\$</b>	<b>\$</b>	20	51	25	53	54	22	26	27	28	29	99	19
9696	4.0	.112				ï	2.2	. 038				_	9.9	999	8.5	148	2.7	.047	6.	016
9238		.143				••	2.3	.040				_	9.9					101	8.5	.148
9599	9.5	.161				-	•.	.017					1.7	•			-6.2	108	7.1	.124
9696		.112				<b>-</b>	12.8	.223					~ .	_ '	1			026	٠,	919
9661		96 -					- 4 - 4	. e.e.				۱ '		019 12	 	4 CIS.	~ ◀	072	. c	. 633
200		.162		_	J. 4	147		98.			₹.	. 667	9.0	9.00			'n	096	4.6	181
1096		. 126		, -	. 2.7	127	_	.002		•	·	. 002	6.	.033			7	056	5.7	660.
9665	4.6	.147				•		002									-5.5	960'-	6.2	. 108
9667		.117				•	4.7	.682				ĩ	5.2			. 0592	o i	051	<u>ا .</u> دن	026
6998		99				. <b>.</b> .	2.0	. 635					 		-2.7		ų i	073	2	.692
9612		.124		•			 •	.026			ď	9	n e	600.		.002 -2	٠. ٥	047 - ABB	ان دن ه	. 861 181
2 2 3 6	. ^			-	,	?	ı	456			•		. 6	900				1.00		952
9615	. 5	<b>2</b>				_		.024				1			3.2			686	7.4	. 129
9617		1.38				•	,	967				_	•			. 038 -2	ю.	049	7.0	. 122
9619		.145						. 026				1	n			1.914	4.2 -	073	4.2	.073
9628		8. 8.		~	<b>4.</b>	.147 -1	ni (	623		•	60	014	9.0					684	5.1	. 689
9621		2				1	  -  -	9/9'- 67.0					9 . e	999.9		116 -	0 0	999. 1	, .	. 642 680
9624		154					_	.024				•	80					031	4.2	.073
9625		 				-		.026				_						075	5.3	. 692
9626		. 148 84 :				• `		016				-		9.88	<b>c</b>		-1.0°	052	<u>.</u> .	.033
9627		25				7						۲ ۳	1 c	1001		900	֓֞֝֝֝֝֝֝֝֝֝֝ ֓֓֞֓֞֓֞֓֞֞֞֞֞֩֞֞֩֞֩֞֩֞֞֩֞֩֞	. 662 - 651	, r	9. 8 80 8
9639	•	164			.5	166	; <del>-</del>	.637		••	2.4	.042						061	5.7	660.
9631		33.					4	.056					<del>-</del>	•••			-5.9	103	7.0	.122
9633		.126				••	2.4	. 042				_	9.9	9.666			-	072	6.9	. 120
9634		131					œ.	.016										960.	4.4	. 129
9641		154				• `	! 	002				- '					ر 1.00	068	4. V.	679.
9646		.120					<b>*</b> !	.024				- `						082		9
9647		. 145				• •	· •	.082				· • •	7.7	740. I		e/e -		1.678 1.678	 	. 1.50 8.41
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#60# 0.68.1		77.				•						1						073	6.2	168
965		2				•	2.7	947				•						651	0.0	0.00
9662		124				Ĩ	-	021				. –		4)			-	052	4.3	.075
29663		138				J-		.017				_						.017	1.6	. 028
9664		.152				•		003					5.8	T	9.		<u>.</u>	072	7.9	. 138
9665	6.9	.115				I		628				_	9.0	0.000	• •	077 -2	o.	051	7.9	. 138

		3	LANDING DATA	1	MODEL E	E-20		uss e	NTERPR	USS ENTERPRISE (CVN-65)	/N-65)			N	NICHT LANDINGS	AD INGS				
999		- 4	Z U	S Z V	ר ע			8	,	ANGL	ш	•	PITCH RATE		ROLL RATE	WTE	F. P. A	÷.	YAW	*
2	5	_	8		4		5	•	8	œ	1		AT TD	5	AT	5	AT TD	5	AT TD	5
	930	3	DEG	2	DEC	2	DEC	3	DEG	3	DEG	3	DEG	2	DEG	8	DEC	<b>8</b>	DEG	2
<b>∓</b>	42	\$	\$	\$	\$	47	\$	6	20	5	25	33	5	22	26	57	20	20	8	5
9996	7.6	31.					₩.	.014				•	6.6	8.888 -6.2		108 -2	2.7	.047	9.	.017
9667	7.2	.126					-:	. 002				-4	_			.117	1.4.1	677	3.2	.056
8998	7.8	38						002				-,		. 963 -1		023 -4	-	072	2.6	.045
9672	<b>.</b>	<u>.</u>				•	<u>.</u>	077				. •	-	_		208 -6	i, e	110	S. 5	960.
9676		21.					, • •	66/ 617				7	2.2	638 -5.	v 60	7 68.	! !	688 682	. c	889. 188
9696	4.	.147				•		963				•			9	010 -1		628	ij	. 665
9681	•	.115						. 005				~			6.9	.129 -2	80	049	2.5	. 038
9682	n	.127				1	_	047				1			_		· •	042	3.0	. 052
2 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5		141						999.				_					60 r	687	ص ب	.19
							ų,	20 C				•		0 000.			· • •	665	٠ ن	66.
		? <b>:</b>					D. C	200.				ī '	» o			4 000.	ų -	.6/3	* - i	, ee,
6830		162						- 914				•			2.6	.045 -2		047	- e	990
9696	9	.120				1		017				7		ı	۰		~	108	8.2	.143
9692		.166						. 921				<b>.</b>	9		<b>.</b>		-5.3 -	692	8.9	.155
9693		.122						. 924					2.1	. 637 6			•	023	2.2	. 038
9694	_	169		<b></b>	•	 82 		. 963			7	.003						061	2.1	.037
9693		126				•		044				·	0	0.000 -4.3		075 -5	1 8.6 1		 	<u>∓</u> 8
						_	. e 	9/2				- 🕶	o	8.01-020.		2. 283.		***	7.4	120
	9 0	155					6.7	1117					0		3.5			. 687	7.7	¥2. 42.
9702		Ξ.					2.5	.044				ï		ı				028	2.7	.047
9763		.128					3.8	996.				_	•		8.9			101	5.3	. 092
976	ų,	3					 	. 026				_								689
9787		<u> </u>					5.7	.065				•	, ia 1 ia	.014 0.0 7 7 2 2 7 7		8.000 J	ا د ھ	. <b>6</b> 52	ر ا ا	101 878
97.6	2.7	126				•		- 935				-2					•	887	4	989
9712		59					7.1	.124				4		ŀ			10	110	7.2	.126
9713	_	.120						007				_		9.000			-3.8	966	5.5	960.
9717		.145					œ.	.016				_	•	.000	•			696	5.1	.089
9718	ب ب	88						662				₹	o. •	. 986 7			•	<del>0</del> 03	o. •	986. 8
87/8		77.					5.5	3 · C				•		ı		7- 970'-	! /:7-	, 45 d	- •	1.007   053
12/4		5 5					7 0	170.				-					ו ספ		) (c	113
9724		50				ı		856				-	2 2	-				- 916	9	080
9726	7.2	.126					! =	.002				•	9.9	•		•		061	6.2	168
9727	6.2	201						993				<b>.</b>					_	054	4.6	. 986
9729	4.6	.99				'	_	028				•	.2		_	,	<u>-</u>		<del>-</del> -	. 072
9730	5.2	. 691				•	+: T	624				era	e.	.052 -2.(	ω.	045 2	۲.	. 047	r. †	075

REREAD	NUMBER			•	-	•	•	•	- (	<b>5</b> (	<b>9</b> (	~ •	<b>-</b>	- 6	•	_	•	•	-	•	-	_	•	•	<b>D</b> -	- •	•	-	•	- (	•	<b>&gt; G</b>	<b>&gt; G</b>	•	•	•	•	•	-	•
ARR GEAR	RUNOUTS	8	82	6.	426.7	424.2	426.7	424.2	431.8	429.3	5.62	426.7	428.7	426.7	419.1	424.2	429.3	419.1	426.7	429.3	424.2	424.2	429.3	424.2	424.2	421.6	426.7	426.7	419.1	420.7	<b>B</b> 6	7007	424.2	6	429.3	429.3	429.3	424.2	429.3	421.6
A.R.	\$	Z	5	•	168	167	168	167	170	89		9 9	<u> </u>	168			169	165							) £	5			165	8	9 6	9	167		169			167	169	166
BAROMETRIC	PRESSURE	¥ ₹	8	760.5	760.2	760.2	760.2	760.2	769.2	769.2	7.00.7	769.2	789.2	760.2	769.2	760.2	769.2	760.2	760.2	760.2	769.2	760.2	769.2	769.2	766.2	760.2	769.2	769.2	760.2	7.09.2	761.2	7.10/	761.2	761.2	761.2	761.2	761.2	761.2	761.2	761.2
BARON	PRES	IN HC	79	29.94	29.93	29.93	29.93	29.93	29.93	29.93	28.87	29.95	20.00	29.93	29.93	29.93	29.93	29.93	29.93	29.93	29.93	29.93	29.93	29.93	28.82	29.93	29.93	29.93	29.93	28.82	29.97	78.87	20.87	29.97	29.97	29.97	29.97	29.97	29.97	29.97
40F		ပ	78	5	2	2	5	5	2	5 2	7	5 5	; ;	2	2	21	21	5	13	2	21	5	5	<b>7</b>	2 2	; <del>,</del> ,	7	7	2	7	₽ :	D <b>G</b>	<u> </u>	. <del>.</del>	5	5	2	₽	5	₽
<b>}</b>		•	11	65	69	69	69	69	8	8	D (	D 0	3 8	9	69	69	69	69	69	69	69	69	69	8	2 6	9	69	69	69	9	ខ្ល	2 4	) £	8	5	3	65	65	65	65
DECK ROLL		8	76	.014	•	007	. 002	.010	919	919.	719	1 . I	100				047		_						1.614				024		i	9 8		9	. 621	916	•	6	. 609	916
DEC		DEG	75	€.	<b>E</b> Q.	<b>†</b>	Τ.	•	Ď.	1		ָּהָ הַי	1	1	0	2	-2.7	.8	9.0	<b>†</b>	2	1.5	1.2	7	ן ק	9	6.	1.8	7	-2.4	, i	• •	. «	) a	1.2	6		0.0	ĸ	o.
DECK PITCH		8	*	003	007	995	993	007	- 995	- 665	Can.	002			003	993	997	003	003	003	003	005	993	. 963	. 1 6 6 7	500	005	005	007	663	002	996.			662	002	003	003	003	995
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٩	SPEED	Ş	72	=	^	7	7	7	<b>~</b> (	٠,	٠ (	<b>-</b> r	٠,		. ~	_	7	~	7	7	_	7	7	<b>^</b> '	- 1	. ~	~	7	<b>6</b> 0 (	n	<b>د</b> د	•	<b>0 4</b>	<b>*</b>	•	•	•	€0	80	€0
SHIP.		₹	7	22	2	<b>±</b>	=	2	7	2 :	2 !	2 :	2 =	2 =	2	2	2	2	2	2	2	5	2	2	2 :	5 12	2	2	<b>o</b>	<b>D</b>	<b>e</b> :	= ;	= :	. •	, <del>-</del>	7	5	5	5	5
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200	TYPE		8	70100	5829	50200	59299	50200	58286	59129	20200	50120	2070C	2070	50120	50200	50200	50120	50200	59100	50100	59200	29299	50200	20126	59199	50200	59199	56266	29299	79120	00707	26266	78288	50200	50200	59100	58288	50120	50100
SIDE	5		2	3	7	2	3	336	Į.	7	3	3	3 3	3	3	3	342	3	342	ž	23	3	345	*	3 :	3 7	342	ž	3	7	¥;	ξ.	ţ	ŝ	342	3	Ħ	342	<b>6</b> 97	341
WIRE	Š		67		ກ	2	7	*	<b>17</b>	ימ	9 (	י מ	) r	) P	n	n	n	*	n	n	*	n	n	•	+ r	•	n	n	<b>→</b> 1	מ		•	? <b>r</b>	•	8	4	'n	*	~	+
RAMP TO TO	DISTANCE	3	2	8	3	2	3	2	5	2 2	8	8 :	3 2	3 2	<u> </u>	3	3	8	5	8	85	5	72	<b>S</b>	2 =	2	2	28	2	2	2 :	2 :	: f	3 8	: *	-	2	101	92	\$
PAS .	DIS	E	2	282	273	23	3	288	167	<b>3</b>		226	200	12	94	222	272	315	<b>38</b>	296	2	<b>50</b>	238	313	222	Š	787	248	99	2	283	2 5	, , , , , , , , , , , , , , , , , , ,		242	33	286	333	249	310
OFF-CENTER	DISTANCE	*	2	Y	†	9	7	1	?	† .	† '	? 9	7	î	٠ ٦	?	q	Ŷ	?	ņ	†	†	?	7	11	9	†	7	ę,	1	<b>ب</b>	7 .	? 4	? ?	4	•	†	1	7	ņ
OFF	DIST	E	3	91-	-12	10	7	-12	<b>=</b> :	<b>+</b> (	7.	- 1	P =	? 7	-12	7	15	-16	F	-15	-12	-12	=	7	77	2 2	1.0	-12	-15	2	-13	<b>?</b> :	֓֞֜֝֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֡֓֓֓֡֓֡֓֓֓֡֓֓֡֓֡֓֡֓	? 4	5.	•	+	+	-20	-13
9	Š		2	9696	9598	9599	888	96	8662			0000	9690	9612	9613	9614	9615	9617	9619	9620	9621	9623	9624	9625	9626	9628	250	263	9633	3	9641	9 6	100	9	25.5	9655	9662	9663	9664	9665

USS ENTERPRISE (CVN-65)

LANDING DATA - MODEL E-20

		3	LANDING DATA	1	MODEL	E-20		USS	K	RPRIS	USS ENTERPRISE (CVN-65)	<del>1</del> -65)			z	IGHT	NICHT LANDINGS	s			
9	8	OFF-CENTER	RAMP TO	55 57	WIRE	SIDE	200	3	₹	SHIP	DECK PITCH	PITCH	DECK	DECK ROLL	12	TEMP	BAROMETRIC	TRIC	ARR	ARR GEAR	REREAD
ě	۵	DISTANCE	DISTANC	TANCE	₹	<b>છ</b> ં	TYPE	200E	B	SPEED							PRESSURE	URE	2	RUNOUTS	NUMBER
	•	z E	t	3					₹	E/S	DEC	8	DEC	\$	<b>I</b>	ပ	E H	오 로	Z	₹	
2	•	3	2	2	67	2	2	70	7	22	22	7.	22	78	11	78	78	80	5	82	
999	1		329	<u>=</u>		¥	60200		5	•	2	003	-	. 662	65	8	29.97	761.2	•		•
667	T		284	2	n	¥	50120		5	•	-	002	<b>-</b>	.028	99	6	29.97	761.2		426.7	•
9	1	•	ž	3 ;	<b>◆</b> ¢	<b>2</b>	50 50 50 50 50 50 50 50 50 50 50 50 50 5		2:	•	• • •	007		919.	۶ د	₽:	29.97	761.2		429.3	•
2/0	Ť			7 5	N 4	3	59196		= =	<b>0 C</b>	7 6	200	• •	916	0 49 0 49	9 5	78.87	761.2	20.5	429.3	- 6
676	7	††	88	2	n	7	58288		: 2	<b>^</b>	. ?	. 963	: =	919	65	 	29.97	761.2		429.3	•
3	7	·	<b>707</b>	8	n	602	50200		2	7	2	003	•	.010	65	5	29.97	761.2	169	429.3	-
5	7		327	2	:	7	<b>Se100</b>		2	^	2.	993	7	. 003	55	18	29.97	761.2		<b>.</b>	•
29	7	•	53 53 53	2 3	n .	75	50100		2:	<b>~</b> :	- (	002	7.	. 621	29	<u> </u>	29.97	761.2		426.7	- (
3 :	7	•	9	2 5	• •	<b>;</b>	50120		2 :	<b>~</b> !		- 963 500	* ·	.024	ខ្ល	9	29.97	761.2		426.7	<b>S</b>
3	ī'	•	748	۲:	? •	<b>3</b> 8	9079C		2 :	۱ -	- (	200	•	199	g :	0 0	/A. 87	7.10/	20	C. 874	•
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3	7	•	280	2	112	3	50120		2	. ~	•	766		. 619	8 8	6 6	29.97	761.2	-	426.7	•
8	7	Ĭ	274	2	•	75	50120		2	~	2	003	1	.012	83	2	29.97	761.2	-	424.2	•
692	7	·	ž	102	*	ž	50100 00100		7	7	-	. 662	9.	. 028	65	<b>5</b>	29.97	761.2		419.1	•
693	Ŧ	•	784	8	n	¥	20200		5	7	S:	- 669	1.2	.021	<b>6</b> 5	₽	29.97	761.2		431.8	•
<b>7</b> 6	, -	•	282	2 8	י מ	<b>2</b> 3	56.56 6.56 6.56		2:	<b>~</b> r	-	002	6: 1	616 616	20	<b>≅</b> :	29.97	761.2	170	431.8	<b>6</b> -
	Ĭ	•	5 5	8 3	•	3 5			2 5	- 5	· ·		ó.	• 6 • 6	2 4	0 9	78.87	769.5		9.0	- 4
	ī		2 <b>49</b>	? 2		S	76299		3 2	7 2	- ?	.003	- •	.028	8 8	. <del>.</del>	29.94	768.5	•		• •
Ž	ī	-	25	1	2	ž	50200		2	<b>1</b> 2	9.9	9.00	-	.002	2	<b>6</b>	29.94	760.5	25	428.7	•
702	7		220	2	n	3	50200		23	12		9.00	4.	667	8	5	29.94	766.5		429.3	•
3	T		281	8	rs (	3	56266		22	=	-	. 002	s.	. 869	65	₩.	29.94	769.5	•	124.2	•
2	7		2 2	5 6	י מי	*	58286		22	= :		999		002	g :	<b>10</b>	29.94	760.5	167	424.2	<b>B</b> (
	7		15	8 2	<b>4</b> P7	3	50200		; ;	2 2		990	9 -	916	3 2	0 <u>«</u>	29.94	768.5		421.6	• •
710	ī	Ī	232	7	n	3	50120		23	2	9.0	999		003	5	5	29.94	760.5		424.2	•
712	7	-	<u>5</u>	21	~	342	<b>59200</b>		24	12				026	8	8	29.94	760.5	-	429.3	•
713	ī		287	82	n	ž	<b>50100</b>		74	12	4	. 003	2	003	65	2	29.84	760.5		429.3	•
717	7 3	-	78	2 :	n	3	20200		7	2	- 6.6	900.	<u>-</u> '	9	S	<b>2</b> (	29.94	760.5		426.7	•
2	7		218	8 :	N	3	92196		*	7	- ·	. 662	<u>.</u>	9.6	<u>و</u> د	0 :	29.84	769.3	ှ ဂို	- 6	N •
	•		2 2	5 3	•	*	98797		* 6	2 :	• •	/86.		819	2 4	0 :	* A . A .	769.0		9.6	<b>D</b> (
7 (	1		B 7	5 5	4 6	3 5			;;	7 5			_	200.	2 4	0 9	10.00	768.5		120.7	<b>,</b>
724	1	77	193	9	4 ~	3	50200		7 ;	2 2	9 -	. 662		926	3 29	. <u>.</u>	29.94	760.5		426.7	1 0
726	ī	٠	99	2	*	*	50120		7	2	-	992		007	5	20	29.94	760.5	•	124.2	•
727	ī	·	313	8	*	345	50120		7	12	2	993	6.6	0.000	65	<b>8</b> 2	29.84	760.5	166	121.6	•
729	7	 	282	8	•	343	50100		74	12	9.9	9.999	ø.	919	65	8	29.94	769.5	•	121.6	•
736	1	7 <b>9</b>	247	22	n	341	50100		54	12	-	. 002	ņ	.003	65	8	29.94	760.5	168	128.7	•

# S-3 DAY

		٦	LANDING		3	DATA - WODEL S-3	?		uss e	AT ERPR	USS ENTERPRISE (CVN	\$				DAY LANDINGS	NDINCS		
PARE.         PERPO.         MIN SP* A TD         FF           S 10H M/S 1	Æ-J	Ž,	=	3	*	NO-VE		>	EOR	<b>₹</b>	Z Z	85	<u>.</u>	KWPA	\$	11	רונו		[GHT
8         M/S         NA					Ą		5							Z		5	FF		
25         13         4         15         13         14         15         16         17         18         19         23         14         15         14         15         16         17         18         16         23         23         23         11         16         17         18         16         23 </th <th>KS KM</th> <th></th> <th>3</th> <th>yı</th> <th></th> <th></th> <th></th> <th></th> <th>Ş</th> <th></th> <th>K K</th> <th></th> <th>s/n</th> <th></th> <th></th> <th></th> <th></th> <th>LBS</th> <th>æ</th>	KS KM		3	yı					Ş		K K		s/n					LBS	æ
25         13         4         2         99         46         105         54         1.07         1.10         37500           25         13         4         2         99         46         104         53         1.11         1.10         35100           25         13         4         2         99         46         104         53         1.11         1.00         35500           25         13         4         2         90         46         104         53         1.11         1.00         35500           26         13         4         2         90         46         104         53         1.11         1.00         35500           26         13         4         2         90         46         104         53         1.11         1.10         35500           26         13         4         10         53         1.11         1.10         35500           26         13         4         10         53         1.11         1.10         35500           26         13         4         4         10         53         1.11         1.10         35500	*	•			_	_	•	•	=	2	2	<b>±</b>	55	•	11	2	2	5	23
25         13         4         2         99         46         104         53         1,116         1,10         35,00           25         13         4         2         99         46         104         53         1,11         1,10         36,00           25         13         4         2         99         46         104         53         1,11         1,10         36,00           25         13         4         2         99         46         104         53         1,11         1,10         36,00           26         13         4         2         99         46         103         53         1,11         1,10         35,50           26         13         5         3         90         46         103         53         1,11         1,10         35,50           26         13         5         3         90         46         103         53         1,11         1,10         35,50           26         13         4         40         103         53         1,11         1,10         35,50           26         13         4         40         10         53	96	2	~	2	5 5	_	~	3	\$	105	*			1.07				37886	16783
25         13         4         2         86         46         165         54         115         198         35460           25         13         4         2         164         53         116         1         106         3560           25         13         4         2         164         53         111         1         106         3560           25         13         4         2         164         53         111         1         106         3560           26         13         4         2         165         53         111         1         106         3560           26         13         5         3         4         163         53         111         106         3560           26         13         5         3         6         4         163         53         111         106         3560           26         13         5         3         6         4         163         53         116         35         116         35         35         116         35         35         116         35         35         116         35         35	98	2	3.	••	2	•	~	2	\$	<u>=</u>	3			1.18		1.1		36100	16375
25         13         4         2         89         44         164         53         116         116         100         35000           25         13         4         2         89         45         164         53         116         100         35000           25         13         4         2         80         45         164         53         111         110         35000           26         13         4         2         80         46         163         53         111         110         35000           26         13         5         3         86         46         163         53         111         110         35500           26         13         5         3         86         46         163         53         111         100         35500           26         13         5         3         86         49         163         53         111         100         35500           26         13         5         3         86         49         100         35         116         35         35000           26         13         4	2	ខ្ល	=		2	_	~	2	9	<b>10</b> 5	ž			1.15		8		36400	16511
25         13         4         2         164         53         111         116         116         35600           25         13         4         2         86         45         164         53         111         100         35600           26         13         4         2         86         46         165         53         111         100         35600           26         13         5         3         96         46         163         53         111         100         35600           26         13         5         3         96         46         162         53         111         100         35600           26         13         5         3         96         46         162         53         116         35600         176         35600           26         13         5         3         96         46         162         53         116         116         35600         176         35600         35600         35600         35600         35600         35600         35600         35600         35600         35600         35600         35600         35600         35600	<b>2</b> 6	2 9	3 :		2:	•	n (	8	7	•	3			1.16		2 :		36300	16466
25         13         4         2         64         53         1.11         1.16         35500           26         13         4         2         96         46         103         53         1.11         1.16         35500           26         13         5         3         96         46         103         53         1.11         1.06         35500           26         13         5         3         96         46         103         53         1.11         1.06         35500           26         13         5         3         96         49         103         53         1.16         1.06         35500           26         13         5         3         96         49         103         53         1.17         1.06         35500           26         13         5         10         48         105         55         1.17         1.06         35500           27         14         2         1         86         55         1.17         1.06         35500           24         12         2         1         86         55         1.17         1.06         35		· ·			7 -		× •	<u> </u>	7, 4		2 2			7		B 1		3688	16236
25         13         4         2         86         46         163         53         1.11         .96         35560           26         13         5         3         84         43         163         53         1.11         .96         35560           26         13         5         3         84         43         163         53         1.14         1.06         35560           26         13         5         3         84         43         163         53         1.14         1.06         35560           26         13         5         3         84         43         163         53         1.14         1.06         35560           26         13         5         3         96         46         163         53         1.16         1.16         35560           24         12         2         1         84         160         55         1.17         1.06         37560           24         12         2         1         85         1.17         1.06         37560           24         12         2         1         1.16         37560         37560	3 5	2 2	. =		! =		• •	2	2	1	3 2			3 -				35,800	16230
26         13         5         3         62         42         163         53         1.14         .96         35566           26         13         5         3         96         46         163         53         1.14         .96         35566           26         13         5         3         96         46         162         52         1.15         1.16         35566           26         13         5         3         96         46         162         52         1.15         1.16         35566           26         13         5         3         96         46         162         52         1.15         1.16         35566           26         13         5         3         96         46         162         52         1.15         1.16         35566           24         12         2         1         87         47         186         55         1.17         1.96         35566           24         12         2         4         186         55         1.17         1.96         35766           24         12         2         1         8         4	3	· ?	- 3					ă	4	201	3 2			=======================================		-		35500	16103
26         1.3         5         5         96         46         163         5.3         1.14         1.00         35500           26         1.3         5         3         96         40         163         5.3         1.19         1.10         35500           26         1.3         5         3         96         49         102         5.2         1.19         1.10         35500           26         1.3         5         3         96         49         102         5.2         1.19         1.10         35500           24         1.2         2         1         96         4.5         106         5.5         1.17         1.00         35500           24         1.2         2         1         96         4.5         106         5.5         1.17         1.00         37400           24         1.2         2         1         97         4.6         106         5.5         1.17         1.00         37400           24         1.2         2         1         97         4.6         106         5.5         1.17         1.00         37400           24         1.2         2<	2		3		2			92	7	163	3			=		8		35600	16148
26         1.3         5         94         46         16.5         5.5         1.16         1.19         1.26         1.56         25.56         1.19         1.19         35.56         25.56         1.19         1.19         35.56         35			-		2		n	3	9	163	S			<b>-</b> :-		- 90		35500	16103
26         13         5         3         84         43         103         5.3         1.09         1.09         1.09         1.09         1.09         3.5500         25.00         2.00         2.55	<u>-</u>	=	+		5	-	2	2	\$	163	3			1.13		8.		35500	16103
26         13         5         3         96         48         102         52         1.19         1.10         1.10         3.400           26         13         5         3         96         48         102         52         1.15         1.20         3.400           23         12         2         1         99         51         106         55         1.21         1.00         3.400           24         12         2         1         90         55         1.17         1.00         3.700           24         12         2         1         92         47         106         55         1.17         1.00         3.700           24         12         2         1         92         47         106         55         1.17         1.00         3.700           24         12         2         1         92         47         106         55         1.17         1.00         3.700           24         12         2         1         96         46         106         55         1.14         1.00         3.700           24         12         2         1         96 </td <td><b>3</b></td> <th>2</th> <td>Ŧ</td> <td>2</td> <td>2</td> <td>•</td> <td>2</td> <td>\$</td> <td>7</td> <td>103</td> <td>S</td> <td></td> <td></td> <td>1.09</td> <td></td> <td><b>8</b>.</td> <td></td> <td>35500</td> <td>16103</td>	<b>3</b>	2	Ŧ	2	2	•	2	\$	7	103	S			1.09		<b>8</b> .		35500	16103
26         13         5         3         96         49         102         52         1.15         1.20         34700           26         13         5         3         96         44         106         55         1.21         1.00         35500           24         12         2         1         96         55         1.17         1.00         37500           24         12         2         1         96         45         106         55         1.17         1.00         37600           24         12         2         1         97         48         106         55         1.17         1.00         37600           24         12         2         1         97         48         106         55         1.17         1.00         37600           24         12         2         1         96         46         106         55         1.17         1.00         37600           24         12         2         1         96         46         106         55         1.16         1.00         37600           27         14         2         1         97         46 <td>2 25</td> <th>2</th> <td>2</td> <td>7</td> <td>2</td> <td>•</td> <td>n</td> <td>9</td> <td>6</td> <td>102</td> <td>25</td> <td></td> <td></td> <td>1.19</td> <td></td> <td>1.10</td> <td></td> <td>34800</td> <td>15785</td>	2 25	2	2	7	2	•	n	9	6	102	25			1.19		1.10		34800	15785
26         13         5         3         96         46         163         53         1,16         1,19         35500           24         12         2         1         96         51         166         55         1,17         1,00         35500           24         12         2         1         96         46         106         55         1,17         1,00         37500           24         12         2         1         92         47         106         55         1,17         1,00         37500           24         12         2         1         94         48         106         55         1,17         1,00         37500           24         12         2         1         94         48         106         55         1,17         1,00         37500           24         12         2         1         94         48         106         55         1,14         1,00         37500           24         12         2         1         94         46         106         55         1,14         1,00         37500           27         14         2         1 <td></td> <th></th> <td>-</td> <td></td> <td>2</td> <td>-</td> <td>2</td> <td>8</td> <td>9</td> <td>102</td> <td>25</td> <td></td> <td></td> <td>1.15</td> <td></td> <td>1.20</td> <td></td> <td>34700</td> <td>15740</td>			-		2	-	2	8	9	102	25			1.15		1.20		34700	15740
2.5         1.2         1.20         1	-	-	7		2:		P) •	2 :	<b>9</b> ;	163	2			<b>1</b> .1		1.10		35500	16103
24         12         2         1         95         45         106         55         1.15         1.00         38400           24         12         2         1         92         47         107         55         1.17         1.00         37500           24         12         2         1         94         46         107         55         1.17         1.00         37500           24         12         2         1         96         46         107         55         1.14         1.00         37500           24         12         2         1         96         46         107         55         1.14         1.00         37500           27         14         2         1         96         46         106         55         1.16         1.00         37500           27         14         2         1         96         46         106         55         1.16         1.00         37500           26         13         2         4         1         1         1.00         37500           26         13         2         4         1         1         1		2 1	4 3		7 5			2 2	5 5		6 Y			27.		8 8		37488	16985
24         12         2         47         167         55         1.17         1.06         38406           24         12         2         1         92         47         166         55         1.17         1.06         37506           24         12         2         1         94         48         106         55         1.17         1.06         38106           24         12         2         1         94         48         106         55         1.14         1.06         38106           24         12         2         1         94         48         106         55         1.14         1.06         38106           27         14         2         1         91         47         101         55         1.16         1.06         37406           27         14         2         1         91         45         106         55         1.16         1.06         37406           26         13         2         1         85         48         1.06         55         1.16         1.16         1.16         1.16           25         13         2         1         86		2	2		12:		-	3	<b>\$</b>	90	8			1.15		6.		37700	17101
24         12         2         47         106         55         1.18         1.00         37500           24         12         2         48         107         55         1.17         .90         38300           24         12         2         1         94         48         106         55         1.14         1.00         39100           24         12         2         1         96         46         106         55         1.14         1.00         39100           27         14         2         1         91         47         101         55         1.12         1.00         37400           27         14         2         1         91         47         101         55         1.10         1.00         37400           26         13         2         1         95         40         1.10         1.10         35700           26         13         2         1         85         4         1.10         1.10         35700           25         13         2         1         86         49         105         54         1.14         1.10         35700	<u>=</u>	=	'n	7	12		_	85	4	107	35			1.17		1.68		38400	17418
24 12       2 1       93 45       107 55       1.17       .90       38360         24 12       2 1       94 45       106 55       1.14       1.00       39100         24 12       2 1       97 50       106 55       1.12       1.00       39100         27 14       2 1       90 46       106 55       1.12       1.00       37200         27 14       2 1       91 47 101 52       1.21       1.00       37200         27 14       2 1       91 47 101 52       1.21       1.00       37200         26 13       2 1       97 45 106 55       1.10       37200         26 13       2 1       95 46 105 54       1.10       1.00       37200         26 13       2 1       95 46 105 54       1.16       1.00       35900         25 13       2 1       96 46 105 54       1.14       1.00       35900         25 13       2 1       96 49 105 54       1.14       1.00       35900         25 13       2 1       96 44 105 54       1.17       1.00       35900         25 13       2 1       96 44 105 54       1.17       1.00       37700         28 14       2 1       96 46 105 54	_	=	'n		•		-	85	<b>47</b>	106	22			1.18		- 90		37600	17055
24       12       2       1       94       45       106       55       1.14       1.09       35100         24       12       2       1       96       46       107       55       1.10       1.09       37200         27       14       2       1       96       46       106       55       1.21       1.09       37200         27       14       2       1       97       49       166       55       1.10       1.09       37200         26       13       2       1       87       49       165       54       1.10       1.09       37300         26       13       2       1       85       49       165       54       1.10       1.09       37300         26       13       2       1       85       46       165       54       1.10       1.10       36500         25       13       2       1       86       49       165       54       1.14       1.10       36500         25       13       2       1       86       49       166       55       1.14       1.10       36500         28		2	i				- 1	2	<b>\$</b>	197	S .			1.17		8.		38300	17373
24       12       2       1       96       46       107       55       1.12       1.00       35100         27       14       2       1       96       46       106       55       1.10       .00       35100         27       14       2       1       91       47       106       55       1.10       1.10       37200         26       13       2       1       87       45       106       55       1.10       1.00       37300         26       13       2       1       85       49       165       54       1.10       1.00       37300         25       13       2       1       85       46       165       54       1.16       1.10       36500         25       13       2       1       86       49       165       54       1.14       1.10       36500         25       13       2       1       86       49       165       54       1.14       1.10       36500         28       14       2       1       86       46       106       55       1.17       1.19       36500         27		2	ñ		- •		- •	\$ 2	? :	99	6			<u> </u>				990/0	919/1
27     14     2     1     10     55     1.10     .99     37460       27     14     2     1     91     47     106     55     1.21     1.09     37460       26     13     2     1     87     45     106     55     1.10     1.09     37200       26     13     2     1     87     45     106     55     1.10     1.09     37200       26     13     2     1     85     46     105     54     1.16     1.10     36500       25     13     2     1     86     49     106     55     1.14     1.00     36500       25     13     2     1     86     49     106     55     1.14     1.00     36500       26     14     2     1     85     44     106     55     1.17     1.00     36500       28     14     2     1     86     46     106     55     1.13     1.00     36500       28     14     2     1     86     46     106     55     1.17     1.10     36500       27     14     2     1     80     46 <td< td=""><td></td><th>2 3</th><td>5</td><td>,</td><td>? ?</td><td>•</td><td>- •</td><td><b>\$</b></td><td><b>8</b></td><td>9 6</td><td>א מ</td><td></td><td></td><td>: :</td><td></td><td></td><td></td><td>90.85</td><td>17383</td></td<>		2 3	5	,	? ?	•	- •	<b>\$</b>	<b>8</b>	9 6	א מ			: :				90.85	17383
27     14     2     1     91     47     101     52     1.20     1.10     34000       26     13     2     1     87     45     106     55     1.10     1.00     3730       26     13     2     1     87     45     106     55     1.10     1.00     36500       25     13     2     1     85     46     105     54     1.14     1.00     36500       25     13     2     1     86     49     105     54     1.14     1.10     36500       26     14     2     1     86     49     105     54     1.14     1.10     36500       28     14     2     1     85     44     104     55     1.13     1.00     36300       28     14     2     1     80     46     106     55     1.17     1.10     36500       28     14     2     1     80     46     106     55     1.17     1.10     36500       29     14     2     1     80     46     106     55     1.17     1.10     35000       27     14     2     1 <t< td=""><td></td><th>2</th><td>4</td><td></td><td>: =</td><td></td><td>-</td><td>2</td><td>4</td><td>100</td><td>8</td><td></td><td></td><td>19</td><td></td><td>6</td><td></td><td>37400</td><td>16965</td></t<>		2	4		: =		-	2	4	100	8			19		6		37400	16965
27     14     2     1     87     45     166     55     1.16     1.09     37300       26     13     2     1     87     45     166     55     1.16     1.09     35300       25     13     2     1     85     46     165     54     1.16     1.19     36500       25     13     2     1     86     49     165     54     1.14     1.19     36500       28     14     2     1     85     44     164     53     1.13     1.09     37700       28     14     2     1     85     44     164     53     1.17     1.19     36500       28     14     2     1     85     44     164     53     1.13     1.90     37700       28     14     2     1     80     46     166     55     1.17     1.19     36500       28     14     2     1     80     46     166     55     1.17     1.16     35600       27     14     2     1     80     46     164     53     1.15     1.16     35900       27     14     2     1     <		2	Ŧ		-		_	5	4	=	52			1.21		1.00		34000	15422
26         13         2         1         87         45         196         55         1.16         1.99         37396           26         13         2         1         95         49         195         54         1.16         1.19         36596           25         13         2         1         86         49         195         54         1.14         1.19         36596           25         13         2         1         86         49         105         54         1.14         1.19         36596           28         14         2         1         85         44         104         55         1.17         1.09         37709           28         14         2         1         86         46         106         55         1.13         1.09         37709           28         14         2         1         80         46         106         55         1.13         1.09         37709           28         14         2         1         80         46         106         55         1.11         1.19         36500           27         14         2         1 <td>•</td> <th>2</th> <td>'n</td> <td></td> <td>7</td> <td></td> <td>-</td> <td></td> <td></td> <td>106</td> <td>22</td> <td></td> <td></td> <td>1.20</td> <td></td> <td>1.10</td> <td></td> <td>37200</td> <td>16874</td>	•	2	'n		7		-			106	22			1.20		1.10		37200	16874
26     13     2     1     95     49     105     54     1.16     1.10     36960       25     13     2     1     69     46     105     54     1.14     1.10     36700       25     13     2     1     66     55     1.14     1.16     36500       28     14     2     1     66     44     105     54     1.17     1.09     37300       28     14     2     1     60     46     106     55     1.13     1.09     37700       28     14     2     1     60     46     106     55     1.17     1.19     3680       28     14     2     1     60     46     106     55     1.17     1.10     3680       28     14     2     1     80     46     106     54     1.17     1.16     36500       27     14     2     1     80     46     104     53     1.18     1.16     35900       27     14     2     1     80     46     104     53     1.20     1.20     1.20     1.20		2	4		5		-	87	\$	<b>5</b>	22			1.10		<b>8</b> .		37300	16919
25     13     2     1     89     46     105     54     1.16     1.19     36700       25     13     2     1     64     43     106     55     1.14     1.90     37400       25     13     2     1     6     49     105     54     1.16     1.90     36500       28     14     2     1     96     46     106     55     1.13     1.09     37700       28     14     2     1     90     46     106     55     1.17     1.19     36800       28     14     2     1     80     46     106     55     1.17     1.10     36800       27     14     2     1     80     46     106     53     1.15     1.16     35900       27     14     2     1     80     46     104     53     1.20     1.20     1.20     1.20		2	₹	•	2	_	-	<b>6</b>	ş	105	2			1.10		- 0 <b>0</b>		36966	16738
25     13     2     1     84     43     106     55     1.14     1.09     37400       25     13     2     1     86     49     105     54     1.14     1.19     36500       28     14     2     1     85     44     104     55     1.13     1.09     35300       28     14     2     1     80     46     106     55     1.13     1.09     35300       28     14     2     1     80     46     106     55     1.17     1.19     36800       27     14     2     1     80     46     104     53     1.15     1.16     35900       27     14     2     1     80     46     104     53     1.20     1.20     1.20     1.20	2 97	1	2		2	-	-	8	\$	105	\$			1.16		1.10		36700	16647
25     13     2     1     96     49     105     54     1     <	<b>3</b> 6	2	₹		5 5	-	-	ž	3	106	S			<b>*</b> :		<del>-</del>		37400	16965
28         15         3         2         86         44         165         54         11.16         .90         36400           28         14         2         1         85         49         167         55         11.17         1.09         37300           28         14         2         1         90         46         106         55         11.19         1.00         37700           28         14         2         1         90         46         105         54         11.17         1.10         35600           27         14         2         1         80         46         104         53         1.18         1.10         35900           27         14         2         1         80         46         104         53         1.20         1.20         35100	<b>3</b>	<b>*</b>	₹		5		-	9	6	105	<b>5</b>			1.1		1.10		36500	16556
28 14 2 1 85 49 167 55 1.17 1.06 37866 28 14 2 1 85 44 164 53 1.13 1.09 3.6369 28 14 2 1 86 46 166 55 1.19 .80 37786 28 14 2 1 89 46 165 54 1.15 1.16 3.6569 27 14 2 1 89 46 164 53 1.20 1.20 1.20 35196	200	2	Ŧ		5	-	2	8	ŧ	105	<b>5</b>			1.16		8.		36400	16511
28 14     2 1 85 44 164 53     1.13     1.00     36306       28 14     2 1 96 46 166 55     1.19     .80     37706       28 14     2 1 89 46 165 54     1.17     1.19     36809       28 14     2 1 91 47 165 54     1.15     1.16     3550       27 14     2 1 89 46 164 53     1.20     1.20     1.20     36106	4 97	7	3		7		<u>,,,</u>	<b>6</b>	9	107	55			1.17		<b>8</b> .		37800	17146
28 14     2 1     96 46 166 55     1.19     .86     37786       28 14     2 1     89 46 165 54     1.17     1.19     36869       28 14     2 1     91 47 165 54     1.15     1.16     36589       27 14     2 1     89 46 164 53     1.26     1.26     1.29     1.29     36186	2	2	₹		<u> </u>	_	-	8	ŧ	<u>\$</u>	S			1.13		- 90		36300	16466
28 14     2     1     89 46 105 54     1.17     1.19     36800       28 14     2     1     91 47 105 54     1.15     1.10     36500       27 14     2     1     89 46 104 53     1.20     1.20     1.20     1.20     36100	2 96	2	3		7		-	3	\$	106	35			1.19		8		37700	17101
28 14     2     1     91     47     165     54     104     53     1     118     1     10     3590       27     14     2     1     89     46     104     53     1     1     20     1     1     2     1     1     30     36     1     30     1     30     1     30     1     30     30     1     30     30     1     30     30     1     30	38	2	Ŧ	•	7		-	8	9	105	ž			1.17		1.10		36800	16692
27 14 2 1 85 44 164 53 1.18 1.19 35966 27 14 2 1 89 46 164 53 1.29 1.29 1.29 36166	2 83	2	4		=======================================		-	5	47	105	<b>5</b>			1.15		1.10		36500	16556
27 14 2 1 89 46 104 53 1.20 1.20 1.20 36100	96 2	2	Ŧ	•	-		-	2	ŧ	104	S			1.18		1.10		35900	16284
	88	2	2	•	<u>-</u>		-	8	4	10	53			1.20		1.20	1.28		16375

WEIGHT		×	2	16194	16057	16012	16194	16857	15921		36	CB/CI	1681	15695	15558	16311	15558	15466	16375	15649	16103	16012	17464	15649	15649	16466	16375	16420	17262		16284	16428	17055	16148	16738	16556	16602	16556	16602	16602	16511
*		r <sub>B</sub> S	5	35700	35486	35300	35700	35400	35100		90000	2000	35,200	34600	34300	36400	34388	34100	36100	34588	35500	35300	38588	34500	34500	36300	36198	36200	20100	900/5	35000	1678A	37600	35600	36900	36500	36600	36500	36600	36600	36400
LIFT	77		9						<b>3</b> .						8							- 90						<b>8</b>													<b>-</b>
LIFT	5		5	3.	8	<b>3</b>	1.10	8	2	- ·		B 3	2	8	8	8.	<b>8</b> .	<b>8</b>	1.20	1.10	<b>8</b> .	<b>8</b> .	<b>3</b> .	8	<b>8</b>		<b>2</b>	<b>8</b>	<b>8</b>	B :	-	2	1.20	1.10	-:	1.20	1.1	1.20	8	<b>2</b> .	<b>.</b>
\$	<b>*</b> <b>9</b> <sub>5</sub>		11																																						
KVPA	2		2	1.1	1.20	1.17	1.13	1.24	1.16	,	7.		7	9	1.19	1.23	1.13	-:-	1.27	1.18	1.18	 	<del>-</del> -	=:	1.17	1.2	<u>*</u>	1.21	2 :				1.17	1.27	1.10	1.21	1.20	1.21	1.21	1.22	1.18
V.dSA		¥ S	5																																						
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VPAMIN		¥	13					2 3			7 5						22	52	3	_										_	3 2					20	2		<b>3</b>	3	2
>		3	12	-	3	163	104	163	3	3	79.	70	3 5	182	101	105	101	<u>=</u>	<u>=</u>	102	163	163	168	102	102	104	104	<b>6</b>	/01	0			100	163	105	105	105	105	105	105	105
VEOR		\$	=	Ŧ	3	+	4	3	\$	\$ :	<b>?</b> :	<b>?</b> :	? 9	;	\$	\$		<b>‡</b>	3	\$	\$	3	‡	\$	9	<b>4</b>	7	3	2 :	? ;	? {	2	\$	‡	‡	45	7	4	Ŧ	42	\$
>		3	=	2	6	92	9	113	6	2 :	? 6	: ;	` <b>'</b>	2	6	3		78	163	3	2	8	2	2	8	6	8	2	5	2		, ×	2 2	9	2	83	79	5	2	5	11
	PEDP.	Ş	•	10	so.	•	n	5	<b>1</b> 0	<b>5</b> 0 1	n •	n =	n e	<b>4</b> 7	~	7	~	n	n	~	n	~	n	7	~	~	N	~	N (	N .	? <b>r</b>	, ,	מי	~	n	~	n	n	רי	n	~
13. •	2	₫	•	•	=	=	=	=	=	2 :	2 :	2 :	2 5	=	*	'n	40	*0	80	'n	40	'n	•	•	•	~	~	~	יי	? (	•	•	•	•	•	•	•	•	•	•	~
WIND-VEL	PAR.	\$	^	2	2	2	2	2	2	2:	2 :	2 :	2 =	2	=	<b>±</b>	<b>±</b>	<u>*</u>	<b>±</b>	<b>±</b>	<b>±</b>	<b>±</b>	=	2	2	12	17	<u>_</u>	<u>-</u> :	<u> </u>	÷ :	: =	2 2	=	•	=	•	2	<b>e</b>	2	ç
	٤	₫	•	*	2	<b>78</b>	<b>79</b>	<b>5</b>	2	2	8 3	9 8	, 5	2	2	8	8	28	2	8	2	2	32	2	22	3	2	3	3:	3;	\$ >	;	3	3	8	3	90	3	2	3	33
VE-FILM		\$	•	\$	3	7	ţ	25	7	<b>?</b> :	? ;	; ;	? 9	9	4	5	Į	<b>\$</b>	3	+1	7	\$	<b>\$</b>	42	<b>4</b>	7	Į	7	7 :	<b>;</b> ;	;	; ;	<b>.</b>	2	<b>\$</b>	47	\$	4	47	+	‡
Ţ X		\$	•	I	2	I	=	102	2	<b>3</b> :	8 :	8 2	3	2	2	3	3	6	Ĭ	2	Z	2	3	5	2	Z	2	2	2 :	5 8	2 2	3 2	3	2	2	5	2	=	=	<b>6</b>	2
4	_	\$	7	=	3	3	3	3	5	3	8 5	8 9	3	2	2	3	2	20	3	3	3	3	62	3	=	3	5	3	3 :	:	3	1 2	3	6	3	2	3	2	5	3	3
MAN	2	₫	~	=======================================	124	2	117	128	=	= :	• :	:	2 2	121	120	128	1:	=======================================	132	120	122	123	120	21	_ 	127	=	126	126	* 5		Š	124	5	124	127	126	127	127	128	123
8	Š.		•	<b>2</b> 2	3	2	Ī	77	;	3 :		} ;	3	3	\$	<b>\$</b>	\$	į	<b>†</b>	\$	467	<b>9</b>	3	652	3	3	3	987	3		8	3	8	9	892	982	988	207	200	8	ŧ

DAY LANDINGS

USS ENTERPRISE (CV 15)

LANDING DATA - MODEL S-3

			WEING		- 4	DATA - MODEL 5-3	3		Š	S ENTE	RPRIS	USS ENTERPRISE (CVN-62,	, 19°			DAY LANDINGS	NDINGS		
997	M	4.	VE-F1U	3	-	WIND-VEL	<b>ដ</b>		VEOR		VPAMIN		V.dSA	KVPA	\$	LIFT	LIFT	-	WEIGHT
8	2	_			P.	÷	PERP.							3	<b>∀</b> 35	5	Ŧ		
	₹	\$	2	Ş	2	<u>-</u>	<b>3</b> ₹	₹ \$	N WS		KN M/S	N X	E A	v				S	Š Š
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•	128	3	=	4	37	2	n	28	4	÷	95	•		1.22	ىم	8.		36500	16556
2	123	3	2	‡	2	•	n	2 82	~	7	95 5	*		1.1		<b>8</b>		36600	16602
2	25	3 :	2 :	<b>?</b>	5	<u>.</u>	<b>~</b> (	2	T (	= : 1 :		n :		1.2		2 :		36300	16466
į	2 :	3 :	2 :	<b>?</b> :	5	<u>.</u>	r) r	8 :				n •		1.28	• -	8 :		35486	16057
2		: 2	2	<b>;</b> 4	3 3	2 2	2 17	2 2	•			) M		1.26		1.20	-		16012
2	126	2	2		こち	<u>_</u>	, ,,	200	•	2		, <b>2</b> 2		1.23		2		35000	15876
į	124	3	2	<b>\$</b>	これ	7	n	2 85	4	= 1		n		1.10	_	1.00		35900	16284
-	122	3	3	<b>3</b> i	ま	7	<b>n</b>	<b>2</b>	•			<b>n</b>		1.18	_	1.10		35900	16284
= :	2 3	3 :	2 :	Ç:	٠ ۲		, ,	~ ;	•	2 :		n,		1.21		1.10		36666	16336
	3 5	3 5	3		\$ >	: <u>:</u>	? ?	7 6			20.00	<b>^</b>		7. 10 9. 40	• -	<b>8 8</b>		33000	1651
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110	123	3	2	9	ー	2	n		Ī	2		n		1.20		8.		35500	16103
918	129	3	2	2	ス	7	,,	2	•	15 21	103 53	n		1.25		8.		35500	16163
=	=	3	95	42	ス	7	n	2	•	7		n		1.13	_	1.20			16012
929	124	3	2	7		2	2	2				n :		9.		1. T	<b>8</b> .		16420
26	2	3 3			3:	<u>- !</u>	. ·	2 6		_	162 52			1.27		<b>8</b> 3		34460	10001
222	22.	3 8	2 2				 P 10			9 5		) #1		1.12		1.10		35000	15876
924	3	5	_			2	•	28		2		n		1.26		1.10		35300	16012
976	=	5		•		17	•	28	•	5 5	•	2		1.16		1.10		35000	15876
927	2	3				7	•	50	•	2		~		1.26		- 9		34588	15649
959	115	3				2:		90	•			n		1.12		<b>8</b> .	•	35000	15876
27.0	3 5	2 2	_		- 3 =	<u>.</u> •	• <b>-</b>			: 5	70 E01	7 6		1.22		1.20	P		17600
1121	126	3			Ī	2	•	200	-	Ť				1.16		1.10	1.10		17872
1123	123	3			_	5	•	2		÷		•		1.1		8.			17696
1124	124	į	2		_	2	<b>.</b>	2		_	-	•		<b>*</b>		<b>8</b> .		39500	17917
128	= :	5 ;			- ,	2 9	~ .	<b>*</b>						 	_	<b>8</b> 8		39588	71871
112/	122	3 :				*	, ,	5 3		- '				1.1		<u> </u>		40004	****
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7	124	3			7 7 7	2	N	5				•		1.15		2		39000	17696
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25.	125	3			27	<u>*</u>	~	<u>=</u>	<b>E</b>	11	187 55	'n		1.17		1.10		37900	17191
28	120	62			27 -1	<u>*</u>	C1	96		_		•		1.15		- 8		36896	16692
25	11	3			27	<b>±</b>	~					so i		1.1		1.10		37400	16965
1150	110	2			27	<u>*</u>	~	- 65		¥ \$	107 55	<b>5</b>		= -		<b>2</b>		38200	17325

			3	LANDING DA	TA -	DATA – MODEL S-3	3		5	SS EN		USS ENTERPRISE (CVN-6.	₹	•			DAY LANDINGS	DINGS			
8	\$	WA		VE-FILM		WIND-VEL	Ę		VEOR	8	VPAMIN	×	V.dSA	<	KWPA	₹	LIFT	111		WEIGHT	
ğ.	F	2			<u>,</u>	PAR.	<b>2</b> 6	ď							Z	٧.	5	4.6			
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-	~	n	•	•	•	^	•	•	•	=	12	5	<u>*</u>	5	9	17	6	<b>5</b>	<b>59</b>	21	
3	122	3	8	\$	27	<b>±</b>	~	_	ž	\$	107	25			1.14		<b>8</b> :		38166	17282	
=	127	3	2	5	8	<b>±</b>	~	_	<u>=</u>	25	107	33			1.19		-:-		37800	17146	
162	128	3	Ĭ	5	28	<b>:</b>	~	-	98	<b>6</b>	104	S			1.23		1.10		36300	16466	
<b>3</b>	124	3	2	<b>?</b> :	23	<b>±</b> :	<b>7</b>	_	2 :	<b>=</b> :	101	25			1.23		8		34100	15468	
3 5	2 2	3 3	3 3	<b>?</b>	2 2	5 t			2 4	<b>?</b> ;	197	ន្តម			<u>-</u> :-		8.		27986	17101	
2	72	3	8	; ;	3 8	. <del>.</del>			3 2	<b>\$</b>	<u> </u>	3 23			. 13				36300	16466	
3	5	2	Z	<b>‡</b>	2	5	-	-	2	<b>\$</b>	96	8 8			1.15		2		37600	17055	
346	117	3	3	2	2	12	~	_	8	5	107	55			1.69		<b>1</b> .00		35000	17237	
247	122	3	8	5	ล	12	~	-	8	<b>0</b>	107	55			1.14		1.20		38200	17328	
95	=	5	8	2	ຊ	12	~	-	88	<b>\$</b>	106	55			1.11		- 8 -			17010	
3	= 1	3	2	<b>?</b>	7	=	~	_	ž	<b>?</b> ;	107	55			8		8	8.	•	17418	
3	=	5	6	3	7	= :	~	_	2	<u>ت</u> ا	= :	57			8		<b>1</b> .10		40100	18189	
5	= :	8	3	<b>?</b> :	<b>7</b>	= :	~ (	<b>-</b> •	5	<b>;</b>	<b>2</b> :	٠ د د			1.07		1.10		37690	17055	
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3 3	5	3 2	<b>B</b> 8	<u>.</u>	5 5	= =	<b>,</b>		3 1	3 2	) <u>4</u>	n v			2:-				3/200	17121	
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1357	2	3	5	Š	7	12	~	_	2	2	=	57			1.17		86.		4000	18144	
256	123	3	8	2	7	12	~	_	8	9	165	\$			1.17		1.10		37000	16783	
330	23	į	≣	25	7	12	~	_	115	8	167	55			1.18		- 90.		37800	17146	
990	10	5	\$	<b>9</b> ;	<b>*</b>	7	~	_	2	<b>9</b> (	107	<b>S</b>			1.1		1.10		37900	17191	
	2			3 :	* :	2 :	N (			25	601	8 1			5.18		9 6		20000	17963	
	128	à <b>3</b>	<b>i</b>	t 3	; ;	2 2	N 6		<b>2</b> 6	\$ <b>\$</b>	9 6	0 <b>1</b> 0					9 6		39586	17917	
795	128	3	Ĭ	3	7	7	~	<b>,</b>	8	2	106	55			1.21		1.10		37500	17010	
365	200	62	2	<b>\$</b>	7	12	~	_	93	47	106	55			1.13		1.66		37700	17101	
286	126	2	102	22	*	12	~	-	2	<b>\$</b>	109	26			1.16		1.20		39400	17872	
1367	23	3	8	<u>.</u>	2	2	~	_	8	<b>9</b>	107	55			5.15		1.10	•		17237	
200	2	2	2	<b>?</b>	*	2	~	_	92	47	105	<b>4</b>			<b>*</b> :		- 10 - 10	1.10		16647	
1376	2	62	8	<b>?</b> ;	*	7	•	•	2	<b>.</b>	105	<b>.</b>			<b>*</b> :		- 6		36700	16647	
1377	2	95	6	3	7	7	•	•	2	6	105	<b>7</b>			* :		99.		37666	16783	
1378	=	5	9	<b>?</b>	7	7	•	•	1	į	105	ż.			51.7		. Je		26800	16692	
<b>78</b>	23	3	2	5	23	~	•	•	8	8	105	<b>5</b>			1.17		80	;		16511	
<b>100</b>	112	8	3	7	2	<b>±</b>	•	•	8	<b>\$</b>	104	53			98 :		- 00	- 10		16194	
302	15	<b>9</b>	92	<b>\$</b>	2	<b>±</b> :	•	•	2	\$	<b>1</b> 0	: :			1.10		- 00		36100	16375	
200	5	25	2 :	<b>\$</b> (	2 3	<b>±</b> ;	•	• •	į	•	<b>Ž</b>	3 :			<u>.</u> .		8.		36300	16466	
	122	3 8	\$ 6	<b>P</b> 4	2 5	<b>:</b> :	•	<b>.</b>	<b>.</b>	₽ ₹	* *	3 5			<u> </u>				15000	16466	
<u> </u>	2		ò	D	9	£	Þ	•	2	-	<u> </u>	2			:				2000	1070	

			3		- YI	NG DATA - MODEL S-3	3		<i></i>	USS ENTERPRISE (CVN-65	TERPR	1SE (	CANTE	eg.			DAY LANDINGS	DINGS			
9 3	X		VE-F	3		WIND-VEL	VEL		¥	VEOR	Š	VPANIS	V.dSA	ج	KWPA	\$	111	LIFT	3M	WEIGHT	
ě	5				ã	PA.	400	<b>9</b> .							3	<b>∀</b>	5	7			
	\$	\$	₫	Ş	₫	Ş	₫	\$	\$	¥	3	R K	\$	<b>¥</b>					S	Ã	
-	~	•	•	6	•	7	•	•	•	=	12	2	<b>±</b>	5	5	11	6	9	<b>50</b>	2	
1517		5	8	<b>(</b> +	<b>56</b>	2	~	_	8	2	9	Š			. 69		1.0		39386	17826	
1524	=	5	š	7	74	12	~	-	87	<b>.</b>	109	26			. 88		1.10		39300	17626	
1527	123	3	2	5	2	12	~	-	85	47	168	8			<b>-</b>		1.1		38700	17554	
25.5	=	5	3	•	2	12	~	-	8	<b>4</b>	107	55			1.12		<b>8</b> .		37900	17191	
999	124	3	8	7	z	17	•	m	3	3	107	55			1.16		1.20		37900	17191	

9			AIRCRAFT	••	KING S	PEED A	SINKING SPEED AT TOUCHDOWN	N			CL 10E	GLIDE PATH ANGLE AT TD	NGLE A	OT T	WHEEL HEIGHT	EIGHT	HOOK HEIGHT	1CH1
2	NOSE	¥	PORT	<b>4</b>	S	STBO	AVC		FREE-FLICHT	E E	8	<b>8</b>	<b>8</b>	>	OVER RAMP	3	OVER RAMP	ag .
	\$	\$	2	\$	5	Ş	Ş	<b>₹</b>	Ş	Ş	DEC	3	930	3	FT	3	E	3
2	2	74	22	<b>38</b>	72	28	20	8	5	32	S	ħ	35	36	37	25	80	•
35	6.2	 •	6.2	<b>.</b> .	*:	2.0	<b>6</b>	<b>a</b> .			4.5	990	2.4	140.	12.8	a.v	10.1	7.7
3	9.	2.1	7.8	7.4	7.0	2.1	7.4	2.3			5.9	.050	2.2	. 036	16.6	5.1	14.6	4.5
787	<b>3.5</b>	1.7	5.0	<b>.</b>	7.7	2.3	9.9	7.9			2.5	. 039	<del>.</del>	. 032	12.2	3.7	<b>8</b> .	9.8
376	-	<b>.</b>	<b>9</b> .5	<b>5.8</b>	9.7	2.5	<b>8</b> .5	2.5			2.5	¥0.	4.5	.043	14.2	<b>4</b> .3	<b>9.</b> E	3.0
77	7.	7.7	7.0	7.4	7.5	2.3	7.7	2.3			2.1	. 637	2.3	.041	13.4	<del>-</del>	11.2	4.0
372	<b>9</b> .	2.1	7.0	7.4	<b>.</b>	2.1	7.3	2.5			2.8	949	7.4	.042	14.6	÷.5	12.0	3.7
22	- 0	2.5	7.0	2.1	6.7	5.0	æ.	2.1			2.1	.637	<b>a</b> :	. 634	14.3	<b>+</b> :	12.2	7.5
*		5.0	<b>*</b> (	7. •	*.	2.3	œ .	- 1			2.7	.047	2.1	.637	- : <b>-</b> :	n. •	e (	٠ • •
775	· •		, e		, e	- c						942		940	0 -	o •	7.5	0 · v
378		•		. 6	7.7	7	. 60	2.5			2.0	.035	2.6	.045	12.9	9.0	9.9	3.2
370	5.5	-	8.0	1.7	5.1	-		9.			a. -	.034	9.	.028	<b>1.</b>	3.5	-	2.8
3	7.1	7.7	7.3	2.5	7.6	2.3	7.1	2.2			2.8	.048	<b>5</b> .0	. 035	17.0	5.5	14.8	4.5
Š	<b>9</b> .	1.7	8	<b>.</b>	5.5	•. •	5.6	1.7			2.5	.044	9.	.027	14.4	<b>+</b> .+	12.1	3.7
382	3.8	1.2	9. 9.	<b>-</b>	6.7	<b>5</b> .	6.7	7.0			5.9	. 050	2.1	. 637	14.6	4.5	12.0	3.7
22	7.1	7.7	-:	5.5	7.0	2.7	9.0	7.4			2.3	. 040	2.5	. 038	14.4	<b>+</b> .	12.2	3.7
3	9.7	2.7	• •	٠. ت.	<b>9</b> .	<b>5.8</b>	10.2	ر. د.			3.0	.053	5.8	.051	13.6	<del>-</del> -	10.7	n.n
800	<b>9.</b> 0	2.8	<b>.</b> .	3.3	9.7	<b>5.8</b>	10.3	J. 1			2.6	. 045	J. 1	. 855	14.8	÷.5	12.8	0.0 0.0
60	7.4	2.5	7.0	<b>7.</b>	7.5	2.3	<b>6</b> .	7.4			2.8	.049	7.4	.042	14.5	<b>+</b> •	e :	۵. و
385	<b>9</b> .0	2.5	7.8	7.4	- :	2.5	٥.	7.4			3.2	.055	5. 9.	.046	15.1	<b>4</b>	12.7	a i
200	٠. ن	٠. د.	? •	5.0 6.0		2.5	- 6				2.7	828	2.3	.040	11.5	υ·.	<b>8</b> 0 (	2.7
	*:	2. c	 	 • .	9.6	2.3	D .	<b>7.</b>			9 Y	* S	7.7	BC0.		- •	0. e	2.5
0 0		7	- •			n r	7 .	÷ ;			. r	• •	- 0	759.		o •		» «
	, r						. «	, c				655		956	14.1	7	? =	9 7
980	6.2	•		3.2	7.4	2.3		2.7			9.0	.053	3.0	.057	15.2	<b>9</b> .	12.5	8.8
į	5.0	7. 9.	<b>9</b> .0	2.7	9.0	7.7	8.5	5.6					2.5	.043				
ŧ	5.7	1.7	3.2	•:	3.6	=	3.6	-:			2.4	.042	r	. 022	<b>+.</b> +	<b>*</b> .	11.7	3.6
<b>‡</b>	7.5	2.3	<b>.</b>	7.4	7.0	2.1	7.6	2.3			2.7	.047	2.7	.046	12.4	<b>6</b> 0	<b>6</b> .7	<b>9</b> .
\$	<b>9</b> .0	7.	7.2	7.7	6.3	<u>-</u>	<b>9</b> .	2.1			J. J	. 058	4.4	- 4	16.4	<b>.</b>	13.7	4.2
=	5.7	7.7	<b>.</b>	7.7	9. 9.	<b>.</b>	<b>†</b> .	<b>.</b>			7.4	. 042	2.3	.039		0.	<b>6</b>	9.
=	•	<b>9</b> .	<b>9</b> .0	<b>.</b>	5.3	<b>e</b> .	S.	<b>8</b> .			5.8	.051	7.	. 036	13.0	4.2	<b>-</b>	4.0
412	7.	7.7	7.5	7.5	7.5	7.7	7.1	2.5			2.8	. 648	2.6	.045	13.4	<del>-</del>	<b>-</b>	7.7
413	8.7	5.6	<b>†</b> .	•	9.0	2.1	9.0	5.0			2.7	.047	2.3	940	11.2	<b>→</b>	9.5	2.5
<b>‡</b>	<b>8</b> .	2.7	<b>.</b>	٠, ٠	<b>8</b> .7	9. 7.	7.0	7.8			3.5	.055	J. 5	.061	16.6	-	5.5	<b>-</b> '
<del>1</del> 2	7.4	2.3	<b>9</b> .	7.	7.7	2.3	7.3	7.7			2.7	.047	5.5	.044	14.1	<b>4</b> (	<b>9</b>	. S
10	7.7	2.3	7.7	7.4	7.0	2.1	7.5	2.3			J. 6	.062	2.7	.047	<b>18.6</b>	5.7	16.2	<b>.</b>
417	4.0	5.	4.2	 	5.3	-	<b>4</b> .8	5.5			2.5	446	7.7	.030	13.1	<b>4</b> (	10.2	- ·
423	<b>+</b> .	<u>.</u>	6.5	<b>7</b> .	6.5	<b>7</b>	<b>.</b>	<b>o</b> .	1		7. 9.	848	7.7	838	12.9	ص ا	5.5	3.2
2	5.7	1.7	<b>4</b> .0		4.5	<b>1.</b>	4.7	<b>+</b> :	4.7	<del>*</del> .	3.0	. 653	9.	.028	15.4	4.7	13.2	<b>0</b> .

		3	LANDING DATA		MODEL 5-3	7	5	SS ENTE	USS ENTERPRISE (CVN-6	CONFE				DAY CA	DAY LANDINGS			
9			AIRCRAFT	_	KING S	SINKING SPEED AT TOUCHDOWN	TOUCH	N			GLIDE PATH ANGLE AT TD	ATH A	GLE A	5	WHEEL HEIGHT	EIGHT	HOOK HEIGHT	IGHT
2	NOSE	SE	POR	<b>=</b>	ST	STBO	AVC		FREE-FLIGHT	ICHT		_	8		OVER RALP	<b>3</b>	OVER RAMP	d N
	2	Ş	\$	Ş	£	Ş	£/S	¥ s	Ş	S A	DEG	3	DEC	880	E	3	E	3
23	23	*	22	8	23	<b>58</b>	29	2	5	32	33	Ť	33	82	33	23	82	6
432	9.3	2.8	5.3	2.8		2.8	<b>.</b>	2.9		-,	3.5	190	•	.059	17.3	5.3	14.7	÷.5
3		2.8	<b>+</b> . •	3.2	9.5	2.9	<b>a</b>	٠, ٠		<b>.</b>	٠	999	٠.	.066	17.5	5.2	15.1	•
2 3			n.	<u>.</u> (		- r	• •			r, r		.055		.637	a :	÷.	12.3	7.7
3		, ,		2.6		, r	- K	9.7		3 F.		96.7 96.7	• K	929	13.6	4 4 5 0	12.6	10 o
1	7.3	2.2	•	2.7	9.5	. 6	9.0	9.7	9.0	2.8		.059			15.3		12.3	
1	9.0	<b>5</b> .0	4.7	<b>*</b> :-	7.2	2.2	6.3	<u>.</u>				. 059	_		16.6	5.1	13.4	<del>-</del>
1	8.8	9.0	10.5	3.2	<b>†</b> .	3.2	10.5	3.2		•	•	978			19.2	<b>3.9</b>	16.2	5.0
3	<b>→</b> .	ر د . د	12.1	2.7	1.2	4.0	11.7	٠. م		•	-	.077			21.3	<b>9</b>	18.3	5.6
5	<b>.</b>	2.7	7.0	5.5	7.0	2.3	•	7.6		r, ,	•	957			13.1	<b>.</b>	. e. :	ر ا
70	•	7.0	٠ •	P (		7 ·	•	D . C		,	•	909			16.6	<b>.</b>	13.2	<b>4</b> (
2 4	- v	. v		7.7	7.0	۲. د. د		9 9	a	, c	- •		9 d 7 r	. e	D •		12.0	۲.,
3 5	, r					, c			•		•	649				• •	D . C	• •
3	12.3		12.5		12.1		12.3	7.0 7.0		,				920	? <u>*</u>	•	c.7	٠. د
\$	7.7	2.3	4.0	-		<b>a</b> .	4.9	<b>a</b>		<b>P</b> )	•	953		943	12.8	a.n	7.6	3.0
465	4.0	7.6	<b>.</b>	2.7	9.5			2.8		~	60	948		.043	16.7	5.1	14.7	4.5
<b>166</b>	9.0	5.6	8.2	2.5	8.3		8.2	2.5		~	٠	957		.046	16.7	5.1	14.4	+
467	6.7	7.7	7.8	2.4	<b>9</b> .1	2.5	9.0	7.4			2.7	047		. 039	15.6	<b>4</b> .8	13.3	<b>.</b>
460	8.5	<b>.</b>	7.6	2.3	<b>.</b>	<u>.</u>	<b>9</b> .9	2.1	8.9	2.1	•	649	-	. 941	14.7	÷.	12.4	ري 8.0
5			7.7		<b>16.</b> 2			6. L		•		.073		.66	- ·	n. •		 
70	 	7.7		2.0		5. c	. o	 		<b>.</b>	? ◀	9.49 9.49	, r	6 4 6 5 4 6	+ a	• «	• •	o
3		. 6	7.6	2.3	7.8		6.2	4.		מי נ	3.7	964	2.5		13.8	4.5	=	4.0
2	10.7	3.5	0.7	9.	10.3	_	10.0	٦. م		<b>P</b> 3		.067	-		20.0	6.1	17.3	5.3
997	•	<b>5</b> .0	<b>†</b> .	<u>.</u>	6.5		<b>†</b> .	2.0	4.9	1.9	2.7	.047			12.8	a. n	10.2	3.1
3	•	7.7	6.5	5.6	8.5	2.8	G. 9	2.7		<b>.</b>		. 963	-		14.8	4 ·	<b>8</b> . :	9.0
	- •	, v		, c		7.7	» r	, , , ,		NF	8. r	100.		948 848	 	· •	2.0	0 0 7 F
3	9 00	9.0	10.2	-	10.2		10.2			• ▼	9 04	986			21.7		6.0	5.7
8	4.	7.	0.9	2.1	5.7		4.0	•		~~	2.5	944			14.2	4.4	7.	4.0
300	8.8	2.7	4.9	2.0	5.0	<b>.</b>	6.2	<b>9</b> .		~	·	. 968	Ī		14.3	<b>+</b> .+	1.5	3.5
188	9.0	5.6	8.0	2.7	7.0	2.1	8.2	2.5		P	3.7	965	·		15.7	4.8	13.0	<b>4</b> .
882	7.6	2.3	7.2	2.5	7.	2.1	7.1	2.5		•	·	.070	-	.046	16.9	5.2	14.0	4.4
895	5.0 0.0	<b>e</b> .	<b>6</b> .	- .5	5.	 5.	9.	 		~,	Ī	999	-		16.5	•	13.7	4.5
988	<b>0</b> .	2.7	-	<b>5.8</b>	S	8.8	2.0	2.8		<b>-</b> 3		.058	Ī		9.6		15.3	4.7
897	<b>9</b> .0	<b>5.8</b>	<b>-</b>	2.5	<b>8</b> 9	2.7	<b>→</b> .	5.6		•	•	982	2.0		20.3	6.2	17.7	4.
888	7.8	2.4	9.0	2.7	7.7	2.4	4.6	2.8		P3 (	8.8	952	2.0	951	16.8	 	14.0	4 i
888	4.	2.5	7.7	<b>7.</b>	8.5	2.5	7.7	7.7	•	,	ر. د	961	2.8	050	5.5	<b>+</b> ·	a :	9.0
•	7.4	7.7	6.7	2.0	7.1	2.1		2.0	<b>.</b>	<b>8</b> .	· -:	924	7. 9.	635	16.7	<u>.</u> م	13.d	4.2

NOSE	PORT	E	S180	8	AVG		FREE-FLIGHT	IGHT.	<b>10</b>	•	8	>	OVER RAMP	RAMP	OVER RALLP	d the	
Ş	S	\$	2	<b>₹</b>	٤/٤	Ş	٤/٤	¥	DEG	3	930	3	E	*	E	2	
*	8	28	23	<b>58</b>	58	8	5	32	3	*	35	36	37	23	8	9	
2.7	9.9	2.7	. O	2.8	9.5	2.8			4.6	. 059	3.4	. 969	18.1	5.5	15.6	4.7	
<b>5.8</b>	11.2	4.6	8.8	2.7	19.1	3.1			4.3	.075	4.2	.073	14.0	4.4	11.4	3.5	
<b>7.6</b>	9.0	5.6	9.3	2.5	8.3	2.5			2.7	. 046	2.7	946	15.4	4.7	12.7	3.8	
3.5	11.2	4.6	9.5	2.8	10.2	3.1			3.4	.058	9.0	.053	15.3	4.7	12.6	a.b	
7.4	7.7	ė	3.3	•:	7.8	œ.	3.1	<b>.</b>	3.0	. 052	-:	.020	14.2	4.4	10.7	3.3	
3.2	<b>.</b>	J. 7	10.2	J. 1	10.2	J. 1			4.7	. 681	3.2	.056	20.7	6.3	18.0	5.5	
2.7	<b>1.</b> 4	ا ا ا	<b>6</b>	5.8 6.6	10.5	3.5			4.6	929	3.7	.064	<b>4</b> .	ص ص	16.5	٠. ف	
9 .	* •	, v	<b>8</b> .5	5.5	ø ;	7.e			ы. 6. с	.657	9.5	. 846 8.	16.3	e .	4.5	- c	
; c		• •	•		? •	• •				0/0		646	0.07	- •	- :	7.6	
		,,		, c		 			0 <b>-</b>	45.0		2.5	. ¥	9 6			
-		5.5	•	2.8	. 2	2.6			-	1/0	3.2	926	21.0	*	18.2	- 40	
2.8	10.2			2.5	•	2.7			3.6	.062	3.2	.056	20.7	<b>6</b> .0	17.9	4.0	
7.4	6.7	2.0	8.8	9.	6.5	2.0				.049	2.3	.039	14.6	4.5	11.5	3.5	
2.8	<u>-</u>	2.8	4.0	2.6	<b>0</b> .0	2.7				.053	ري 9.5	. 052	15.7	4.8	13.1	<b>6.</b>	
2.5	•	2.7	<b>19.</b>	3.2	9.7	5.8				. 691	<b>+</b>	.071	16.4	5.1	13.9	4.2	
2.3	<b>.</b>	2.1	5.4	<b>9</b> .	•.	<b>-</b> .6	6.3	<b>a</b> :		944	<u>:</u>	. 629	13.7	4.5	10.7	<b>3.3</b>	
3.8	12.8	3.0	12.3	3.7	12.4	3.8				.084	<b>+</b> . <b>+</b>	.076	20.3	6.2	17.7	4.6	
۵.	 	٧.	10.0	2.2	10.5	3.5			÷:	. 072	u.5	.061	18.8	5.7	16.2	a. +	
7.7	5.5	1.7	<b>.</b>	<u>.</u>	<b>8</b> .8	<b>9</b> .			3.2	. 056	2.0	.635	19.0	S. 60	16.0	o. †	
2.5	7.2	2.5	9.9	7.0	<b>†</b> .	<b>a</b> .				. 051	2.1	937	15.6	4.8	12.7	G.0	
	<b>o</b> (		-	7. 9.	<b>o</b> i	5.9				. 967	۵. و	, ,	20.8	n (	9.9	5.5	
7.7	9.6	2.3		7.7	7.4	2.5				900	9.6		• · ·	2.0	? !	* 0	
, c		, c	9 6	, c	B 6	, . • •	7 6	,	- 4	+ C - C - C - C - C - C - C - C - C - C	, c	946	. <del>.</del>	. ·	• - - - -	7.6	
	15.8		2.8				:	•		697	9.0	686	24.5	7.5	21.8	7.9	
9.0	10.0	3.2	16.6	3.2	9.0		e. =	3.3	3.6	. 062	3.0	.052	21.7	9.9	19.0	5.8	
2.7	<b>1.</b> *	3.5	11.5	3.5	11.2				3.5	.062	3.6	. 962	17.1	5.2	14.6	4.5	
2.7	•	2.7	9.6	<b>5.8</b>	9.0	2.8			3.8	990	J. 0	. 052	16.6	5.1	13.6	4.2	
2.8	9.7	٠. د.	7.6	0.0	<b>9</b> .	5.9			3.7	.065	J. J	.058	16.8	5.1	14.2	n. <del>4</del>	
2.5	<b>8</b> .0	2.7	<b>8</b> .5	7.6	9.0	2.7			2.5	.044	2.7	.047	13.2	<b>.</b>	10.8 8.9	n.	
ري 1.	13.8	4.7	13.5	<del>-</del>	3.0	4.5			•	170	. t	. 679	19.2	9. ·	16.5	0	
7.7	. s	2.3	9.5	2.3	7.7	7.4			2.4	- 4	2.4	.042	13.4 	<b>-</b> :	9. e	ы.	
3.2	1.2	4.0	<b>6</b> .7	ري •	<b>19</b> .4	3.2			3.5	. 060	3.3	. 058	12.1	3.7	o.	<b>7.</b>	
7.4	<b>9</b> .5	5.0	9.0	7.6	9.5	2.8			3.3	.057	J. 1	.054	15.3	4.7	12.2	3.7	
2.5	6.7	2.1	<b>8</b> .3	2.5	7.5	2.3			3.0	.052	2.8	.045	15.6	4.8	12.8	œ.	
2.7	9.7	 	7.3	2.2	8.7	2.6			3.9	.068	0.N	.052	14.2	<b>4.</b> 4	<b>+</b> :=	ر د ن	
J. 7	10.2	J. 7	10.0	3.3	10.5	3.2			3.8	.067	4.0	.059	17.4	5.3	15.0	<b>4</b> .6	
2.2	<b>9</b> .9	2.1	5.7	1.7	9.9	<b>5.0</b>			2.7	.047	2.1	. 036	17.2	5.5	14.7	<b>4</b> .5	
3.2	<b>0</b> .0	3.0	19.4	3.2	9.0	J. 0			J. 1	954	4.0	.020	18.0		14.6	÷.	
		4 4 6 5 6 7 6 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7			8.11.8.1.4.1.9.1.4.4.1.9.1.9.1.9.1.9.1.9.1.9.1	8.9 9.7 1.2 2.7 2.7 2.7 2.7 2.7 2.7 2.7 2	8.9 2.7 8.5 2.9 8.2 2.9 8.2 2.4 8.9 2.7 8.3 2.4 8.9 2.7 8.3 2.7 8.3 2.4 8.9 2.7 8.3 2.4 8.9 2.7 8.3 2.4 8.9 2.7 8.3 2.4 8.9 2.2 2.8 10.1 3.1 11.4 2.9 8.2 2.8 10.2 2.9 11.4 2.9 8.2 2.9 11.4 2.9 8.2 2.9 11.4 2.9 8.2 2.9 11.4 2.9 8.2 2.9 11.4 2.9 8.2 2.9 11.4 2.9 8.2 2.9 11.4 2.9 8.2 2.9 11.4 2.9 8.9 2.7 7.2 8.9 2.7 7.2 8.9 2.7 7.2 8.9 2.7 7.2 8.9 2.7 7.2 8.9 2.7 7.2 8.9 2.7 7.2 8.9 2.7 7.2 8.9 2.9 7.2 8.9 2.9 7.2 8.9 2.9 7.2 8.9 2.9 7.2 8.9 2.9 7.2 8.9 8.9 2.9 7.2 8.9 8.9 2.9 7.2 8.9 8.9 2.9 7.2 8.9 8.9 2.9 7.2 8.9 8.9 8.9 8.9 8.9 8.9 8.9 8.9 8.9 8.9	8.9 2.7 8.5 2.9 8.2 1.1.2 2.4 8.9 2.7 18.1 3.1 18.1 1.2 3.4 8.9 2.7 18.2 2.8 8.2 2.7 18.1 3.1 18.1 1.2 2.8 8.2 2.7 18.1 3.1 18.1 1.1 1.2 2.8 8.2 2.8 2.8	8.9 2.7 8.5 2.9 8.2 2.8 8.2 2.8 8.2 2.8 8.2 2.4 8.9 2.7 10.1 3.1 10.2 3.4 8.9 2.7 10.1 3.1 10.2 3.4 8.2 2.5 8.3 2.7 10.1 3.1 10.2 2.8 8.2 2.8 8.3 2.3 10.4 3.1 10.2 2.8 10.2 2.8 10.2 2.8 10.2 3.1 10.4 2.9 8.2 2.8 10.2 2.8 10.2 2.9 11.4 2.9 8.2 2.8 10.2 2.9 11.4 2.9 8.2 2.8 10.2 2.9 11.4 2.9 8.7 2.9 8.7 2.9 8.7 2.9 8.1 2.8 8.7 2.9 8.7 2.9 8.1 2.8 8.4 2.9 2.7 2.9 8.1 2.8 8.4 2.9 2.7 2.9 8.1 2.8 8.4 2.9 2.7 2.9 8.1 2.8 8.4 2.9 2.9 2.9 2.9 2.9 2.9 2.9 2.9 2.9 2.9	11.2 3.4 8.9 2.7 10.1 3.1 8.6 2.6 8.2 2.8 8.3 2.3 1.0 1.0 3.4 8.9 1.2 2.9 8.2 2.8 8.3 2.8 8.3 2.8 1.2 3.1 10.2	11.2 3.4 8.5 2.9 8.2 2.8 1.1.2 3.1 1.8 2.7 16.1 2.1 11.2 3.4 8.8 2.7 16.1 2.1 11.2 3.4 8.8 2.7 16.1 2.1 11.2 3.4 8.8 2.7 16.1 2.1 16.2 2.7 16.1 2.1 16.2 2.7 16.1 2.1 16.2 2.7 16.1 2.1 16.2 2.7 16.1 2.1 16.2 2.7 16.2 2.1	8.9 2.7 8.5 2.9 8.2 2.8 3.4 .059 3.4 2.7 11.2 3.4 8.8 2.7 18.1 3.1 18.2 3.4 8.8 2.7 18.1 3.1 18.2 3.2 18.2 3.1	8.9 2.7 8.5 2.9 8.2 2.8 3.4 655 3.4 655 3.4 11.2 3.4 8.5 2.8 8.2 2.8 11.2 3.4 8.5 2.8 8.2 2.8 11.2 3.1 8.2 3.1 11.2 3.4 8.5 2.7 10.1 3.1 10.2 3.1 1	8.9         2.7         9.5         2.9         9.2         2.8           11.2         3.4         9.9         2.7         10.1         3.1         4.3         9.9         3.4         .069           11.2         3.4         9.9         2.7         11.0         3.4         .059         3.4         .069           11.2         3.1         10.2         3.1         1.0         3.6         .052         11.1         .08           11.1         3.1         10.2         3.1         1.0         3.6         .052         11.1         .08         .05         1.0         .08         .05         1.0         .06         .05         1.1         .08         .05	8.9         2.7         8.5         2.9         8.2         2.8         3.4         .059         3.4         .069         3.4         .069         3.4         .069         3.4         .069         3.4         .069         3.4         .069         3.4         .069         3.4         .069         3.4         .069         3.2         .041         .072         .041         .072         .042         .042         .043         .042         .043         .043         .043         .043         .044         .049         .049         .043         .044         .049         .044         .049         .044         .049         .044         .049         .044         .049         .044         .049         .044         .049         .044         .049         .044         .049         .044         .049         .044	8.9         2.7         9.5         2.9         9.2         2.8         9.4         9.9         3.4         969         19.1         9.5         4.5         4.5         4.5         4.5         4.5         4.5         4.5         4.5         4.5         4.5         4.5         4.5         4.7         969         3.5         4.7         969         19.4         4.7         4.7         969         3.7         969         19.4         4.7         4.7         969         3.7         969         19.4         4.7         4.7         969         3.7         969         19.4         4.7         4.7         969         3.7         969         19.4         4.7         969         3.7         969         19.7         9.8         19.2 <th>8.9         2.7         8.5         2.8         8.2         2.6         8.5         2.4         .669         18.1         5.5         18.6         2.6         18.6         2.7         .665         3.4         .669         18.1         5.5         11.4         4.7         18.6         2.7         .666         2.7         .666         18.6         2.7         .666         18.6         2.7         .666         18.6         2.7         .666         18.6         2.7         .666         18.6         2.7         .666         18.6         2.7         .666         18.6         2.7         .666         18.6         2.7         .666         2.7         .</th>	8.9         2.7         8.5         2.8         8.2         2.6         8.5         2.4         .669         18.1         5.5         18.6         2.6         18.6         2.7         .665         3.4         .669         18.1         5.5         11.4         4.7         18.6         2.7         .666         2.7         .666         18.6         2.7         .666         18.6         2.7         .666         18.6         2.7         .666         18.6         2.7         .666         18.6         2.7         .666         18.6         2.7         .666         18.6         2.7         .666         18.6         2.7         .666         2.7         .

D D			AIRCR	AFT SI)	KING :	938	AIRCRAFT SINKING SPEED AT TOUCHDOMN	DOMEN			GL 1DE	GLIDE PATH ANGLE AT TD	YGLE A	T 10	WHEEL HEIGHT	нетсят	HOOK HEIGHT	ІСНТ	
2	<b>Ž</b>	MOSE	PORT	<b>.</b>	S	ST80	AVC	O	FREE-FLICHT	LIGHT	84 A	*	<b>8</b>	>	OVER RALP	d de	OVER RAMP	d A	
	S	Ş	2	Ş	2	¥S	5,5	K K	F/S	M/S	DEG	3	DEG	8	E	3	E	3	
22	23	**	23	<b>38</b>	23	<b>38</b>	53	2	5	32	S	ň	25	36	33	8	or S	<b>\$</b>	
1160	7.9	2.4	6.5	2.9	8.7	2.6	9.1	2.8			2.9	. 051	2.7	940	15.0	<b>4</b> . <b>6</b>	12.0	3.7	
1161	7.8	7.4	7.9	7.4	9.0	2.6	₹.	2.6			2.8	. 050	2.5	.043	15.6	4.0	13.1	4	
1162	7.8	7.4	9.3	2.9	8.7	2.7	9.5	2.8			3.8	. 967	2.9	.051	16.6	5.1	14.2	<b>4</b> .3	
107		<b>7.</b>	6.7	<b>9.</b>	9.0	7.4	<b>9</b> .	7.6			2.8	. 048	2.9	. 051	12.9	3.0	8.0 8.0	3.0	
165	•	7.7		•	7.4	2.2	<b>9</b> .9	2.1			3.6	. 063	2.3	.041	9.0	3.3	7.5	2.3	
99 :	8. /	7.4	7.8	7.	- •	7.8	4	7.6			۵. 9.	. 053	2.9	.050	5.3	4.7	12.4	S. B	
) S	D .	 •	• •	* - * -	- 4	.,	٠. د. د	7 7 7			۵. د د	.057	4 . 4 .	.042	<b>5</b> .	4 F	1.0	۵. و	
1346	1			. «							0 -	828				D 4		. v	
1347	7.0	9.	7.0	2.0	8.2							963		9 6	7.7	•	. <u>.</u> .	0 E	
1346	-:	2.8	6.7	•	8	2.7	6	2.7			3.2	.057	2.7	947	13.0	•	•		
1349	9.0	7.0	•	1.0	0.0	2.1	6.5	7.0	6.3	0.	2.5	.038	7.1	637	10.8	3.3	. 60	7.	
1350	5.6	5.8	12.0	3.0	11.6	3.5	1.0	3.6			3.7	. 964	8.5	.067	13.7	4.7	11.2	4,	
1351	7.9	7.4	7.4	2.2	9.0	2.6	•.	7.4			3.2	. 056	9.8	.046	15.9	4.8	13.2	<b>6</b> .	
1352	<b>0</b> .0	2.7	9.3	2.5	5.7	1.7	8.7	2.8			3.1	. 054	2.7	946	14.5	<b>*</b> · <b>*</b>	12.0	3.6	
33	e.	=	-	<b>a</b> .	4.7	<b>*</b> :	5.8	<b>e</b> :			2.8	.049	•	.028	12.1	3.7	10.1	J.1	
9	<b>*</b> !		9.0	<b>.</b>	4.6	- 1	ب د د	<b>.</b>				.052		.633	12.4	Ø. 7	9.7	J. 0	
			5.5	3.2	10.1	n.	10.3	٠, ۱			<b>-</b> 1	.054		926	12.0	3.7	4.0	5.9	
		,	72.5	٠.٠ .٠	= °	, ,	12.2	7			ص ب	.067		.074	16.1	a .	٠. د. د.	<del>-</del> .	
					) r		•	? <b>•</b>			? •	/co.	? • ? •	. 600 67.6	5 4 5 4	. ·	7 . 2	7.0	
1359	*	.0	•	3.2	=	4	10.7	9 7			60	990	4.	626	15.1	4	12.6		
1366	7.5	2.3		2.8	7.9	2.4	9.9	2.7				.058	_	.050	13.2	0.4	. e.	 	
1361	8.7	7.6	9.5	2.8	10.2	3.1	9.3	2.8				. 058	_	.049	15.5	4.7	13.1	<b>.</b>	
1362	<b>.</b>	•.7	1.6 1.6	J.5	11.7	3.6	10.9	3.3				. 699		.072	16.5	5.0	13.4	<del>-</del> :	
	- (	5.0	 	 -	<b>0</b>	9.0	10.0	J				.046	2.7	946	16.4	9.	14.2	<b>4</b> .4	
	9.6	7.6	<b>P</b> . (	9.6	7.9	7.4	. B	2.5				.055	7.4	042	15.5	4.7	13.3	<del>-</del>	
	- ·	- •	B. (	2.7	2.5	4 I	19.1	 				. 655		.057	17.0	2.5	7.4.V	<b>+</b> :	
	· · ·	,		,			6.71					959.		)	o •	n e	:		
	•		-	; -		) <b>-</b>	Y -		•	•	•	97.0		700.	7 7	. ·	9	- v	
		2.5	-	2.8	9	2.1		2.4	)	:		957		949	13.8	4.2	7.1	, P	
	11.4	u.5	10.7	2.5	10.4	3.2	10.6	3.5				.057		926	20.5	8.5	1.01	5.5	
1378	<b>9</b> .0	7.0	<b>.</b> .	<b>.</b>	5. 5.	<b>.</b>	9. <b>6</b>	1.7						. 032					
1382	9.5	2.5	<u>-</u> :	<b>*</b> .	0.	<b>u</b> .u	12.5	۵. 9				.063	_	.671	16.1	<b>4</b> .0	12.8	a. D	
1384	• ·		<b>0</b> .	7.7	<b>9</b> .0	7.0	<b>8</b> .	2.1	<b>6</b> .5	7.0	3.0	.052	_	. 656	13.6	<del>-</del> -	10.6	3.2	
1395	S. G	7.7	7.6	2.3	7.1	7.5	7.5	2. 2.			2.8	.049	2.7	947	12.5	<b>8</b> .0	6.7	ი. მ.	
286		7.7	n (	2.8	* 1	7.0	<b>8</b> 0 (	2.7				•	0. (	1651	•	,	•	•	
	D (		? .		0 10 10	- (					8.6	649	D :	250			9.5.6	Ð,	
•	D. \	7	? •	<u>.</u>		7.1	D D	7.1				<b>2</b>	Z.4	-	2.0	7.4	) e. /	٠.	

DAY LANDINGS

USS ENTERPRISE (CVN-65,

AIRC	AIRC	AIRC	œ	IRCRAFT SII	SINKING SPEED AT TOUCHDOWN	PEED AI	TOUCH	DOMN			GLIDE	GLIDE PATH ANGLE AT TD	MCLE A	T T0	WHEEL	MHEEL HEIGHT	HOOK HEIGHT	EI CAT
NOSE PORT STBO AVG	PORT STB0	STBO	STBO			<	5	<b>y</b>	FREE-FLIGHT	LIGHT	<b>å</b>	DI-14	<b>8</b>	>	OVER	RAP	OVER RALP	3
F/S W/S F/S W/S F/S W/S F/S	F/S W/S F/S W/S	N/S F/S N/S	F/S 14/S	K K	K K	2		R/S	53	Ş	DEC	3	DEC	3	E	3	E	_
23 24 25 26 27 28 29	25 26 27 28	26 27 28	1 27 28	<b>38</b>		28		2	ភ	32	z	Ä	ş	38	31	8	8	\$
6.9 2.7 9.2 2.8 6.6 2.6 8.8	9.2 2.8 8.6 2.6	2.6 8.6 2.6	2.6	2.6		8.		2.7			3.0	. 853	S. 0	. 053	14.5	*.*	12.1	~
2.8 9.0 2.8 10.9 3.3	9.6 2.8 16.9 3.3	2.6 10.9 3.3	J. 7	J. 7		-		J. 7			3.5	.061	и. В	.057	18.5	5.6	16.1	<b>÷</b>
3.2 9.9 3.0 9.6 2.9	9.9 3.0 9.6 2.9	3.0 9.6 2.9	2.0	2.0		.7		3.0			3.3	. 658	2.8	.050	13.7	4.2	11.4	'n
2.0 7.3 2.2 6.4 2.0	7.3 2.2 6.4 2.0	2.2 6.4 2.0	7.0	7.0		7.1		7.7			5.4	. 042	2.3	.040	13.1	•.	10.3	 
2.3 11.6 3.5 9.3 2.8	11.6 3.5 9.3 2.8	3.5 9.3 2.8	7.8	7.8		11.2		4.6			5.0	. 687	4.2	.073	21.9	6.7	<b>1</b> 0.0	'n

993		-	H C H	2	ا ا ا			ROL	٠.	NGL	w	a.	PITCH RATE	RATE	ROLL RATE	<b>WIE</b>	<del>ار</del> 9	<b>«</b>	X	
9	2	_	8	~	F		2	0	8	•	4		7	5	M	<b>5</b>	AT TD	2	AT TO	_
	DEC	3	930	3	DEC	3	OEG	3	DEG	3	DEG	3	DEG	3	DEG	3	9	3	DEG	3
Ŧ	43	3	‡	\$	\$	<b>‡</b>	\$	<b>\$</b>	3	51	52	3	\$	8	88	22	8	8	3	5
S S	4.8	\$	5.3	. 692			<b>9</b> .	.031	1 +:1	. 967			₹.	. 967	-2.3(	940	-2.9 -	051	2.6	. 045
3,	3.2		3.3					84	2.4	.042		1	e.			.058 -2	.7 -	047	5.8	101.
2	2.8	<b>:</b>	5.5	989		•	2.4	042	J.3	. 023		1	- -			166 -4	 	075	4.0	.147
57	•:		<b>0</b> .	98			_	962	2.0	.035		•	1 0:	016 1	۲.	.030 -1.8		831	1.8	.631
371	3.2	55	<b>6</b> .	986			~	86	5.3	. 023		7	_	019 1	٠.	.023 -2	-2.3 -	948	2.5	. 044
372	5.7	8	5.5	966			_	. 602	2 -	003		1		995 4	•	. 686 -1		028	2.8	.049
272	•:	3.	<b>*</b> : <b>*</b>			1	_	ess	6.7	.117		~	2.8	. 051	1.2	.021 -2.5		044	4.2	.073
27.	4.2		4.4	. 675			_		1.8	014		_		.028	1.07	079 -2.6		045	4.8	.084
376	7.4	. 075	6.7	.117			2	•	ı	031		_	1.3		ĸ,	.669 -3.(		063	4.4	.075
LS L	2.5	83	<b>+.</b>	.077				.016	1.0	.017		1	•	•	, ,	. 982 -1	-1.7 -	636	4.0	.070
378	<b>.</b> .	. 828	5.3	. 892		1		- 93e	1.5	- <del>0</del> 09		7	<u>'</u>	037	•	.052 -2.2		838	4.0	.070
2	4.2		3.S	969				997	1.5.	005		_		. 619.	د:		-2.6 -	045	3.3	.058
3	2.3	3	4.2	.073		•		017	2.6	.045			۲.	. 912	•	- 635 -	.7 -	012	3.3	. 058
Ŗ	÷.5	. 679	<b>.</b>	196.		•	-2.2	036	ų	. 003		ı	<b>1 ★</b> :	007	 4.	.042 -4	1	J. 886	4.0	.112
282	<b>.</b>	. 60	5.5	960.				<b>600</b> .	2.0	.035			ĸ.	600.				072		660.
28	4.0	3	4.7	. 662		•	n	040	7	.003		1	~	005	'n	. 969 -2			- 1.1	636
200	2.5	5	4.0	.112				.017	<b>+</b> .	. 024		-7.			5.3	.092 -2.7		-	-2.1	637
900	<u>۔</u>	\$	3.6	3		•		035	7.	012		7			5.1			075	<b>4</b> .6	. 686
Š	•.		6	8		•				÷10.		•	1	016	<b>*</b>			058		012
392	٠, د.		<b>*</b> :			1			-2.5	038		_		- 629	i *:				_	016
200	•		<b>†</b> .	.112			_			. 865		T			_		•		~	638
<b>18</b> 0	2.2	85	7.0	. 122						1.044		1			ر د.		_	•		628
200	S.8	99	9. •	.007		•			-2.2 -	eSe		_			ı		_	989	7.5	5.
980	<b>+</b> : <b>+</b>		•.	50 50		•			9.1	016		ī			2.8	.049 -2.	_	637	3.2	. 056
787	S. 8	999	6.7	.117		1	-2.3		- 8.	014		7	1.0	028 4	4.6	.1- 880		028	8.8	.063
200	5.2	\$	5.7	<b>8</b>		•	•	017	4	.003		ī	1.6	028 14		.244 0.	_	900.0		.017
\$	2.5	į				1	. 2	023				~	2.1	. 637	3.8	<b>990</b>	J.	075	6.5	.13
\$	5.5	98	<b>+</b> .9	.12			1.2			.023		_	œ.	. 833	7	.003 -2.6	•	045	3.6	.063
<b>\$</b>	4.5	939	<b>9</b> .	50 50		•	. 6.7		-2.3 -	040			۲.	.012 3	2.5	.056 -1.7		636	1.7	.636
\$	<b>+.</b>		5.2	. 692			r. –			636		•		0.000	•	.676 -3.3		058	•. •.	.676
=======================================	<b>4</b> .6	8	6.9	.120		•	9.7	633	.3.	965			Ξ.	.002	7.7	.073 -2	-2.2 -	838 -	• • •	.678
=	3.8	990	5.4	<b>468</b> .		•	-7.		9.1	010		_	L. 1	.023 3	6.0	.063 -2.		042	3.3	. 058
412	5.1	600	8.2	. T.			<b>*</b> :	.024 –	-1.2 -	021		•	•	D. 866 -1	.2 .	021 -4	- 9	084	5.5	.626
4:3	2.8	150.	7.0	.122			_		5	969		•	6.2	.1062	-2.8 -	T		884	4.5	.679
+	4.5	.073	7.1	.124		•	-2.2	636	•	.010		ī	ı		•	. 686 -3.		961	2.3	. 040
415	1.5	.026	5.2					010	1.0.1	031			7.	•	80	1.061	- 1	682	<b>9</b> .	. 105
416	9.0	998	4.3	.075		1	•	042 -	1.9	033		•			2.1	.037	ا ا	.075	3.6	.063
417	5.2	5	6.8	119			. 2.	003	9.9	<b>9</b> . <b>9</b>			₹.	7 700.	·	677 -3	1	. 068	<del>-</del> :	.072
423	2.8	.049	5.0	. 987		•	•	017	1.6			~	.7		2.7	.047 -2	9.	.045	4.5	.079
\$	<b>9. 4</b>	\$	3.8	999.	5.4	\$	-2.0	035	- 5.	905	-2.0	.035 2	-	. 037	ر. د.	.023 -3	1 80	. 966	. 2.	. 995

DAY LANDINGS

USS ENTERPRISE (CVN-65,

		3	LANDING DATA	1	MODEL S-	?	_	USS ENTERPRISE (CVN-6	ERPRI	SE (CV	9			DAY	DAY LANDINGS	NGS				
8		P : 1	H O	2	3 1 6			R 0 L	٧	٦ ک	ш	۵.	PITCH RATE		ROLL RATE	ME	r. 9.	÷	YAW	
2	2		8		Ŀ		5		8		44		AT TD	٥	AT 1	<b>5</b>	AT TD	۾	AT TD	•
	930	3	DEC	3	DEC	3	930	3	DEC	3	DEG	3	930	3	DEC	8	DEG	\$	DEG	3
Ŧ	42	2	‡	<b>4</b>	\$	47	\$	9	3	51	25	33	54	55	26	21	88	20	8	5
Ē	3.3	3	÷.0	3		_	'n	.023 -1	•	033		1	•	014 -2.	4	. 042 -3		996	-2.1 -	637
2	5.8	<u>=</u>	3.0	999			_	.036 -1.(	•	017		-2.8	•	045 9	•	.168 -1	•		•	.028
3	. B. B	9	6.2	2		_	•			200		•	•		_			065	~	. 003
į		3:	n .	25		1 9		016 -2	<b>~</b> ~	1.040 1.540	đ	2 11		.035 8.		.152 -2.	~ <	<b>6</b> .6		.014 954
2 2	· ·	1		270						. 916	•									. 661
2	4.0	3	8.2	3		T	•			669		7	Ť	686 7	•		_	22		.007
2	4.2	5	7.9	=		1	•	.986 -3.	<b>.</b>	659		~	2.7			•	-	<b>1</b>	_	016
= :	•	2 3		. 602		- •	_ 4	5 i	ທຸເ	60 c		7.	i •	042 -1.	α.	129.	_	•		113
						77		- 710.		• • •		_	P	1 2	i - o	6/2		7.40	<b>~</b> 4	. <b>6</b> 12
		ž		3		7		916	. 7			₹		. 676 - 3.2	ı				 	682
915		25		3		_	•		! ?! <b>†</b>	073		•								.021
110	5.9	3		.126		_	s.			028				<b>4</b> 600.		. 884 -5	i	687		. 637
918	2.8	3		. 692		7	, 1	•	•	687			•				~	926		002
919	•	3	- 1		,				ų,	26.	•	† : :	•	1	٠.		ໍ	986		. 108 6.
956	•	2 2	2.5	127	•••			1-851-1	ų r	- 929 -	i D	. /1 <b>.</b>	י פיי	.623	• •	.112 -2.	i 1	246 467	-2.5	5 6 6 6 1 1
922		2 5	; +;	16		7		035	; <del>-</del>	919			. ~	.003 -1.7				,		. 940
923	•	111	9.0	.115			_	. 663	ĸ,	.026		'n	-			040 1	_	•		637
924	•	5	9.0	.115		-5.		049 J	• (	.052		♥ (		.075 6			•	2		938
926		3	2,7	į		- 1		- 710. - 710.	I D •	831 559		<b>N</b> 1	  	* • • • • • • • • • • • • • • • • • • •	•	.5- 6/6.		<u>.</u>	0 c	979
928		3 5		3			. <b>.</b>	. <b>66</b> . –	,	-, 936		-		. 628			-	820.1	. 6	645
928	3.4	ž	0.	128	5.3	- 200		014	7		7	612 -2.7		647 -2	i	042 -3		658	1.7	.023
932	5.8	<b>=</b> :	0.0	.052	,		ni (	600	•	9.00	•			968 1	<b>e</b> j (		Ť	2	•	710.
121	e.	3 ;	n. 0	225	4.0	- 480.	~ •	. 621	- •	. 602		.e. 71e.	ь,	1.063	•	0.666 -2.7	•	/40	4. 1	ر 1
24	5.2	3 2		79		ט נ		.059 -2		047		<b>)</b>	٠ ٨	. 96	•					.963
126	5.5	203		. 662		7			_	9.00				600	٠. دو			2	_	. 054
1127	4.5	679	5.2	<b>8</b> .		7	•	•	7	021		-2.2		038	ŭ.		_	95	_	005
132		2	<b>9.</b>	<b>3</b>		1	1.7			.047		7		129	ni i		•	635	5.7	.065
*	÷.5	929	5.7	600		7.	•		7.7	85e.		a. T	-	•	· .		•	121	2.5	.056
92		3	<b>.</b>	9		7 '	· · · · · · · · · · · · · · · · · · ·		9 7			•	 	7 200	2 6	.127 -1.	- •	919	D 4	129.
	•					ī	i 9 - 1	3	. «	940		•	•		! <b>→</b> •		•	1	ا - د	. <b>9</b> 54
25.	4	3	2 2			1		. 916	-	.002		_			• 💠			£		- 660
156	+7	987	2.7	.065		7		.040	0	014		1	.2	963 -2	,			928	_	.033
158	•••	265	5.3	. 692		7		•		628		•	•	-		.031 -2	i •	935	5.1	688
120	-	2	7.0	<u> </u>		T	- 9.7	631	1 •	919.			<b>.</b>	17 -1	e e	628 -3	•	925	2.5	***

8			Z O	Z Z				R 0 L	۲ >	Z C	w	<b>a.</b>	PITCH RATE	RATE	ROLL RATE	ME	۵. ا	÷.	YAN	_
9	2	_	8		*		2	_	8		14		<b>Y</b>	2	AT 1	5	14	2	AT TO	2
	9	3	90	3	9	3	930	3	DEG	3	DEG	3	DEG	3	DEC	3	DEC	3	DEG	3
=	7	2	\$	\$	<b>‡</b>	41	\$	<b>\$</b>	2	5	25	3	*	8	8	27	8	\$	3	5
3	9.0		6.9	2.		ı	*		2.1	.637		4		.012	1.7	599	1 +	. 659	2.5	***
<u>=</u>	•	3	5.1	3		_	-:	6.	•:	7		ī	1.4.1	. 024 -1	.5	.026 -3.		3.	5.	. 626
252	-	. 672	2.7	3		7	-2.7	. 44	3.1	654		7	•	642		.045 -3	-	. 654	•	8.
Ī	4.3		7.3	.127		_	<b>+</b> .	.024	•	<b>8</b> .		•	i 0:1	110.	. e.	88e -	ų.	•	•	916
Š	7.0	2	7.5				ė		2.1 -	037		^	7.3	.127	 	.080 -2	1 •	. 042	4.7	. 662
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167	9.0	3		\$		Ť	*	077	•	918			•		7	•	1	- 150.	-2.2	036
3	2.7	Ş	7.	.122		ľ	•		1.2 -	. 021		T	.2	. 873		•	•	.045	1.2	. 621
3	4.7	<b>8</b> .	2.5	. <b>8</b> 2		7	-	67	2.2	• =			œ.	1 230		•	j.	3	6.7	.117
2	+.7			3		T	- 2.	623	•	=			- -	. 662	*.	.0772	ų.	. 638	3.8	999
3	•	8	7.2	. 127		-3	٠. ا	33		5			ų.	200	•	.014 -2		.047	3.5	5
į	J. 5	ž	:	.120		3	7.	. 623	2.2	. 856.		. 623	יי ייי	•	8.	190	i.	. 656	4.3	.075
3	4.7	<b>.</b>	4.2				•	9	1.7	97		7	•		-	-	7	. 056	4.2	.073
2	9.0	=	S.	E		_	•	. 71		600		~		.0655	5.2	2	í e	. 968	8.7	. 152
22	4.7		5.1	\$		-3		<u>.</u>	5.7	<b>66</b>			'n	. See .	).  -  -	45	•	. 635	2.1	. 637
3	<b>.</b>	Ş	9.0	3		•	٠	8	•	.017		~	•	.045	•	•	í •	. 035	S. S.	969
3	<b>7</b>	. 675		2			<b>.</b>	=				_	•	. 122	<b>.</b>	-	1 -	.072	7.4	.042
3	n (	3	4.0	3		•	<b>+</b> (	8	- :	082		7		- 633	•	•	•	.052	٠ ;	910
3	2.7	5	5.1			÷ '	De (	25.		052		7		185			ن. ا	673	9.	.687
5	7.7	3	•			; ·		028	<b>o</b> . (	3		•	i • i	667	* 1		: - (	. 550.	*.	e59
3	•	3		9		7.	•	042	7.7	.021					ī 		) 10 (	0 t 0	<b>-</b> (	700
3	4.7	25	٠, د د	. 675		•		012		36.		7 '		866 -2	5.5		 	.052	÷.	989
3	7.	.117	-	2		ī '	·	024	1 * :	024		7	'n.	026	~ .		1 • 1	. 659		. 663
<b>.</b>		5		2		7	_	1.054	1 9:	017			•	002		-	i.	*	•	
2		=	, ,	= !		- (		91.	i n	. 999		T '		- 986 -	i •:		ı P	.075	•	<b>?</b>
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<b>Š</b>	<b>+</b>		7.7	5		•		*:01*		<b>.</b>		-	ų.	.026	*		ا ھ	.651	-	002
2	•	2		8		,	٠.		- 7	200		. '	· ·	012-16	ı •		! -	698	ر د د	90.
3		2	4.5	Š		7	i.	**	0	996		<b>-</b> 7		. 665	* 1		80 i	.631	<b>.</b>	. e.
ž	٠ •	3	7.7	<u> </u>		<b>5</b> 0	ų			. 662			-	. 982 -	 	162 -3.	D	658	2.7	. 665
3	-	<u>.</u>	6.2	2 2 7		1 88 1	9.	ı	3.2	. 956	2.1	637	_	- +10.			1	.070	2.1	.037
376	9.e	3	•	8		_	•. •.		J. 6	.063		ī	1 -	010			ı	. 023	- -	. 637
277	ري. 0.	3	₽.	.075		•	•	 	-	. 002		~		. 942	· -		n I	.058	7.7	. 637
378	•	.115				7	-2.6 -	045				ĭ		. 863		. 968 -2.	٠ •	. 649	• • •	624
29	<b>.</b>	3	7.7	. 126		T	Ņ	021	۲.	.012		7	9.0	171 13	5.2	.239 -1.	- -	.019	<b>+</b> :-	. 024
<b>10</b> 0	4.7	8	0.0	. 120	•	98	- 7		3.3	. 858.	 	.005	-	. 882	.2	- 120	1 0	10.	<b>9</b> .	. 628
<b>2</b>	5.7	\$	6.2	<u> </u>		7		- 636	<del>-</del> .	.002		7	1	044	4.	.024 -3	9	.063	4.2	.673
200	<b>6</b> .0	296.				•	- 7:-	. 012				7	ن. ا	023 3	7	.065 -3	1	. 659	<b>.</b> .	.023
<u> </u>	<del>-</del>	. 672	5.5	. 802		ī	· +:	024	ė	616.		~	•	.035 2	a.	•	•	999	•	. 028
1410	6.2	3	7.7	*		7	-	. 019.	7 -	.012		1		.012 -3	e.:	898	<b>8</b> 9	990.	- - -	017

	3	AT TO	3	5	. 127
	AVA	7	DEC	2	2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2
	÷	2	3	80	672 659 663 665 651
	F. P. A.	AT TD	DEC	38	
NCS	RATE	2	3	22	.024 -4.1 110 -5.4 .021 -5.6 .023 -5.7 .063 -2.9
DAY LANDINGS	ROLL RATE	AT TO	DEC	26	
8	MTE	2	DEG RAD	55	
	PITCH RATE	AT TD		ņ	4-14-6
	-		3	S	11
^	w	4	DEG	25	
USS ENTERPRISE (CVA	ROLL ANGLE		3	2	
EBPRI	۷	8	DEG	52	2.2.2
JSS EN	A 0 L		3	<b>\$</b>	. 044 -1.2 . 026 -2.8 . 0101 . 040 -3.3 033 -2.8
_		4	DEG	\$	2.2. 4.2. 6.6.6.6.
?			3	<b>†</b>	
NODEL 5-3	6 1	4	DEG	7	
¥ - K	Z Z		3	\$	6.00 6.00 7.1. 7.1.
CANDING DATA -	I U	8	930	\$	4404
3			3	3	
		2	220	42	
	8	ş		7	1517 1524 1527 1538 4586

ğ	7	OFF-CENTER	0T 0T 9110	0 0	31 INE	<b>\$10</b> E	2	2	SHIP		ğ	DECK PITCH	DECK ROLL	BOLL	100	9	BAROMETRIC	TRIC	ARR CEAR	SEAR CEAR	REREAD	
ě	0151	DISTANCE	DISTANCE	MCE	ġ	Š	346	3005 3005	SPEED	8							PRESSURE	URE	RUNOUTS	UTS	NUMBER	
	E	3	E	*				_	3	Ş	DEC	3	DEG	3	<b>L</b>	ပ	IN HG	3	Z	5		
2	2	3	3	3	67	2	2	2	7	72	22	*	22	78	11	92	82	2	5	82		
35	=	7	263	2	•	747	70200		*	~					3	71	36.01	762.3	•	0.0	•	
3	-15	1	276	3		725	70120		4	~	*	667		90.	3	71	•	762.3	•	0.	•	
2	-12	1	25	2	n	727	<b>3</b>		+	7	'n.	- 969	-	962	3	11	29.97	761.2	168 4	426.7	•	
5	-	7	25	2		724	70120		*	7	s.	- 669	-	002	3	17	29.97	761.2	•	•	•	
27	7	7	278	2	-	724	70120		*	7	· s	- 969	-	002	3	1	29.97	761.2	•	•.	•	
22	Ŧ	7	<b>3</b> 41	2	~	737	56120		•	7	5	- 969	-	962	63	1	29.97	761.2	166 4	421.6	•	
22	7	7	3	5	-	724	<b>3</b>		•	, ,	'n	969	-	002	63	7	29.97	761.2	•	•.	•	
24	=	7	<b>3</b> ‡9	2	~	22	58286		•	7	ņ	- 969	-	002	3	1	29.97	761.2		426.7	•	
376	7	7	<b>788</b>	2	n	747	56266		•	7	Š.	000	-	002	63	_	29.97	761.2	165 4	419.1	•	
27	~	7	<b>584</b>	87	2	22	<b>20200</b>		+	7	'n	669	-	002	63	17	29.97	761.2	167 42	424.2	•	
378	=	?	<b>58</b>	2	•	724	3		•	7	'n	669	-	002	63	12	29.97	761.2	167 43	424.2	•	
27	7	7	253	1	N	747	56128		+	7	'n	. 669	-	~. 002	2	17	29.97	761.2	167 42	424.2	•	
3	F	?	285	87	*	725	2 2		+	7	ę.	- 600	-	002	63	17	29.97	761.2		419.1	•	
Ē	21-	1	257	2	n	724	<b>8</b>		+	7	'n	- 669	-	002	63	1	29.97	761.2		428.7	•	
28	-	7	234	7	~	747	56200		*	7	ė.	669	-	002	S	17	29.97	761.2	167 42	424.2	-	
2	?	ī	293	8	*	725	<b>8</b>		'n	7	*	007	9.1	016	S	12	29.97	761.2		426.7	•	
3	=	7	220	67	~	35	50200		n	7	*	007	6.	016	63	17	29.97	761.2	169 4%	429.3	~	
3	~	-	275	3		747	70123		~	~	*	007	~	003	3	7	29.97	761.2	•	•.	•	
5	r	7	276	<b>9</b> 5		725	76166		n	7	7	993	-2.3	040	63	7	29.97	761.2	•	9.0	•	
382	7	7	266	5	•	747	70100		n	7					63	17	29.97	761.2	•	•.	•	
200	7	7	247	22	•	22	76296		n	7	4.	007		002	63	7	29.97	761.2		0.	•	
ž	~	-	313	<b>8</b>	4	747	50120		n	7	· •:	007		005	5	17	29.97	761.2		428.7	•	
395	7	7	261	2	n	724	50100		~	~					63	17	29.97	761.2		431.8	•	
200	7-	7	3	ā	n	22	56100		n	~	J.	.005	2-	. 003	63	17	29.97	761.2		426.7	•	
26	-12	†	248	92	n	747	50100		n	7	•	999.	œ,	916	63	17	29.97	761.2		429.3	•	
986	7	7	282	2	n	725	50100		so.	n	<del>-</del> .	. 662	- 9.1-	028	53	1,	29.97	761.2	169 42	429.3	•	
\$	7	7	<b>79</b>	8	-	335	70120		6	n	*	007	1.4	867	63		29.97	761.2		•	•	
<b>‡</b>	ç	7	213	5	n	736	56266		'n	n	· ;	002		010	63	17	29.97	761.2		429.3	•	
<b>\$</b>	-12	1	233	7	N	735	200		'n	n	· ?		-1.5-	026	63		29.97	761.2		426.7	•	
3	7	7	172	3	~	736	58266		*	~	9.6			995	63		29.97	761.2		429.3	•	
=	-12	Ť	219	<b>8</b> 7	7	725	50100		•	7	•	9.00	1.5.1	005	3	_ `	29.97	761.2		429.3	_	
=======================================	+	†	<b>3</b> 6	2	n	727	56266		•	7	•	999	- 5.1	005	63		29.97	761.2		429.3	-	
412	7	7	263	3	n	736	56266		•	7	•	0.000	- 5	005	63	7	29.97	761.2	169 42	429.3	•	
413	-12	†	227	8	~	724	50123		4	7	9.6	999	1.3.	965	63	77	29.97	761.2		429.3	•	
<b>*</b>	=	7	286	2	+	22	50100		4	7	• •	9.00	.3.	. 665	63	17	29.97	761.2		426.7	•	
415	1	ī	289	3	+	724	50120		4	~					63	17	29.93	760.2		426.7	_	
=	7	7	287	87	•	725	56166		4	7	•	999	1.3	005	62	7	29.93	760.2		426.7	•	
417	7	7	282	6	n	725	50120		+	7	•	900.		005	62		29.93	769.2		426.7	•	
423	10	Ŷ	257	28	n	736	50100		4	7	•	900.		005	62	17	29.93	760.2	168 42	426.7	-	
3	7	7	278	2	n	725	50100		*	7	9.	9.00		005	62	7	29.93	760.2		426.7	•	

		₹	ANDING DATA	IA - E	1300M -	3		uss E	M E	PRISE	USS ENTERPRISE (CVN-65)	-63)			2	3	DAY LANDINGS				
995	1	OFF-CENTER	OT OT THE	5 5	WIRE	SIDE	9	2	SH P		DECK PITCH	₹	DECK ROLL	שנו	10	٩	BAROMETRIC	TRIC	\$	ARR CEAR	REREAD
ġ	018	DISTANCE	DISTANCE	ANCE	₹	₹	3	<b>300</b>	SEED	a							PRESSURE	JRE	RUNOUTS	UTS	NAMBER
	E	3	E	3					5	Ş	DEG	3	DEC	3	<b>L</b>	ပ	N HG	3	2	8	
2	3	3	2	3	5	3	8	•	7	22	2	*	25	92	11	28	28	2	5	83	
<b>4</b> 52	7	7	273	3	~	326	\$61 <b>6</b> 0		*	~	•	8		59	62	17	29.93	760.2	168	426.7	8
3	-13	9	278	2	*	736	50120		•	~	•	. 666	3	003	62	17	29.97	761.2	167.4	424.2	_
3	-12	7 '	261	3	(	725	70120		<b>4</b> ·	~	,			;	62	2	29.97	761.2		•	•
<b>;</b> ;		9 9	2 2 2	22	~	747	20120		+ +	<b>,</b>	•			<b>96</b> 5	2 62	22	29.97 29.97	761.2	Ž.	426.7	
:	7	7	249	? \$	~	725	90120		•	. ~	•	986	. 5.	596	; <b>2</b>	2:	29.97	761.2	3	426.7	- •
3	7	?	269	2	ı	736	70200		•	~	•	88	3	965	62	7	29.97	761.2	•	•	•
į	-12	9	234	7		736	70120		*	~	•	. 666	3-	005	62	12	29.97	761.2	•	•.	
3	57	ę	257	2	n	725	56128		*	1	-	062		900.	25	2	29.97	761.2		429.3	_
<b>3</b>	<u>.</u>	<b>9</b> .	213	2 :	~ :	736	50120		<b>4</b> ·	1 ~ :		062	_	9.00	25	_	29.97	761.2		426.7	
<b>Ş</b>	÷ •	1 1	1 2	3 :	·	724			<b>.</b>	N 6	- 4			98.	3 5	<u> </u>	29.97	761.2		429.3	- (
3	? :	7 '		5 2	• •	8	97190		• •	<b>,</b>	_			700	7 9	` !	78.87	7.10/		7.424	<b>D</b> (
3		? 1		8 F	7 F	5 5	20120		• •	N 6	i (			042 	2 2	: :	78.87	761.2		426.7	• •
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	•	7	228	2	, K	736	50120		•	· ~	)		)	}	62	: 2	29.97	761.2		424.2	-
	7	1	281	2	ì	724	70120		•	1	<b>.</b> i		-2.4	042	2	7	29.97	761.2		•	•
	=	?	249	2	n	747	<b>36188</b>		+	<b>N</b>	i •			014	62	7	29.97	761.2		429.3	-
	7	1	256	2	n	724	50120		*	1	i • • · ·			635	62	7	29.97	761.2		424.2	-
	-	7	275	3	7)	724	56200		+	! ~			-2.3	040	62	7	29.97	761.2	3	426.7	~
55	7:	7	2 5	3 :		745	76296		<b>+</b> •	1 : 7 :		<b>9</b> 62	•	÷ .	<b>:</b>	2:	29.92	760.0	• •	•	• •
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3	+	1	192	3		7	2010		<b>n</b>	1 ' 7				10.	2	9	29.95	760.7	•	0.0	•
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22	=	?	238	2	~	727	50120		n	1 ~	! 	003		921	9	2	29.95	769.7	2°	428.7	•
3	7	7	222	<b>:</b>	•	147	70100		י מ	N (		.002	1.2	621	8	2 :	29.95	768.7		•	• •
	֓֞֞֞֞֓֓֞֟֝֓֓֟֝֟֝֓֓֓֟֟֝֓֓֟֟֟֓֓֓֟֟֓֓֟֟֓֓֟֟	• 1		<b>.</b>	•	3 7	70126		3 F	, ,	i -	700		200	8 5	2 0	20.00	7.00.7	_ 		• ^
3	-	7	242	: *		745	<b>8</b>		, 17	. ~					99	9	29.95	766.7	•	•	•
	7	7	28	=	•	745	50100		n	1	i -:-	662		669	99	6	29.95	7.09.7		426.7	~
	91	7	2	8	-	747	50200		n	7	5			993	99	6	29.95	760.7	50	429.3	•
	+1-	1	212	3	8	7	<b>Se 100</b>		n	7				021	99	2	29.95	769.7	2 2 4	426.7	8
692	Ŧ	7	228	2		<b>*</b>	76188		7	N 1	i 	992	· + · ·	667	99	9	29.95	769.7		•	•
993	-15	Ŷ	267	5	7	727	<b>Se 188</b>		n	~					99	<u>.</u>	29.95	760.7	168 169	429.3	•
90	-	?	<b>341</b>	2		744	70108		~	7				035	99	5 7	29.95	760.7	•	•	•
897	-13	ş	228	8		735	70100		7	7		003	ا. ا	005	99	<b>5</b>	29.95	769.7	•	0.0	•
980	4	7	282	2		25	70100		n	7		003	•	919	99	5 2	29.95	760.7		0.0	•
888	î	7	229	2	~	*	50230		<b>~</b>	~		!		1	99	9	29.95	769.7		426.7	•
Ĩ	-12	†	246	22	~	<b>35</b>	5 5 6 6		<b>+</b>	N .	•	910	2	963	9	~ <del>•</del>	29.95	760.7	7 20 7	429.3	•

DAY LANDINGS

Fig. 10   1574ACT   10   10   10   10   10   10   10   1	P	OFF-CENTER	OT OT TANA	5 5	WIRE	SIDE		٠. <b>١</b>	3		DECK PITCH	PITCH	DECK	שרר:		401	BAROMETRIC	ETRIC	<b>8</b>	APR GEAR	REREAD	
Mary   Mary	DIS	TANCE	0157	304	9	Š	TYPE	3000	3	a							PRES	SURE	\$	DUTS	NUMBER	
64         65         67         68         69         73         74         75         76         77         78         76         77         78         76         78         76         77         78         76         78         76         78         76         78         76         78         76         78<	E	3	E	3					3	Ş	930	3	DEG	3	<b>L.</b>	ပ	2	呈	=	8		
-2 253 66 173 5912 6 1 2 1 2 1 2 1 2 1 2 1 2 1 2 1 2 1 2	3	3	2	3	6	3	3	•	7	22	22	*	75	78	72	28	2	2	5	82		
- 5 155 51 757 59120	7	7	293	2		32.	70120		•	7	•	9.00		014	9	<u>a</u>	29.95	769.7	•	•	•	
-2 255 91 3 739 95290	•	?	<b>3</b>	3	-	747	50120		•	7		.003		010		9	29.92	769.7	176	431.8	•	
211         64         741         59123         4         2.0        0	7	7	<b>3</b> 8	5	n	32	56200		+	7		- 669		023		2	29.82	769.7	168	426.7	7	
0         256         775         256         785         276         785         786         4         2         -         -         0         256         785         776         716         2 <th>7</th> <td>ņ</td> <th>211</th> <td>3</td> <td>7</td> <td>741</td> <td>50123</td> <td></td> <td>*</td> <td>, 4</td> <td></td> <td> 010</td> <td></td> <td>014</td> <td>8</td> <td><u>•</u></td> <td>29.82</td> <td>760.7</td> <td>168</td> <td>426.7</td> <td>7</td> <td></td>	7	ņ	211	3	7	741	50123		*	, 4		010		014	8	<u>•</u>	29.82	760.7	168	426.7	7	
-223 660 2 745 58100	7	•	3	2	~	745	<b>Sei Se</b>		4	7					8	<u>•</u>	29.92	769.7	169	429.3	•	
-2 285  96	2	7	223	3	~	7	<b>3 5 8</b>		4	7		967		019		<u>•</u>	29.95	769.7	167	424.2	-	
-5 234 77 2 744 50100	ŗ	7	283	3	*	745	<b>S</b>		4	, 4		. 993		007		9	29.92	760.7	168	426.7	•	
4         234         71         2         735         50120         4         2         -6         -610         -1.6         -620         6         19         20.95         766.7         166           -4         236         78         372         50120         4         2         -6         -607         -607         -6         19         20.95         766.7         166           -4         286         86         775         50120         4         2         -7.2         -607         -1.6         -607         66         19         20.95         766.7         166           -4         286         86         3         725         50100         4         2         -2         -603         -2.1         -603         66         19         20.95         766.7         166           -5         286         86         3         727         50100         4         2         -1         -603         -610         -610         -610         -610         -610         -610         -610         -610         -610         -610         -610         -610         -610         -610         -610         -610         -610         -610	5	7	22	2	7	744	<b>Se : es</b>		+	,		010		021		9		760.7	167	424.2	-	
→         219         67         2 72         50120         →         2 -2         −061         −1.8         −014         60.         19         28.05         760.7         166           J         286         78         3 730         50100         →         2 -4         −007         −1.8         −01         20.5         760.7         168           J         286         80         3 735         50200         →         2 -2         −003         −2.1         −037         66         19         29.05         760.7         168           →         286         90         3 735         50200         →         2 -2.2         −003         −2.1         −037         66         19         29.05         760.7         168           →         286         3 74         50100         →         2 -2.2         −003         -2.2         −03         500.7         168           →         286         3 74         50100         →         2 -2.2         −003         66         19         29.05         760.7         168           →         287         5020         →         2 -2.2         −003         -0.6         19         29.05	12	†	7	7	~	235	50120		+	7		. 618		028		2		760.7	168	426.7	~	
4         256         78         3         739         50100         4         2         -4         -007         -1.6         -026         61         19         28.55         768.7         169           -1         282         86         4         747         50120         4         2         -2         -003         -2.1         -037         66         19         28.55         768.7         168           -4         284         88         3         727         50100         4         2         -2.1         -002         -1.1         -016         66         19         28.55         768.7         168           -3         13         24         73         26100         4         2         -2.1         -002         -1.1         -016         66         19         28.55         768.7         168           -3         240         73         26100         4         2         -2.6         -016         6.0         19         28.55         768.7         168           -3         240         70         260         4         2         -6.6         -6.016         6.016         19         28.55         768.7         <	<u> </u>	†	218	6	~	727	50120		*	7		003	•	014		2		760.7	168	426.7	~	
-3         282         68         4         747         59120         4         2         -2         -083         -2         -081         66         19         29.85         768.7         168           -1         286         91         4         745         58200         4         2         -2         -080         -2.1         -081         66         19         29.85         768.7         168           -3         244         28         1         730         58120         4         2         -2         -080         -2.1         -081         66         19         29.85         768.7         168           -3         246         3         73         58100         4         2         -6         -010         66         19         29.85         768.7         168           -3         248         3         727         58100         4         2         -6         -010         66         19         29.85         768.7         168           -3         280         3         727         58100         4         2         -6         -010         66         19         29.85         768.7         168     <	2	†	<b>3</b> 2	2	n	32	200		*	, 4	<b>*</b> :	667	-	028	9	<u>.</u>	29.82	760.7	169	429.3	-	
-1         286         91         4         745         58289         4         2         -2         -8         -10         66         19         29         55         760         7           -4         282         3         735         58289         4         2         -2         -10         -10         66         19         29         55         760         7         169           -3         178         54         1         730         56120         4         2         -1         -00         11         -010         66         19         29         55         760         7         169           -3         240         73         240         74         56100         4         2         -6         -010         66         19         29         55         760         7         160           -3         240         75         56100         4         2         -6         -000         2         -6         10         26         19         29         55         760         760         760         760         760         760         760         760         760         760         760	4	7	282	8	•	747	50120		4	7						æ	29.92	769.7	169	429.3	•	
262         89         3         735         56206         4         2        2        6        6        6        6        6        6         10         66         19         20         20         760,7         166           -3         173         50100         4         2        6        601        6         19         20         20         760,7         168           -3         240         73         240         74         50100         4         2        6        601         66         19         20         27         760,7         168           -4         220         74         50100         4         2        602        6	1	7	296	=	•	745	58288		4	~		003		037		2	29.82	760.7	168	426.7	•	
-4         264         86         3         727         56166         4         2         -2         -603         -2.1         -603         6         19         29         57         166         7         168           -3         178         54         1         736         56126         4         2         -1         -602         11         -618         66         19         28         56.7         168           -4         226         76         7         56166         4         2         -6         -6         19         28         56.7         168           -4         226         76         7         56166         4         2         -6         -6         19         28         56.7         168           -3         226         66         3         75         56166         4         2         -7         -607         -7         168         76         76.7         168         -7         168         76.7         168         76.7         168         76.7         168         76.7         168         76.7         168         76.7         168         76.7         168         76.7         168	<u> </u>	1	262	2	n	735	<b>26200</b>		•	~		663		016		2	29.82	760.7	170	431.8	•	
-3         178         54         1         736         50120         4         2         .1         .002         1.1         .016         61         2         .05         16         19         28.95         766.7         168           -3         240         73         2         747         50100         4         2         .6          6         19         28.95         766.7         168           -4         222         68         2         747         50100         4         2          6          19         28.95         766.7         168           -3         283         86         3         735         50100         4         2          6          6         19         28.95         766.7         168           -1         280         86         3         74         50100         4         2          6         19         29.95         766.7         168           -1         280         86         9         9         9         9         9         766.7         168           -1         280         86 <t< td=""><th>2</th><td>†</td><th><b>7</b>64</th><td>2</td><td>n</td><td>727</td><td><b>39</b> <u>18</u></td><td></td><td>+</td><td>7</td><td></td><td> 003</td><td></td><td> 037</td><td></td><td>2</td><td>29.82</td><td>769.7</td><td>168</td><td>426.7</td><td>•</td><td></td></t<>	2	†	<b>7</b> 64	2	n	727	<b>39</b> <u>18</u>		+	7		003		037		2	29.82	769.7	168	426.7	•	
-3         240         73         2         747         50100         4         2        6        9	4	?	178	z	-	35	50120		*	7		. 002		9.		9	29.82	760.7	169	429.3	-	
-4         229         70         2         741         50100         4         2         -603         66         18         29.95         760.7         168           -3         282         66         3         745         50100         4         2         -6         -603         66         18         20.95         760.7         168           -3         282         86         3         725         50100         4         2         -7         -602         -6         18         20.95         760.7         168           -1         282         86         3         724         50120         4         2         -7         -602         -6         18         66         19         20.95         760.7         168           -1         282         85         3         744         50120         4         2         -1         -602         -6         -003         66         19         20.95         760.7         168           -1         282         87         747         50120         4         2         -4         -602         -6         -603         -6         -603         -6         -603	•	?	240	2	~	747	<b>S</b> <b>S</b> <b>S</b> <b>S</b>		4	~		010		016	9	<u>e</u>	29.82	769.7	168	426.7	~	
-4         222         68         2         747         50160         4         2            0.00           0.00           0.00           0.00            1.00 </td <th>2</th> <td>†</td> <th>220</th> <td>2</td> <td>~</td> <td>741</td> <td>56166</td> <td></td> <td>4</td> <td>~</td> <td></td> <td></td> <td></td> <td></td> <td>9</td> <td><u>e</u></td> <td>29.95</td> <td>760.7</td> <td>168</td> <td>428.7</td> <td>-</td> <td></td>	2	†	220	2	~	741	56166		4	~					9	<u>e</u>	29.95	760.7	168	428.7	-	
-3         263         86         3         735         56260         4         2         -4        067         6         .06         66         19         29         55         766.7         165           -1         282         86         3         727         50100         4         2        1        062         .4         .016         66         19         29.95         766.7         166           -1         286         8         3         74         50120         4         2        1        067        2        063         66         19         29.95         766.7         167           -1         253         77         2         741         50120         4         2        1        067        2        063         66         19         29.95         766.7         167           -1         253         77         2         741         50120         4         2        1        067        2        063         66         19         29.95         769.7         167           -2         24         77         50100         4         2        1	2	†	222	2	14	747	<b>3618</b>		+	~		009	ĸ	. 003	99	6	29.92	769.7	169	429.3	<b>-</b> -	
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## NADC-91124-60

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## S-3 NIGHT

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	3		<b>S8</b>	28	38586	37500	36600	37500	37700	990/5	30900	37500	40000	37000	36500	37100	39400	37.500	35766	35700	35500	35388	34700	33900	33600	35200	34100	37000	33788	33788	33300	36289	35400	35200	35900	39800	39400	38500	38800
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	WEIGHT		_	•	17600	17418	17282	17146	17237	1004/	17055	16919	17237	16420	16919	16647	16012	16194	16647	10140	16194	16912	16057	15584	15921	15286	15196	15332	14969	16194	163/3	15286	18699	18144	18853	18099	18189	18053	17917
	*		LBS	<b>59</b>	3888	38400	38100	37800	38000	38999	37600	37300	38666	36200	37300	36700	35300	35700	36788	35696	35700	35300	35400	34400	35100	33700	33500	33800	33000	35700	36166	31700	39998	4000	39800	39900	40100	39800	40500
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DATA - MODEL S-3	WIND-VEL	<u>~</u>	₹	•	•	n	n	~	ימי	) <b>-</b>	) P7	n	n	n	~	<b>n</b>	<b>1</b> 3	ימ	7	2 6	י י	n	<b>7)</b> (	7 F	מי נ	n	n	n	r)	n (	י מ	) 1		17	n	n	n	n	•
8	×	PÆ.	Ş	7	•	17	17	1	_:		: 2	2	1	11	1	_	-	2 :	2:	2 :	: 2	2	17	2 :	- 2	1	17	1	<b>∞</b>	<b>2</b> 9	₽:	2 =	2	5	5	5	5	5	•
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	3	Ş		-	959	956	9211	9212	22	5170	9219	9217	9210	9219	9221	9222	9228	9229	220		927	9235	9236	9237	9239	9241	9242	9244	9245	9246	8248	9220	9294	9295	9236	9297	9536	9299	

	_		Š	21	7826	17736	7826	7554	8899	17418	17690	17373	17690	7282	17237	17146	17055	17237	16919	6874	16965	16783	16647	16647	16556	16647	6284	16466	15967	5558	5422	16057	5332	17010	17010	16874	16783	16406	16194
	WEIGHT		LBS	<b>50</b>	•	•	_	- '	_ •				- '											•	•		•				_	_ '	_						
õ			_	**	39300	39100	39300	38700	39999	38400	39000	38300	39888	20100	38666	37800		38999	37300	37200	3/400		36700	36700	36500	36700	35900	36300	35200	34300	34000			37500	37500	37200	37000	20200	32/88
ANDING	LIFE	<u> </u>		6													1.10	1.00			8	3											1.10						
NIGHT LANDINGS	LIFT	2		₽	<b>8</b> .	1.00	- 19	1. 9. 9.	-	1.10	1.10	1.00	 	e :	 60		1.10	1.66	- .8	<b>8</b>	9	98	1.88	- .98	1.20	8. 6	1.00	1.20	- 8	1.20	1.10	- 10	- 10	<b>6</b> 6.	1.50		8 8	8 :	
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62)	V.dSA		<b>¥</b>	5																																			
USS ENTERPRISE (CVN-65)	Ş		ž	<b>±</b>																																			
RISE	VPAMIN		<b>¥</b>	5	56	28			6 % 6 %						S &						8			5.	* *		6 2			52									3
ENT ERF	\$		\$	7	5	168	<u></u>	5	9 6	107	168	197	2 :	107	167	19.7	100	107	106	196	96.		105	105	105	105	167	10	103	101	101	163	<u>•</u>	100	106	100	165	10	104
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2		PERP.	Ş	•	7	~	~	~	N 6	٠ ٦	~	N	~	N (	<b>~</b> c	4 0	۱ ۲۷	8	~	~	~ <	4 6	· ~	~	N	~ (	4 6	۰ ۵	~	~	7	7	7	~	n	7	י ניו	r) (	n
EL S-3	WIND-VEL	Δ.	2	•	n	n	ח	<b>"</b>	7	) P)	~	n	~ '	ים	r) r	) M	7	n	2	n	· ·	7	•	~	n	<b>"</b>	) F	) P7	7	n	n	n	n	en i	'n	S	<b>9</b> 0 1	ים	n
- 140061	X	PA.	<b>\$</b>	_	5	5	5	5 ;	5 5	5	2	5	5 :	2	5 t	2 5	2	5	5	5	2 :	2 \$	2	5	_			2	5	5	5	_	_	- 5	5	5	5	<u>.</u>	5
DATA	_		<b>∑</b>		7	7	7	<b>3</b> :	3 P	<b>5</b> 5	3	3	<b>3</b> 2	3	3 7	3 7	8 8	3	7	<b>3</b>	3 :	3 2	3	7	7	<b>3</b>	5 5	3 3	3	3	7	3	7	3	3	3	<b>3</b>	<b>3</b>	3
LANDING	VE-F1UA		<b>\$</b>	60	52	3	\$	5	3 3	3	7	\$	<b>;</b>	3 ;	\$	\$ \$	\$	\$	\$	\$		3 3	_	47		-			_	-					 5	2	<b>?</b> :	P :	\$
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	9	ĕ		-	3	Š	2	3		9316	9312	25	110	2	500		925	9321	9322	9323	324	220	9228	9329	3	9332	3 2	575	25.0	33	3	241	9346	9456	370	9462	9464	9469	9472

			NE ON	0	ATA -	DATA - MODEL	3		7	SS EN	TERPR	USS ENTERPRISE (CVN-65,	<del>∑</del> <del>}</del>	3			NIGHT	NIGHT LANDINGS		
997	\$	VPAF	VE-F1	3		WIND-VEL	VEL		Ā	VEOR	VPAMIN	z	V.dSA	<b>.</b> <	KVPA	\$	LIFT	LIFT	WEI	WEIGHT
į	F	5			<u>a</u>	PAR.	90	<u>م</u>							Z	<b>∀</b> .dS	5	33		
	Ş	\$	Š	\$	\$	\$	\$	Ş	- 3	Ş	₹ 2	s/n	z X	N/S					rBs	Š
_	~		•	•	•	^	•	•	•	=	2	£	<b>±</b>	5	5	11	<b>5</b>	6	<b>59</b>	21
*2*	123	3	2	\$	3	5	•	n			103	3			1.10		1.10		35166	15921
173	122		85	+	3	15	80	n			100	S			1.18		<b>8</b> .		35800	16239
477	120		2	<b>\$</b>	3	5	80	n			163	S			1.16		1.20		35500	16103
<b>\$</b>	2		7	8	3	5	40	<b>n</b>			103	3			1.03		96		35000	15876
5	126		8	\$	3	5	10	2			102	25			1.23		1.20		34900	15831
3	22		8	\$	3	5	•	n			102	25			1.22		1.88		34788	15740
542	121		ž	\$	27	<b>±</b>	~	_			107	55			1.14		1.10		37800	17146
556	=		6	<b>\$</b>	21	<b>±</b>	~	_			105	54			1.08		1.10		37000	16783
366	117		2	9	27	<b>±</b>	~	_			105	54			1.1		- 8		36700	16647
565	123		20	\$	3	15	n	7			105	5			1.18		8		36400	16511
369	=		2	2	3	5	n	7			<u>1</u>	3			1.09		1.00		36300	16466
575	122		87	47	3	5	n	~			104	33			1.18		1.00		35800	16239
287	8		7	37	28	<u>*</u>	ĸ	-			102	25			.97		1.10		34700	15740

PORT STBO ANG FREF-FLIGHT BHM BW BW BW BW BW BW BW BW BW BW BW BW BW	PORT         STREP FLIGHT         BMM         FOUR PAMP           f/S         M/S         F/S																		
## ## ## ## ## ## ## ## ## ## ## ## ##	1, 2, 10, 10, 10, 10, 10, 10, 10, 10, 10, 10	0	ŞE	2	R.	ST	2	AVG		FREE-FL	IGHT	<b>E</b>		8	>	OVER	SAMP	8	SAMP.
### 25	9.1         2.8         27         26         29         31         32         33         34         35         36         37         38           7.2         2.8         8.6         2.6         8.7         2.0         8.9         2.7         8.9         35         86         9.9         37         38         37         38           1.0         2.2         8.6         2.6         8.9         2.7         8.9         3.7         86         8.9         3.7         86         8.9         3.7         86         8.9         3.7         86         8.9         3.7         8.9         8.9         3.7         8.9         3.9		Ş	5	Ş	٤	Ş	2	Ş	r/s	N/S	DEG	2	DEC	2	E	3	E	3
9.1 2.8 19.4 2.6 9.7 2.8 9.8 3.9 9.8 3.9 9.8 3.9 9.8 3.9 9.8 3.2 9.7 2.8 9.8 2.8 2.8 9.8 2.7 2.8 9.8 2	9.1 2.8 19.4 3.2 9.7 3.9 9.8 3.9 3.9 3.9 3.9 3.9 3.9 3.9 3.9 3.7 3.9 3.9 3.9 3.9 3.9 3.9 3.9 3.9 3.9 3.9		*	ន	<b>38</b>	22	<b>58</b>	2	8	5	32	33	ħ	SS.	92	37	8	80	9
9.2 2.8 8.6 2.6 9.3 2.8 6.9 2.7 2.8 1.3 2.8 1.8 2.6 8.5 2.8 6.9 2.7 2.8 2.8 2.8 2.8 2.8 2.8 2.8 2.8 2.8 2.8	9.2 2.8 8.6 2.6 9.3 2.8 6.9 2.7 2.7 3.4 10.8 2.8 8.5 2.6 8.5 2.8 8.9 2.7 2.8 8.9 2.7 2.8 8.9 2.7 2.8 8.9 2.7 2.8 8.9 2.7 2.8 8.9 2.7 2.8 8.9 2.7 2.8 8.9 2.7 2.8 8.9 2.7 2.8 8.9 2.7 2.8 8.9 2.7 11.8 2.8 8.9 2.7 11.8 2.8 8.9 2.7 11.8 2.8 8.9 2.7 11.8 2.8 8.9 2.7 11.8 2.8 8.9 2.7 11.8 2.8 8.9 2.7 11.8 2.8 8.9 2.7 11.8 2.8 8.9 2.7 11.8 2.8 8.9 2.7 11.8 2.8 8.9 2.7 11.8 2.8 8.9 2.7 11.8 2.8 8.9 2.7 11.8 2.8 8.9 2.7 11.8 2.8 8.9 2.8 2.8 2.8 2.8 2.8 2.8 2.8 2.8 2.8 2.8		2.6	<b>9</b> .1	2.8	10.4	3.2	9.7	<b>5</b> .	<b>9</b> .8	3.0			3.5	. 666				
7.8 2.4 8.7 2.6 8.5 2.6 8.5 2.6 8.5 2.7 3.8 4 8.7 2.6 8.5 2.7 3.8 4 8.7 2.6 8.5 2.7 3.8 4 8.7 2.6 8.8 2.7 3.8 4 8.7 2.6 8.8 2.7 3.8 4 8.7 2.6 8.8 2.7 3.8 4 8.7 2.6 8.8 2.7 3.8 4 8.7 2.8 8.8 2.7 3.8 3.8 4 2.8 8.8 2.7 3.8 3.8 4 2.8 8.8 2.7 3.8 3.8 4 2.8 8.8 2.7 3.8 3.8 3.8 3.8 3.8 3.8 3.8 3.8 3.8 3.8	7.8 2.4 8.7 2.6 8.5 2.6 8.8 2.8 8.8 2.8 8.8 2.4 8.7 2.6 8.5 2.6 8.8 2.7 2.8 8.5 2.6 8.8 2.7 2.8 8.8 2.4 8.7 2.8 8.8 2.4 8.7 2.8 8.8 2.4 8.7 2.8 8.8 2.7 3.8 4.8 2.4 8.8 2.7 3.8 4.8 2.8 3.8 8.8 2.4 3.8 3.1 18.2 2.1 18.2 2.1 18.3 2.1 18.2 2.1 18.3 2		2.7	9.7	2.8	<b>9</b> .0	5.6	<b>9.</b> 3	2.8	9.9	2.7			4.6	.059				
10.8 5.3 8.4 2.6 8.7 2.9 8.7 2.9 8.8 2.7 2.9 8.8 2.7 2.9 8.8 2.7 2.9 8.8 2.7 2.9 8.8 2.7 2.9 2.9 2.9 2.9 2.9 2.9 2.9 2.9 2.9 2.9	10.8 5.3 8.4 2.6 8.7 2.9 8.7 2.9 8.8 2.7 2.9 8.8 2.7 2.9 8.8 2.7 2.9 8.8 2.7 2.9 8.8 2.7 2.9 8.8 2.7 2.9 8.8 2.7 2.9 8.8 2.7 2.9 8.8 2.7 2.9 2.9 2.1 10.2 2.		7.0	7.8	7.4	8.7	5.6	8.5	5.6					2.7	. 647				
8.3 2.5 8.6 2.4 8.8 2.7 8.8 2.7 8.8 8.8 2.7 8.8 8.8 2.7 8.8 8.8 2.7 8.8 2.1 16.2 3.1	8.3 2.5 8.6 2.4 8.8 2.7 2.7 2.8 3.9 3.9 3.1 3.6 3.9 3.1 3.6 3.9 3.1 3.6 3.1 3.6 3.9 3.1 3.6 3.1 3.1 3.1 3.1 3.1 3.1 3.1 3.1 3.1 3.1		2.5	e. =	n. n	<b>4</b> .	<b>5.6</b>	<b>9</b> .7	<b>5</b> .8					4.	999.				
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11.3 3.4 12.3 3.7 11.8 3.6 16.2 2.1 16.	11.3 3.4 12.3 3.7 11.8 3.6 19.8 2.1 19.2 2.1 19.2 2.1 19.2 2.1 19.2 2.1 19.2 2.1 19.2 2.1 19.2 2.1 19.2 2.1 19.2 2.1 19.2 2.1 19.2 2.1 19.8 19.8 19.8 19.8 19.1 19.2 2.1 19.8 19.8 19.8 19.8 19.8 19.8 19.8 19		2.7	<b>.</b>	٠. د	<b>.</b>	<b>7</b> .	o. 0	2.7					7. 9.	. 656				
19.2  3.1  19.2  3.1  19.2  3.1  19.2  3.1  19.2  3.1  19.2  3.1  3.2  3.3  3.3  3.3  3.3  3.3  3	10.2 3.1 10.2 3.2 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0		4.5	2.2	4.0	12.3	3.7	11.8	3.6					G. 5	. 969				
6.8 5.7 1.7 6.8 5.2 1.6 5.2 1.8 6.8 5.7 1.8 6.8 5.7 1.8 6.8 5.7 1.8 6.8 5.7 1.8 6.8 5.7 1.8 6.8 5.7 1.8 6.8 5.7 1.8 6.8 5.7 1.8 6.8 5.7 1.8 6.8 5.7 1.8 6.8 5.7 1.8 6.8 5.8 1.8 6.8 5.8 1.8 6.8 5.8 5.8 5.8 5.8 5.8 5.8 5.8 5.8 5.8 5	5.8 2.1 7.1 2.2 6.8 2.1 6.4 1.2 7.1 2.2 6.8 2.1 6.4 1.2 7.2 6.8 2.1 6.4 1.2 7.2 6.8 2.1 6.4 1.2 7.2 6.8 2.1 6.4 1.2 7.2 6.8 2.1 6.4 1.2 7.2 6.8 1.8 5.2 1.8 5.		٠. ٥.	10.2	J. 7	19.2	٦. ۲.	10.2	J. 7					3.5	.061				
5.6 5.7 5.2 5.6 5.7 5.7 5.6 5.7 5.7 5.7 5.7 5.7 5.7 5.7 5.7 5.7 5.7	5.6 1.6 5.1 1.6 5.2 1.6 5.2 1.6 5.2 1.6 5.2 1.6 5.2 1.6 5.2 1.6 5.2 1.7 7.9 5.9 1.8 5.9 1.8 5.9 1.8 5.9 1.8 5.9 1.8 5.9 1.8 5.2 1.7 7.9 5.9 1.8 5.9 1.8 5.9 1.8 5.9 1.8 5.9 1.8 5.9 1.8 5.9 1.8 5.9 1.8 5.9 1.8 5.9 1.8 5.9 1.8 5.9 1.8 5.9 1.8 5.9 1.8 5.9 1.8 5.9 1.8 5.9 5.9 5.9 5.9 5.9 5.9 5.9 5.9 5.9 5.9		<b>.</b>	6.9	2.1	7.1	2.2	<b>8</b> .9	2.1					<b>5</b> .6	.046				
10.4 3.2 8.9 2.7 10.0 3.1 10.0	19.4 3.2 8.9 2.7 19.6 3.1 1.9 1.9 1.9 1.9 1.9 1.9 1.9 1.9 1.9 1		<b>+</b>	S.0	<b>.</b>	5.1	7.6	5.2	9.					1.7	. 030				
5.7 5.7 5.7 5.7 5.7 5.7 5.7 5.7	5.7 1.7 7.6 2.1 6.3 1.9 1.8 2.4 1.9 2.4 2.4 2.8 2.8 1.8 6.9 1.8 2.4 2.4 2.4 2.4 2.4 2.8 6.8 1.8 2.4 2.4 2.4 2.8 6.8 1.8 6.8 1.8 6.8 1.8 6.8 1.8 6.8 1.8 6.8 1.8 6.8 1.8 6.8 1.8 6.8 1.8 6.8 1.8 6.8 1.8 6.8 1.8 6.8 1.8 6.8 1.8 6.8 1.8 6.9 1.8 1.8 6.9 1.8 1.8 6.9 1.8 1.8 6.9 1.8 1.8 6.9 1.8 1.8 6.9 1.8 1.8 6.9 1.8 1.8 6.9 1.8 1.8 1.8 6.9 1.8 1.8 1.8 6.9 1.8 1.8 1.8 1.8 1.8 1.8 1.8 1.8 1.8 1.8		7.4	19.4	3.2	0.	2.7	10.0	7.					٦. د.	. 053				
19.8	19.8 3.3 9.9 2.7 10.4 3.2 7.9 2.4 7.9 2.4 7.9 2.4 7.9 2.4 7.9 2.4 7.9 2.4 7.9 2.4 7.9 2.4 7.9 2.4 7.9 2.4 7.9 2.4 7.9 2.4 7.9 2.5 2.5 2.2 8.0 2.4 2.5 2.5 2.5 8.0 2.4 8.7 2.7 2.3 8.5 2.6 8.0 2.4 8.7 2.7 2.3 8.5 2.6 8.0 2.4 7.1 2.2 7.2 2.3 8.5 2.6 8.0 2.4 7.1 2.2 7.1 2.2 2.3 8.5 2.6 8.0 2.4 7.1 2.2 7.1 2.2 2.3 8.5 2.6 8.0 2.4 7.1 2.2 2.3 8.5 2.5 8.0 2.1 7.1 2.2 2.3 8.5 2.3		-	5.7	1.7	7.	7.7	6.3	0.					6.	.034				
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7.9	7.9 2.4 7.6 2.4 7.9 2.4 7.9 2.4 7.9 2.4 7.9 2.4 7.9 2.4 7.9 2.4 7.9 2.4 7.9 2.4 7.9 2.4 7.9 2.4 7.9 2.5 9.1 2.8 8.2 2.5 9.1 2.8 8.2 2.5 9.1 2.8 8.9 2.4 8.7 2.7 2.3 8.5 2.6 8.9 2.4 8.7 2.7 2.3 8.5 2.6 8.9 2.1 7.9 2.7 7.9 2.7 7.9 2.1 7.9 2.1 7.9 2.1 7.9 2.7 7.9 2.1 7.9 2.		£.	5.7	1.7	9	-	6.0						6.	. 831				
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7.3 2.2 2.9 6.6 2.4 6.7 2.4 6.7 2.7 2.4 6.7 2.4 6.7 2.7 2.7 2.8 6.8 6.8 2.4 6.7 2.7 2.7 2.8 6.8 6.8 2.4 6.7 2.7 2.7 2.8 6.8 6.8 2.4 6.7 2.7 2.7 2.8 6.8 6.8 2.4 2.7 2.7 2.7 2.8 6.8 6.8 2.4 2.7 2.7 2.7 2.8 6.8 6.8 2.7 2.8 2.7 2.8 2.4 2.8 2.4 2.8 6.8 2.4 2.8 2.7 2.8 2.4 2.8 2.8 2.4 2.8 2.8 2.7 2.8 2.8 2.7 2.8 2.8 2.7 2.8 2.8 2.7 2.8 2.8 2.7 2.8 2.8 2.7 2.8 2.8 2.7 2.8 2.8 2.7 2.8 2.8 2.7 2.8 2.8 2.7 2.8 2.8 2.8 2.7 2.8 2.8 2.8 2.8 2.8 2.8 2.8 2.8 2.8 2.8	7.3 2.2 9.1 2.8 9.2 2.5 7.7 2.9 10.8 2.4 9.6 2.4 9.7 2.7 2.7 2.3 9.6 2.4 9.7 2.7 2.7 2.3 9.6 9.5 2.8 9.6 2.4 9.7 2.7 2.3 9.6 9.5 2.4 9.7 2.7 2.3 9.6 9.5 2.4 9.7 2.7 2.3 9.6 9.5 2.4 9.7 2.7 7.8 2.3 5.9 1.8 6.9 2.1 7.0 2.1 1.9 7.2 2.2 7.8 9.8 2.7 10.2 2.3 11.0 7.2 2.2 2.8 9.1 2.8 9.3 2.8 9.3 2.8 9.3 2.8 9.3 2.8 9.3 2.8 9.3 2.8 9.3 2.8 9.3 2.8 9.3 2.8 9.3 2.8 9.3 2.8 9.3 2.8 9.3 2.8 9.3 2.8 9.7 2.9		1.7	5.0		5.0	<b>.</b>							0.	424				
9.6 2.9 10.8 2.4 10.1 2.7 2.7 2.2 2.9 2.4 2.7 2.7 2.3 3.9 2.4 3.1 10.1 2.7 2.7 2.3 3.9 2.4 3.1 10.1 2.7 2.7 2.3 3.9 2.4 3.2 3.1 10.1 2.7 2.7 2.3 2.9 2.7 2.7 2.7 10.2 2.7 2.7 10.2 2.7 2.8 10.2	9.6 2.9 10.8 3.3 10.1 3.1 5.7 2.2 2.9 5.9 1.8 7.9 2.4 2.7 2.7 2.3 8.5 2.6 8.9 2.4 2.7 2.7 2.3 8.5 2.6 8.9 2.4 2.7 2.7 2.3 5.9 1.8 6.9 2.1 7.9 2.1 1.9 7.2 2.3 5.9 1.8 6.9 2.1 7.9 2.1 1.9 7.2 2.2 2.3 5.9 1.8 7.1 2.2 2.2 2.3 11.8 7.2 2.2 2.8 5.3 11.9 7.2 2.2 2.8 5.3 11.9 7.2 2.8 5.3 11.9 7.2 2.8 5.3 11.9 7.2 2.8 5.3 11.9 7.2 2.8 5.3 11.9 7.2 2.8 5.3 11.9 7.2 2.8 5.3 11.9 7.2 2.8 5.3 5.9 5.3 5.9 5.3 5.9 5.9 5.9 5.9 5.9 5.9 5.9 5.9 5.9 5.9		2.7	7.3	7.7	-	2.8	8.3	2.5					2.4	. 042				
9.5 2.9 8.9 2.4 8.7 2.7 7.9 8.9 2.4 8.7 2.7 7.9 8.9 2.4 8.7 2.7 7.9 8.9 7.1 8.9 7.9 7.1 8.9 7.9 7.9 8.9 7.1 8.9 7.9 7.9 8.9 7.1 8.9 7.9 8.9 7.1 8.9 7.1 8.9 7.1 8.9 7.1 8.9 7.1 8.9 7.1 8.9 7.1 8.9 7.1 8.9 7.1 8.9 7.1 8.9 7.1 8.9 7.1 8.9 7.9 8.9 8.9 7.9 8.9 8.9 7.9 7.9 8.9 7.9 7.9 8.9 7.9 7.9 7.9 7.9 7.9 7.9 7.9 7.9 7.9 7	9.5 2.9 8.9 2.4 8.7 2.7 7.5 2.3 8.5 2.6 8.9 2.4 7.7 2.7 7.5 2.3 8.5 2.6 8.9 2.4 7.9 2.1 7.9 2.1 7.9 2.1 7.9 2.1 7.9 2.1 7.9 2.1 7.9 2.1 7.9 2.1 7.9 2.1 7.9 2.1 7.9 2.1 7.9 2.1 7.9 2.1 7.9 2.1 7.9 2.2 7.7 10.2 2.2 2.8 8.0 2.4 10.2 2.8 9.2 2.8 9.1 2.6 9.3 2.8 9.3		2.5	0.0	7.0	£.8	2.0	1.01	7.					3.6	. 962				
7.7 2.3 6.5 2.6 6.0 2.4 7.5 2.5 2.6 6.1 1.9 7.6 2.1 7.6 2.1 1.9 7.6 6.1 1.9 7.6 6.9 2.1 7.6 2.1 7.2 2.1 7.2 2.1 7.2 2.2 7.2 7.2 7.2 7.2 7.2 7.2 7.2 7.2	7.7 2.3 8.5 2.6 8.0 2.4  5.8 1.8 7.0 2.1 6.1 1.9  7.5 2.3 5.0 1.8 7.0 2.1  7.5 2.3 5.0 1.8 7.1 2.2  8.2 2.7 10.4 3.2 9.0 2.7  7.6 2.4 10.2 3.1 9.2 2.8  9.1 2.6 9.5 2.9 9.3 2.8  9.6 2.4 7.9 2.4 9.2 2.8  9.8 2.4 7.9 2.4 9.2 2.8  9.8 2.7 3.9 9.3 2.8  9.8 2.7 3.9 9.3 2.8  9.8 2.7 3.9 9.3 2.8  9.8 2.7 3.9 9.3 2.8  9.8 2.7 3.9 2.4 3.2 9.2  9.8 2.7 3.9 2.4 3.2  9.8 2.7 3.9 2.4 3.2  9.8 2.7 3.9 2.7 3.9  9.8 2.7 3.9 2.9 3.7  9.8 2.7 3.9 2.7 3.9  9.8 2.7 3.9 2.7 3.9  9.8 2.7 3.9 2.7 3.9  9.8 2.7 3.7 3.7 3.8 2.9  9.9 2.7 3.7 3.8 2.9  9.1 2.8 6.0 1.4 4.6 1.4  9.7 2.7 2.7 3.8 2.7  9.7 2.7 3.8 2.7 2.7 3.8 2.7  9.7 2.7 3.7 3.7 3.8 2.7  9.8 2.7 3.7 3.7 3.8 2.7  9.8 2.7 3.7 3.7 3.8 2.7  9.8 2.7 3.7 3.7 3.8 2.7  9.8 2.7 3.7 3.7 3.8 2.7  9.8 2.7 3.7 3.7 3.8 2.7  9.8 2.7 3.7 3.7 3.8 2.7  9.8 2.7 3.7 3.7 3.8 2.7  9.8 2.7 3.7 3.7 3.8 2.7  9.8 2.7 3.7 3.7 3.8 2.7  9.8 2.7 3.7 3.7 3.8 2.7  9.8 2.7 3.7 3.7 3.8 2.7  9.8 2.7 3.7 3.7 3.8 2.7  9.8 2.7 3.7 3.7 3.8 2.7  9.8 2.7 3.7 3.7 3.8 2.7  9.8 2.7 3.8 2.8 3.8 3.8 3.8 3.8 3.8 3.8 3.8 3.8 3.8 3		2.3	9.5	0.	•	2.4	8.7	2.7					3.0	. 052				
5.8 1.8 7.9 2.1 6.1 1.9 6.2 2.3 2.3 2.3 2.4 2.3 2.4 2.3 2.4 2.4 2.4 2.4 2.4 2.4 2.4 2.4 2.4 2.4	5.8 1.8 7.0 2.1 6.1 1.9 7.5 2.3 7.0 2.1 7.2 2.2 7.2 7.2 7.2 7.2 7.2 7.2 7.2 7.2		7.7	7.7	2.2	8.5	2.6	8.0	2.4					3.0	. 053				
5.9 1.8 6.9 2.1 7.0 2.1 1.8 6.2 2.2 2.2 2.2 2.2 2.3 2.3 11.0 2.3 2.3 2.3 2.3 2.3 2.3 2.3 2.3 2.3 2.3	7.5 2.3 5.9 1.8 6.9 2.1 7.0 2.1 6.9 2.1 7.0 2.1 7.0 2.1 7.0 2.1 7.0 2.2 2.2 2.3 5.9 1.0 7.1 2.2 2.2 2.3 5.9 1.0 7.1 2.2 2.3 5.9 1.0 7.1 2.2 2.3 5.9 1.0 7.2 2.2 2.3 5.9 1.0 7.2 2.2 2.3 5.1 1.0 5.3 11.0 5.3 11.0 5.3 11.0 5.3 11.0 5.3 11.0 5.3 11.0 5.3 11.0 5.3 11.0 5.3 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0		2.5	5.0	<b>.</b>	7.0	2.1	6.1	<b>.</b>					2.2	. 638				
7.5 2.3 5.9 1.8 7.1 2.2 2.7 2.8 6.2 1.8 7.1 2.2 2.7 2.8 6.2 1.8 7.1 2.2 2.7 2.8 6.2 1.9 7.2 2.2 2.8 7.8 5.8 11.0 2.3 11.	7.5 2.3 5.9 1.8 7.1 2.2 8.8 8.2 1.8 7.1 2.2 8.9 8.7 2.2 8.8 8.2 8.7 10.5 3.2 9.9 2.7 8.8 8.8 8.3 11.9 3.3 10.2 3.1 8.3 10.2 3.1 8.3 10.2 3.1 8.3 10.2 3.1 8.3 10.2 3.1 8.3 10.2 3.1 8.3 10.2 3.1 8.3 10.2 3.1 8.3 10.2 3.1 8.3 10.2 3.1 8.3 10.2 3.1 8.3 10.2 3.1 8.3 10.2 3.1 8.3 10.2 3.1 8.3 10.2 3.1 8.3 10.2 3.1 8.3 10.3 10.3 10.3 10.3 10.3 10.3 10.3 10		<b>.</b>	5.0	<b>9</b> .	6.9	2.1	7.0	2.1					2.4	. 041				
8.2 2.3 10.4 3.2 9.9 2.7 7.8 2.4 10.2 3.3 10.2 2.8 2.7 10.3 3.3 10.2 2.8 2.7 10.3 3.3 10.2 2.8 2.8 2.4 10.2 2.8 2.8 2.4 10.2 2.8 2.8 2.4 10.2 2.8 2.8 2.8 2.8 2.8 2.8 2.8 2.8 2.8 2	8.2 2.5 6.2 1.9 7.2 2.2 7 8.8 2.7 16.8 3.3 11.0 3.3 16.2 3.1 7.2 2.2 7 8.8 2.4 16.2 3.1 9.2 2.2 7 8.8 2.4 16.2 3.1 9.3 2.8 9.3 2.7 9.3 9.3 2.7 9.8 9.3 2.7 9.8 9.3 2.7 9.3 9.3 2.7 9.3 9.3 2.7 9.3 9.3 2.7 9.3 9.3 2.7 9.3 9.3 2.7 9.3 9.3 9.3 9.3 9.3 9.3 9.3 9.3 9.3 9.3		<b>9</b> .	7.5	2.3	3.0	<b>9</b>	7.1	2.2					2.5	. 043				
8.2 2.5 6.2 1.9 7.2 2.2 8.8 2.7 16.5 3.2 9.2 2.8 7.8 2.4 16.2 3.1 9.2 2.8 7.8 2.4 16.2 3.1 9.2 2.8 7.8 2.4 16.2 3.1 9.2 2.8 7.8 2.4 16.2 3.1 9.3 2.8 9.3 2.8 9.3 2.8 9.3 2.8 9.3 2.8 9.3 2.8 9.3 2.8 9.3 2.8 9.3 2.8 9.7 2.9 9	8.2 2.5 6.2 1.9 7.2 2.2 2.8 5.3 11.0 5.3 10.2 2.8 7.8 7.2 2.8 7.8 2.4 10.2 5.1 9.2 2.8 7.8 2.4 10.2 5.1 9.3 2.8 9.1 2.8 9.3 9.3 9.3 9.3 9.3 9.3 9.3 9.3 9.3 9.3		7.6	6.7	7.0	÷.	3.2	•	2.7					3.1	.054				
8.8 2.7 16.3 3.2 9.2 2.8 7.8 2.4 10.2 3.1 9.3 2.8 7.8 2.4 10.2 3.1 9.3 2.8 7.8 2.4 10.2 3.1 9.3 2.8 7.8 2.4 10.2 3.1 9.3 2.8 7.8 2.4 7.8 2.4 9.2 2.8 7.8 2.4 7.8 2.4 7.8 2.4 7.8 2.4 7.8 2.4 7.8 2.4 7.8 2.4 7.8 2.4 7.8 2.8 9.7 2.9 9.7 2.9 9.7 2.9 9.7 2.9 9.7 2.9 9.7 2.9 9.7 2.9 9.7 2.9 7.8 2.7 3.5 1.1 6.6 2.9 7.4 7.8 2.7 3.5 1.1 6.6 2.9 7.4 7.8 7.7 2.9 7.7 2.3 7.7 2	8.8 2.7 16.3 3.2 9.2 2.8 7.8 2.4 16.2 3.1 9.3 2.8 9.1 2.8 9.3 11.0 3.3 11.0 3.3 11.0 3.3 11.0 3.3 11.0 3.3 11.0 3.3 11.0 3.3 11.0 3.3 11.0 3.3 11.0 3.3 11.0 3.3 2.8 9.3 2.8 9.3 2.8 9.2 2.8 9.2 2.8 9.2 2.8 9.2 2.8 9.2 2.8 9.7 2.9 9.7 2.9 9.7 2.9 9.7 2.9 9.7 2.9 9.7 2.9 9.7 2.9 9.7 2.9 9.7 2.9 9.7 2.9 9.7 2.9 9.7 2.9 9.7 2.9 9.1 1.1 6.6 2.0 9.1 9.8 2.7 9.8 9.8 9.8 9.8 9.8 9.8 9.8 9.8 9.8 9.8		2.4	8.2	2.5	6.2	<b>0</b> .	7.2	2.5					5.6	. 046				
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9.1 2.6 9.5 2.9 9.3 2.6 8.6 2.6 2.6 3.0 3.8 2.7 8.8 2.7 8.4 2.6 8.8 2.7 8.4 2.6 3.9 3.0 3.8 3.6 8.8 2.7 8.4 2.6 3.9 3.7 8.8 2.4 7.9 2.4 2.5 2.9 3.7 2.9 3.8 2.7 3.5 1.1 6.6 2.9 3.9 3.0 3.8 2.7 3.5 1.1 6.6 2.9 3.9 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0	9.1 2.6 9.5 2.9 9.3 2.6 8.6 2.6 2.6 2.6 2.6 3.2 7.8 2.4 9.2 2.8 8.8 2.7 8.4 2.6 3.9 8.7 2.9 8.7 2.9 8.7 2.9 8.7 2.9 8.7 2.9 8.7 2.9 8.7 2.9 8.7 2.9 8.8 2.7 3.8 1.8 3.5 1.1 4.6 1.4 4.6 1.4 4.6 1.4 4.6 1.4 4.6 1.4 4.6 1.4 4.6 1.4 4.6 1.4 4.6 1.4 2.8 8.8 2.7 2.7 8.8 2.7 2.3 8.6 2.9 1.8 7.7 2.3 8.6 2.7 2.7 2.3 8.6 2.7 2.7 2.3 8.7 2.7 2.3 8.7 2.7 2.3 2.7 2.7 2.3 2.7 2.7 2.9 2.6 1.9 2.7 2.7 2.7 2.7 2.9 2.6 1.9 2.7 2.7 2.7 2.7 2.9 2.8 2.7 2.7 2.7 2.9 2.7 2.7 2.9 2.8 2.7 2.7 2.7 2.9 2.8 2.7 2.7 2.7 2.7 2.9 2.8 2.7 2.7 2.7 2.9 2.7 2.7 2.9 2.7 2.7 2.9 2.7 2.7 2.9 2.7 2.7 2.9 2.7 2.7 2.9 2.7 2.7 2.9 2.7 2.7 2.9 2.7 2.7 2.9 2.7 2.7 2.9 2.7 2.7 2.9 2.7 2.7 2.9 2.7 2.7 2.9 2.7 2.7 2.9 2.7 2.7 2.9 2.7 2.9 2.7 2.9 2.7 2.9 2.7 2.9 2.7 2.9 2.7 2.9 2.7 2.9 2.7 2.9 2.7 2.9 2.7 2.9 2.9 2.7 2.9 2.9 2.9 2.9 2.9 2.9 2.9 2.9 2.9 2.9		2.6	7.8	7.4	10.2	 T.	5.0	8.8					J. J	. 058				
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7.8 2.4 7.9 2.4 8.2 2.5 8.8 8.8 2.7 3.5 9.5 2.9 8.8 2.7 3.5 1.1 6.6 2.0 1.7 8.8 2.7 8.8 1.8 3.5 1.1 4.6 1.4 1.4 1.4 1.4 1.4 1.4 1.4 1.4 1.4 1.4	7.6 2.4 7.9 2.4 6.2 2.5 2.6 8.6 2.6 10.7 3.3 9.5 2.9 2.9 2.9 2.9 2.7 3.5 1.1 6.6 2.0 1.4 6		9.0	9.8	9.0	9.3	2.9	9.7	2.9					3.8	990.				
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NIGHT LANDINGS

USS ENTERPRISE (CVN-65,

TA-3 DAY

no#

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ноок нејснт	OVER RAMP	E	92																																			
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AT TD	BV.	3	ş	.047	. 063	.054	. 647	.058	.636	. 969	e. 64.0	679. 196	.633	. 053	.043	810.	. 026	.042	. 958 	• • • •	. 672	.061	.046	.043	. 659	986	.048	.055	.054	.048	929	.033	.051	.079	990.	.046	. 640 	.056
WGLE	Ď	DEC	85	2.7	3.6	3.1	2.7	3.3	1.7	J.5	2.7	· •	6.	3.1	2.5	- 0.	1.5	7.4		2.5 7.5	, <del>4</del>	5.5	2.7	2.5	4.6	2 K	2.7	3.2	٠. ا	2.8	•	0.	2.9	4.0	S. 3	9.0	7. 10. 10.	3.2
PATH /	3	3	ž																																			
GLIDE PATH ANGLE AT TD		DEG	33																																			
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2	_	<b>\$</b>	8	2.2	2.8	2.6	6.	2.8	9.	<b>3.</b> 0	o .		1.7	2.7	2.2	1.2	•.	<b>a</b> . (		7.7	- 4	4.0	2.4	1.7	+ ·	7 7. 7.7	2.4	2.7	2.7	2.7		9.6	2.7	4.2	4.6	2.6 0.0	<b>6</b> .0	2.5
SINKING SPEED AT TOUCHDOWN	AVG	5	8	7.1		4.0	6.3	9.2	5.2	6.7	?.0		5.5	9.0	7.4	<b>•</b> .	5.5	6.2		7.7		7.5	7.9	5.7	ا - ا	7.7	7.0	<b>9.</b> 0		. v	9	6.7	9.0	3.7	1.2	8. G	o .	. +
ED AT		\$	<b>58</b>	1.8	2.5	7.4	2.7	2.8	S	4.0	* .		*	2.6	2.1	-:	 5.	<b>9</b> 1	7.7	· •	9 10	4.0	2.7	<b>.</b>	י פיק	3.0	2.4	2.9	9.6	, , , , , , , , , , , , , , , , , , ,		7.4	2.8	3.6	5.5	۲.,	2.5	 
365 296	STBO	2	23	•	n.	7.8	7.2		<del>-</del>	- (	•	• •		6.5	6.0	٠.	e.	5.G				2.	8.9	-	•		•	'n.	•	<b>.</b>	•		-	•	_	8.7		^ <b>→</b>
SINKI			_	8		•	7	7	 	·	D ,		4	0	•	n n	4	<b>.</b>	<b>D</b> (	n 0	•=	=		9	2 12	3 12.6	4	•		\ ;	2 6		7 9	7 12.0	-	<b>D</b>	2 '	, . , .
AIRCRAFT	For	Ş	2	સં	'n	ä	<u>-</u>	ä	÷	ri (	'n·		; <b>-</b>	'n	4	<b>-</b>	<u>-</u>	٠i ،	n (	, ,	, w	'n	<u>-</u>	<b>-</b> 1	ri (	i n	6	તં	તં (	, ,	i	; <b>-</b>	7	÷	'n	લં	ri (	i i
¥.	_	2	22	8.3	<b>9</b> .0	8.5	5.2	8.7	•	= '		7 .	8		8.5	4.2	5.5		* •	7.5	2	=		4.5	5.5	16.7	7.9	4.0	- (	9 :	. =	8	8.0	13.4	11.2	7.6	<b>a</b> (	
	NOSE	\$	7	2.2	5.9	2.7	-	7.4	e,	6.0	, i	,	2.1	2.5	2.5	7.7	1.7	1.7	2.7	7. P		•	7.7	2.0	'n	2.2	2.3	2.0	7.7	, c		2.4	9.0	3.8	<b>9.</b>	2.8	<b>6</b> .0	2 i
	2	٤	23	7.3	<b>.</b>	8.7	÷.	7.7	•	• •	?:		•		8.2	4.2	4.5		•	•		•	7.8	6.7		9. C	7.5	6.7	7.2	•		7.8	0.0	12.6	9.0	D.0		. e.
895	2		ដ	950	956	9211	9212	9213	9214	9215	9216	9218	9210	9221	9222	9228	9229	9236	9231	2528	9235	9236	9237	9238	9239	9242	924	9245	9246	9248	9230	928	9295	9536	9297	9538	929	9 5

NICHT LANDINGS

USS ENTERPRISE (CVN-65)

FREE-FLIGHT BHW BVV OVER RAMP  S F/S IM/S DEG RAD DEG RAD FT IM  31 32 33 34 35 36 37 38  5 7 10 21 0077  5 5 1.7 2.1 2.1 0074  5 5.5 1.7 2.0 004  5 5.5 1.7 3.0 004  5 5.5 1.7 3.0 004  5 5.5 1.7 3.0 004  5 5.5 1.7 5.5 004  5 5.6 004  5 5.6 004  5 5.7 004  5 5.8 1.7 5.8 004  5 5.8 004  5 5.8 004  5 5.9	A TROSAST S.	_	_	_		KIN	PEFD AT	TOUCH	Z			GLIDE	PATH A	WGLE ,	17 70	WHEEL HEICHT	451047	1	HOW HETCHT
W/S         f/S         W/S         DEG         RAD         FT         M         FT           3.6         31         32         33         34         35         36         39         4           3.5         31         32         33         34         35         36         39         4           3.5         3.5         35         34         35         36         39         4           2.5         3.4         35         36         37         36         39         4           2.5         3.5         3.5         36         37         36         39         4           2.5         3.6         3.7         366         37         36         39         4           2.5         3.6         3.7         36         37         36         39         4           2.5         3.6         3.7         36         37         36         39         39         4           2.6         3.5         3.6         3.7         36         37         36         39         39         39         39         39         39         39         39         39         39	STBO	708			STBO AVC	98 AK	¥		4.5	FREE-FI	L1941		3	6	! : ≥	83	9	8	PA P
31 32 33 34 35 36 37 39 39  32 664  33 664  34 686  37 1 2 1 664  37 1 686  37 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	F/S W/S F/S W/S F/S W/S F/S	F/S W/S F/S W/S	N/S F/S N/S	F/S 14/S	Ş		5		Ş	F/S	Ş	DEG	3	DEC	3	E	×	E	3
2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2	23 24 25 26 27 28 29 3	25 26 27 28 29	26 27 28 29	27 28 29	26 29	<b>58</b>		ν,	•	5	32	SS	*	25	36	37	2	80	\$
8. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2.	3.2 11.5 3.4 11.5 3.4 11.4	11.5 3.4 11.5 3.4 11.4	11.5 3.4 11.4	11.5 3.4 11.4	3.4 11.4	4 11.4		2	49					3.2	. 056				
2.7 2.4 4.2 5.4 5.4 5.4 5.4 5.4 5.4 5.4 5.4 5.4 5.4	11.5 3.5 11.1 3.4 11.3	11.5 3.5 11.1 3.4 11.3	3.5 11.1 3.4 11.3	11.1 3.4 11.3	3.4 11.3	11.3		-,	4					3.7	<b>.064</b>				
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2.7 2.7 2.7 2.8 2.8 2.8 2.8 2.8 2.8 2.8 2.8 2.8 2.8				11.0 2.0 11.0	3.6			• • •	. 20					0.0	896				
2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2	3 2.7 9.9 3.0 8.7 2.7 9.7	9.9 3.6 8.7 2.7 9.7	3.0 8.7 2.7 9.7	8.7 2.7 9.7	2.7 9.7	6.7		•	G.					2.8	.050				
**************************************	2.8 8.9 2.7 8.5 2.6 8.7	8.9 2.7 8.5 2.6 8.7	9 2.7 8.5 2.6 8.7	8.5 2.6 8.7	2.6 8.7	8.7		••	9.					2.5	. 043				
2	2.3 11.8 5.6 10.3 3.1 11.1	11.8 5.6 10.3 3.1 11.1	3.6 10.3 3.1 11.1	10.3 3.1 11.1	3.1 11.1	1.1		٠,	*:					3.7	. 964				
2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	7.8 2.4 7.3 2.2 7.5	7.8 2.4 7.3 2.2 7.5	1 2.4 7.3 2.2 7.5	7.3 2.2 7.5	2.2 7.5	7.5		•	۲.					2.1	. 037				
	3.9 10.1 3.1 9.3 2.8 9.7	10.1 3.1 9.3 2.8 9.7	3.1 9.3 2.8 9.7	9.3 2.8 9.7	2.8 9.7	6.7	_	٠,	•					3.5	. 056				
	3.0 9.0 2.7 7.1 2.2 8.5	9.0 2.7 7.1 2.2 8.5	2.7 7.1 2.2 8.5	7.1 2.2 8.5	2.2 8.5	<b>8</b> .6		4	<b>•</b>	<b>6</b>	2.6			2.8	.050				
2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2	7.3 2.2 8.3 2.5 7.6	7.3 2.2 8.3 2.5 7.6	2.2 6.3 2.5 7.6	6.3 2.5 7.6	2.5 7.6	9.°			2.	7.1	2.1			9 °					
2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2	2.7 5.1 2.5 5.4 2.5 5.3	2.1 2.5 B.4 2.6 B.4	2.5 6.4 2.6 6.4	2.4 2.4 G	2.6									2.5	246				
2. 2. 6. 7. 7. 7. 7. 7. 7. 7. 7. 7. 7. 7. 7. 7.	1.8 7.8 2.4 6.9 2.1 7.5	7.8 2.4 6.9 2.1 7.5	2.4 6.9 2.1 7.5	6.9 2.1 7.5	2.1 7.5	7.5	_	~	n					2.3	.639				
6. 1.1 1.4 1.4 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5	5.4 1.7 5.7 1.7 5.6	5.4 1.7 5.7 1.7 5.6	1.7 5.7 1.7 5.6	5.7 1.7 5.6	1.7 5.6	5.6		_		5.5	1.7			7.0	.034				
6. 1.1 1.1 1.2 1.2 1.2 1.2 1.2 1.2 1.2 1.2 1.2 1.2	0.01 10.0 0.1 10.0 4.0 11.0 0.0 0	10.0 0.1 10.0 4.0 11.0	0.1 0.4 0.00 T.0	8.11 4.4 W.W.	4.6	<b>9</b>	•	-, ,	• !					o. 0	.061				
6.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1	7.5 7.5 7.5 7.5	7.5 7.5 7.5 7.5	7.0 7.7 7.1	16.6	;		7.7		•						7				
6. 1.1 1.1 1.2 2.2 2.2 2.2 2.2 2.2 2.2 2.2 2.2 2.2				5.4 7.6 9.6	7.7	D 0		- •						3.6	. 655 655				
6. 1.1 1.1 1.2 2.2 2.2 2.2 2.2 2.2 2.2 2.2 2.2 2.2	2.3 9.1 2.8 7.3 2.2 8.7	9.1 2.8 7.3 2.2 8.7	2.8 7.3 2.2 8.7	7.3 2.2 8.7	2.2 8.7	7.0			, ,					3.2	926				
2. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5.	2.4 6.8 2.7 7.9 2.4 8.7	8.8 2.7 7.9 2.4 8.7	2.7 7.9 2.4 8.7	7.9 2.4 8.7	2.4 8.7	6.7	_	a	•					2.5	.043				
8. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5.	8.4 2.6 7.0 2.1 8.6	8.4 2.6 7.0 2.1 8.6	2.6 7.0 2.1 8.6	7.0 2.1 8.6	2.1 8.6	9.6		~	•					5.6	. 046				
6.0 1.1 1.1 1.2 1.3 1.4 1.6 1.6 1.6 1.6 1.6 1.6 1.6 1.6 1.6 1.6	3.9 11.5 3.5 12.7 3.9 11.7	11.5 3.5 12.7 3.9 11.7	3.5 12.7 3.9 11.7	12.7 3.9 11.7	3.9 11.7	11.7		~	•					3.5	.061				
2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.	3.4 11.4 3.5 10.7 3.3 11.1	11.4 3.5 10.7 3.3 11.1	5.5 10.7 5.3 11.1	10.7 3.3 11.1	3.3 11.1	1.1		ń	+					0	. 962				
2.6 1.1 2.8 8.8 8.8 1.9 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0	3.0 8.2 2.5 10.3 3.1 9.2	8.2 2.5 10.3 3.1 9.2	2.5 10.3 3.1 9.2	10.3 3.1 9.2	3.1 9.2	0.5		ď	<b>6</b> 0					5.2	.043				
3.6 1.1 2.8 8.1 8.1 1.2 1.4 1.4 1.6 1.6	2.00 0.14 0.00 0.1 0.10 0.11	5.4 1.6 5.0 1.5 5.1	1.6 5.0		1.0	5.1			•					<b>7.0</b>	<b>934</b>				
2. 5 2. 5 3. 5 4. 5 5 6. 5 7 7 7 8	0.0 1.0 0.0 0.0 0.0 4.0 0.0 T.0.0	10.0 U.U 10.U U.U 10.0	0.01 10.0 n.o. n.o.	10.4 5.1 10.6	3.1 10.6	9.0	_	ri ·	~	,	,			и. С.	.657				
2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 -	1.9 3.3 1.8 5.4 1.6 4.1	3.3 1.0 5.4 1.6 4.1	1.0 5.4 1.6 4.1	5.4 1.6 4.1	1.6 4.1	- <del>-</del> -	_	-	~	ص. ص	<u>-</u>			œ.	. 615				
2 - 2 - 2 - 6 - 6 - 6 - 6 - 6 - 6 - 6 -	2.8 9.8 3.0 10.1 3.1 9.9	9.8 3.0 10.1 3.1 9.9	3.0 10.1 3.1 9.9	9.0 1.1 1.0	3.1 9.9	o.	_	'n	•					2.0	. 658				
2 1 2 1 2 2 1 2 4 4 5 6 5 6 4 4 5 6 6 6 6 6 6 6 6 6 6 6	6.6 2.0 7.4 2.3 6.7	6.6 2.0 7.4 2.3 6.7	2.0 7.4 2.3 6.7	7.4 2.3 6.7	2.3 6.7	6.7	_	ď	•					<b>7</b> .0	.034				
2. ± 2. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5.	1.9 5.1 1.5 5.9 1.8 5.4	5.1 1.5 5.9 1.8 5.4	1.5 5.9 1.6 5.4	5.9 1.8 5.4	1.8 5.4	4.8	_	_	۲.					-	. 020				
. 4.2.	1 2.7 8.3 2.5 10.4 5.2	8.3 2.5 10.4 5.2	1 2.5 10.4 5.2	10.4 3.2	3.2		£.0		2.8					5.8	.651				
3.6	1.8 6.9 2.1 5.2 1.6 5.5	6.9 2.1 5.2 1.6 5.5	2.1 5.2 1.6 5.5	5.2 1.6 5.5	1.6 5.5	5.5		•	7.					<b>+</b> :-	. 025				
3.6	7.4 2.3 7.9 2.4 7.7	7.4 2.3 7.9 2.4 7.7	2.3 7.9 2.4 7.7	7.9 2.4 7.7	4 7.7	4 7.7	_	•	2.3					7.4	.042				
	10.6 3.2 7.7 2.3 9.6	10.6 3.2 7.7 2.3 9.6	3.2 7.7 2.3 9.6	7.7 2.3 9.6	3.0°	3.0°	9.0	••	6.					3.6	. 963				

NIGHT LANDINGS

USS ENTERPRISE (CNN-6.,

200			AIRCRAFT		MCING S	PEED AT	SINKING SPEED AT TOUCHDOWN	NIO.			CL IDE	РАТН А	GLIDE PATH ANGLE AT TD	T T0	WHEEL HEIGHT	EIGHT	HOOK HEI	HEIGHT
ş	\$	HOSE	2	PORT	STBO	2	AVC	,-	FREE-FLICHT	.1GH		*	\$	>	OVER R	RAMP	OVER RA	3
	٤	\$	٤	\$	2	\$	2	Ş	2	¥	DEC	3	DEG	3	E	3	E	3
2	22	*	8	28	22	28	<b>38</b>	2	2	32	3	ħ	z	36	37	8	90	\$
****	•	<b>.</b>	5.5	1.7	7.8	4.4	•.	9.						.028				
12	9.9	2.7	=	٠. ت	5.3	<b>9</b>	7.7	2.3					2.7	946				
144	7.7	2.3	9.5	2.9	8.3	2.5	8.8	2.7						.054				
3	10.2	2.7		2.7	•.	٠. د.	5.6	5.9						. 967				
Ī	S. 5	1.7	9.0	2.7	7.8	2.4	8.3	2.5						.041				
3	•	-:	: •:	9.0	5.8	<b>9</b> .	<b>-</b> .	2.5						.047				
<b>275</b>	7.8	7.7	7.1	2.5	7.2	2.2	7.1	2.5						. 036				
<b>3</b> 55	7.4	2.3	6.3	2.5	6.3	<del>.</del>		2.5						. 048				
<b>3</b> 58	7.3	2.5	9.0	7.6	9.0	2.7	<b>9</b> .3	2.8						.052				
<b>3</b>	0.0	2.7	÷.	7.9	1.5	3.5	9.0	J. J.						. 060				
9269	<u>.</u>	7.7	÷.	3.2	₹.	3.2	10.2	3.1						. 069				
9575	6.3	2.8	8.e	3.3	6.2	<b>a</b> .	10.5	3.2						.062				
9587	•.	<b>9</b> .	7.4	2.3	7.8	2.3	7.5	2.3						. 059				

8		-	I U	S Z V				R 0 L	ر ۲	C	w	Δ.	PITCH RATE	ATE	ROLL	RATE	r. G	÷.	X	_	
ð	5		8		7.5		5		8		4		AT TD	٩	¥	<b>5</b>	AT	10	AT TD	ρ	
	330	3	DEC	2	DEC	3	DEG	3	DEC	3	DEG	3	DEG	3	DEG	3	DEG	\$	OEG	3	
<b>∓</b>	4	2	\$	<b>.</b>	\$	41	\$	<b>9</b>	3	21	25	53	*	22	88	57	28	20	8	5	
317	5.5	\$			5.1	8	.5	8		ī	i <del>•</del>	924 9	•	999 -5	ن. ا	. 6925	9	869	8.9	.155	
2	4.7	. 682		•	*.		2.0	635		-	E	<b>631 6</b> .	•		9.9	.185 -4	'n	075	9.6	.157	
8	4.7	. 682				•	+.7	. 662				ì	i	912 -1	1.3			058	9.4	. 686	
2	<b>9</b> .	2					<u></u>	919				<b>9</b>	•				+	. 629	8.2	.143	
22	J. J	89					1.2	021				-2	~				•	051	3.3	. 658	
<b>58</b>	•	<b>8</b> .				- •	2.5	<b>1</b>				_	_		2.5			066	2.8	.040	
2	7.5	86				- •	2.7	44				-7.		637 1	1.2(	.073 -5	•	894	<b>6</b> .0	.157	
3	•						-	962				ľ		014	9.0	980 ·	<u>.</u>	065	4.6	.059	
3	<b>4</b> .	. 675				7	'n	<b>6</b> 36				ī			۲.		<u>-</u>	- 619	5.2	. 691	
2	-	8				4	'n	692				_	_			£- 660.	'n	- 928	-2.9	. 051	
2	J. 7	<b>5</b>				7	~	638				-2.	_		2.9		Ī	163	9.5	. 166	
3	4.0	8				7	۲.	047				i	_	002 -4	1.5	. 679	8.5-	. 966	5.	. 626	
<b>\$</b>	8. 8.	8				7	۰	ess				-	<b>a</b>	. 033	5.1	.054 -2	*	042	#. 8.	. 031	
3	₩.	\$				7	'n	061				7	_	030 -1	9.	017 -1	'n	926 -	1.5	026	
\$	4.5							.019				-		.017	7		1 4.7	077	5.7	660.	
3	5.7	8					_	.016				i	•		-2.1		_	037	2.0	.035	
3	9.8	=				1	7	621				2.5			4		_	054	6.1	016	
151	4.7	.662					2.2	. 038				7		052 -5.	~	- 669 -	-3.3	058	4.6	. 686	
3	4.2	.073						8				7		066	4.9		·	031	.5.	669	
57	9.0	88						.045				ľ	'				-3.3	058	2.5	.044	
50	<b>.</b>	8				ï	-2.0	035				-					-3.8		- 5.1-	023	
3	6.1	<b>9</b>					~	.003				7					4.2		- 4.1-	624	
5	4.5	Š				7	~	636				<b>†</b>		007	4.6	. 659	-2.9	051	·	010	
162	4.4	.077				- •		.042				7		019-1	9.		-2.1	037	_	.047	
3	4.7	.662				•		010				_	 		8.2.		1.9	033	0.0	9.88	
99	<b>9</b> .	79				ï	~	038				7			-2.5		-3.0	052	7.	.003	
167	5.5	98.				ľ		054				4.7					-3.6 -	063		007	
17	5.1	89.						. 028				-2.2					-2.7 -		_	.068	
172	J. 6	S				1	-1.2	021				9.			_		i 0.†		- - -	019	
175	•	.687				•		002				7				.199 -3	r.	058	7	012	
176		<b>3</b>				ſ	6.2	061				ĸ	2.0		7.7	.021 -3	ะ		- 5.7	023	
111	4.0	98				•	7	012				,		914 1	=	4 610.	~	073	6.7	.117	
3	4.0	3				7	ĸ	026				-1.7	i	636 -3	-3.8	066 -2	_	047	<b>6</b> .	. 031	
186	47	602				ſ	. 7.3	-, 965				_		626 -7	-7.5 -		-4.9	986	1.7	. 030	
201	7.5	131				1		058				_	•					- 410.	_	986	
101	•	82B				7		- 026				4				164 -3	~	056	3.4	.059	
107	4	17						663							'n		•	084	5	.026	
9		<b>9</b> 87				-		930				6	•	. 999	0		-	075	5.7	660	
3	) e	. e				•		- 916				7		940		930 -2	,	. 047	- 7.	. 636	
	) <del> </del>											•	) }	ı	ا ي .			400	•	626	
¥	)  -	3											· }		•		•		:	) }	

NICHT LANDINGS

USS ENTERPRISE (CVN-65)

		3	ANDING DATA	ı	MODEL S-3	ņ		USS ENTERPRISE (CVN-65)	ERPRIS	رد (د <u>۸</u>	<b>←65</b> )			2	NIGHT LANDINGS	NOINGS				
8		-	Z Z	Z V	n n			ROL	٠,	S C	w	Q.	PITCH RATE	RATE	ROLL RATE	RATE	r. 9.	خ ٠	YAW	•
2	2		8		i.		5		g		9		AT TD	5	AT TD	5	AT TD	2	AT TD	2
		3	DEG	3	DEG	3	930	3	DEG	3	DEG	3	DEG	8	DEG	8	DEC	8	DEG	3
<b>=</b>	7	\$	<b>‡</b>	\$	\$	47	<b>\$</b>	<b>Q</b>	8	51	25	53	\$	55	98	22	8	28	99	5
200	<b>4.3</b>					7	7.	936					œ.	-		.178 -2	۲.	.047	4.6	.059
200	5.1	. 689				ī	· -:	919					.,					112	5.1	. 689
211	•	51.				_		926				- •						070	<b>*</b> :	.077
212	• •					' ]	)    - 	<b>66</b> 2				- «	• • •		7.7-	126 -4 - 968 -4		1.004 1.004	ر د . د	.061
12		979				7		647				מינ						679	. 5	. 026
1215	-	.072				7		042				-7	<u>'</u>							019
216	5.5	986						999				7	_			.054 -3		965	2.0	.035
217		.112				7		086				•						026	B	101
218	4.7	. 622				7		047				7						986.	1.7	939
219		. 679				Τ'		673				רי	ر. د د					687	٠. ١	.012
122	7.0					?							• •	`	1 ./-	1. 1.04 96.4	1 7.7		. ¢	. 616 65.0
226						•						•						96.1	9 0	4.6
1220	9 17	145				7	ن د :	023				. ~					-	035		962
236	÷.5	. 679				ī	n	023				7	'				-			960.
1231	4.7	.062				ī	•	021							6.5					035
1232		.122		_	8.8	119 -2	-2.4	042		ï	-2.1	637 -1.	 	-						911
24	•	. 165				ī	i a:	033				•	ю,			.631 –2				023
225		. 606 607				•	, , , ,	. e.e.				7	+ 10	<b>6</b> 24 961	, , , ,	866 912 -4	  	-, <del>6</del> 52 -, <b>6</b> 82		012
1237		982				_		.021						ı	_	1.14				.045
238	_	.120				•		005				•			_		-2.2 -		+:	.072
239		<b>3</b>				7		023				7	•			105 -4	1 10 1		4.4	. 677
175		926				Ϋ`	-2.3	<del>0. 0</del>				* •	4 4 0 c		9 . 9 .	.045			9. <del>.</del>	649
7 7						i i		909.				?			9		֡֝֜֜֜֜֜֜֜֜֜֜֓֓֓֓֓֜֜֜֜֓֓֓֓֓֓֓֓֓֓֜֜֜֜֓֓֓֓֓֜֓֜		. «	101
245		. 667				•		<b>916</b>				ę,		•				056	i vi	600
1246	•	. 677				•		667				7					-3.5	061	s.	600
1249	_	. 654				ī		636										686	4.2	. 673
1251		<b>9</b>				7		963				<u>, , , , , , , , , , , , , , , , , , , </u>								. 033
1250	5.8	• •				•		010				?								023
294	a.	989				ï		1.044				_						063		012
282						ī		7.61				1 9	, d	. 646		J- 800		2CB	֓֞֜֜֜֜֝֜֜֝֓֓֓֓֓֓֓֓֓֜֝֓֓֓֓֓֓֓֓֡֜֝֡֓֓֓֓֡֜֝֡֓֡֓֡֝֡֡֡֝֡֡	
2007		28.				' 7		1.050				,			١	. 600. –				999
298	4					′ T		939				7			_	120		058	. –	.037
958	3.3	929				ī		623								.005 -3		854	1.0	.017
9366	2.4	.042					•	.014				2.7	_	.042	-2.9 -	035	:	072	ĸ.	600.
198	 -	. 689				•	د	920				ī	_	.017	₹.	. 667 -4	1 6	070	ø.	.016

		3	LANDING DATA	1	S 1300M	3		nss	ENT D&	USS ENTERPRISE (CVN-65)	¥ €()	<b>?</b>			N	NICHT LANDINGS	DINGS				
990		P	X U	× <	n n			8	1 .	Z V	6 L E		ā	PITCH RATE		ROLL RATE	ME	F. P. A.	₹	YAW	-
2	2	_	8		9			2		8		7		AT TD	_	AT T	5	AT TD	2	OT TA	٥
	9	3	930	2	930	3	DEG	<b>2</b>	930		<b>2</b>	DEG	2	DEC	8	DEG	3	DEG	3	DEC	3
ŧ	7	2	:	\$	\$	4	\$	•	8	5	22	53		5	22	26	27	88	28	2	19
2000	4.0	\$					-3.0	052					-3.2		7	•		М			.035
1	8. 8.	<u>.</u>					•	=	_				÷.		-	ين .		<b>6</b> 0 s		į	028
2 6	• •						v. 2.	566					* <del>*</del> •		016 .5 024 -2.8		.614 -5	o	647 -	• •	
95,00	3.5	\$						.012					0.	_			.073 -3.				.059
	<b>7.</b> 4	. 662					ا ا						-2.6 2.0	<b>.</b>	945 -B.	<b>+</b> 4	147 -3. - 887 -4	<b>4</b> ¢	059		.161
9312	7 7	3					•	.070	_				7							- 6.	
9313	8.0	. 103					-2.7	047					0.0		7	ĸ.		+	_		.183
<b>1</b> 26	<b>8</b>	= = =					7.7								044 2 53 -	· - •	.037 -2.	•	045 945		<b>9</b> 12
2778	) r	61						995	_				-7.8	ı	- 6	, r			945	•	972
512	. 4	2.						.012					1.7		<b>,</b> –	, <b>e</b> ë		. 60	066	7.7	7.
9318	4.3	.075					7	002						a.	.016 3	•		-3.2	056	8.3	.145
9320	4.7	.082		-,	5.3		-1.7	030			-1.7			<b>.</b>			.082 -1	<b>+</b> :	024	<b>+</b> · <b>+</b> ·	.677
9321	÷.5	8.		•	٠.4	. 675	• ·	028			-1.7	636		033	1	•	0474	٠	<b>6</b> 79	 	131
7758	. •	<b>8 8</b>					Y 45	200	_				_		636 -1.	. e		•	<b>04</b> 2	9 -	196
9324		<u>.</u>					8.6	. 049										₹.	677	2.7	. 047
9325	4.7	.002		4	1.7	. 062	<b>+</b> :	.024			1.2	. 921	_		.021 -1	7		<b>.</b>	692	6.4	980
9326	4.4	<b>7</b> 5					7 0	. 963	_				9. 6	ı	. 010-12 047	ห์ ∢ เ	2185. 9872	÷ =	<del>0</del> 94	α. α	. 166
9259	. 7	52					;	002					•		. 000			'n	679	9.	.168
53.	4.5	. 673					-	017					0.0		4	•			631	5.4	<b>.</b>
9332	n 0	3					* •	007	_				-2.5		r) •		.061 -3	-3.2 2.2	926		.115
33		2 0						3.	_				; ·		7				675	. t . 5.	.026
9335	•						-7. 4.	042					2.5		•				049	<b>+</b> (	.007
923		9					ו י	- 683							5.5 5.6 5.6 5.6		U- 840.	, i	- 6 - 6	٠ د د	999.
934	-	.072											2	ı			.021 -3	, ru	198	. v.	148
175	<b>9</b> .	\$					7:	019	_										677	3.7	. 965
9346	<b>9</b> .4	198			<b>9</b> .0	<b>8</b>	-2.0	035			-7.8	051	<b>.</b>	•		ų (			<b>9</b> 66	9 7	. 649
200	, , ,	3					9 4	9.0.					7 7		628 -1.6 - 631 -6 2		168 1	, t	1.00.1 40.1	? 0	5.7
9462	. e.	79					7	075					4.						072		999
9464	0.n	. 052					-3.8	966	_				7	١	•	_		+	694	7.4	.042
8469	-:	919					ų.	. 865	- <b>-</b> -				، نــ		٠ ٣	<del>-</del> •		<u>ب</u>	045	- 6	141
<b>94</b> 72	o	996						084					77		ī <b>«</b>	, e	154 - 154 - 1	<b>,</b>	<del>6</del> 00 <del>0</del> 12		969.

NICHT LANDINGS

USS ENTERPRISE (CVN-65)

REREAD	NUMBER			6	• •	•	-	•	•	•	9	-	•	•	0	•	•	•	•	•	-	•	•	•	•	•	•-	•	•	•	•	•	•	•	•	•	•	•	•	•	•	
		₹	82	6	431.8	426.7	426.7	428.7	429.3	426.7	9.9	429.3	429.3	424.2	426.7	<b>6</b> .0	9.9	429.3	9.9	6.6	426.7	431.8	426.7	<b>9</b> .0	429.3	<b>6</b> .	431.8	424.2	426.7	426.7	424.2	<b>.</b>	426.7	424.2	424.2	431.8	<b>9</b> .0	9.9	429.3	9.9	429.3	
ARR GEAR	RUNOUTS	×	19	•	176 43			168 42	169 42	168 42	•	169 42			168 42	•	•	169 42	•	•			168 42		169 42						167 42			67 42		178 43	•	•	169 42	•	169 42	
RIC	Æ	H H	80	759.7	·		Ċ	759.7	759.7	759.7	759.7	_	_	_	_	759.7	759.7	_	759.7	759.7	_	_	_	_	_	_		_	_		_		_	_	769.7	759.2	759.2	759.2	759.2	759.2	_	
BAROMETRIC	PRESSURE	IN HG	82	29 91	29.91	29.91	29.91	29.91	29.91	29.91	29.91	29.91	29.91	29.91	29.91	29.91	29.91	29.91	29.91	29.91	29.91	29.91	29.91	29.91	29.91	29.91	29.91	29.91	29.91	29.91	29.95	29.95	29.95	29.95	29.95	29.89	29.89	29.89	29.89	29.89	29.89	
TEMP		ပ	78	17	12	17	17	17	17	17	17	17	17	17	17	17	17	17	17	17	17	17	17	17	17	17	1	17	1	17	_	_			17	17	<b>7</b>		79	20	20	ì
<b>1</b> 6		<b>L</b>	11	2	2	83	63	63	3	63	63	63	S	83	63	63	63	3	63	63	63	63	63	63	63	63	63	63	63	3	63	63	63	63	63	63	68	89	89	89	ď	3
ROLL		3	78	9.0	016	667	910	016	014	002	016	042	009	. 605	014	012	021	005	007	.014	031	010	669	031	002	002	007	ا. 939 ا	047	949	033	031	014	9.00	002	995	002	.037	030	030	900	
DECK ROLL		DEC	22	•	0	+	9.1	6.1	8	_	•	_	1.5		-	7		.3	4.4	<b>æ</b>	-1.8 -	9.		-1.8 -	-	-	-			_		- 8: T		9.9		-		_	_	_	_	
11CH		8	*	663	992	003	. 992	. 007	. 003	.007		٠	. 010	. 993	. 005	. 005	- 010.	. 010	002	. 005		. 010	. 995		. 997	. 999						667	.010	. 669	. 992	. 965	995	997	9.666	005	696	
DECK PITCH		DEC	22		· -	7	Τ.	+:	~	*	9.		•	.2	٠.	٠ ?:	9.		· -	٠ ت	9.	• •	٠ ٣:	6	• •	6.		: :				• •	9.	'n	-			*	9.0		4	:
	a	N/S	72			~	~	4	~	, 4	, 4	,	7	7	7	~	7	7	7	7	7	7	, u	7	7	8		, N	7	N	~	, 4	7	, 4	7	*	7	7	8	7	,	•
SH.	SPEED	Š	7	*7	n	n	n	n	n	n	n	n	77	n	n	n	n	n	n	n	~	m	n	n	m	7	n	<b>m</b>	<b>m</b>	2	r	n	n	n	n	7	4	*	*	4	4	۲
3	300 300		92																																							
200	TYPE		8	78186	20.00	50200	56266	<b>36</b> 1 <b>66</b>	<b>Se188</b>	56166	66120	<b>30</b> 100	59100	<b>36</b> 1 <b>6</b> 8	56166	60200	66266	50120	<b>60</b> 100	60120	<b>99</b> 199	56166	<b>58</b> 288	70120	<b>20</b> 200	66126	20 20 20 20 20 20 20 20 20 20 20 20 20 2	2	20 20 20 30 30 30 30 30 30 30 30 30 30 30 30 30	36166	2	70120	50120	56128	50200	56186	70120	70120	50100	70100	56166	
SIDE	ġ		2	741	75	735	747	7	727	#	33	74.7	745	727	3	33	727	33	35	7	747	745	7	<b>*</b>	727	35	*	*	7	3	747	727	727	745	75	7	3	235	737	744	745	•
WIRE	Š		67		7	+	-	*	n	*		n	*	*	8			7			n	n	n		n	1	<b>m</b>	•	r)	N	m		n	n	N	7			n		•	•
RAMP TO TD	DISTANCE	3	8	102	3	S	3	\$	\$	8	2	ā	2	2	2	2	<u>\$</u>	3	<u>5</u>	5	2	2	8	85	92	2	3	<b>5</b> i	2	3	3	3	2	5	2	2	87	3	7,	28	5	5
RAMP	DISI	E	2	118	274	311	224	===	276	283	281	297	289	262	238	292	¥	224	337	28	312	278	201	Ş	<b>52</b>	328	261	297	22	724	271	272	241	267	231	238	286	210	243	256	288	3
MER	¥CE	2	3	ī	7	7	ņ	1	7	7	7	Ŷ	7	7	T	?	•	7	-	7	1	†	7	7	7	7	φ,	7	7	Ť	1	7	†	1	7	ę	1	1	†	T	-	)
OFF-CENTER	DISTANCE	E	2	ç	Ϋ́	†	-13	12	7	9	÷	9	†	ņ	<b>*</b>	7	7	÷	•	7	ž	2	<u>_</u>	1	4	4	Š	ę.	۲ :	-12	<u>-</u>	4	<u>.</u>	5	7	5	12	<u> </u>	<u> </u>	Į.	•	•
997	ě.		ŭ																																					9298 -		

RCREAD	NUMBER			•	-	•	•	•	•	- (	•	φ.	(	•	•	•	•	•	•	•	•	•	•	<b>6</b>	<b>5</b>	<b>.</b>	- 4	•	- «	. –	•	-	•	•	-	•	•	~	-	•	•	•
ARR GEAR	RUNOUTS	8	82	431.8	429.3	429.3	429.3	<b>0</b> .0	<b>9</b> .	431.8	429.3	9.9	43. B	9	426.7	431.8	0.0	426.7	434.3	428.7	0.0	429.3	429.3	9.6	431.8	<b>9</b>	9 9	9 5	428.7	431.8	428.7	426.7	429.3	429.3	429.3	424.2	429.3	429.3	426.7	<b>0</b> .0	426.7	6.0
\$	\$	Z	5	170	169	169	169	•	•		69	• ;	170	•		170	•	168	7	168	•	169	169		9/	9 (	•	9				168	169	169	169	167	169	169	168	•	168	•
BAROMETRIC	SURE	¥ ₹	88	759.2	759.2	759.2	759.2	759.2	759.2	759.2	759.2	759.2	759.2	759.2	759.2	759.2	759.2	759.2	759.2	759.2	759.2	759.2	759.2	759.2	759.2	759.2	7.807	7.867	750.2	759.2	759.2	759.2	759.2	759.2	759.2	759.5	759.5	759.5	759.5	759.5	759.5	759.5
BAROM	PRESSURE	IN HG	78	29.89	29.89	29.89	29.89	29.89	29.89	29.89	29.89	29.89	29.89	29.88	29.89	29.89	29.83	29.89	29.89	29.89	29.89	29.89	29.89	29.89	29.89	29.89	89.68	80.67	20.67	29.89	29.89	29.89	29.89	29.89	29.89	29.90	29.90	29.90	29.90	29.90	29.90	29.90
TELP		ပ	78	79	<b>5</b>	8	<b>5</b>	<b>3</b> 9	<b>5</b> 9	58	79	58	58	9	70	8	<b>39</b>	<b>70</b>	<b>79</b>	<b>79</b>	<b>79</b>	29	30	8	29	8	9 6	9 6	9 6	39	<b>9</b>	79	<b>8</b>	20	70	22	22	22	22	77	22	22
_		Ŀ	11	89	89	89	68	8	89	89	8	<b>8</b> 9 9	<b>2</b>	8	<b>8</b>	<b>68</b>	89	89	89	89	89	89	8	8	8	8	8	8 8	9 4	3	89	89	89	89	89	7	7	7	7	7	7	7
DECK ROLL		8	8	838	002	010	.007		i	. 885	900	669	919	9.	. 12	667	0.000	. 002	.012	. 669	. 614	. 624	. 995	024	919	.997	+19	2 6	200.1	- 992	995	•	- 995		992	009	.012	. 995	. 993	014	.012	9.000
DEC		DEG	22	-1.7	7	9.	₹.	7		i.	9.	,		<b>.</b>		4.1	0.0	<del>-</del>		ď.	æ,	<b>→</b> :	J.	4.	Ď.	•	i i	Ÿ.					1	6.	ï	i.		"	~	8	۲.	0.0
DECK PITCH		3	*	010	995	0.000	012	667	009	012	. 663	600.	012	012	007	010	609	667	005	002	012	005	663	010	607	. 993		7.004		- 965	010	600	.002	010	-,010	667	010	012	-, 669	009	669	669
DECK		DEC	2		٠.	9.0	7	<b>+</b>	٠. ت	۲.	7.	ų.	- 1		<b>+</b> :	9.	٠. د	<b>*</b> :	۳.	-	7	ا.			÷ (		7 •	- •	9 4			5	-	9.	9.	4.	9.		ا. د	ر. ت	٠. د	<u>بر</u>
	8	K/S	72	~	~	~	~	~	~	~	~	~ •	, N	~	, ,	~	~	~	~	~	~	~	~	~			v c	٠, ١	4 6				~	~	7	4	*	•	*	+	+	*
SH P	SPEED	\$	7	*	*	*	*	*	4	n 1	י מ	· ·	י ני	ומ	n	~	n	7	m	n	n	<b>17</b>	n :	י מ	י מ	י מ	? <b>-</b>	3 -	3 ~	P2	17	17	~	m	n	~	^	7	^	^	^	^
3	3005		92																																							
200	TYPE		8	50100	50120	50200	<b>56288</b>	78288	70100	50120	28286	79126		70120	<b>20120</b>	50120	70120	50100	<b>50</b> 100	50120	66126	58288	59129	76120	56128	70120	20100		8 9	5	50120	56168	50100	50120	86166	56126	56200	56166	50100	60200	50120	69169
SIDE	ġ		3	737	7	35	233	737	*	737	?	#:	?	7	3	737	744	74	75	737	741	2	7	5	33	*		? ;		735	745	737	7	745	744	725	755	737	725	737	737	725
WIRE	€.		61	n	~	~	n			n 1	n	•	7	į	4	7		~	n	*		n	*	(	n			¢	4 1	P P7	~	~	*	n	n	*	n	8	*		*	
RAMP TO TD	DISTANCE	2	2	2	47	8	2	87	ž	2	2	102	=	8	ž	92	2	78	5	8	2	2	<b>10</b>	<b>8</b>	<b>8</b> 2	<u>.</u>	3	5 5	? 2	8 8	2	3	ž	5	8	8	5	72	8	102	92	2
3	018	E	3	25.6	134	195	274	269	9	262	265	3	3	3	8	Š	325	256	297	323	327	22 22 28	332	321	257	2	25		,	255	223	207	310	265	283	320	267	235	281	335	301	313
MER	MCE	3	2	†	ş	1	7	†	?	<b>9</b>	7	7.	?	?	ī	7	7	?	7	7	7	†	N ·	† '	?	ī	† •	- (	7	9	7	ņ	1	?	ņ	1	7	-	1	1	ş	1
OFF-CENTER	DISTANCE	t	3	<b>*</b>	-12	-12	4	-13	•	9	4 :	<b>•</b> :	<u>-</u>	• •	7	F	7	F	=	4	ş	-12	•	2 :	= '	? :	2,	າ ;	7 5	2 5	?	-1 5	13	7	97	-12	۴	-22	2	-13	-13	7
995	Š		62																																		-			•	Ţ	9473

NIGHT LANDINGS

USS ENTERPRISE (CVN-65)

		3	MDING DATA	ī	MODEL S	Z		USS E	NT CS	PRIS	USS ENTERPRISE (CVN-65)	-65)			Z	GHT	NIGHT LANDINGS				
8	OFF-CENTER	MEG	RAMP TO	0T 0T	WIRE	SIDE	200	3	3.5		DECK P	PITCH	DECK	POLL	15.6	Q.	BAROMETRIC	IRIC	AR	ARR CEAR	REREAD
ð.	DISTANCE	ACE	DIST	DISTANCE	Š	Š	TYPE	3000	SPEED	8							PRESSURE	Æ	3	RUNOUTS	NUMBER
	t	3	E	3					ž	M/S	DEC	8	DEC	8	<b>L</b>	O	IN HG	¥	2	3	
62	3	2	8	9	67	2	8	7	7	72	2	*	25	76	11	78	8	8	5	82	
474	51-	9	9	4	4	737	50100		_	*	•	010	+	667	17	22	29.90	759.5	167	24.5	•
1		1	284	: \$	•	725	90.00		_	•	٠	662	-:	.019	7	22	29.80	759.5		<b>.</b>	•
477	5	9	915	4	4	725	56166		~	4		003	_	012	7	22	29.90	759.5	168	126.7	•
3	7	1	5	3	•	725	69128		_	•		667	۲.	.012	7	22	29.80	759.5		0.0	•
į		1	231	?	•	755	50120		_	•		010	+.	667	7	22	29.90	759.5		124.2	_
	9	7	3	2	•	725	58286		_	4		. 96.3	2.5	.638	7	22	88.87	759.5	169	128.3	•
3	-	7	320	5	•	7.85	50120		4	~		- 909		012	7	77	29.92	760.0		426.7	•
3	•	· ?	322	3	•	2	70100		ĸ	2		667	7	. 003	7	77	29.93	760.2	•	<b>.</b>	•
3	•	17	202	3	4	746	20.00		10		8	- 969	9.1	010	7	77	29.93	769.2	168	126.7	•
ş	2 7	1	257	*	<b>9</b> 7	735	20.00		*	12		969	6.1	016	7	22	29.83	769.2		129.3	•
3	•	7	NIN	3	)	35	60100		10	<b>P</b> 7	- 2	003	7	. 003	7	22	29.93	760.2	•	0.0	•
7		9	240	2 %	<b>P</b>	740	59199		· •	P7		- 995	9	.010	71	22	29.93	760.2	169	129.3	•
5	2 17	-	327	<b>. .</b>	→	740	50200		10	מו	. 7	. 993	-	.002	7.	22	29.93	760.2	168	126.7	•
į	)		į	)		:			ı												



		5	LANDING D	ATA -	DATA – MODEL RA-38	<b>8</b>	ደ	S ENTE	USS ENTERPRISE (CVN-65)	<u>ر</u> ع	65)			DAY L	DAY LANDINGS			
			AIRCR	AFT SI	PAFT SINKING SPEED AT TOUCHDOWN	£80 A1	TOUCHD	Z S			GLIDE	GLIDE PATH ANGLE AT	NGLE A	5	WHEEL	HEIGHT	HOOK HEIGHT	I GAT
2	MOSE	¥	2	DRT.	STBO	٩	¥		FREE-FLIGHT	18H	<b>&amp;</b>	<b>8</b> +	<b>&amp;</b>	>	SER.	RAMP	OVER RAMP	3
	٤	\$	2	\$	2	\$	2	Ş	2	¥	DEG	3	DEG	2	E	3	E	2
Z	2	*	23	36	72	28	78	9	2	32	z	¥	33	98	37	8	80	4
Ĭ	6.0	2.7	9.5	2.6	4.6	2.6	4.6	2.6			3.5	.061	2.5	.043	14.8	4.5	11.5	ņ
\$		9.0	9.0	7.7	<b>+</b> .•	3.5	10.4	3.2			3.2	.056	4.6	. 059	17.2	5.2	13.8	+
<u>\$</u>	-	2.8		<del>.</del>	<b>9</b> .0	2.1	<b>9</b> .	5.0			2.6	.046	5.0	.035	14.3	<b>+. +</b>	10.5	'n
2	13.0	•:	13.3	<del>-</del>	13.7	4.2	13.5	<del>-</del> :			5.2	969.	4.0	. 069	21.1	4.9	17.6	'n
2	<b>19.</b> 2	J. 7	÷.	J. 3	11.5	3.5	11.2	4.0			4.9	.085	3.9	. 968	19.4	3.9	16.1	4
117	12.2	7.7	1.5	3.6	= - -	J. 6	1.6	3.5			<del>-</del> :	.071	g. 5	.068	17.1	5.2	13.7	÷
13	<b>.</b> .	2.5	9.5	, ,	<b>.</b> .	2.5	9.3	2.3			3.2	.055	7.4	. 042	17.8	5.4	14.9	*
120	12.8	9.0	13.2	•	÷.	4.3	13.7	4.2			3.9	.068	<b>4</b> .6	.081	17.1	5.2	13.9	÷
123	<b>↑</b> .=	3.5	<b>10</b> .6	3.5	<b>-</b>	J. 7	<b>19.</b>	3.2			4.3	920.	3.0	. 053	18.8	5.7	16.0	4
125	10.8	3.3	=	3.1	<b>.</b> e.	٠. د.	<b>19.</b>	3.1			3.9	.068	4.6	. 059	18.1	5.5	14.8	4
127	<b>19.</b>	J. 7	7.8	7.4	<b>.</b>	2.7	8.3	2.5			2.5	. 044	2.3	.041	14.7	4.5	11.2	'n
128	<b>=</b> .	4.5	<b>†</b> .	2.8	<b>†</b> .	2.9	<b>4</b> .	2.9			3.3	.057	2.8	.049	14.2	4.3	11.2	ņ
3	7.7	2.3	8.8	<del>.</del>	5.1	1.5	5.6	1.7	5.1	9.	2.4	.043	8.	.032	12.2	3.7	4.0	તં
3	8.0	2.7	11.7	0.0	1.5	3.5	₽. •	3.5			5.0	. 688	<b>6</b> .4	.070	13.6	4.1	8. 8	'n
137	<b>1.6</b>	J. 5	12.3	J. B	12.7	a. n	12.6	3.8			4.2	.072	<b>6</b> .	.070	20.0	6.1	16.5	'n
55	<b>.</b>	<b>9</b> .	<b>9</b> .0	5.9	•	2.7		2.8			<del>-</del> -	. 672	5.9	.051	18.9	5.0 10.00	16.1	÷
3	7.2	2.5	10.3	J. 7	B.	۵. د	10.0	J. 7	10.1	3.1	<del>-</del> -	.071	3.3	. 058	16.7	5.1	13.1	4
- 5 5	<b>.</b>	2.5	<b>9</b> .7	<b>.</b>	6.3	<del>.</del>	6.3	<b>6</b> .			5.8	.051	1.7	. 636	12.9	ø. N	ю. О	ņ
<u>+</u>	12.9	G. 7	12.9	8.0	13.4	<del>-</del> -	13.2	<b>•</b> .			3.7	.064	3.7	. 965	21.2	6.5	18.8	'n
155	<b>0</b> .0	5.8	<b>0</b> .0	<b>•</b> :	8.8	2.7	<b>→</b>	5.9			3.7	.065	4.6	. 059	21.8	9. 9	18.2	'n
455	10.8	3.3	10.8	3.3	10.3	٠. ۲.	10.4	3.2			3.5	. 061	3.2	. 056	16.8	5.1	13.5	4
457	1.2	4.5	<b>.</b>		10.2	3.1	10.0	0. 0.			3.9	.068	3.3	.057	16.8	5.1	12.9	'n
439	10.8	3.3	<b>9</b> .	2.8	4.0	2.9	5.5	2.9			4.6	.059	5.9	.051	19.3	8.9	15.7	÷

		3	LANDING DATA	1	MODEL RA-38	<b>3</b>	_	uss en	TERPRI	USS ENTERPRISE (CVN-65)	N-65)			8	DAY LANDINGS	INGS				
8		P 1 T C	T O	Z Z	<b>u</b>			R 0 L	ب	ANGL	w		PITCH RATE	MTE	ROLL RATE	RATE	F. P. A.	خ	YAW	_
ð	Ę		g		*		5	_	g	~	9		¥	£	¥	£	7	ę	AT TO	٩
	220	3		3		2	DEG	3	DEC	2	DEG	2	DEG	3	DEG	2	930	2	930	3
ŧ	42	\$	\$	\$	\$	47	<b>\$</b>	<b>\$</b>	8	2	22	3	*	53	80	27	88	20	8	5
Ī	8,8	3		3		•	9	. 010	2.4	642		-,	0.	898	ĸ	. 669 -2		047	9.0	150
Ē	•		3.8	986.		_			5.1	669			_				-	072	9.9	150
3	9.			100.		_	1.5	. 026 -		966		•					-2.9	851		.617
2	3.2			.037						005		7	-1.2 -		-2.5	044 -2		047	•	. 992
113	2.3			.631		ī			- <del>+</del> -	024		ī	ı					052	6.2	. 108
117	7.0			15		ī	٠.	021 -1	•	028								838		.056
119	2.1			. 645		-		.017	<b>6</b> .	. 033		_	<u>-</u>					058	3.8	. 966
<u>2</u>	7.7			3		ï	_	052	-:	.019		7	1					670	7.9	138
23	7. 9.			.021			۲.	.012	1.7	.030		••	2.0	. 035	3.0			. <b>96</b> .	3.2	. 056
125	2.3	-				•			_	9.999		_						- <b>6</b> 60	<b>+</b> .	.164
127	4.7			3		7	ı		-2.8 -	049		٠,	*	1			-2.4		4.6	. 059
128	2.1			• 49		_	<b>1.5</b>	. 926 -		031		•,	*					061	<b>+</b> .0	.181
35	¥.4			•	4.5	.079	-5.1			<b>963</b> −.	1.7	982	9.	.105	2.9	.051			8.8	.154
134	S.5			. 052		ï	-2.2			019		ī							-:	.194
137	8.8			. 652		ī			, 8.	014		-			1				7.0	.122
50	2.5			. 623		ī	1.4.1	•		047		•,		191	3.2	.056 _	-		6.6	.173
113	÷.5			•	. <del></del>	770.	2.3		_	010 -	. 6:1-	833 1	1 9.7	989		.045 -	-	031	<b>5.</b> 4	<b>9</b> 6
146	P			. 856		ī	1.8		•	000		•	6.1	.070	-	. 602 -		963	<b>.</b> .	.159
148	•			1		•	1.8.1		1.0.1	017		•	•	ı		.047 -:	-2.7	647	5.7	. 699
55	2.7			88		ī	1 7:T	_	- 1.1	838			•			.191		054	0.	. 140
<b>5</b> 5	8.8			. 658		_	<b>0</b> .		- 7	012			۲.					061	7.1	.124
457	<b>9</b> . <b>4</b>					_			9.0	999.		•	1.7		•		-3.4	059	7.0	. 122
623	9.5			.072		ī	1.0		Ī	007		•	2.9	.051	9		·	073	6.9	105

		3	CANDING DATA	•	MODEL RA-38	8-₹		USS E	NT ES	USS ENTERPRISE (CWI-65)	<u>₹</u>	<b>6</b> 5)			ă	3	DAY LANDINGS				
8	2	off-cortex	RAMP TO	5 5	WIRE	3018	8	3	SHIP PIES		DECK PITCH	¥5	DECK ROLL	ROLL	100	α.	BARONETRIC	RIC	2	ARR GEAR	REREAD
ě	015	DISTANCE	DIST	DISTANCE	Š	ĕ	395	300	SPEED	a							PRESSURE	Æ	\$	RUNOUTS	NUMBER
	E	2	t	*					- 5	Ş	DEC	2	DEC	3	<b>L</b>	- U	¥	£ ₹	X	5	
2	3	3	3	3	6	2	8	2	7	27	23	*	22	8	11	28	79	2	5	82	
3	-17	Ŷ	216	3		122	70120		~	7	L).	5995	2 -	. 963	39	5	30.15	765.8	•	•	-
2	7	7	282	2		124	70200		~	1	2	983		002	29	_	36.15	765.8	•	0.0	-
3	7	7	281	3		122	60230		~	2		883	7-	012	59	5	30.15	765.8	•	0.0	•
2	-12	1	218	3		124	66126		n	7	٠	863	i	002	29	15	36.15	765.8	•	0.0	•
2	ņ	7	221	67	7	124	56120		~	8					29		36.15	765.8	•	<b>.</b>	•
117	4	7	226	2	~	124	50123		•	i R	i -	002	1.4.1	867	29	_	30.15	765.8	•	•	-
2	T	ī	282	2	~		50120		•	7	2	. 963		002	20	_	30.15	765.8	•	0.	•
2	-	?	228	2	n		56188		•	22		993	2 -	003	29	5 3	30.15	765.8	•	•	-
23	-12	7	223	2	7		50120		•	23		005	- 5.1	005	29	5	30.15	765.8	•	•	-
25	1	7	256	2	n		50123		4	8					29	5 3	30.15	765.8	•	0.0	-
127	7	7	268	25	n		56188		•	2	8	- 600	-1.4-	024	29	5	30.00	763.5	170	431.8	-
128	2	7	224	2	~		59288		•	, i		883	1.4.1	007	59	53	39.96	763.5	170	431.8	_
3	7	?	262	2	~		50100		•	21		662	1.6.	010	29	5 3	30.06	763.5	170	431.8	-
3	-13	ŋ	147	<b>4</b>			66128		•	~					99	9	39.96	763.5	•	0.0	•
2	-12	1	234	۲	n		50200		•	2	.5.	. 969	1.5	969	99	9	30.00	763.5	170	431.8	7
2	-15	7	246	r	~		56126		4			002	1.9	016	69	9	39.96	763.5		431.8	8
3	-13	†	214	3	-		86128		•	22		003		014	99	9	30.06	763.5		436.9	-
9	-	?	218	2	~		56123		'n	J J	_	005	1 .00 1	014	99	? 9	30.06	763.5	170	431.8	-
\$	7	7	277	ĭ	*		56366		s	3.1.5	Ť	- 600 -		026	5	9	39.96	763.5	169	425.3	-
2	7	7	316	3	*		50123		s	n					61	_	30.00	763.5	200	426.7	•
2	1	7	237	2		124	76266		4	N 1	i +	867	7-	012	62		29.97	761.2	•	0.0	<b>,-</b> -
53	7	7	225	2		124	70120		<b>+</b>	2	2		1:1-	019	62	7 2	29.97	761.2	•	<b>.</b>	•
55	4	7	272	3	•	124	50100		+	2				007	62	7 2	29.97	761.2	88	426.7	•

## **RA-3B NIGHT**

			200	¥	ATA -	DATA - MODEL RA-38	F 84	8	-	USS ENTERPRISE (CVN-6)	ITERPR	) 3SI	₹ 3	(0)			NICHT LANDINGS	ANDING	10		
995	VPAF	5	VE-F!	3		WIND-VEL	-vel		7	VEOR	MA	VPAMIN	Š	V.dSA	KVPA	\$	UFF	HI	¥	MEICHT	
Š	2				0.	PAR.	PER	è.							Z	٧ &	Ę	1			
	\$	\$	₫	\$	\$	\$	₹	Ş	₹	Ş	\$	Ş	₹	K/S					<b>S</b>	Š	
-	~	2	•	•	•	^	•	•	•	=	12	5	=	5	•	11	₽	<b>2</b>	<b>30</b>	12	
500	126	2	102	25	7	2	•	8			12	8			1.12		1.10		47500	21546	
9536	128	8	2	3	22	2	*	~			1	<b>8</b>			1.12		<b>8</b>		49100	22272	
50	124	3	=	47	3	17	•	2			115	28			1.98		8.		50100	22725	
299	131	6	8	3	2	17	•	n			115	29			1.1		1.10		50100	22725	
1142	124	Z	8	41	32	=	•	2			115	28			1.67		<b>.</b>		59100	22725	
9149	131	67	6	3	ň	17	•	2			==	29			1.15		1.00		49100	22272	
203	137	2	\$	3	3	7	•	2			=	29			1.20		1.38		49100	22272	
9210	123	3	2	<b>4</b>	3	17	n	~			112	8			1.10		<b>-</b>		47300	21455	
1225	130	7	105	3	*	17	~	~			=	29			1.21		1.20		49200	22317	
9226	129	3	2	\$	ħ	17	n	7			114	29			1.1		1.10		48600	22045	
2233	127	Ş	2	<b>4</b>	お	17	n	7			112	28			1.13		1.00		47100	21365	

		3	AND ING D	ATA -	DATA - MODEL RA-38	87-78	2	SS ENT	USS ENTERPRISE (CVN-63)	9- <b>₩</b> \)	6			NICHT	NIGHT LANDINGS			
2			AIRCR	WT SI	AFT SINKING SPEED AT TOUCHDOWN	PEED A	T TOUCH	NHOG			GLIDE	PATH A	GLIDE PATH ANGLE AT TO	5	WHEEL HEIGHT	EIGHT	ноок нетснт	IGH
2	NOSE	SE	2	FX.	S	STBO	AVG	O	FREE-FLICHT	1CHT	<b>25</b>	*	¥	>	OVER R	RAMP	OVER RAMP	<b>A</b>
	2	\$	2	\$	2	\$	2	Ş	5/2	K/S	DEC	3	DEC	3	E	3	E	3
22	22	*	22	<b>56</b>	22	<b>92</b>	8	2	5	32	33	ň	35	86	37	8	39	\$
8	<b></b>	3.2	7.4	2.5	6.5	2.0	7.0	2.1					•	6.32				
9626	10.2	۵.	<u>-</u>	3.1	12.3	3.7	<b>10</b> .0	3.2					3.7	994				
500	. S.	2.8	10.6	3.2	<b>0</b> .0	 	10.2	3.1					4.6	.059				
9662	7.3	2.2	7.7	2.3	7.7	2.4	7.7	2.3					2.2	938				
9142	<b>=</b> .8	3.3	11.2	4.0	12.0	3.7	11.6	3.5					3.9	998				
9148	<b>+</b> .=	S. 50	1.6	3.5	•. =	4.5	11.3	3.5					10	.062				
9263	5.1	<b>9</b> .	7.4	2.3	<b>8</b> .8	<b>.</b>	7.1	2.5					2.1	.637				
9210	<b>.</b>	5.8	<b>8</b> .5	2.6	<b>9</b> .0	2.9	9.0	2.7					9.0	.052				
9225	12.4	3.8	1.5	J. 5	<b>3</b> .	0.Y	11.7	3.0					D. D.	.062				
9226	S.	5.8	<b>16.5</b>	3.5	10.2	3.1	10.2	٦.٢					4.5	.059				
9233	<b>8</b> .3	2.5	8.2	2.5	8.9	2.8	₹.	2.5					-	.053				

		3	LANDING DATA	_	- MODEL RA-38	<b>8</b> 7	_	JSS DA	USS ENTERPRISE (CVN-65)	<u>بر</u> پر	£-63			Ž	<b>₹</b>	LANDINGS				
200			I U	Z Z	X C L E			ROL	ROLL ANGLE	N C	w	_	PITCH	RATE	שפרר	RATE	ŗ.	F. P. A.	YAN	_
2	5		8		£		5		8		7		¥	5	7	Ę	OT TA	£	AT 70	2
	220	3	930	3	DEC	3	DEG	3	DEC	8	DEG	3	DEG	3	DEG	2	DEG	3	DEG	3
<b>=</b>	7	\$	‡	\$	\$	41	\$	<b>\$</b>	90	51	25	53	\$	55	90	22	28	20	8	5
8	-	=						925								. 911.				.124
959	4.7	982				1	•	054				. •	2.5	. 444	-5.6 -	898 3.8	-	966	2.8	.049
500	2.0	.052						2963								.077-11				.230
962	4.2	.073						919				•				.003				.070
1142	2.7	<b>3</b>				•	•	200				1				.082 -1	-			.070
149	2.0	33						.017								.059	-			. 129
263	5.8	=				ſ	•	.052				•				.059 -	•			.126
210	7.0	543						600								. 105			•	638
225	 	.023				•	•	.002								. 150.				. 856
1226	2.9	159				1	•	.023								. 673	-			.145
233	2.1	.037				•	2	993								.028 -1	-			. 038

	REREAD	NUMBER			•	-					_				
	ğ	3												_	_
	GEAR	RUNOUTS	8	82	406.4	434.3	•	•	434.3	431.8	434.3	429.3	0.0	434.3	429.3
	<b>A</b>	\$	Z	5	9	7	•	•	171	170	171	169	6	17	169
SS	BARCMETRIC	SURE	<b>₽</b>	8	761.0	761.0	759.7	759.7	759.7	759.7	759.7	759.7	759.7	759.7	759.7
NICHT LANDINGS	BAROM	PRESSURE	N H	79	29.96	29.96	29.91	29.91	29.91	29.91	29.91	29.91	29.91	29.91	29.91
E GH	9		ပ	78	2	18	₽	9	1	1	17	11	17	1	1
	=		<b>L</b>	1	*	9	2	3	3	3	63	63	3	3	63
	ROLL		<b>3</b>	92	002	010	. 026	.012	. 005	. 019	037	014	010	9.000	.018
	DECK		DEC	22	ī	0	 	.,	٦.	-	-2.1	<b>80</b>	9.1	9.9	9.
ENTERPRISE (CVN-65)	PITCH		8	*	609	. 003	007	869	007	007	993	007	003	003	0.000
SE (C	DECK		DEG	2		ņ	<b>+</b> .	ا. ئ	<b>+</b> ,	<b>+</b> :	2	<b>4</b> .1	2	2	9.9
MPR I	SHIP	SPEED	¥.	72	2	N	n	n	~	~	7	~	~	~	~
			Ş	7	10	~	50	60	*	•	2	n	n	n	n
22	2	300		2											
	200	346		8	t-8200	50.00	50120	66126	50123	50123	50100	50120	60123	58188	50120
<b>3</b>	SIDE	ġ		3	124	124	124	122	124	<b>5</b>	24	124	<u>*</u>	124	24
MODEL RA-38	WIRE	ġ		6	•	~			73	•		*		n	4
1		¥	=	2	Ξ	2	=	z.	Ξ,	<b>9</b>	9	2	2	2	±
DATA	RAMP TO TO	DISTANCE		_											-
LANDING DATA		5	E	S	299	262	232	171	2	789	184	Š	254	7	5
₹	OFF-CENTER	DISTANCE	3	3	7	7	7	?	7	† '	ę,	7	7	7	7
	7	DIS	E	3	7	- 72	1	÷	1	2	100	7	7	F	7
	8	8		2	8	862	5	9002	9142	9148	9293	9218	9225	9226	9233

T-2C DAY

WEIGHT		KG	21	4329	4329	4329	4329	4329	4329	4329	4329	4329	4329	4329	4329	4238	4329	4329	4329	4329	4329	4465	4329	4329	4284	4284	87C4	4193	4329	4148	4102	4057	4102	4012	4329	4012	4057	4329	3921	4102	4329
WEI		LBS	70	9544	9544	9544	9544	9544	9544	9544	9744	100	82.	9544	9544	9344	9544	9544	9544	9544	9544	9844	9544	9544	9444	9444	****	9244	9544	9144	9044	8944	9044	8844	9544	8844	8944	9544	8644	9044	9544
LIFT	<u>.</u>		19																																						
LIFT	5		81	1.88	1.10	1.10	1.10	.00	- 90 -		9 8	1.19	1.00	1.00	1.00	96.	1.00	96.	96.	1.10	8	- 60	8.	- 9	<b>8</b>	 8 .	90.	 6	99	96.	1.00	1.00	1.00	1.59	1.00	96	1.00	1.10	96.	96	1.66
⋧	<b>∀</b> .ds		11																																						
KVPA	Z		91	1.14	1.13	1.13	1.1	1.23	1.12	.09	9	1.16	1.15	1.07	1.03	1.10	1.04	1.03	1.11	1.13	1.02	1.17	1.15	1.09	=	1.96	20.	2 =	60.	1.09	1.09	1.12	1.13	1.28	1.06	1.04	1.06	1.07	1.1	1.08	1.18
V.dSA		N/S	5																																						
S		ž	<b>±</b>																																						
VPAMIN		N/S	5	49	49	49	49	49	49	<b>\$</b>	? 9	4	6	6	49	4	4	49	49	<del>4</del>	<b>\$</b>	9	<b>4</b>	6	6	6	<b>7</b>	) K	4	48	8	48	\$	41	<b>6</b>	47	48	49	47	₩	49
<u>₹</u>		ž	12	96	96	96	96	96	96	96	ם מ	9 6	96	96	96	95	96	96	96	96	96	97	96	8	8	8	8 6	. S	96	46	93	93	93	92	96	92	93	96	9	93	96
VEOR		M/S	Ξ	88	39	<b>÷</b>	ŧ	42		9 !	<b>}</b>	3 7	4	‡	¥,	‡	39	32	4	<b>4</b> 8	38	48	4	9	‡	‡ :	9	\$ 4	4	39	9	42	39		34	38	40	39	Ř	45	40
>		ž	10	73	75	79	79	<b>8</b>		8	5 8	8	8	86	67	85	76	63	8	87	70	8	8	71	8	8	<b>B</b> !	2 /	, E	76	77	8	76		67	73	67	76	67	18	77
	PERP.	M/S	•	•	-	-	-	-	-	<b>,</b> ,	- •			-	_	-	-	-	-	_	<b>,-</b>	-	•-	-	-	-	- •			-	_	-	-	-	-	-	-	-	-	-	-
WIND-VEL	g.	¥	€0	7	7	8	7	7	8	~	7 (	4 0	1 0	1 00	8	8	~	~	8	8	~	7	8	α	~	~	7	N 6	10	8	7	~	7	8	8	8	7	8	8	7	7
	PAR.	¥S	^	<b>±</b>	<b>*</b>	<b>±</b>	<u>*</u>	<u>*</u>	<u>*</u>	<b>:</b>	<b>:</b> :	<b>1</b>	2 = =	7	<b>±</b>	<b>*</b>	<u>*</u>	<b>±</b>	<b>*</b>	<b>*</b>	<b>*</b>	<b>*</b>	<b>*</b>	2	2	2	77	2 #	2 =	17	2	2	2	2	2	2	2	2	7	2	13
	α.	\$	•	27	27	27	27	27	27	27	7 5	, e	2 6	26	27	28	28	<b>58</b>	28	27	27	27	<b>58</b>	<b>50</b>	22	23	74	8 8	3 6	28	78	26	26	76	25	22	25	25	78	26	26
VE-FILM		¥S	80	2	42	45	42	47	Ŧ	<b>?</b> !	ę ę	? 3	7	9	3	39	37	8	Ŧ	42	2	\$	42	Ŧ	42	<b>?</b>	÷ :	<b>?</b>	7 9	9	6	7	<b>4</b>	47	39	37	80	4	39	39	45
VE-		Š	4	3	8	82	82	6	8	2	1 8	` <b>«</b>	3 2	78	7	76	71	•	79	5	7	87	87	28	5	2		Š	5 5	78	75	78	7	92	26	7	*	77	75	75	87
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*		\$	~	116	168	109	109	118	107	105						104	56	8	107	100	8	114	Ĭ	101	Ē	<u>•</u>	è	60	5 3	Š	101	9		118	10	, <b>5</b>	Ğ	19,	101	10	Ë
	ġ		-	1686	1687	1688	1689	1690	1691	1692	1693	1808	1607	1698	1699	1701	1703	1784	1705	1766	1767	1708	1769	1710	1711	1758	1759	1760	3 5	1765	1767	1768	1769	1779	1771	1772	1773	1774	1775	1776	1777

USS ENTERPRISE (CVN-65)

	•		8	21	4329	4329	1420	1329	4329	200	1329	4329	1329	1329	1329	1238	4182	1148	4329	4957	1556	4329	1329	004	4329	1102	1284	1329	1329	1329	1329	1329	1329	4375	1102	1329	4102	1284	4329	193
	WEIGHT		SS	20	9544 4		•		9544								9044		9544		-		9544														•			9244
NGS	LIFT			<del>0</del>	0,	<b>.</b>	<b>.</b>			, ,	,	<b>.</b>		<b>.</b>	·	<b>,</b>	<i></i> u		. 0,	•	7		ω.				•	•	_	•	<b>.</b>	<b></b>	<b></b>		3.00	<b></b>		•	•	<i>y,</i>
DAY LANDINGS	LIFT	TO FF		<b>8</b>	1.00	1.00	1.00	1.20	99.		1.16	1.00	1.00	1.99	<b>9</b> 6.	99.	 	 - 6	. <del>.</del>	1.88	<b>8</b> 6.	1.10	 8. :	9 6	9 6	99.	- 80.	1.10	- 99	1.10	<b>8</b> .	1.00	1.10	1.00	1.10	<b>8</b> .	<b>.</b>	- 00	- 90	- 00
-	\$	₹.		11																																				
	KWPA	MIN		16	1.10	1.17	1.12	1.19	1.05		1.08	1.1	1.09	1.08	1.10	1.65			1.15	1.10	1.10	1.09	1.15	= :	1.05	=	1.05	1.18	1.15	1.15	1.08	1.05	1.05	1.69	1.02	1.07	<del>1</del> .19	1.06	1.07	<b>*</b>
(52)	V.dSA		K/S	5																																				
USS ENTERPRISE (CVN-65)	N S		ž	<b>±</b>																																				
RISE	VPAMIN		N/S	5	6	6	8	49	<b>\$</b>	7	4	40	49	49	49	6	<b>\$</b> :	9 4	9	8	8	<del>4</del>	<del>\$</del>	8 !	<b>? ?</b>	<b>\$</b>	\$	49	49	6	49	6	6	64	₽	4	4	4	6	4
NTERP	Š		ž	12	90	96	97	96	96	9 6	8	96	96	96	96	88	56	3 2	96	93	88	8	98	97	2 8	0	8	96	96	96	96	96	8	8	8	96	93	8	96	94
USS E	VEOR		K/S	Ξ	\$	\$	8	4	8	; ;	9	3	\$	\$	<b>\$</b>	60	ţ :	•	. <del>.</del>	7	42	‡	<b>=</b> :	:	<b>;</b> ;	4	4	45	42	<b>4</b>	42	37	<b>\$</b>	39	8	<del>+</del>	42	38	37	8
	-		\$	5	8	88	23	96	92	8 8	3 %	3	8	8	82	76	6	) i	- <b>8</b>	82	20	8	8	6	8 2	78	11	8	82	88	82	7	11	22	2	8	<b>8</b>	70	7	89
2 2		PERP.	Ş	0	-	-	•	•	• •	•		-	-	-	_	-	- •			-	-	-	-	<b>-</b> ,		-	_	-	_	-	-	-	-	-		-	-	-	•	•
DATA - MODEL T-2C	WIND-VEL	۵.	₹	60	7	8	•	•	•	PC	· ~	~	7	~	~	<b>7</b>	~ (	<b>,</b>	1 7	7	8	8	~	7 (	, c	1 7		~	7	7	~	~	~	7	~	8	7	8	•	•
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	3		S S		Ñ	Ñ				, ,	•	22	•••												3 2									<b>58</b>						<b>5</b> 8
LANDING	VE-FIL		<u>₹</u>	4			-		男: さ:			-		-	•	-	•			-	-								-	-		-							_	61 42
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	305	ě	_	<b>-</b>	-	-			282	·	-				•			•		-	-	-	-			-	-		•	•									-	1893

MINO-VEL NEOR VPAMIN VSP'A KVP KVP LIFT LIFT LIFT WEIGH WEIGH M/S KN M/S		3		1 4	NG DATA — MODEL T-2C	1-20		5	S ENT	ERPRI	USS ENTERPRISE (CVN-65)	N-65			u	DAY LANDINGS	<b>COINGS</b>		
VAS         ININ         SP-A         ININ         SP-A         ID-B         FF           4/5         IOM         W/5         IOM         W/5         IOM         W/5         IOM         W/5         IOM         W/5         IOM         IOM </th <th>VPAF</th> <th>Ţ.</th> <th>301</th> <th></th> <th>V-QVIW</th> <th>Ē</th> <th></th> <th>VEO</th> <th>œ</th> <th>₩.</th> <th></th> <th>. dSA</th> <th></th> <th>ΛPΑ</th> <th>\$</th> <th>LIFT</th> <th>LIFT</th> <th>¥</th> <th>IGHT</th>	VPAF	Ţ.	301		V-QVIW	Ē		VEO	œ	₩.		. dSA		ΛPΑ	\$	LIFT	LIFT	¥	IGHT
4/5         NA         M/5         NA         NA <th>٤</th> <th></th> <th></th> <th>Ž</th> <th>ď.</th> <th>E</th> <th>o.</th> <th></th> <th></th> <th></th> <th></th> <th></th> <th>_</th> <th></th> <th></th> <th>2</th> <th>#</th> <th></th> <th></th>	٤			Ž	ď.	E	o.						_			2	#		
4         28         7         8         9         11         12         13         14         15         16         17         18         19         20           44         28         13         30         40         71         37         35         40         1.10         1.00         1.00         3544           40         25         25         40         1.10         1.00         1.00         3544           40         25         26         40         1.10         1.10         1.00         3544           40         25         12         30         45         30         40         1.00         3544           41         25         12         30         45         40         1.00         3544           42         25         30         40         40         1.10         1.10         1.10         3544           43         30         40	Ş	₹	Ş		Ş		\$						S					SS .	S S
40         26         13         9         71         37         95         49         1.10         1.00         9444           41         24         12         12         0         73         35         49         1.10         1.00         9344           41         24         12         10         74         35         49         1.10         1.00         9344           42         12         12         0         74         35         49         1.10         1.00         9344           42         22         12         24         25         49         1.12         1.00         9344           42         22         11         2         1         74         30         49         40         1.12         1.10         1.10         9344           42         22         11         2         1         74         30         40         1.13         1.10         1.10         9344           42         22         11         26         40         1.12         1.10         1.10         1.10         9344           42         22         11         26         40         40	n	•	n	•	7	•	•						15	9	11	8	19	70	2
41         24         12         10<	3	78	\$	<b>58</b>	5	•	•	7	37	92	<b>\$</b>		_	6		1.00		9444	4284
41         24         12         6         83         43         55         49         108         108         9444           40         23         12         6         6         64         45         49         110         108         9844           41         23         12         6         6         64         45         93         49         110         108         9844           41         23         12         6         6         64         45         93         49         110         108         9844           41         23         13         96         49         110         110         110         9844           42         23         14         14         96         49         110         110         9844           42         23         16         49         110         110         110         9844           42         23         14	3	2	Ŧ	<b>3</b>	12	•	•	73	88	56	49		-	<b>9</b> -		1.00		9344	4238
43         23         14         23         49         14         23         49         14         23         49         14         23         14         14         23         12         9         74         33         49         11         13         10         94         44         44         23         44         11         13         10         96         44         44         23         44         11         13         10         96         44         44         23         44         11         13         10         96         44         44         23         44         11         13         10         96         44         44         13         46         44         11         14 </th <th>3 :</th> <th>2</th> <th><b>7</b> i</th> <th>77</th> <th>72</th> <th>•</th> <th>•</th> <th><b>3</b> :</th> <th><b>?</b></th> <th>S</th> <th><b>9</b></th> <th></th> <th>_</th> <th>8</th> <th></th> <th>1.00</th> <th></th> <th>9444</th> <th>4284</th>	3 :	2	<b>7</b> i	77	72	•	•	<b>3</b> :	<b>?</b>	S	<b>9</b>		_	8		1.00		9444	4284
42         22         11         23         14         35         44         11         35         44         45         35         45<	<u> </u>	٤;	g (	2 :	2 :	•	•	<b>★</b> 8	<b>9</b> , 1	3	o •		- •	ج و		 6 .		9344	4238
42         22         1         24         38         93         46         1.13	7 2	? 2	} ;	3 2	2 2	<b>.</b>	<b>.</b>	8 4	\$ <b>13</b>	2 2	• <b>•</b>			6 C				8844	4017
41         21         11         2         1         76         39         64         1.05         1.10         1.10         1.10         9544           45         21         11         2         1         74         39         49         1.10         1.10         1.00         9544           45         22         11         2         1         74         36         49         1.10         1.00         9544           44         22         11         2         1         39         49         49         1.10         1.00         9544           45         22         11         2         1         79         49         49         1.10         1.00         9544           45         22         11         2         1         79         49         49         1.10         1.00         9544           45         22         11         2         1         79         49         49         1.10         1.10         9544           45         24         12         2         1         49         49         1.10         1.10         9544           46         24	3	2	7	2	: <del>_</del>	~~	·	*	<b>8</b>	26	. <b>.</b>		_	<u>.</u>		96		8944	4957
45         21         11         2         179         41         96         49         11.13         .79         9544           45         22         11         2         1         44         45         96         49         11.16         11.96         9544           46         22         11         2         1         44         45         96         49         100         9644           41         22         11         2         1         49         97         50         11.12         11.00         9644           45         22         11         2         1         96         49         97         50         11.12         11.00         9644           45         24         12         2         1         74         96         49         11.17         11.00         9644           45         24         12         2         1         74         96         49         11.17         11.10         9644           46         24         12         2         1         14         97         50         11.17         11.10         9644           41         24	25	2	Ŧ	2	=	~	_	92	39	96	6		-	. 65		1.10	1.10	9544	4329
4.3         22         11         2         1         84         4.5         96         49         1.10         1.00         9544           4.6         22         11         2         1         36         49         1.00         1.00         9844           4.1         22         11         2         1         36         49         1.11         1.10         9844           4.2         21         2         1         3         36         49         1.11         1.10         9844           4.2         21         1         2         1         36         49         1.11         1.10         9844           4.2         21         2         1         36         49         1.11         1.10         9844           4.2         2.5         13         36         49         1.10         1.00         9844           4.5         2.4         3         36         49         1.17         1.00         9844           4.6         2.4         3         49         49         1.10         3644           4.6         2.4         3         49         49         1.10	8	8	\$	5	=	~	_	20	<b>‡</b>	96	<b>\$</b>		-	.13		.70		9544	4329
42         22         11         2         7         34         96         49         1.08         1.08         1.09         9544           44         22         11         2         1         96         49         97         59         1.15         1.19         9544           44         22         11         2         1         96         49         1.12         1.19         9544           45         22         11         2         1         96         49         1.11         1.09         9544           45         22         13         96         49         1.19         1.09         9544           46         24         12         2         1         96         49         1.19         1.09         9544           46         24         12         2         1         96         49         1.17         1.19         9544           41         25         12         2         1         96         49         1.10         9644         1.11         1.10         9544           41         25         14         96         49         1.12         2         1.12	2	2	2	22	=	~	_	<b>*</b>	2	96	6		-	.10		8		9544	4329
46         22         11         2         1         96         49         56         1.15         1.28         9844           44         22         11         2         1         75         39         96         49         1.12         1.06         9844           45         22         11         2         1         75         39         96         49         1.12         1.06         9844           45         25         11         2         1         45         49         49         1.17         1.16         9544           46         24         12         2         1         7         96         49         1.17         1.16         9644           46         24         12         2         1         7         96         49         1.17         1.16         9644           41         23         12         2         1         97         96         1.16         1.16         9644           41         23         14         97         56         1.16         1.16         9644           41         23         14         94         48         1.16         <	3	<b>8</b>	42	2	= :	~	<b>.</b>	2	<b>8</b> 2	96	<b>9</b>		_	80		1.00		9544	4329
41         22         11         2         1         59         59         1.05         1.09         9844           44         22         11         2         1         59         49         59         1.12         1.19         9844           45         22         11         2         1         95         44         97         50         1.19         1.19         9844           45         24         12         2         1         96         49         1.17         1.19         9544           46         24         12         2         1         74         36         49         1.17         1.19         9544           46         24         12         2         1         96         49         1.17         1.19         9544           41         23         14         96         49         1.17         1.19         9544         1.11         1.19         9544         1.11         1.19         9544         1.11         1.19         9544         1.19         1.19         9544         1.19         1.19         9544         1.19         1.19         1.19         1.19         1.19 <td< td=""><th><b>3</b></th><th>2 3</th><td><b>.</b></td><td>2</td><td>= :</td><td>~</td><td></td><td>96</td><td>6</td><td>6</td><td><b>8</b></td><td></td><td>-</td><td><u>.</u></td><td></td><td>1.20</td><td></td><td>9844</td><td>4465</td></td<>	<b>3</b>	2 3	<b>.</b>	2	= :	~		96	6	6	<b>8</b>		-	<u>.</u>		1.20		9844	4465
45         22         11         2         1         95         44         97         59         1.11         1.00         9544           45         24         12         24         12         41         96         49         1.17         1.10         9544           45         24         12         1         74         96         49         1.17         1.00         9544           46         24         12         2         1         97         96         49         1.17         1.00         9544           46         24         12         2         1         97         96         49         1.17         1.00         9644           41         22         1         2         1         97         96         49         1.17         1.00         9644           41         22         1         2         1         77         40         94         48         1.13         1.10         9644           41         22         1         7         40         94         48         1.10         1.10         9644           42         22         1         7	7 ¥	8 2	÷	2 2	= :	N 6		*	9		9 9			છે. <del>ટ</del>		9.		9844	4465
42         25         13         2         1         79         41         96         49         1.10         1.00         9544           46         24         12         2         1         74         36         49         1.17         1.10         9544           45         24         12         2         1         34         95         49         1.17         1.00         9544           41         23         12         2         1         91         47         95         49         1.17         1.10         9544           41         23         12         2         1         94         48         1.13         1.10         9544           42         22         11         2         1         77         49         48         1.13         1.10         9544           42         22         11         2         1         76         94         48         1.11         1.10         9544           42         22         11         2         4         48         49         1.10         1.10         9544           42         22         11         2	3 %	3 2	: 9	3 2	==	, ~	-	5 K	3 4		9 6			7 2		. 6		9844	4465
45         24         12         24         47         96         49         1.17         1.19         9544           46         24         12         2         1         47         36         49         1.07         1.06         9444           45         24         12         2         1         83         43         1.17         .96         9444           41         23         12         2         1         80         41         97         59         1.06         1.10         9444           41         22         11         2         1         85         44         94         48         1.16         1.10         9544           41         22         11         2         1         77         40         94         48         1.16         1.10         9544           41         22         11         2         1         76         96         49         1.11         1.10         9544           41         22         11         2         1         46         1.11         1.10         9644           42         12         12         14         48 <t< td=""><th>8</th><th>5</th><td>2</td><td>12</td><td>5</td><td>· ~</td><td>_</td><td>2</td><td><b>: :</b></td><td>98</td><td>9</td><td></td><td>_</td><td>9-</td><td></td><td>. 6</td><td></td><td>9544</td><td>4329</td></t<>	8	5	2	12	5	· ~	_	2	<b>: :</b>	98	9		_	9-		. 6		9544	4329
40         24         12         1         74         36         49         1.07         1.00         9544           45         24         12         2         1         74         36         49         1.17         .90         944           41         25         14         95         49         1.17         .90         944           41         25         14         94         48         1.13         1.10         9244           42         22         11         22         1         66         49         48         1.13         1.10         9244           42         22         11         2         1         74         48         1.11         1.10         9244           42         25         14         84         1.11         1.10         9244           42         23         14         48         1.11         1.10         9244           43         24         48         1.11         1.10         9244           41         25         14         48         1.11         90         9444           41         25         14         48         1.11<	8	8	<b>\$</b>	*	12	~	_	=	47		8		~	.17		1.10		9544	4329
45         24         12         24         13         45         49         9444           46         24         12         13         14         95         49         122         190         9444           41         23         12         12         190         9644	25	2	<b>?</b> !	5	12	(4)	_	*	<b>8</b>	•	6		_	.07		1.00		9544	4329
41         25         12         2         1         91         47         95         48         1.10         9244           41         22         11         2         1         77         46         94         48         1.10         9244           41         22         11         2         1         77         46         94         48         1.10         1.10         9244           42         22         11         2         1         76         39         94         48         1.11         1.10         9244           45         22         11         2         1         76         39         94         48         1.11         1.10         9244           45         23         12         2         1         87         48         1.11         1.10         9144           41         23         12         2         1         87         49         49         1.11         1.10         9144           44         28         35         49         49         1.11         1.00         9144         1.10         9144           44         28         13         <	5	6	<b>Ş</b> :	* 2	2 :	~ •		2 :	<b>3</b> :	•	<b>9</b> 9		- •	- 8		<b>6</b> 6.		444	4284
44         22         11         2         1         97         98         1.10         9244           42         22         11         2         1         85         44         84         48         1.10         9244           41         22         11         2         1         76         96         48         1.11         1.10         9244           42         22         11         2         1         76         39         94         48         1.11         1.10         9244           45         23         12         2         1         76         39         94         88         1.11         1.10         9144           41         23         12         2         1         76         39         94         88         1.11         1.10         9144           41         23         12         2         1         87         48         1.11         1.10         9144           44         26         13         2         48         1.10         1.10         9144           44         26         13         48         49         1.10         1.10 <t< td=""><th>8 :</th><th>3 8</th><td>₽;</td><td>* ?</td><td>2 :</td><td>7 6</td><td></td><td>- 6</td><td><b>;</b></td><td></td><td>2 9</td><td></td><td>- •</td><td>77.</td><td></td><td>8.</td><td></td><td>***</td><td>4284</td></t<>	8 :	3 8	₽;	* ?	2 :	7 6		- 6	<b>;</b>		2 9		- •	77.		8.		***	4284
42         22         11         2         1         77         40         94         48         1.16         1.09         9244           41         22         11         2         1         76         46         94         48         1.11         1.19         9144           45         23         12         2         1         76         39         94         48         1.11         1.19         9144           41         23         12         2         1         76         39         94         48         1.11         1.19         9144           41         23         12         2         1         76         39         94         48         1.11         1.19         9144           41         23         12         2         1         87         49         1.09         1.09         9444           41         26         13         9         49         1         109         1.09         9444           44         26         13         48         49         1         109         1         1         96         49         1         1         1         1	3 2	8 2	; <b>3</b>	3 2	2 =	7 6		22 6	; <b>3</b>	, , ,	9 60			9 <u>5</u>		9 -		9844	4465
41         22         11         2         1         87         45         96         49         1.05         1.16         9544           42         22         11         2         1         76         39         94         48         1.11         1.16         9144           45         23         12         2         1         76         39         94         48         1.11         1.16         9144           41         23         12         2         1         76         39         94         48         1.11         1.16         9144           41         23         12         2         1         66         35         49         1.11         1.16         9144           44         26         13         2         4         93         48         1.17         1.16         1.16         9144           46         24         12         2         1         66         97         48         1.17         1.16         9144           49         13         1         1         1         1         1         1         1         1         1         1         1	3	2	42	22	=	~	_	11	ę	76	2		-	10		- 90		9244	4193
42         22         11         2         1         76         46         94         48         1.11         1.16         9144           45         23         12         2         1         76         39         94         48         1.11         .90         9044           41         23         12         2         1         66         35         95         49         1.07         1.06         944           41         25         12         2         1         67         35         95         49         1.07         1.06         944           44         26         13         2         1         67         34         93         48         1.09         1.06         984           46         24         12         2         1         67         34         93         48         1.06         1.06         984           46         24         12         2         1         34         92         47         1.06         1.06         984           49         13         2         1         64         49         47         1.08         1.08         1.08         1.08	22	2	Ŧ	22	=	~	_	. 22	<b>5</b>	•	6		_	.05		1.10		9544	4329
45         23         12         2         1         76         39         94         48         1.17         1.16         9144           42         23         12         2         1         87         45         93         48         1.11         .90         944           41         25         12         2         1         87         45         95         49         1.09         1.00         944           44         26         13         2         1         66         34         93         48         1.09         1.00         9844           46         24         12         2         1         97         36         97         1.17         1.00         9844           49         24         12         2         1         97         36         47         1.10         1.10         9844           40         25         13         6         49         47         1.10         1.10         9544           41         24         12         2         1         81         49         49         1.08         1.08         1.09         9544           41 <td< td=""><th>3</th><th>95</th><td>7</td><td>77</td><td>=</td><td>~</td><td>_</td><td></td><td><b>6</b></td><td></td><td><b>\$</b></td><td></td><td>_</td><td>=</td><td></td><td>- - - -</td><td></td><td>914</td><td>4148</td></td<>	3	95	7	77	=	~	_		<b>6</b>		<b>\$</b>		_	=		- - - -		914	4148
42       23       12       2       1       64       45       93       46       1.07       1.06       9444         41       25       12       2       1       65       35       95       49       1.07       1.06       9444         44       26       13       2       1       67       34       93       46       1.09       1.06       9844         46       24       12       2       1       97       56       1.17       1.06       9844         46       24       12       2       1       37       92       47       1.18       1.19       8844         41       24       12       2       1       47       1.19       1.19       8844         41       24       12       2       1       81       42       47       1.19       1.19       8844         41       24       12       2       1       81       42       43       1.08       1.09       9544         41       24       12       2       1       80       41       96       49       1.09       99       9544         42	57	6	<b>\$</b> :	2	2 5	~	<b>-</b> ,	•	<b>6</b> 0	•	<b>.</b>		-	.17		<del>-</del> 10		9144	4148
41       25       12       2       1       65       35       49       1       87       49       49       1	3 8	<b>5</b> 8	7:	2 :	77	N (	_ ,		Ç;	•	<b>.</b>		- 1	= {		8.		9044	4102
44       26       13       2       1       66       34       93       48       1.10	76	? ;	<b>;</b> ;	3 3	7 ;	N (		-	3 5	•	<b>P</b> (		- ,	<b>)</b> :		99.	•	*	4284
46     24     12     2     1     97     56     97     56     1.17     1.06     9844       39     24     12     1     74     36     97     1.06     .96     8844       40     25     13     2     1     64     33     92     47     1.06     .96     8844       41     24     12     2     1     81     42     96     49     1.09     .96     9544       42     23     12     2     1     80     41     96     49     1.06     9544       42     23     12     2     1     84     43     96     49     1.07     1.10     9544       42     23     12     2     1     84     43     96     49     1.09     1.09     9544       36     23     12     2     1     73     36     49     1.07     1.00     8544       41     23     12     2     1     81     42     96     49     1.07     1.10     9544	8 2	8 5	; ;	9 %	2 5	4 C		•	2 \$		2 5			0 g			-	#0# #0#	4528
39     24     12     2     1     74     38     92     47     1.08     .99     8844       40     25     13     2     1     64     33     92     47     1.19     1.19     8844       41     24     12     2     1     64     33     92     47     1.19     1.19     8844       42     23     12     2     1     80     41     96     49     1.08     .90     9544       42     23     12     2     1     84     43     96     49     1.09     1.09     8544       36     23     12     2     1     73     38     90     46     1.07     1.00     8544       41     23     12     2     1     81     42     96     49     1.07     1.00     8544	9	2 2	3 4	2 2	2 2	. ~			9 6	2 6	9 9		-	1.5		8		9844	4465
40         25         13         2         1         64         33         92         47         1.10         1.10         8844           41         24         12         2         1         81         42         96         49         1.08         .90         9544           42         23         12         2         1         80         41         96         49         1.08         .90         9544           41         22         11         2         1         80         49         1.07         1.10         9544           42         23         12         2         1         84         43         96         49         1.09         1.00         9544           36         23         12         2         1         73         38         90         46         1.07         1.09         8544           41         23         12         2         1         81         42         96         49         1.07         1.10         9544	5	92	90	7	12	~	_		82	•	(1)		_	88		96		8844	4012
41     24     12     2     1     81     42     96     49     1.09     .90     9544       42     23     12     2     1     80     41     96     49     1.06     .90     9544       41     22     11     2     1     80     43     96     49     1.07     1.10     9544       42     23     12     2     1     73     36     49     46     1.07     1.00     8544       41     23     12     2     1     81     42     96     49     1.07     1.10     9544	25	1	\$	23	13	8	_	-	33	•	11		-	9.		1.10		8844	4012
42     23     12     2     1     80     41     96     49     1.08     .90     9544       41     22     11     2     1     83     43     96     49     1.07     1.10     9544       42     23     12     2     1     73     36     90     46     1.07     1.00     8544       36     23     12     2     1     73     36     90     46     1.07     1.00     8544       41     23     12     2     1     81     42     96     49     1.07     1.10     9544	3	8	<del>-</del>	<b>3</b>	12	~	_	<b>20</b>	42	98	<b>\$</b>		-	<b>6</b> 0.		96		9544	4329
41     22     11     2     1     83     43     96     49     1.09     1.09     9544       42     23     12     2     1     73     36     49     1.07     1.09     9544       36     23     12     2     1     73     36     90     46     1.07     1.09     8544       41     23     12     2     1     81     42     96     49     1.07     1.10     9544	3	5	42	23	12	~	_	9	÷	96	6		_	.08		96		9544	4329
42 23 12 2 1 84 43 96 49 1.09 1.00 9544 38 23 12 2 1 73 38 90 46 1.07 1.00 8544 341 23 12 2 1 81 42 96 49 1.07 1.10 9544	22	2	Ŧ	22	=	7	-	3	<b>4</b> 3	96	6		-	.07		1.10		9544	4329
38 23 12 2 1 73 38 90 46 1.07 1.00 8544 41 23 12 2 1 81 42 96 49 1.07 1.10 9544	3	5	42	23	12	~	_	<b>4</b>	<b>5</b>	96	6		-	60.		1.00		9544	4329
41 23 12 2 1 81 42 96 49 1.07 1.10 9544	3	*	8	23	12	7	-	23	89	96	9		-	.07		1.00		8544	3876
	25	2	Ŧ	23	12	8	_	<b>=</b>	42	96	6		-	.07		1.10		9544	4329

			3		- Y	NG DATA — MODEL T-20	1-20			NS EN	TERPA	USS ENTERPRISE (CVN-65)	CVN-6	2)			DAY LANDINGS	ND INGS		
997	WAF	5	VE.	71 (4		WIND-VEL	VEL		*	VEOR	A A	VPAMIN	V.dSA	٠.	KVPA	\$	LIFT	LIFT	WE	WEIGHT
ě	5	_			ã	PAR.	PERP.	ø.							K	<b>∀</b> ঞ	5	<u>1</u>		
	Š	Ş	₫	Ş	\$	¥,	\$	X X	\$	E N	ž	S/M	¥	S/M					SS	8
-	~	2	•	80	•	^	•	•	•	=	2	5	<b>±</b>	5	91	17	5	6	20	21
1949	+==	88	2	<b>4</b>	54	72	8	_	79	<b>‡</b>	96	6			1.19		1.00		9544	4329
1950	<b>5</b>	3	8	÷	<b>5</b>	12	8	_	2	39	46	48			1.10		96		9244	4193
1951	107	8	3	\$	<b>5</b>	12	7	-	8	9	96	49			1.12		- 99		9544	4329
1953	<b>.</b>	25	E	\$	<b>5</b>	12	~	-	2	8	8	<b>\$</b>			1.07		1.10	1.10	9144	4148
1955	102	25	2	7 ;	75	77	~	_	8	<b>\$</b> ;	95	64			1.07		1.00		9444	4284
1956	2	2	9	8 <u>2</u>	*	72	~	-	69	2	\$	<b>\$</b>			99.		 8 6		4	4148
1937	120	2 2	2 :	<b>?</b> ;	<b>*</b> 5	2 :	~ <		<u>.</u>	<u>.</u>	6	<b>6</b>			1.26		99.9		4408	4529
000		7	8 :	; ;	<b>*</b> ?	7:	N (	- •	5 6	?:	n (	) (			- 6		9 -		9544	4739
1901	3	\$ 2	5 =	7 5	; ;	2 5	٠,		3 5	? ;	9 6	P [					- 6		8744	3966
1964	2	\$ 8	5 2	4 4	; 5	<u>.</u> e	, ,		8 2	; ;	2 6	• •					1.19		9446	4284
1965	3	3	5	4	2	: <b>=</b>	1	_	<b>2</b>	13	9	6			1.09		1.00		9344	4238
1966	2	8	2	‡	22	=	7	_	8	‡	96	64			1.13		1.19		9544	4329
1967	<b>5</b>	3	3	3	22	=	7	-	88	Ŧ	86	20			1.07		1.10		16644	4556
1969	102	25	2	<b>:</b>	7	7	~	<b>-</b>	28	<b>4</b>	8	<b>\$</b>			1.09		1.20		9144	4148
1970	=	22	2	<b>9</b> :	33	<u>.</u>	<b>7</b>	<b>,</b>	2	8	56	<b>4</b>			9.		1.20	1.20	9644	4182
Z 2	5	8 9	8 8	\$ :	3 :	2 :	N (	- •	8 3	;;	2 6	9			- -		-		9 2 4 4	4420
1972	2 8	? ;	2 5	<b>ا</b>	3 5	7 :	, c		\$ 5	<b>?</b>	3 8	9 6			9. 40				9544	4329
1974	6	5 3	: 2	<b>,</b>	3 2	: <b>:</b>	• ~		<b>. .</b>	3 =	2	£ 4			1.03		96.		9244	4193
1975	112	3	3	4	2	=	· ~	_	8	‡	96	6			1.17		1.10		9544	4329
2044	=	5	8	<b>\$</b>	77	=	-	_	8	49	97	20			1.21		1.20		9844	4465
2046	102	25	2	Ŧ	73	=	-	_	3	32	97	20			1.05		1.00		9744	4420
2047	3	3	5	7	2	= :	-	-	<b>3</b>	3	6	<b>S</b>			1.06		1.60		9744	4428
2 <b>6</b> 48	2 5	3 2	<b>5 2</b>	<b>7</b>	2 2	= =	<b>~</b> c		8 2	‡ ;	9 6	÷ 5			 86		1.66		9644	42/3
2856	2	3	5	: 4	5	: <b>=</b>	۱ ۸		<b>5 5</b>	42	6	8 6			1.05		1.00		9744	4420
2051	5	8	6	<b>\$</b>	2	Ξ	ч	_	3	3	8	49			1.1		1.20		9444	4284
202	107	S	2	ŧ	7	Ξ	8	-	<b>2</b>	<b>.</b> 3	96	49			1.12		- 98		9544	4329
2053	2	š	2	<b>∓</b>	7	=	М	-	82	<b>4</b> 8	96	6			1.04		1.10		9544	4329
2054	Ē	25	2	<b>‡</b>	22	=	7	-	8	3	96	<b>4</b>			1.05		8	96.	9544	4329
2022	3	3	ē	7	75	=	N	_	5	42	8	64			. 69		9.		9344	4238
2026	2	8	3	<b>3</b> :	22	= :	~	<b>-</b>	8	‡	8	69			1.12		ee		4400	4238
2057	= :	£ 5	2 3	\$ ;	2 2	= ;	<b>N</b> (	<b>-</b> ,	2 3	3 :	100 i	<b>6</b>			9		1.28		4478	4238
2026		5		2	<b>5</b> :	= :	7	<b>-</b> •	166	2	6	9			3.5		9	99.	***	4236
2059	2	<b>\$</b> :	٤ ۲	g :	<b>e</b> (	9 ;	~ (	<b>-</b> .	8	‡ :	6	6			9.		69.		9444	4284
2060	=	5	2	<b>\$</b> :	55	= :	11	<b>-</b> ·	8	9 9	60	<b>6</b>			7.7		 66.	•	9344	4230
2061	2	5	۶ :	<b>;</b>	5	<b>=</b> ;	~ •		85	7 :	8	<b>6</b>			96.		99.	 B	9344	4238
2063	6	ž :	\$ 3	<b>;</b>	5	= :	7		<u>a</u> 8	47	8	<del>2</del> 6			- 6		8.		##C#	4200
2065	20	3	3	3	20	9	N	_	20	9	40	ş			7. 1.		1.00		1178	つねーナ

	WEIGHT		ă	21		4148	3966	3921 4238	4375	4329	4375	4329	4238	5,5	4238	4193	4057	4193	4238	4193	4102	4102	4057	3966	4102	2966 4148	4102	4012	4057	3966	4193	3876	3070	3785	4375	4329	4329	4329	4284
	WEI		<b>183</b>	20		9144	8744	9244	9644	9544	9644	9544	9344	4400	77%	9244	8944	9244	9344	9244	9644	9944	8944	8744	9944	8744 9144	964	8844	8944	8744	9244	8544	8644	8344	9644	9544	9544	9544	9444
INGS	LIFT	7.		6																			1.10																
DAY LANDINGS	LIFT	70		8	1.00	1.20	. 60	 9	1.10	1.00	96.	- 8	 6 .	9 6		.00	8.	1.00	1.00	98	 60 6	9 -	.00	96	<u>.</u>	 9 6	99.	1.10	<b>8</b> 6.	1.20	- 60	8. 6	e	. 6	1.10	1.20	1.20	1.00	1.20
	\$	<b>∀</b> .ds		1																																			
	KVPA	K		16		1.06	<del>-</del> :		1.09	1.09	1.09	1.10	e.		. 6.	1.10	1.01	1.05	1.05	1.08	 	3 =	1.09	1.09	1.07	1.00	1.04	1.01	1.09	- 1 <del>0</del>	5.13	<u>*</u> :	. 6	1.12	+1.	1.13	1.19	=	1.17
<b>3</b> 2)	V.dSA		N/S	5																																			
USS ENTERPRISE (CVN-65)	Š		₹	<b>±</b>																																			
11SE	VPAMIN		N/S	5		<b>\$</b> !	;	÷ 9	<b>\$</b>	<b>\$</b>	4	<b>\$</b> :	<b>\$</b>	? 9	7	8	₽	\$	<b>4</b>	<b>4</b>	<b>?</b> \$	<b>4</b>	<b>4</b>	4	<b>\$</b> :	÷	<b>\$</b>	4	<b>4</b>	4	<b>\$</b>	<b>?</b>	} {	9	<b>\$</b>	4	<b>4</b>	6	4
1589	\$		\$	12		6	6 6	. G	9	96	96	96	8	9 6	) (C	3	93	\$	8	6	2 2	8	8	95	2 3	2 4	8	92	93	87	\$	<b>B</b> 6	3 5	8	8	96	8	8	92
SS EN	VEOR		N/S	=	Ŧ	7	5 S	2 <b>4</b>	2	<b>£</b>	<b>•</b>	<b>3</b> i	3:	- 4	<b>4</b>	<b>4</b>	8	39	೫	3 :	<b>R</b> 5	3 2	‡	8	8 8 8	‡ <b></b>	2	<b>\$</b>	8	<b>6</b>	7	8 3	5	3 5	7	<b>∓</b>	47	7	7
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ING DATA - MODEL T-2C	WIND-VEL		\$	~	~	~	~	~ -	. ~	~	~	~ .	<b>.</b> .	. ~	. ~	~	~	~ .	~ -			_	_	<u>~</u> .	~ ~		_	_				_	•	_	<u>~</u>	-		<b></b>
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65)	V.dSA		K/S	5																																		
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9	MIN	PAR.	Ş	~	5	1	2	<b>:</b>	2 2	2	2	12	12	7	7 5	7:	2 =	2	12	7	12	2	2 5	: 2	2	7	2 :	2 =	<b>*</b>	<b>±</b>	<b>±</b>	<b>±</b>	<b>±</b>	<b>₽</b>	÷.	<b>5</b> 3	2 :	4
ATA -		۵.	\$	•	25	22	52	22	2 2	2	22	24	74	5	<b>%</b> :	7 6	3 %	2 5	7	<b>5</b>	7	77	<b>*</b>	7	2	<b>5</b>	33	3 2	2 5	8	28	28	28	2	8	3	3 3	
	VE-F1UM		Ş	80	<b>\$</b>	4	\$	\$	12	2	‡	42	\$	<b>‡</b>	4:	7 ;	<b>?</b>	<b>\$</b>	7	47	\$	7	‡ ;	=	3	\$	25	<b>?</b>	} =	3	7	<b>‡</b>	42	7	8	<b>;</b>	2 :	
CAND IN	<u> </u>		₫	*	8	<u>=</u>	3	2	2 2	3	8	87	2	2	2	2	\$ 2	5	2	8	28	8	2 3	2	3	2	2	2 7	2	7	8	2	=	2	2	2 3	3 8	
	₽	_	¥\$	n	30	8	5	60	6 8	8	57	S	3	3	<b>%</b>	2 :	8 \$	3	3	3	3	3	8 8	3	3	2	<b>?</b> :	8 2	3	25	57	8	8	8	3	5	ខ្លួ	
	VPAF	2	<b>∑</b>	8	115	116	118	115	= <b>2</b>	5	Ξ	<u>5</u>	=======================================	3	2	8 8	2	=	2	116	112	116	2 :	1	2	112	91		10.7	102	=	5	60	107	2	-	8 :	
		Š		-	2543	2544	2545	2546	2548	2549	2550	2551	2552	2553	2554	2000	7555	2559	2566	2561	2562	2564	2565	2567	2568	2570	2571	27.27	2574	2575	2576	2577	2578	2579	238	2561	2962	3

	WEIGHT		¥	5	4329	4329	4329	4511	4465	4329	4329	4465	4238	4465	4375	4284	4329	4329	4148	4329	4329	1017
	WE		<b>S87</b>	<b>39</b>	9544	9544	9544	9944	9844	9544	9544	9844	9344	9844	9644	9444	9544	9544	9144	9544	9544	4760
INGS	LIFT	14		6								1.00									1.10	
DAY LANDINGS	LIFT	2		<b>5</b>	96	- .00	96	- 99	1.00	- 96.	1.00	1.00	- 90.	1.20	1.20	1.10	1.10	96.	1.10	1.19	1.10	-
	≩	<b>∀</b> .ds		17																		
	KWPA	Z		<b>5</b>	1.13	1.1	1.15	1.1	1.03	.97	1.15	1.03	1.04	1.06	1.15	1.17	1.01	1.20	1.09	1.12	1.1	1.08
65)	V.dSA		S/M	<b>5</b>																		
ENTERPRISE (CVN-65)	\$		ž	=																		
RISE	VPAMIN		M/S	13	4	49			56									4	•	4	<del>4</del>	_
NT ERP	\$		Ž	12	90	96	96	98	97	96	96	97	95	97	96	95	96	96	94	96	96	76
uss e	VEOR		s/x	Ξ	‡	Ŧ	‡	\$	37	42	42	4	37	4	‡	42	37	4	35	<b>‡</b>	9	3
	>		₹	•	8	79	90	87	7	82	6	78	72	92	8	87	72	92	8	79	1	71
0		PERP.	\$	•	-	-	-	-	-	-	-	-	_	-	-	_	-	-	-	-	_	-
NG DATA - MODEL T-20	-VEL	0	₹	•	8	7	7	~	~	8	8	8	7	-	~	7	-	7	~	8	8	•
3007	WIND-VEL	PAR.	Ş	^	7	12	12	12	72	12	=	=	=	=	=	=	=	5	72	12	<b>=</b>	5
17A -		ã	₹	•	23	74	7	23	23	23	22	77	77	22	5	5	77	22	23	54	28	76
	3		Ş	•	\$	42	Į	‡	<b>?</b>	26	<b>4</b>	\$	g	42	\$	\$	8	<b>4</b>	<b>∓</b>	<b>*</b>	42	4
3	VE.		₹	*	2	87	2	2	F	?	2	28	92	5	2	2	73	2	2	3	5	F
	4	_	Ş	•	90	83	57	26	5	\$	57	5	8	3	57	57	8	20	25	8	20	3
	VPAF	5	\$	~	6	106	100	5	2	2	100	2	8	103	=	=	97	13	102	107	100	191
	99A	Š		-	2586	2587	2588	2589	2590	2591	2592	2593	2594	<b>†0</b> †	4063	4177	4313	133	253	4535	4705	104

993			AIRCRAFT		KING S	SINKING SPEED AT TOUCHDOWN	TOUCH	N O			GL 1DE	PATH /	GLIDE PATH ANGLE AT TO	0T TO	WHEEL HEIGHT	EIGHT	HOOK HEIGHT	1GH1
2	NOSE	SE	PORT	<b>7</b> 4	ST	STBO	AVG		FREE-FLIGHT	FH	SF-R	2	6	A M	OVER RALLP	AMP.	OVER RAMP	AMP.
	53	Ş	2	Ş	٤	Ş	<b>5</b> /2	S/M	F/S	M/S	DEG	8	DEG	8	E	3	E	3
23	23	<b>5</b>	22	<b>38</b>	22	<b>98</b>	50	8	3	32	23	Ř	35	36	33	88	39	6
1686	6.3	1.9	7.2	2.2	7.5	2.3	7.3	2.2			3.3	. 058	2.8	.049	18.4	5.6	15.7	4.8
1687	6. 9	2.1	9.0	7.0	<b>9</b> .0	<b>.</b>	6.5	5.0			3.5	.061	2.5	.044	12.4	3.8	<del>.</del> 6	2.8
1568 888	<b>3.</b> ♦	<b>9</b> .	5.3	<b>•</b> .	4.7	<b>→</b> :	5.0	5.5			2.4	. 042	<b>-</b> .6	. 028	14.3	<b>+</b> .+	1.5	3.5
1689	6.7	2.1	7.0	2.1	3.7	<u>-</u>	5.3	<b>9</b> .			2.7	. 947	9.	. 033	17.2	5.5	14.6	<b>+</b> .+
1690	4.0	1.5	ы. В	1.2	0. 10.	1.2	3.8	1.2			2.0	.035	- 0.	.018	13.9	4.2	1.3	3.5
1691	7.4	2.5	9.7	2.3	7.3	7.7	7.6	2.3			,	1	2.7	.047	;	,	•	
1692	<b>*</b>	*	4.7	<del>*</del>	<b>4</b>	-	÷.	<b>*</b>			<u>-</u>	.055	 	. 023	77.7	4.6	<b>.</b>	2.7
1693	7.2	7.5	7.7	2.3	<b>.</b>	<b>.</b>	<b>6</b> 0	<b>7</b>			٠. -	.054	5.9	.051	15.8	<b>4</b> .	13.2	<b>6</b> .
1695		<b>.</b>		2.1	7.3	7.7	7.2	7.5			٠. ا	. 955	9. 9.	. 052	16.2	<b>4</b>	13.7	4.2
1696	4.5		4	-	8. 8.	<b>.</b> .		1.7			ر د د	.062	5.6	645	15.6	<b>4</b> .8	5. 6.	<b>4</b> .
1697	<b>9</b> .	<b>5.8</b>	Ø.	2.7	<b>9</b> .3	<b>5.</b>	<b>9</b> .0	2.7			3.3	.057	8. 0.	ř.	14.7	÷.5	12.5	g.
1698	11.2	4.6	<b>.</b> 5	3.5	12.0	3.6	1.3	4.6			<b>+</b> : <b>+</b>	.677	4.8	. 083	18.7	5.7	15.7	<b>4</b> .8
1699	٠. م.	7.4	<b>9</b> . E	3.6	7.5	2.3	-	2.5			<b>+</b> .+	. 677	3.5	.061	17.2	5.5	14.3	<b>b</b> .4
1701	11.7	0.0 0.0	<b>9.9</b>	J. J	13.1	<b>6</b> .	<b>6</b> . E	3.6			4.0	. 070	6.4	. 885	17.6	5.4	14.8	<b>4</b> .5
1763	10.6	3.2	<b>1</b> .0	J. J.	<b>a</b> .	9. 9.	10.4	3.2			3.9	. 968	4.7	.081	19.3	8.8	16.4	9. 9.
1764	7.2	7.5	12.3	0. 0.	7.5	2.3	10.0	3.0			<del>-</del> -	. 972	4.5	.079	16.6	5.1	13.1	<b>4</b> .0
1705	7.6	2. 2.	<b>.</b>	2.7		7.4	4.	5.6			2.5	. 039	3.5	. 056	4.0	n. <del>4</del>	÷.	d.5
1786	<b>o</b> . +			•	<b>.</b>	-	5.7	1.7			2.5	.044	7.0	. 034	17.9	ا دن	15.7	<b>4</b> .
1707	<b>6</b>	2.7	٠. د		<b>6</b>	2.1	6.2	<b>o</b> .			2.3	. 949	7.8	. 046	10.0	0.0 0.0	7.	7.7
1706	<b>0</b> .	2.1	<b>6</b> .	- 7	. S	<b>7.0</b>	6.7	5.0			2.6	. 946	2.3	.040	13.8	4.5	<b>-</b> :	J. 55
7.00	7.0	5. 5.		5.6	<b>o</b>	5.9	4.	5 9 9			5.9	.051	ا ا	. 058	15.1	<b>4</b> :	12.7	8. 9.
171	5.7	1.7	- 0	, i	÷ 1	<del>•</del> •	٠ ن ن	9 ·			2.6	. 936	2.3	940	11.5	υ· 	o ;	7.9
	٠. د د	, i	7.0	D . C	? ;	* ·	? !	o .			? ·	.057	ن د د	750.	16.6		<u>.</u>	? !
00/1	- •	, i	7.6	9 F	0.		:	* 6			7.5	CCB.	2.0	400	D. 00	- 0	+ • - :	
90/-	o r	, ,				- c		9 G			• •	- 6	٠ ن د	. 6	7.01	• •	<u> </u>	, t
1763	7.										) -	45.6	, r	946	, K	) e	=	•
1764		7.0	19.4	3.5	10.7	3.2	1.0				*	.076	4.5	. 673	21.6	<b>9</b>	19.0	
1765	<b>8</b>	2.5	12.6	3.8	7.0	2.1	7.6	2.3			2.6	.045	2.9	.050	18.4	5.6	16.9	4.9
1767	6.7	<b>5</b> .0	6.5	5.0	5.4	9.	6.2	<u>.</u>			3.0	.053	2.5	.044	17.6	4.8	15.0	4.6
1768	6.3	<b>6</b> .	6.3	<b>6</b> .	7.6	2.3	7.7	2.3			3.3	.057	3.2	. 056	14.0	4.4	1.3	4.6
1769	<b>6</b> .1	<b>0</b> .	5.7	1.7	5.3	<b>9</b> .	5.5	1.7			2.1	. 037	7.0	. 035	17.5	5.3	14.7	4.5
1770	<b>4</b> .	9.	<b>4</b> .4	 	4.6	1.7	4.2	۳.					1.2	. 020				
1771	7.7	2.3	8.5	2.5	<b>8</b> .	2.1	<b>8</b> .8	2.1			2.3	.041	7.4	.043	14.5	<b>+</b> .+	<b>=</b>	o.0
1772	7.8	7.4	7.6	2.3	7:	7.5	7.7	2.5			<b>6</b> .	. 033	<b>6</b> .	. 053	13.1	<b>4</b> .	10.3	3.5
1773	7.4	2.3	8.7	2.7	<b>9</b> .	<b>5.8</b>	ø.	2.7			2.7	.047	3.6	. 063	17.7	5.4	7.5	<b>+</b> . <b>+</b>
1774	<b>9</b>	2.1	5.7	1.7	8.2	<del>.</del>	<b>6</b>	<u>.</u>			2.9	. 050	7.4	.041	14.6	4.5	e: =	9. 9
1775	<b>8</b> .3	2.5	4.	5.6	<b>4</b> .	<del>.</del> 0	7.4	2.3			2.6	.045	ъ. В.	. 053	17.3	5.3	14.8	4.5
1776	æ.	5.6		<b>7.8</b>	<b>9</b> .3	2.8	9.5	2.8			2.5	. 039	3.6	.062	13.7	4.2	11.2	3.4
1777	12.4	0. 0.	 -:	2.8	12.8	3.8	10.5	3.2			2.7	.047	3.5	.061	13.9	4.2	10.9	3.3

Main   Main	DON			AIRCRAFT	AFT SIN	WING S	SPEED AT	SINKING SPEED AT TOUCHDOWN	NWO			GL 1DE	GLIDE PATH ANGLE AT TD	VOLE A	5	WHEEL HEIGHT	1E1GHT	ноок нетснт	IGH1
W/S         F/S         F/S         W/S         F/S         W/S         F/S         F/S <th></th> <th>Ž</th> <th>'n</th> <th>8</th> <th>RT</th> <th>S</th> <th>8</th> <th>AV AV</th> <th><b>(3</b></th> <th>FREE-FI</th> <th>IGHT</th> <th>H</th> <th>*</th> <th>8</th> <th>&gt;</th> <th>OVER F</th> <th>da.</th> <th>OVER R</th> <th>d M</th>		Ž	'n	8	RT	S	8	AV AV	<b>(3</b>	FREE-FI	IGHT	H	*	8	>	OVER F	da.	OVER R	d M
24         25         26         27         28         29         39         31         32         35         36         37         38         39<		£/S	K/S	Ş	\$	F/S	N/S	£/\$	s/m	£/\$	s/x	DEG	<b>2</b>	DEG	<b>2</b> 8	E	7	E	3
2.5         8.1         2.5         7.6         2.1         7.5         2.3         2.6         6.05         2.6         6.05         2.1         6.05         1.1         6.05         1.1         6.05         1.1         6.05         1.1         6.05         1.1         6.05         1.1         6.05         1.1         6.05         1.1         6.05         1.1         6.05         1.1         6.05         1.1         6.05         1.1         6.05         1.1         6.05         1.1         6.05         1.1         6.05 </th <th></th> <th>23</th> <th><b>5</b></th> <th>22</th> <th>28</th> <th>27</th> <th>28</th> <th>23</th> <th>30</th> <th>3.</th> <th>32</th> <th>33</th> <th>ķ</th> <th>35</th> <th>36</th> <th>37</th> <th>82</th> <th>39</th> <th>40</th>		23	<b>5</b>	22	28	27	28	23	30	3.	32	33	ķ	35	36	37	82	39	40
2.5         9.6         2.9         9.5         9.5         9.5         9.6         9.5         9.6         9.6         9.7         9.7         9.6         9.6         9.6         9.7         9.6         9.6         9.6         9.7         9.6 <th></th> <th>6.3</th> <th>2.5</th> <th>8.1</th> <th>2.5</th> <th>7.0</th> <th>2.1</th> <th>7.5</th> <th>2.3</th> <th></th> <th></th> <th>2.0</th> <th>. 035</th> <th>2.5</th> <th>.044</th> <th>18.8</th> <th>5.7</th> <th>16.3</th> <th>6.0</th>		6.3	2.5	8.1	2.5	7.0	2.1	7.5	2.3			2.0	. 035	2.5	.044	18.8	5.7	16.3	6.0
3         2.6         9.1         2.8         8.6         2.6         4.4         969         3.2         685         2.1         6.4         18.7           2.2         8.1         2.2         8.9         2.7         6.8         4.1         7.9         6.4         18.7         9.6         21.7         9.6         21.7         9.6         21.7         9.6         21.7         9.6         21.8         9.6         21.8         9.6		9.5	2.9	10.2	3.1	9.2	2.8	9.6	5.9			2.9	.051	3.6	. 963	18.9	5.8	16.6	5.1
2.6         8.9         2.7         9.3         2.6         4.1         -671         3.6         652         18.5         6.2         18.5         2.6         6.2         18.5         2.6         6.2         18.5         2.6         6.2         18.5         2.6         6.2         18.5         2.6         6.2         18.5         1.6         5.8         18.5         18.5         18.5         1.6         5.3         18.5         18.5         2.6         6.2         18.5         18		6.3	2.5	8.5	2.6	6	2.8	8.6	5.6			4.6	. 666	3.2	. 056	21.0	4.9	18.7	5.7
2.5         8.9         2.7         6.8         2.7         6.8         2.7         6.8         2.9         8.9         2.6         6.3         1.9         5.8         16.5         2.6         6.3         1.9         5.7         1.6         5.9         1.8         5.7         1.6         5.9         1.8         5.7         1.7         6.6         3.1         6.5         2.6         6.6 <th></th> <th>9.1</th> <th>2.8</th> <th><b>6</b></th> <th>2.8</th> <th>9.6</th> <th>2.7</th> <th>9.3</th> <th>2.8</th> <th></th> <th></th> <th><b>4</b>.1</th> <th>.071</th> <th>3.0</th> <th>.052</th> <th>20.4</th> <th>6.2</th> <th>18.3</th> <th>5.6</th>		9.1	2.8	<b>6</b>	2.8	9.6	2.7	9.3	2.8			<b>4</b> .1	.071	3.0	.052	20.4	6.2	18.3	5.6
2.6         7.3         2.2         8.5         2.6         3.7         18.5         5.6         16.1           2.6         8.2         2.6         9.7         2.7         2.7         2.7         2.7         3.1         064         3.1         053         18.6         5.5         16.1         3.5         3.6         18.6         5.2         17.5         3.5         3.6         18.6         3.5         18.6         5.2         18.6         5.2         18.6         5.2         18.6         5.2         18.6         5.2         18.6         5.2         18.6         5.3         18.6		8.2	2.5	8.8	2.7	8.8	2.1	7.9	2.4			2.8	. 048	3.0	.053	19.0	5.8	16.5	5.0
2.1         5.9         1.8         6.3         1.9         5.7         1.7         2.9         3.5         2.6         5.5         1.8         5.7         1.7         2.9         3.9         1.9         5.7         1.9         6.9         4.3         6.9         5.7         1.1         1.0         5.7         1.9         6.9         4.3         6.9         1.5         1.5         1.5         1.5         1.5         1.5         1.1         1.1         1.1         1.1         1.1         1.1         1.5         2.9         6.9         4.3         6.6         1.5         1.1         1.1         1.1         1.1         1.1         1.2         8.7         1.6         1.5         1.1         1.1         1.1         1.5         1.6         1.5         1.1         1.1         1.1         1.1         1.1         1.1         1.1         1.1         1.1         1.1         1.1         1.1         1.1         1.1         1.1         1.1         1.1         1.1         1.1         1.0         1.0         1.1         1.1         1.0         1.0         1.1         1.0         1.0         1.0         1.1         1.0         1.0         1.0         1.0 <th></th> <th>8.6</th> <th>2.6</th> <th>7.3</th> <th>2.5</th> <th>4.6</th> <th>5.9</th> <th>8.5</th> <th>5.6</th> <th></th> <th></th> <th>3.7</th> <th>.064</th> <th>J. 1</th> <th>. 053</th> <th>18.5</th> <th>5.6</th> <th>16.1</th> <th>6.4</th>		8.6	2.6	7.3	2.5	4.6	5.9	8.5	5.6			3.7	.064	J. 1	. 053	18.5	5.6	16.1	6.4
2.6         9.2         2.6         9.5         2.6         9.5         18.6         5.7         16.3           3.6         1.2         3.1         1.6         3.5         1.6         3.6         13.5         14.7         16.3         3.7         16.4         3.7         16.1         11.1		7.0	2.1	9. 9.	<b>•</b>	Ø. 3	<del>.</del>	5.7	1.7			2.0	. 035	2.0	. 035	4.	5.6	5.5	1.7
2.5         19.8         3.3         13.7         4.2         11.7         4.2         11.7         4.2         11.7         4.2         11.7         4.2         11.7         4.2         11.7         4.2         11.7         4.2         11.7         4.2         11.7         4.2         11.7         4.7         11.7         4.7         11.7         4.7         11.7         4.7         11.7         4.7         11.7         4.7         4.7         4.8         11.8         11.7         4.7         11.	•	 	5.6	8.5	2.8	<b>6</b>	5.0	7.7	2.3			 	.054	9.9	.053	18.8 6.8	5.7	16.3	8.0 .0
2.2         3.5 <th>-</th> <th><u>ه</u>.</th> <th>n 0</th> <th><b>.</b> 8</th> <th>N. 9</th> <th>12.4</th> <th>80 m</th> <th>5.5</th> <th>S. 5</th> <th></th> <th></th> <th>ر و . و</th> <th>. 969</th> <th>4. u</th> <th>.075</th> <th>13.7</th> <th>4.5</th> <th></th> <th>4.6</th>	-	<u>ه</u> .	n 0	<b>.</b> 8	N. 9	12.4	80 m	5.5	S. 5			ر و . و	. 969	4. u	.075	13.7	4.5		4.6
2.7         1.7         5.7         2.9         2.9         2.9         2.9         10.7         2.1         14.7           2.8         1.9         2.9         2.9         2.9         2.9         2.9         1.9         1.7         1.7         1.7         1.7         1.7         1.8         1.9         1.9         1.9         1.9         1.9         1.9         1.9         1.9         1.7         1.7         1.7         1.7         1.7         1.8         1.9         1.9         1.7 <th>_ `</th> <th>٠. در د</th> <th>n 0</th> <th>o i</th> <th>1.2</th> <th>ص د. د</th> <th></th> <th>80 c</th> <th>% 6</th> <th></th> <th></th> <th>2.8</th> <th>.051</th> <th>3.2</th> <th>.056</th> <th>12.5</th> <th>יי פיי</th> <th>6.</th> <th>5.8</th>	_ `	٠. در د	n 0	o i	1.2	ص د. د		80 c	% 6			2.8	.051	3.2	.056	12.5	יי פיי	6.	5.8
2.6         10.5         3.2         10.8         3.3         10.1         3.7         10.6         3.9         10.6         3.1         10.7         10.6         3.9         10.8         3.1         10.1         3.7         10.6         3.9         10.8         3.5         10.8         3.2         10		D P	, ,			9 r		, u	, c				200.	0 6	946		? <b>-</b>	. 4	0 F
2.4         7.2         2.6         5.9         1.8         2.8         .049         1.9         .033         19.5         5.9         17.4           2.4         7.2         2.2         8.6         2.6         8.6         2.6         1.9         .033         1.9         2.9         1.7         1.9         1.7         1.9         1.7         1.9         1.9         1.7         1.9         1.7         1.9         1.7         1.0         1.7         1.0<	-		2.8	10.3	2 2	. 6		10.1				3.7	964	9.5	.068	16.6	5.1	13.5	4
2.4         7.2         2.2         8.6         2.7         8.9         2.4         3.6         .663         2.6         9.1         2.6         9.6         1.6         9.2         1.6         9.2         1.6         9.2         1.6         9.5         1.6         1.6         9.6         1.6         9.6         1.6         9.6         1.6 <th>-</th> <th>6.7</th> <th>2.1</th> <td>5.4</td> <td>-</td> <td>9.9</td> <td>5.9</td> <td>8.0</td> <td>8.</td> <td></td> <td></td> <td>2.8</td> <td>.049</td> <td>1.9</td> <td>.033</td> <td>19.5</td> <td>5.9</td> <td>17.4</td> <td>5.3</td>	-	6.7	2.1	5.4	-	9.9	5.9	8.0	8.			2.8	.049	1.9	.033	19.5	5.9	17.4	5.3
2.6         10.4         5.2         6.9.5         2.6         9.1         2.9         9.2         1.0         9.5         1.6         5.7         16.0         5.7         16.0         16.0         5.7         16.0         17.0         17.0         17.0         2.2         9.0         1.0         2.1         1.0         <	_	8.9	4.7	7.2	2.2	8.8	2.7	8.0	2.4			3.6	.063	2.8	.049	21.3	6.5	19.2	5.9
1.3         4.4         1.4         2.3         7         3.5         1.0         2.2         .636         1.1         .619         10.6         3.2         7.9           2.0         6.6         2.1         6.6         1.1         .615         2.6         .645         18.5         5.6         15.7           2.0         2.2         7.2         2.2         2.2         2.2         3.5         .66         1.7         .647         12.3         5.6         16.7         .647         12.3         5.7         9.2         15.7         9.4         12.3         5.6         14.7         12.3         16.8         15.7         9.4         15.7         9.4         12.3         9.6         17.1         2.2         14.3         9.2         16.8	_	8.5	2.6	10.4	3.2	8.5	2.6	9.1	2.8			2.7	.048	3.6	. 063	18.6	5.7	16.0	6.4
2.0         6.9         2.1         7.2         2.2         7.9         2.1         2.9         .051         2.6         .046         18.3         5.6         15.7         4.9         13.6         2.7         10.5         3.2         3.2         2.9         .051         2.6         .046         18.3         5.6         15.6         4.9         13.6	•	4.4	7.3	<b>*</b> :	<b>+</b> .	2.3	.,	3.3	1.0			2.2	. 038	-:	.019	10.6	3.2	7.9	2.4
2.7         10.5         3.2         6.5         2.6         9.5         2.9         2.6         .045         3.2         .056         16.0         4.9         13.6           2.5         7.7         2.3         7.2         2.2         3.5         .061         2.7         .045         3.2         .056         16.0         4.9         13.6           3.0         9.3         2.6         1.16         2.7         10.4         2.7         1.3         1.16         6.6         6.3         10.7         1.2         1.16         6.2         10.9         17.1         2.1         1.0         1.16         6.2         10.9         17.1         2.2         1.16         6.6         6.2         10.9         17.1         2.2         1.16         8.2         10.5         10.7         <	•	9.9	2.0	<b>9</b> .0	2.1	7.2	2.2	7.9	2.1			2.9	.051	5.6	.046	18.3	5.6	15.7	4.8
2.5         7.7         2.3         7.3         2.2         7.2         2.2         3.5         .061         2.7         .047         12.3         3.7         9.2           4.5         19.2         2.8         15.4         4.7         17.3         5.3         6.6         .116         6.2         7.0         5.2         14.3         9.2         14.3         9.2         14.3         9.2         14.3         9.2         14.3         9.2         14.3         9.2         14.3         9.2         14.3         9.2         14.3         9.2         14.3         9.2         14.3         9.2         14.3         9.2         14.3         9.2         14.3         9.2         14.3         9.2         14.3         9.2         14.3         16.8         19.7         14.3         16.8         19.7         14.3         18.4         19.5         14.3         18.4         19.5         14.3         18.4         19.5         14.7         19.7         19.7         19.7         19.7         19.7         19.7         19.7         19.7         19.7         19.7         19.7         19.7         19.7         19.7         19.7         19.7         19.7         19.7         19.7		80 80	2.7	10.5	3.2	<b>.</b>	5.6	9. S	2.9			5.6	.045	3.5	.056	6.9	<b>9</b> .	13.6	4.2
4.3 18.2         5.6 15.4         4.7 17.3         5.3         6.6 116 6.2 109 17.1         5.2 18.9         17.1         5.2 18.9         17.1         5.2 18.9         17.1         5.2 18.9         17.1         5.2 18.9         17.1         5.2 18.9         5.6 18.9         5.6 18.9         5.6 18.9         5.6 18.9         5.6 18.9         5.6 18.9         5.6 18.9         5.6 18.9         5.6 18.9         5.6 18.9         5.6 18.9         5.6 18.9         5.6 18.9         5.6 18.9         5.6 18.9         5.6 18.9         5.7 18.4         5.7 18.9         5.2 18.7         5.6 18.3         5.6 18.7         5.7 18.7         5.7 18.8		n .		7.7	2.3	7.3	5.5	7.5	7.5			3.5	.061		.047	12.3	7.0	2.5	2.8
2.6         9.3         2.7         9.6         2.7         9.6         2.7         9.6         2.7         9.6         2.7         9.6         2.7         9.6         2.7         9.6         2.7         9.6         2.7         9.6         2.7         9.6         2.7         9.6         2.7         9.6         2.7         9.6         2.2         9.6         3.2         9.6         2.2         9.6         2.2         9.6         2.2         9.6         2.2         9.6         2.2         9.6         2.2         9.6         2.2         9.6         2.2         9.6         2.2         9.6         2.2         9.6         2.2         9.6         2.2         3.7         9.6         2.2         9.6         1.6         2.2         1.4         7         1.6         1.7         1.6         1.7         2.2         2.2         2.2         2.2         2.2         2.2         2.2         2.2         2.2         2.2         2.2         2.2         3.1         9.6         2.6         9.6         1.6         1.5         1.2         1.2         1.2         1.2         1.2         1.2         1.2         2.2         2.2         2.2         2.2         2.2	_	- ·	4.	19.2	0	15.4	4.7	17.3				9.0	.116		.169	7.7	2.0	24.3	* ·
2.9         1.0         2.7         2.9         2.9         2.7         2.9         2.7         2.9         2.9         2.7         2.9         2.9         2.7         2.9         2.7         2.9         2.9         2.7         2.9         2.7         2.9         2.9         2.7         3.5         3.7         3.9         3.7         3.9         3.7         3.9         3.7         3.9         3.7         3.9         3.7         3.9         3.7         3.9         3.7         3.9         3.7         3.9         3.7         3.9         3.7         3.9         3.7         3.9         3.7         3.9         3.7         3.9         3.7         3.9         3.7         3.9         3.7         3.7         3.9         3.7         3.7         3.9         3.9         3.7         3.7         3.9         3.9         4.6         3.9         4.7         13.0         3.9         4.7         13.0         3.9         3.9         4.7         13.0         3.9         3.9         4.7         13.0         3.9         3.9         4.7         13.0         3.9         4.7         13.0         3.9         14.1         3.9         3.9         14.1         3.9 <td< th=""><th></th><th>9.4</th><th>ۍ د د</th><th>? •</th><th>7.8 7.8</th><th>ю «</th><th>2.7</th><th></th><th>7.7</th><th></th><th></th><th>ر د بر</th><th>409.4</th><th></th><th>. 00.0 0.00</th><th>9.07</th><th></th><th>4 . a</th><th></th></td<>		9.4	ۍ د د	? •	7.8 7.8	ю «	2.7		7.7			ر د بر	409.4		. 00.0 0.00	9.07		4 . a	
2.4       1.8       6.7       2.7       2.2       2.6       10.6       2.5       10.4       17.0       5.2       14.7         2.8       7.7       2.4       6.7       2.0       7.6       2.3       3.5       10.6       2.5       14.7         2.8       7.7       2.4       6.7       2.0       2.3       3.5       10.6       13.6       13.6         2.9       7.5       2.3       1.6       6.5       2.0       2.7       046       2.6       045       15.5       4.7       13.5         2.0       6.8       2.1       7.7       2.2       2.7       046       2.6       045       17.1       5.2       14.3         2.4       7.6       2.3       7.7       2.4       2.2       2.7       046       2.6       045       17.1       5.2       14.3         2.4       7.6       2.3       7.7       2.4       2.2       2.7       046       2.6       045       17.1       5.2       14.3         1.6       5.4       1.7       5.5       1.7       2.2       2.7       046       2.6       0.65       17.1       15.0         1.6	_	•				•			, 0				92.6		954	200		2 6	9 6
2.8       7.7       2.4       6.7       2.0       7.6       2.3       3.5       .062       3.2       .055       16.5       5.0       13.5         2.2       7.1       2.1       7.5       2.3       3.1       .054       2.4       .042       15.0       4.6       13.0         2.5       7.5       2.3       1.6       6.5       2.0       2.7       .046       2.6       .045       15.0       4.7       13.2         2.0       6.8       2.1       5.3       1.6       6.5       2.0       2.7       2.6       .045       17.1       13.2         2.4       7.6       2.3       7.7       2.4       2.4       .046       2.6       .045       17.1       13.2         2.4       7.6       2.3       7.1       2.2       7.7       2.4       15.1       17.1       2.2       14.3		7.8	4.			7.1	2.2	7.7	2.5			2.6	.045	2.5	944	17.0	2.5	14.7	4 .0
2.2         7.1         2.1         7.6         2.1         7.5         2.3         3.1         .054         2.4         .042         15.0         4.6         13.0           2.5         7.5         2.2         2.7         .046         2.6         .045         15.5         4.7         13.2           2.0         6.8         2.1         5.3         1.6         6.5         2.0         3.1         .053         2.0         .035         14.8         4.5         12.5           2.4         7.6         2.3         7.3         2.2         7.7         2.4         2.8         .053         17.8         4.7         13.2           2.4         7.6         2.3         7.1         2.2         7.7         2.4         15.1         12.5         14.3         15.1         12.5         14.3         14.3         14.3         14.3         14.3         14.3         14.3         14.1         14.3         14.1         14.3         14.1         14.3         14.3         14.3         14.3         14.3         14.3         14.3         14.3         14.3         14.3         14.3         14.3         14.3         14.3         14.3         12.6         12.6	-	9.2	2.8	7.7	2.4	6.7	2.0	7.6	2.3				.062	3.2	.055	16.5	5.0	13.5	4.1
2.5     7.5     2.3     5.9     1.8     7.2     2.2     2.7     .046     2.6     .045     15.5     4.7     13.2       2.9     6.8     2.1     5.3     1.6     6.5     2.9     3.1     .053     2.9     .035     14.8     4.5     12.5       2.4     7.6     2.3     7.3     2.2     7.7     2.4     7.8     2.9     .035     17.8     5.4     15.1       2.2     6.9     2.1     7.7     2.2     7.7     2.4     1.9     2.7     .046     2.6     .045     17.1     5.2     14.3       1.6     5.4     1.7     5.5     1.7     2.5     2.7     .046     2.6     .045     17.1     5.2     14.3       2.5     9.8     2.1     8.3     2.3     1.8     6.1     1.9     2.7     .048     2.7     .047     16.9     5.2     14.3       2.1     7.7     2.9     2.4     4.3     1.3     6.4     2.9     1.8     6.1     1.9     2.7     .048     2.7     .048     1.7     2.9     14.3       2.1     7.7     2.3     6.7     2.9     0.44     3.9     .041     16.2     4.9		7.3	2.2	7.1	2.1	7.0	2.1	7.5	2.3				.054		.042	15.0	4.6	13.0	4.0
2.6     6.8     2.1     5.3     1.6     6.5     2.0     3.1     .053     2.9     .035     14.8     4.5     12.5       2.4     7.6     2.3     7.3     2.2     7.7     2.4     7.7     2.4     7.7     2.4     7.7     2.4     15.1       2.2     6.9     2.1     7.7     2.3     7.1     2.2     2.7     .046     2.6     .045     17.1     5.2     14.3       1.6     5.4     1.7     5.5     1.7     3.2     .055     1.9     .034     19.5     5.9     16.9       2.5     9.6     1.8     5.9     1.8     6.1     1.9     2.7     .048     2.7     .044     10.5     5.2     14.3       2.1     7.7     2.3     6.7     2.9     2.5     .044     3.9     .041     16.2     4.9     13.2       2.1     7.7     2.3     6.7     2.9     1.8     6.1     1.9     2.2     .043     2.3     .041     16.2     4.9     13.2       2.1     7.7     2.3     6.7     2.9     7.5     2.3     0.44     3.9     .045     21.8     6.6     19.9       2.4     7.4     2.2	-	8.2	2.5	7.5	2.3	5.9	<b>8</b> .	7.2	2.5			2.7	. 046		.045	15.5	4.7	13.2	<b>4</b> .0
7.3 2.2 7.7 2.4 2.8 .859 3.9 .853 17.8 5.4 15.1 7.7 2.3 7.1 2.2 2.7 .946 2.6 .945 17.1 5.2 14.3 5.7 1.7 2.3 7.1 2.2 2.7 .946 2.6 .945 17.1 5.2 14.3 5.7 1.7 5.5 1.7 3.2 .955 1.9 .034 19.5 5.9 16.9 5.8 1.8 5.9 1.8 6.1 1.9 2.7 .948 2.7 .947 16.9 5.2 14.1 5.2 14.7 5.4 1.8 6.4 1.9 2.7 .948 2.7 .947 16.9 5.2 14.7 5.4 1.8 6.4 2.9 2.7 .948 2.7 .947 16.9 5.2 14.7 6.7 2.0 7.5 2.3 2.5 .944 3.9 .952 18.6 5.7 15.6 5.7 15.6 5.9 1.8 6.4 2.0 2.5 .944 3.9 .952 18.6 5.7 15.6 5.7 15.6 5.7 17.2 2.3 7.7 2.3 7.7 2.3 2.7 .948 3.9 .953 13.8 4.2 19.8		6.5	7.0	<b>8</b> .8	2.1	5.3	<b>•</b> .	8.5 5.5	2.0			3.1	.053		.035	14.B	<b>4</b> .0	12.5	3.8
7.7     2.3     7.1     2.2     2.7     .046     2.6     .045     17.1     5.2     14.3       5.7     1.7     5.5     1.7     3.2     .055     1.9     .034     19.5     5.9     16.9       5.8     1.8     5.9     1.8     6.1     1.9     2.7     .048     2.7     .047     16.9     5.2     14.1       5.4     1.6     6.4     2.9     2.7     .048     2.7     .047     16.9     5.2     14.7       4.3     1.3     6.4     2.9     2.2     .043     2.3     6.9     6.2     4.9     13.2       6.7     2.9     7.5     2.3     2.5     .044     3.9     .052     18.6     5.7     15.6       5.2     1.6     5.9     1.8     2.4     .042     2.1     .037     14.6     4.5     12.9       5.7     2.3     2.7     .048     3.9     .053     13.8     4.2     10.8       7.7     2.3     7.7     2.3     2.7     .048     3.9     .053     13.8     4.2     10.8		7.9	7.4	7.6	2.3	7.3	2.2	7.7	7.4			2.8	. 050	3.0	.053	17.8	4.4	15.1	4.6
5.7     1.7     5.5     1.7     5.5     1.7       6.8     2.1     8.3     2.5     1.8     6.1     1.9     2.7     .048     2.7     .047     16.5     5.9     14.1       5.4     1.6     6.4     2.6     1.9     2.7     .048     2.7     .047     16.9     5.2     14.3       6.7     2.6     1.9     2.7     .078     2.6     17.2     5.2     14.7       6.7     2.6     2.9     2.9     2.9     2.9     13.2     4.9     13.2       6.7     2.6     2.3     2.5     .044     3.9     .052     18.6     5.7     15.6       5.8     1.8     6.4     2.0     3.0     .052     2.8     .049     21.8     6.6     19.0       5.2     1.6     5.9     1.8     2.4     .042     2.1     .037     14.6     4.5     12.0       7.7     2.3     2.7     .048     3.0     .053     13.8     4.2     10.8		7.1	2.5	<b>0</b> .	2.1	7.7	2.3	7.1	2.5			2.7	. 046	5.6	.045	17.1	5.2	14.3	<b>+</b> . <b>+</b>
6.8     2.1     8.3     2.5     2.2     .039     3.1     .054     16.5     5.9     14.1       5.8     1.8     5.9     1.8     6.1     1.9     2.7     .048     2.7     .047     16.9     5.2     14.3       5.4     1.6     6.4     1.9     2.7     .078     2.6     .046     17.2     5.2     14.7       4.7     2.9     7.5     2.9     2.5     .044     3.9     .052     18.6     5.7     15.6       5.8     1.8     6.4     2.9     3.9     .052     2.8     .049     21.8     6.6     19.0       5.2     1.8     2.4     .042     2.1     .037     14.6     4.5     12.9       7.7     2.3     2.7     .048     3.9     .053     13.8     4.2     10.8		5.2	9.	₽. •	1.7	5.7	1.7	5.5	1.7			3.2	. 055	o. —	.034	19.5	9	16.9	5.1
5.8     1.8     5.9     1.8     6.1     1.9     2.7     .048     2.7     .047     16.9     5.2     14.3       5.4     1.6     6.4     1.9     2.2     .038     2.6     .046     17.2     5.2     14.7       4.3     1.3     6.4     2.0     2.5     .043     2.3     .041     16.2     4.9     13.2       6.7     2.0     7.5     2.3     2.5     .044     3.0     .052     18.6     5.7     15.6       5.8     1.8     6.4     2.0     3.0     .052     2.8     .049     21.8     6.6     19.0       5.2     1.6     5.9     1.8     2.4     .042     2.1     .037     14.6     4.5     12.0       7.7     2.3     7.7     2.3     2.7     .048     3.0     .053     13.8     4.2     10.8		9.3	2.5	æ. œ	S. 9	6.8	2.1	8.3	2.8			2.2	. 039	3.1	.054	16.5	9.	14.1	4.4
5.4     1.6     6.4     1.9     2.2     .038     2.6     .045     17.2     5.2     14.7       4.3     1.3     6.4     2.6     .043     2.3     .041     16.2     4.9     13.2       6.7     2.9     7.5     2.3     2.5     .044     3.6     .052     18.6     5.7     15.6       5.8     1.8     6.4     2.9     .052     2.8     .049     21.8     6.6     19.0       5.2     1.6     5.9     1.8     2.4     .042     2.1     .037     14.6     4.5     12.0       7.7     2.3     7.7     2.3     2.7     .048     3.9     .053     13.8     4.2     10.8		5.7	7.7	<b>-</b> .	<b>.</b>	ب د د	<b>.</b>	9.	<b>–</b> ∞.	<b>6</b> .1	6.	2.7	8+6	2.7	.047	0. i	2.5	14.3	4.
4.3     1.3     6.4     2.6     2.5     .043     2.3     .041     16.2     4.9     13.2       6.7     2.6     7.5     2.3     2.5     .044     3.0     .052     18.6     5.7     15.6       5.8     1.8     6.4     2.9     .052     2.8     .049     21.8     6.6     19.0       5.2     1.6     5.9     1.8     2.4     .042     2.1     .037     14.6     4.5     12.0       7.7     2.3     7.7     2.3     2.7     .048     3.9     .053     13.8     4.2     10.8		10 t	2.1	9	2.1	4.	9.	÷ .	6. 6.			2.2	979	7.6	946	17.2	5.2	14.7	. ·
2.5 .044 3.0 .052 18.6 5.7 15.6 3.0 .052 2.8 .049 21.8 6.6 19.0 2.4 .042 2.1 .037 14.6 4.5 12.0 2.7 .048 3.0 .053 13.8 4.2 10.8		7.3	7.7	7.9	7.4	<b>+</b> .3	٠. ت	4.	7. 9.			2.5	.043	2.3	.041	16.2	Ø. 1	13.2	<b>9</b> .
3.0 .052 2.8 .049 21.8 6.6 19.0 2.4 .042 2.1 .037 14.6 4.5 12.0 2.7 .048 3.0 .053 13.8 4.2 10.8		6.9	2.	7.7	2.3	6.7	2.0	7.5	2.3			2.5	.044	9.0	.052	8. 8.	5.7	15.6	8.
2.4 .042 2.1 .037 14.6 4.5 12.0 2.7 .048 3.0 .053 13.8 4.2 10.8		7.7	7.4	7.4	2.5	S.	<b>8</b> .	4.	<b>7</b> .			3.0	.052	5.8	.049	21.8	<b>9</b> .9	9.0	S.8
2.7 .648 3.6 .653 13.8 4.2 16.8		5.8	<b>a</b> .	<b>.</b>	<b>6</b> .	5.5	9.	8.9	<del>.</del>			2.4	.042	2.1	. 037	14.6	<b>4</b> .8	12.0	3.7
		6.1	2.5	7.7	2.4	7.7	2.3	7.7	2.3			2.7	.048	9.0	. 053	13.8	4.2	10.8	3.3

USS ENTERPRISE (CVN-65)

997			AIRCRAFT		KING :	SINKING SPEED AT TOUCHDOWN	T TOUCH	NMOQ			CL IDE	GLIDE PATH ANGLE AT TD	WGLE ,	07 17	WHEEL	WHEEL HEIGHT	ноок нетсит	EIGHT
2	8	MOSE	8	PORT	S	STBO	AVG	g	FREE-FLIGHT	LIGHT	<b>5</b> 5	BH#	6	AA A	OVER RAMP	RAMP	OVER RAMP	RAMP
	Ş	Ş	5	¥\$	£/S	N/S	5,5	N/S	F/S	M/S	DEG	RAD	DEG	Š	Ħ	3	E	3
22	23	7	52	26	27	<b>58</b>	29	8	ñ	32	33	*	35	36	37	38	39	9
1895	4.0	2.9	<b>.</b>	2.7	<b>8</b>	2.6	8.8	2.7			3.1	. 055	3.5	.061	18.0	5.5	15.2	<b>4</b> .0
1899	7.1	2.5	<b>9</b> .4	2.6	7.4	2.3	7.9	7.4			2.9	.050	J. 1	. 054	17.8	5.4	15.4	· •
1986	10.3	J. 1	<b>6</b>	5.8	9.5	2.9	9.5	5.8			3.3	.058	<del>-</del> :	. 071	22.9	7.0	20.5	6.3
1961	7.6	2.3	S.	<b>1.8</b>	7.1	2.2	4.9	7.0			5.8	<b>0</b> 00.	2.7	.047	16.A	5.1	14.2	4.4
1902	7.2	2.5	<b>9</b> .	7.8	6.7	7.0	6.1	4.9			3.3	.057	2.7	947	. 91	5.1	14.0	4.3
1963	7.2	2.2	8.8	2.7	4.8	7.5	6.7	7.0			5.6	.046	2.5	‡	14.0	4.3	<del>+</del> .=	3.5
1964	<b>.</b>	2.5	4.9	<b>5.0</b>	ø.	2.1	9.9	7.0			5.6	. 045	7.4	. 042	17.2	5.5	14.9	<b>4</b> .5
1905	5.3	<b>9</b> .	6.3	<b>6</b> .	5.7	`:	<b>.</b>	<b>—</b>	8. 6.	<del>-</del>	2.9	. 050	2.5	.044	17.5	5.3	15.0	<b>4</b> .6
1986	7.1	2.5	7.2	7.5	<b>6</b> . 7	7.4	7.5	2.3			<b>9</b> .	. 928	2.7	.047	10.2	3.1	<b>.</b>	7.4
1967	6.2	<b>a</b> :	5.7	1.7	<b>6</b> .3	<u>.</u>	<b>6</b> .	<b>.</b>			2.5	.043	2.3	.041	15.9	<b>4</b> .8	13.4	<b>+</b> .
606.	5.3	<b>9</b> .	7.4	2.3	<b>.</b>	<b>.</b>	9.9	<b>7</b> .0			3.0	.052	2.5	.044	17.0	5.5	15.0	<b>9</b> .
1910	7.4	2.3	7.4	2.3	5. 0.	 S:	<b>9</b> .6	2.0			3.5	.05€	2.0	. 035	16.4	5.0	14.3	<b>+</b> . <b>+</b>
1911	8.3	2.5	7.4	2.3	3.5	2.6	8.9	2.4					3.0	. 052				
1912	5.7	1.7	7.3	2.2	4.9	5.5	6.3	6.			2.9	.051	2.3	.041	18.7	5.7	16.5	5.0
1913	7.4	2.3	<b>8</b> .	9. 9.	7.2	2.5	æ 6.	2.7			3.3	. 058	ы. В.	990.	17.7	5.4	15.6	4.7
1915	7.8	7.4	12.3	2.7	7.0	2.7	9.6	2.9			4.6	.059	ى ھ.	.067	21.1	4.9	18.6	5.7
1917	6.9	2.1	7.9	7.4	10.8	3.3	7.4	2.3			3.0	. 052	2.7	.048	16.8	5.1	14.7	4,
1918	<b>8</b> .6	2.7	8.2	2.5	9.5	5.8	<b>0</b> .6	2.7			2.8	.049	3.8	990.	18.3	5.6	16.0	<b>₹</b>
1918	S	7.8	13.0	<b>+</b> .	=	4.6	12.1	7.7			3.5	. 056	4.6	. 686	5. 8.	<b>4</b> .∞	13.8	4.5
1920	<b>9</b>	2.5	•	2.7	<b>o</b> .	2.1	<b>6</b> .	7.4			2.5	. 638	9 :	.045	15.2	<b>4</b> .6		<b>4</b> (
1921	•	<b>.</b>	4.	~ ·	<b>9</b>	<b>5.0</b>	5.7	1.7			ا ا	. 055	2.3	.041	20.8		<b>5</b>	
1922	7.4	2.3	<b>9</b>	2.0	<b>7</b> .8	7.7	4.	2.0			2.7	948	2.1	. 936	9.6	<b>.</b>	17.6	4.0
1923		2.0	<b>.</b>	2.9		7.4	- ·	2.6			2.5	828	ر د د	.057	16.6	5.7	16.7	
1924	4. 1	, d		<b>D</b> (	6 F	9 6		9 7			9.6			. e.	20.6	 	9.8	
C781	, r	, .		, , ,		, ,	· •	, c				. 67.0 67.0	, ,	0 4 6		† + o u	. 4	
1927		-			4	2.0	7.				. 6	446	6	1951	18.2	- KG	18.2	
1928	7.7	2.3	7.9	2.4	4.9	-	6.9	7.7			2.2	. 938	2.8	948	16.6	5.1	7.	4.4
1934	<b>9</b> .0	<b>8</b> .	8.7	2.7	7.3	2.2	7.8	2.4	8.1	2.5	3.1	.054	2.8	.048	19.9	6.1	17.7	5.4
1935	9.0	2.8	8.8	2.7	10.1	3.1	8.9	2.7			2.6	. 046	3.6	. 063	29.5	6.2	17.8	5.4
1936	6.3	2.5	<b>6</b> .0	J. 0	4.6	5.6	æ.	2.7			2.8	.049	٦. م	.054	17.8	5.4	15.5	4.7
1937	<b>.</b>	2.7	10.3	3.2	7.7	2.3	8.9	2.7			2.8	.050	ъ. В	. 966	19.3	5.9	16.5	9.
1938	7.0	2.1	<b>9</b> .	<b>.</b>	7.6	2.3	<b>6</b> .3	6.			2.8	.049	5.6	. 045	17.2	5.2	14.2	4.3
1940	8.7	2.7	9.1	2.5	œ.	2.1	8.5	2.5			2.8	. 050	4.6	. 058	18.1	5.5	15.2	4.6
1942	<b>†</b> .	2.8	8.5	<b>5.</b>	<u>.</u>	<b>5.8</b>	₩.	2.6			4.	. 059	3.6	. 964	18.3	5.6 6.	15.6	4.7
1943	4.5	<b>9</b> .	4.	<b>5.0</b>	7.1	2.2	7.0	2.1			3.6	.064	2.8	.048	17.9	5.5	15.4	4.7
1945	8.8	2.7	10.3	 	5.7	1.7	<b>8</b> 9.	2 4			3.6	. 962	3.3	. 058	19.1	8. 8.	16.2	S.0
1946	4.6	2.9	<b>.</b>	2.5	8.6	3.0	<b>8</b> .9	2.7			3.8	990.	3.9	. 968	19.4	5.9	16.6	5.1
1947	5.8	<b>.</b>	7.5	2.3	5.7	1.7	6.8	2.1			3.3	. 957	2.7	.047	22.0	6.7	19.5	8.8
1948	7.5	2.3	<b>↑</b> .	5.9	7.1	2.2	<b>®</b>	7.4			3.3	. 058	٦. ت	.054	21.0	4.9	18.9	5.B

				<b>II</b>	<b></b>		~		•	•	<b>ب</b>	_	_	_	_	_		6		~	6	en.	6	•	•	•	•	•	~	•	•	•	_	~	•	_	•	~	_	·	<b>~</b>	_	<b>.</b>
<b>E</b> IGHT	OVER RAMP	3	4	5.6	₩.	5.7	5.2	5.7	<del>*</del>	5.6	5.5	5.	5.5	<u>.</u>	'n	'n	÷.	4.6	S. N	4.2	5.	3.5	ů	3.6	3.5	g. 3.	4.9	4.9	3.0	3.6	ы 9.	<b>4</b> .	₹	4.2	3.9	2.7	'n	3.	4.4	4.		'n	'n
HOOK HEIGHT	OVER	E	39	18.4	15.6	18.8	16.9	18.5	14.5	16.3	18.0	16.7	17.4	13.5	12.1	12.3	15.0	13.3	12.8	13.7	16.3	12.4	16.4	16.6	12.9	12.7	16.9	15.9	10.9	11.9	12.9	13.3	13.4	13.7	12.8	8.8	10.7	17.2	14.4	14.8	11.8	11.2	11.5
WHEEL HEIGHT	OVER RAMP	3	82	6.3	5.6	6.5	6.9	4.9	5.2	5.6	6.3	9. 9.	6.2	5.4	4.7	4.5	5.4	4.8	4.7	4.9	5.9	4.5	5.9	5.8	4.6	4.8	9.0 9	5.5	4.5	<b>+. +</b>	4.6	<b>4</b> .8	<b>4</b> .8	5.0	4.7	3.5	3.9	6.2		5.2	<b>+</b> . <b>+</b>	4.1	4.2
WHEEL	OVER	E	33	20.7	18.5	21.2	19.6	21.0	17.2	18.3	20.6	19.3	20.5	16.6	15.4	14.7	17.7	15.8	15.4	16.1	19.2	14.9	19.3	18.9	15.2	15.9	18.5	18.2	13.9	14.5	15.2	15.6	15.7	16.3	15.4	11.4	12.8	20.5	17.3	17.1	<b>+.+</b>	13.5	13.8
AT TD	<b>A</b>	3	36	. 054	. 070	. 649	. 051	. 069	. 060	. 024	. 062	. 964	. 694	. 071	. 078	.044	. 032	. 030	.048	. 053	. 085	. 050	. 058	.046	.045	.051	.069	.064	. 052	. 656	. 029	. 032	.057	.068	.043	. 059	.051	.074	.077	. 055	. 053	.042	.026
GLIDE PATH ANGLE AT TD	Φ,	DEG	33	3.1	4.0	2.8	2.9	G. 9	3.5	<b>†</b> .	3.6	3.6	4.5	<del>-</del>	4.5	2.5	6.1	1.7	2.7	3.0	4.9	2.9	3.3	5.6	2.6	2.9	4.0	3.7	3.0	2.8	<del>-</del>	<b>8</b> .	3.3	G. 5	2.4	4.6	2.9	4.3	<b>+</b> : <b>+</b>	3.2	3.0	7.4	7.5
PATH	B-F#	3	ņ	. 065	. 059	. 055	. 054	. 061	.057	. 043	. 065	. 082	690.	. 074	. 964	.047	. 050	. 055	.056	.044	.672	.051	.056	.063	.058	.049	. 658	. 055	.055	.044	. 947	. 040	.069	.056	.045	. 056	.056	.672	. 075	.051	. 647	. 036	.037
GLIDE	æ	930	33	3.7	4.6	3.1	3.1	3.5	3.3	2.5	3.7	4.7	3.9	4.3	3.7	2.7	2.9	3.2	3.2	2.5	4.1	2.9	3.2	3.6	3.3	2.8	3.3	3.2	3.1	2.5	2.7	2.3	4.0	3.2	2.6	3.2	3.2	<del>-</del>	4.3	2.9	2.7	2.0	2.1
	.IGHT	X/S	32				2.5												9.															3.0				+:1			<del>6</del> .		
	FREE-FLIGHT	Ş	5				7.1												6.9															8. 8.				13.4			4.9		
N	G	¥\S	30	2.7	3.0	2.3	2.1	2.8	2.6	<b>+</b> :-	2.9	2.9	+:-	4.6	3.1	7.0	1.7	₹:	1.8	2.4	3.2	2.1	2.3	7.4	2.3	2.3	3.0	3.0	2.5	2.1	<del>+</del> .	1.7	2.4	3.0	2.0	2.9	2.5	3.9	3.2	2.7	2.1	2.0	<del>.</del> .
NKING SPEED AT TOUCHDOWN	AVG	<b>F</b> /S	53	8.8	10.0	7.5	7.0	<b>9</b> .3	4.6	<b>+</b> .	<b>9</b>	4.6	13.4	1.3	10.2	<b>9</b> .9	5.5	4.5	6.9	7.9	10.6	7.0	7.6	7.8	7.7	7.6	10.0	9.7	7.4	7.0	4.7	5.4	7.9	9.8	<b>9</b> .	4.0	9.1	12.8	10.4	8.8	6.9	6.7	4.2
PEED A	8	Ş	87	2.7	J. 7	9 7	 	7.4	2.5	ø.	7. 8.	7.6	4.4	ъ. В.	2.8	1.7	1.7	1.7	6.	<u>۔</u>	4.4	<u>.</u>	2.0	2.8	5.6	2.4	5.6	5.8	<b>.</b>	<b>+</b> :	<u>.</u>	2.5	7.4	2.8	2.1	7.4	2.1	4.6	2.8	<del>•</del>	2.1	1.7	1.2
KING SI	STBO	\$	27	8.7	16.3	9.S	<b>6.</b>	7.9	8.2	2.8	<b>6</b> .6	4.0	14.2	12.4	-	5.4	5.6	5.6	6.2	6.3	14.5	<b>6</b> .3	6.7	4.6	4.0	7.9	8.7	4.0	<b>9</b> .7	4.5	4.3	7.3	7.8	• •	<b>0</b> .	7.7	7.0	15.0	ص د.	3.4	7.0	5.6	3.8
SI	b:	Ş	<b>5</b> 8	3.1	3.0	2.5	2.8	3.2	2.7	<b>5</b> .	<b>9</b> .	ы	<b>.</b>	2.7	ъ. В.	2.3	1.9	 5	6.	2.0	3.2	2.3	2.2	2.5	2.1	2.5	J. 1	<b>e</b> :	2.6	2.3	1.7	<b>+</b> :	3.3	3.2	2.5	3.7	2.5	3.3	3.5	2.8	5.0	2.4	5.
AIRCRAFT	PORT	<b>E</b> /S	22	10.2	9.7	 	9.2	9.0	<b>8</b> .0	6.5	•. •.	0.0	3.3	9.6	1.7	7.6	6.3	5.1	6.2	9.0	4.0	8.2	8.2	6.1	6.9	7.2	6.2	6.1	4.0	7.4	5.S	4.4	<b>a</b> .	<b>→</b> .	7.2	2.1	8.3	10.7	1.5	1.0	6.7	7.9	5.0
	141	\$	24	2.7	2. <b>8</b>	2.7	2.5	_	2.7	_	2.4	_	3.0	J. 1	2.9	2.3	٦.	J. J.	_	<b>m</b>	•	_				2.0	~	_		2.2	<u>.</u>	2.0	2.4	2.8 1	2.3	3.0	2.5	2.6	3.5	2.3	1.7	2.4	<b>5</b> .
	NOSE	ž.	23	8.7	-	9.0	7.3	8.8	8.7	6.1	7.8	9.0	2.8	9.5	4.6	7.7	4.3	4.4	6.9	7.6		8.8	8.3	8.5	7.8	6.5	6.5	•.•	8.4	7.1	4.9	4.9	7.8	9.3	7.4	9.7	9.1	8.7	2.2	7.5	5.6	7.8	<b>6.</b> <del>1</del>
CEC	2		22	1949	1956	1951	<b>35</b>	1955	1956		1958		_	_	1963	1966	1967	1969	_							2046									2055				_				2065

USS ENTERPRISE (CVN-65)

205			AIRCRAFT		KING S	PEED A	SINKING SPEED AT TOUCHDOWN				הר זטר ה	GLIDE PATH ANGLE AT TO	WGLE	<u>≥</u>	WHEEL	WHEEL HEIGHT	HOOK HEIGHT	EIGHT
2	2	MOSE	8	PORT	ST	STBO	AVG	U	FREE-FLIGHT	.1GHT	25	BH¥.	Ď	<b>8</b>	OVER RAMP	SAMP.	OVER RAMP	RAMP
	Ş	Ş	53	\$	5,5	K/S	5,5	S/N	F/S	M/S	DEG	Z.	DEG	8	E	3	t.	×
22	23	74	25	<b>58</b>	27	28	29	30	2	32	33	¥,	82	38	37	25	39	6
2066	9.0	<b>.</b>	5.7	1.7	7.7	2.3	6.7	2.0			2.5	.043	2.2	. 039	13.4	<del>*</del>	11.0	3.3
2067	3.2	- •	<b>9</b> .0	•	3.3	<b>•</b> .	2.7	<b>8</b> 0.			2.6	. 046	œ.	.016	12.7	3.9	10.2	J. 7
2069	7.3	2.5		2.5	9.0	2.9	8.6	2.6			3.7	.064	2.5	. 038	18.9	5.8	16.4	5.0
2070	<b>+</b> .	1.3	7.4	2.3	8.7	2.6	<b>8</b>	2.5			2.8	.048	S. 0	. 053	14.2	4.4	1.9	3.6
2072	9.7	2.8	<b>8</b> .6	2.6	8.0	7.4	4.6	5.6			3.1	. 053	2.9	.050	13.5	<b>+</b> .1	11.0	3.4
2073	1.3	3.5	1.3	4.0	1.5	3.5	11.3	3.5			4.6	. 081	4.2	.074	16.4	5.0	13.8	4.2
2074	6.3	<b>6</b> .	3.7	-:	5.0	<b>.</b>	4.7	<b>+</b> .			2.0	.034	1.7	. 030	11.2	4.6	8.3	2.5
2076	7.3	2.5	<b>+</b> .	<del>*</del> :	7.5	2.3	6.3	6.			<del>*</del> :	. 024	<b>6</b> .	.034	11.5	3.5	9.5	2.8
2017	7.0	d.	<b>9</b> .	7.4	10.5	3.5	9.5	<b>7.8</b>			3.5	.062	4.0	. 969	16.2	o. •	13.7	4.2
2078	5.7	1.7	6.7	<b>7.0</b>	<b>6</b> .9	2.1	6.8	2.1			3.2	. 056	2.8	.049	17.9	5.5	15.3	4.7
2079	9.9	5.0	7.1	2.5	7.9	7.4	6.8	2.1			3.1	.054	2.8	. 648	11.9	3.6	<b>6</b> .	2.7
2000	6.5	2.0	5. 5.	<b>8</b> :	4.7	₹.	5.2	1.6			2.8	.049	1.8	.631	14.2	4.4	12.2	3.7
2083	4.6	5.8	7.4	2.3	8.2	2.5	7.7	7.7			3.0	. 052	J. 1	. 054	13.8	4.2	1.3	3.5
2084		2.8	<b>9</b> .0	2.7	10.8	3.3	8.6	3.0				. 072	3.9	. 067	17.7	5.4	15.2	4.6
2086	1.1	4.6	15.8	4.8	1.4	3.5	13.2	4.0			3.7	.065	S.9	. 102	18.7	5.7	16.0	4.9
2087	5.7	1.7	<b>6</b> .9	2.1	<b>•</b> .	1.2	4.9	9.7		-	3.0	. 052	2.7	.048	17.3	5.3	14.9	4.5
2008	<b>●</b> . =	3.3	10.9	3.3	11.8	9. 9.	1.4	3.5			4.4	.076	4.7	. 682	21.7	9.9	18.8	5.7
2009	6.5	2.0	<b>.</b>	2.7	7.9	7.4	7.2	2.5		,	2.2	. 038	3.0	.053	14.6	4.5	12.2	3.7
2001	<b>8</b> .8	2.1	4.6	<b>5.8</b>	8.8	2.1	<b>6</b> .3	<b>6</b> .		-	3.5	. 062	5.6	.046	17.7	4.0	15.5	4.7
2002	7.7	2.3	7.5	2.3	7.6	2.3	7.6	2.3			2.8	.050	3.1	.054	13.5	4.1	10.8	3.3
2093	6.3	<u>.</u>	9.6	<b>9.</b>	<b>6</b> .	5.	7.3	2.2			2.6	.046	2.7	.048	15.6	<b>4</b> .8	13.1	4.0
2084	4.4	 	•.	- -	5.5	<b>.</b>	S.	1.7	5.3	9.	2.5	.044	6.	. 033	14.2	4.4	12.1	3.7
2002	6.5	<b>5</b> .0	7.0	2.1	4.7	<b>→</b> :	5.2	•. •			2.1	.036	6.	. 033	10.7	J. J	8.2	2.2
2096	<b>4</b> .0	<del>+</del> :	5.4	<del>.</del>	7.2	2.2	<b>6</b> .1	<del>1</del> .9			2.0	. 035	2.5	. 039	13.1	<b>4</b> .0	10.6	3.5
2097	8.2	2.5	7.4	2.3	7.0	2.1	7.0	2.1			2.8	. 046	7.8	.050	14.7	4.5	12.4	3.8
2098	<b>9</b> .	<b>-</b>	5. 8.	<b>.</b>	4.0	<b>5.8</b>	7.9	7.4			3.2	.055	J. 0	.053	16.4	5.0 0.0	13.8	4.2
2009	7.0	2.1	<u>-</u>	2.8	5.8	<b>.</b>	7.3	2.2			4.6	999.	<del>ا</del>	.054	16.1	<b>6</b> .4	13.3	<del>-</del> -
2100	8.8	2.7	•.	2.7	5.6	1.5	6.8	2.1			4.5	. 060	9. 9.	.052	9.6	2.9	6.4	1.9
2102	<b>-</b> .	2.5	10.8	3.3	9.5	2.8	10.5	3.2			4.6	. 969	<del>-</del> -	. 072	17.2	5.2	14.5	4.4
2163	5.7	1.7	4.0	1.2	8.3	2.5	5.7	1.7			3.2	. 056	2.3	.040	16.9	5.2	14.1	4.4
2105	10.3	J. 7	<b>.</b>	2.8	1.6	3.5	10.1	3.1			3.5	. 062	3.9	. 969	15.5	4.7	13.3	4.0
2106	7.3	2.5	6.2	<b>.</b>	4.0	2.6	7.1	2.5			2.5	0 4 4	2.8	.049	14.7	4.5	12.3	3.7
2107	5.9	-	7.8	2.4	<b>8</b> .8	 •	4.9	1.9			2.1	. 637	2.5	. 038	17.1	5.5	14.7	4.5
2108	<b>†</b> .	<b>.</b> .	5.7	1.7	<b>9</b> .9	2.1	6.2	6.			1.7	. 030	7.8	. 045	10.5	3.5	7.7	2.3
2169	<b>9</b> .9	2.1	7.1	2.2	7.4	2.3	7.0	2.1			2.5	.044	5.6	.046	17.9	5.3	15.9	<b>6. †</b>
2170	8.8	2.1	8.5	2.6	5.1	1.6	7.5	2.3			2.9	. 050	5.8	. 050	17.9	5.3	15.6	<b>4</b> .8
2171	5.6	1.7	9.5	2.9	4.5	<b>-</b>	4.2	1.3			3.4	.059	1.7	.031	19.0	5.0	16.2	4.9
2173	3.0	1.5	4.7	<b>+</b> :-	6.7	2.0	6.9	<b>1</b> .8			2.8	.049	2.1	. 037	15.3	4.7	12.9	3.9
2174	12.9	3.9	16.9	5.5	12.6	3.8	14.3	<b>+</b> .+			6.9	. 103	6.9	. 104	17.0	5.2	13.8	4.2
2175	2.4	۲.	3.2	<b>.</b>	3.9	1.2	3.5	-:			2.5	.044	-:	.020	15.8	4.8	13.3	4.0

<b>.</b>	NOSE	PORT	<b>.</b>	S	STBO	AVG	<b>.</b>	FREE-FLIGHT	.IGHT	BHA	*	6	₩	OVER	OVER RAMP	OVER RAMP	RAMP
2	\$	2	Ş	£/\$	\$	<b>5</b> /2	N/S	F/S	S/M	DEG	SS.	DEG	8	E	3	E	3
23	*	22	<b>36</b>	27	28	58	36	31	32	33	*	35	36	37	88	39	6
11.4	3.5	7.6	9.5	8.9	2.1	8.3	2.5			4.6	.059	3.5	. 061	13.4	+	10.4	3.2
8.3	2.5	7.6	2.3	7.0	2.1	7.3	2.5			2.2	. 038	3.1	. 053	16.7	5.1	14.3	*
10.8	3.3	12.9	0. N	10.2	3.1	11.6	3.5			3.0	.052	4.6	. 686	16.6	5.1	14.3	*.
	2.5	1.1	4.5	6.7	<b>5.0</b>	8. S	7.6			3.0	.052	3.1	. 055	15.1	<b>9</b> .	12.7	3.8
7.6	2.3	6.5	<b>5</b> .0	8.7	2.7	7.6	2.3			3.2	.056	3.0	. 052	21.8	9.9	19.4	5.9
<b>9</b> .9	2.1	8.2	2.5	7.3	2.5	7.3	2.5			3.3	.057	4.6	. 059	17.3	5.3	14.7	4.5
8.7	7.6	7.8	7.4	7.2	2.5	7.1	2.5			2.2	. 038	2.7	. 947	1.9	3.6	<b>4</b> .6	2.8
	1.7	ا ا	7.5	- ·	<b>.</b>	4.7	<b>+</b> .			3.1	.054	1.7	. 939	17.1	2.5	14.5	<b>+</b> : <b>+</b>
	2.0	10	5.6	<b>4</b>	<b>*</b> :	S.8	<del>-</del>			2.5	.038	2.3	.040	14.8	4.5	11.7	3.6
2213 8.4	<b>7.</b>	4.	 8	<b>6</b>	<b>5</b> .0	5.5	2.3			2.9	.051	4.6	. 969	- <del>2</del>	S. 50	15.6	<b>→</b> •
		, i	<b>.</b>	<b>9</b> (		ю. •	<b>B</b> .			2.2	. 639	7.4	.043	- - -	ر ا ا	<b>6</b> .	2.7
•	2.5	<b>*</b> :	2.5		2.1	9.9	2. 9. i			2.7	.048	2.8	. 648	20.7	. O	18.5	
4.0	3.2	12.7	ص ص	16.7	n (	- '	4.			2.9	.051	4.4	. 675	21.4	6.5	4.61	න න
6.2	<b>.</b>	÷ (	1.7	7.8	<b>7.</b>	<b>9</b>	7.0			2.8	. 050	2.8	948	20.6		17.9	
•	-	7.7	- 1		1.7	9	<b>*</b>			2.4	.042	<del>-</del>	. 631	12.0	3.7	<b>6</b>	9.
<b>6</b> .6	<b>7</b> .	8.5	5.5	0. i	<b>.</b>	ص ص	2.1			2.6	. 045	2.9	. 858	18.3	6.6	16.2	6.4
	<b>D</b>	<b>-</b> (	<u>ه</u> :	n (	- (	<b>4</b> .7	<b>+</b> !			2.7	.048	<b>6</b> .	. 633	20.4	6.2	18.0	5.5
D 1	2.1	٠. و	2.1	- 0	19 19 19	9.6	2.3			2.9	.050	ا ا	.054	<b>*</b> :		о. •	2.7
3.	7.7	• ;	2.5 5.5	7.0	2.3		2.0			٠. د د	/60.	3.2	. 655	. i	0 0	15.0	÷.
0 0	7.7	-		- 6		7.7	, d			2.5	/69.	<b>4</b> ,	9/9	8.7.	4.	9.0	<b>•</b> •
• 6 • •	9 .	- 5		7. 4	, . ,		, .			? "	140.	- r	409.	- 4	ė i	7. 6.	
	• •	· •				- ~	9 6				945	, c	. 60 6	0.01	, R	18.7	
•	2.6	4	2.5		2.0	6.7					5.0	, c	776	2 7		11.5	
D. 0	2.8	9.0	3.5	6.5	7.9	10.4	3.2			B.	.067	4.	.076	24.3	7.4	21.5	6.5
5.5	1.7	•.	<b>.</b>	5.2	<b>9</b>	5.1	<b>5</b> .5			2.2	.039	2.3	.040	12.8	g.8	10.2	3.1
11.3	J.5	12.6	3.8	<b>.</b>	7.0	10.5	3.2			3.4	. 659	4.2	. 673	18.8	5.7	16.6	5.1
4.9	2.0	7.3	2.5	9. 9.	1.7	8.8	2.1			2.6	.045	2.6	. 945	16.7	5.1	14.3	<b>*</b> : <b>*</b>
•	<b>-</b>	8.8	2.7	9.0	2.0	7.7	7.4			2.8	.048	4.6	. 969	16.9	5.2	14.5	<b>†</b> .
D. 0	2.8	7.9	7.4	<b>9</b> .	7.6	8.2	2.5			2.5	. 044	5.8	. 626	11.0	4.0	8.8	2.7
<b>6</b> .4	- .5	5.4	•.	2.7	•	<b>.</b>	1.2			1.7	. 030	5.	.026	13.9	4.2	11.5	3.5
<b>*</b> .	2.8	<b>.</b>	2.7	<b>9</b> .	<b>9</b> .	5.0	2.8			4.0	. 069	J. B	. 966	17.2	5.2	14.8	4.5
<b>8</b> .	<b>-</b> .5	<b>9</b> .	5.	4.2	 	<b>9</b> .	<del>*</del> :			2.1	. 037	<del>1</del> .8	. 032	12.2	2.7	a. a	۵. م.
8.7	2.7	<b>9</b> .9	2.1	7.9	7.4	7.4	2.3			2.9	.051	3.3	. 657	13.8	4.2	1.0	4.6
7.8	7.7	7.4	2.3	<b>.</b>	2.2	7.7	2.3			2.7	.047	3.1	. 055	16.1	6. <del>+</del>	13.8	4.2
8.8	2.7	19.7	 	7.3	7.7	7.7	2.3			2.6	.045	3.3	.058	14.2	4.4	11.5	3.5
7.9	7.4	7.1	2.1	8.7	2.7	7.5	2.3			3.1	. 055	3.2	. 055	17.4	5.3	<b>+.</b> +	<b>+</b> . <b>+</b>
7.4	2.3	•:	4.6	4.8	<del>.</del>	7.1	2.1			3.2	.056	5.8	. 051	18.4	5.6	15.6	₩.
7.7	7.4	5. 0.	<b>9</b> .	<b>=</b> .	4.6	8.6	2.6			4.3	.075	3.2	. 056	19.7	<b>6</b> .9	17.2	5.2
•	•	1	•	•													

USS ENTERPRISE (CVN-65)

				7	7	6	7	4	n	0.		•	•	<b>o</b>	•	_	_	•	7	•	_	_	_	•	20	n	•	•	•	<b>+</b>	•	<b>a</b>	•	•	₩	<b>0</b>	•	<b>G</b>	7	•	€0	o,	S
ноок нетснт	OVER RAMP	3	4	'n	'n	*	*	'n	÷	g. N		7	4.6	'n	*	<u>ب</u>	'n	<del>,</del>	'n	'n	7.	÷	<b>÷</b>	•	'n	4	'n	ę,	'n	ņ	'n	'n	6	'n	ų.	'n	<b>÷</b>	ņ	'n	<b>÷</b>	'n	'n	'n
<b>H</b> 00H	OVER	E	39	18.7	12.1	13.0	15.6	11.2	14.0	12.9		æ .S	15.1	12.8	13.3	<b>6</b> .8	10.2	13.0	10.4	18.4	23.2	13.4	13.5	19.7	17.9	<u></u>	= •:	16.5	9.7	11.2	<b>8</b> .	19.4	<b>8</b> .	12.3	12.4	19.5	<u>-</u> :	12.7	17.2	13.2	12.5	12.7	1.5
IE1GHT	de la composition della compos	2	8	6.3	<b>+</b> : <b>+</b>	4.7	5.5	<del>-</del> :	5.1	4.7		J. 5	5.4	4.6	<b>4</b> .8	<b>5</b> .8	J. B	4.8	g.8	6.4	7.9	<b>*</b>	<b>6.</b>	6.7	6.1	5.0	4.3	5.8	G.	<del>-</del> -	رن ق	<b>9</b> .	J. 5	4.5	<b>+</b> . <b>+</b>	ø.	9.	<b>4</b> .	5.9	4.8	4.5	4.5	4.5
WHEEL HEIGHT	OVER RAMP	E	37	20.8	14.5	15.4	18.1	13.5	16.6	15.5		7.7	17.8	15.1	15.7	4.6	12.6	15.7	12.8	20.9	25.8	15.9	16.1	21.9	20.1	16.5	<b></b>	18.9	12.7	13.4	12.4	21.7	<b>=</b> .5	14.8	<b>+.</b> +	21.7	16.5	15.7	19.2	15.9	4.9	<del>7</del> .9	13.7
5		2	36	976	.054	. 961	690	.049	.043	. 053	948	.034	.057	.047	. 032	. 055	.042	. 052	999	.054	. 967	.051	. 057	. 089	.046	. 049	. 047	. 969	. 041	.048	. 037	446	.043	.045	. 060	159	986	.073	946	.069	.055	.047	.047
MGLE A	8	DEG	55	6.	3.1	3.5	4.0	2.8							60	_	4.4			_	3.8	_	3.3	_	5.6	<b>20</b>	2.7	G. D	_	2.7	_	5.5	_	5.6		•		~	•	3.9	~	2.7	2.7
GLIDE PATH ANGLE AT TO	*	<b>8</b>	*	.676	. 944	. 969	.052	. 040	.044	.045		.040	.043	.057	.042	.058	.042	. 039	.051	.057	.067	. 051	.047	. 673	.048	. 050	. 055	. 042	.043	.053	.035	.046	.049	.040	. 054	.047	.075	.055	.050	.074	.044	.038	. 058
GLIDE	8	DEG	z	6.4	2.5	3.4	3.0	2.3	2.5	2.6		2.3	2.5	3.3	2.4	J. J	2.4	2.2	2.9	3.3	3.8	2.9	2.7	4.2	2.7	2.9	3.2	2.4	2.5	3.0	2.0	2.6	2.8	2.3	3.1	2.7	4.4	3.2	2.9	4.2	2.5	2.2	3.3
	IGHT	K/S	32			-								•		·	•			-	•		<b>6</b> 0.														•	. •	-	•			·
	FREE-FLIGHT	F/S	ñ																				5.8																				
NWO		N/S	2	3.2	7.4	2.7	3.0	2.1	<del>0</del> .	2.2	<b>.</b>	<b>*</b> :	2.3	2.1	۲.	2.2	- -	2.1	4.7	2.3	2.8	2.3	2.2	3.6	2.1	2.1	2.1	2.8	<del>.</del> 5	1.5	5.5	<b>1</b> .8	<del>.</del>	<del>.</del>	2.7	2.1	3.8	2.7	<del>.</del>	J. 0	2.5	<b>6</b> .	2.1
TOUCH	AVG	Ş	29	10.4	7.8	6.0	9.7	7.0	8.8	7.1	5.8	<b>+</b> .	7.4	<b>9</b> .9	4.2	7.3	5.8	7.0	7.9	7.4	9.0	7.6	7.1	1.9	7.0	<b>6</b> .8	6.8	n. 0	<b>4</b> .8	<b>4</b> .9	5.0	<b>6</b> .0	5.9	5.9	8.8	6.9	12.4	8.9	r: <b>9</b>	9.7	7.1	6.2	6.9
INKING SPEED AT TOUCHDOWN	۰	Ş	28	<b>9</b> .0	7.7	٦.	J. 7	2.1	+:-	<b>.</b> .	J.3	 	<b>5</b> .	<del>.</del>	<b>*</b> :	2.5	 8:	<b>.</b>	2.5	4.7	4.0	7.7	2.5	3.5	2.5	<b>.</b>	<b>5.0</b>	<b>5.8</b>	۲.	1.7	5.5	<b>9</b> .	<b>9</b> .	•	2.7	2.1	3.7	2.8	2.1	7.4	<del>.</del>	1.7	2.0
S SHE	STBO	53	27	<b>a</b> .	7.3	<u>.</u>	 	6.9	4.5	6.3	<b>+</b> .+	<del>+</del>	4.3	6.2	4.7	8.2	6.4	6.1	8.3	9.0	•.•	7.7	9.1	 5.	7.3	<b>9</b> .	4.9	5.0	<b>+.</b> +	5.6	3. <b>e</b>	5.8 .0	<b>9</b> .	5.3	8.7	6.8	2.0		7.0	7.9	6.3	5.7	4.9
S	_	\$	<b>5</b> 8	U.5						2.4																		2.8	5.			<b>.</b>					•				2.5	2.1	2.0
AIRCRAFT	P.O.	5	22	•.	7.8		5.0	8.8	7.8	7.9	7.5	5.3	5.5	8.7	4.7	<b>+</b> .	<b>8</b> .0	7.7	8.8	8.8	5.0	7.7	6.2	2.3	9.9	7.9	7.2	<b>9.</b> 5	<b>6.</b>	<b>4</b> .5	5.9	6.2	7.7	7.1	5.9	7.0	2.0	8. 8.	1.9	 •	7.3	8.	8.8
		\$	*	3.3	2.2	3.2	3.1		2.0	2.2	2.0	•	0.1	2.4	•	2.5	÷.	2.3						_				2.8	1.7	2.3	7.7	- -			_		_			2.9	2.3	2.0	2.1
	HOSE	2	23						6.7		6.7																							5.0						9.5			
	2		22	_		_	_			2257																											_						

_		3	_	n	•	en,	_	•	4		<b>.</b>	•	-	•	ņ	۲.	7	<b>6</b> 0	<b>8</b> .4	ιύ.	•	₩.	*	יה	~	<b>.</b>	יָי	-	٠.	~	-	*	~	6	۲.	o,	<b>.</b>		<b>.</b>	<b>8</b> 0	•	ņ	<b>+</b>
EIGH	S. S.	•	9	'n	3.0	4.5	3.7	4.0	ė	G. 9	2.	<b>-</b>	'n	'n	<b>÷</b>	'n	*	તં	*	n	ĸ	'n	4.6	'n	ď	n	*	તં	ĸ	<b>+</b>	'n	•	ĸ	'n	5.7	a. 3.	'n		'n	<b>8</b> 0.00	ທ່	'n	<b>÷</b>
HOOK HEIGHT	OVER RAMP	E	8	10.7	12.6	14.9	12.2	15.2	21.1	12.1	9	5.1	10.2	16.3	13.7	12.0	13.8	9.3	15.9	11.6	16.4	11.8	11.2	10.9	<b>8</b> .	12.1	14.0	<b>9</b> .9	<b>6</b>	13.7	16.8	20.9	17.1	16.4	18.8	12.7	12.7		12.7	12.5	18.3	10.6	14.4
WHEEL HEIGHT	OVER RAMP	*	8	<b>-</b> :	4.6	5.2	4.5	5.3	7.3	<b>4</b> .5	3.7	7.4	<del>-</del> .	5.0 9.0	6. <del>4</del>	4. 3.	<b>6</b> .4	9.B	5.6	4.6	3. 3.	<b>+</b> . <b>+</b>	4.3	4.2	3.7	4.6	5.2	u. r	9. 9	5.1	9. 9.	7.1	м. В	5.7	6.3	4.7	4.6		4.6	<b>4</b> .0	4.9	<b>6</b> .4	2.5
WHEEL	OVER	E	33	13.3	15.0	17.1	14.7	17.5	23.9	14.7	12.1	6.7	13.5	18.5	16.2	14.9	16.9	11.9	18.3	15.2	19.2	14.3	<u></u>	13.9	12.1	15.0	16.9	19.1	11.7	16.7	19.5	23.3	19.0	18.7	20.6	15.5	13.1		15.1	15.0	21.1	13.0	16.9
T T0	>	3	88	.055	. 050	990.	. 053	. 965	.052	.057	.968	. 021	186	. 068	. 085	.071	. 060	. 022	.068	. 689	.075	.058	.070	. 060	.054	.071	. 086	. 060	. 038	. 968	.073	.034	.052	.055	. 063	.677	.044	.059	. 039	.057	.066	.046	. 069
WCLE A	<b>8</b>	DEG	22	3.2	5.8	3.5	3.0	3.7	3.0	n. n	ر د د	7.5	4.7	G.	4.8	<del>-</del> -	3.5	<b>.</b> .	3.9	5.1	4.3	3.3	4.0	4.5	3.1	<del>-</del> .	4.8	4. P	2.5	3.9	4.2	œ. •	3.0	3.1	3.6	<b>+</b> .+	2.5	4.6	2.3	3.2	8. B.	5.6	3.9
ATH A	_	8	*	926	946	944	953	954	963	052	967	941	965	977	. 966	964	954	938	690	673	976	957	961	948	948	628	984	951	949	926	929	954	047	954	954	055	042		941	653	964	041	628
GLIDE PATH ANGLE AT TD	<b>S</b> +46	DEC	33	~	•	'n	· -	· -		•	ъ.	•		•	E0	۲.	·	~	•	7	"		'n	E0		*		6.	·	~	Ī	·	Ĭ	Ī	3.1	3.1	•		2.3	•	3.7	2.4	· •
G	<b>₩</b>	N/S	32	<b>"</b>	~	~	מ	מי	n	יכיו	ימי	~	m	*	רי	n	m	8	*	•	•	•	רח	7	~	מי	*	8	N	•	~	n	~	מי	מי	m	~		~	-	2.7 3	8	רי
	Free-Flight	£/S	5																																						6.0		
<b>Z</b>		K/S	8	2.0	2.2	<b>5.</b> 8	2.3	8.8	2.5	2.5	7.8	<u>ه</u>	٦.	2.8	4.6	3.2	2.5	<b>9</b> .	3.0	4.5	3.5	2.7	2.5	2.7	2.6	5.8	3.3	2.5	9.	2.7	۵. و.	5.	2.2	2.3	2.8	4.6	1.7	2.3	1.7	2.5	2.7	œ. -	2.8
NKING SPEED AT TOUCHDOWN	AVG	5	58	6.5	7.1	8.5	7.6	4.6	7.2	8.3	7	<b>9</b> .	10.2	D. G	1.3	10.4	8.1	4.6	10.0	1.3	11.6	ø. ø	4.6	8.7	4.6	9.6	11.0	8.2	5.3	8.7	<b>8</b> .	<b>4</b> .9	7.1	7.6	9.5	11.3	5.7	7.5	5.7	8.3	<b>9</b> .	6.3	<b>.</b>
EE0 A1	6	\$	28	<b>9</b> .	<u>.</u>	7.7	2.3	5.6	4.4	5.6	-	7.	4.0	3.2	3.5	3.3	1.7	=	2.4	<b>+</b>	2.8	<b>.</b>	5.8	5.8	<del>.</del>	٠. ت	5.9	2.8	1.7	2.5	ر. د.	7.5	2.3	2.3	۵. ه.	3.5	5.0	5.6	<u>.</u>	2.5	<b>5.0</b>	2.2	2.6
KING SP	STBD	5	27	9.	<b>.</b>	7.7	7.6	9.0	<b>8</b> .0	8.7	_ •	<b>-</b>	<u>-</u> -	6.5	9.0	0. 1	5.7	3.7	7.8	13.0	9.2	<b>.</b>	9.5	4.0	6.3	10.2	<b>9</b> .0	<b>.</b>	6	7.4	• •	J. 0	7.6	7.6	<b>8</b> .	1.6	4.9	<b>9</b> .0	<b>6</b> .3	<b>8</b> .1	8.6	7.2	6.5
	E	\$	<b>5</b> 0	2.4	2.3	2.8	2.3	۳.	7.0	2.7	2.5	ė	2.8	2.5	3.5	2.7	3.e	<u>-</u>	4.6	٠. ٠.	3.7	3.5	4.0	7.4													2.0	2.3	1.7	2.6	5.9	<b></b>	2.9
AIRCRAFT S	PORT	2	22	7.8	7.4	9.3	7.4	-:	4.9	• •	9.7	2.0	2.5	8.2	<b>†</b> .	8.8	o. 6	3.5	1.2	6.0	2.3	.5 .5	11.2	• •	<b>9</b> .0	9.0	2.2	7.3	3.B	<b>9</b> .0	S.	<b>5</b> .6	<b>6.9</b>	9.0	4.6	•.	9.0	7.4	5.5	9.6	4.0	<b>.</b> .	9.7
	4.4	Ş	<b>34</b>	2.3	2.0	2.3	2.2	2.6 1	2.0	5.6	5.8 	•	2.5	8.8	3.6	۵.1	2.1	۲.	_		Ť	•	3.3	_	_	_	٠	_		2.2	2.5	1.7	2.2	2.6	2.9	3.3	•.	<b>*</b> :-	<b>.</b> .	2.4	2.5	2.1	2.9
	MOSE	ž	22	4.4	٠. دن	9.4	2.2	3.6	٠. دن	4.6	<b>.</b>	2	2.5	 	o. -	9.2	 6.	~.	4.6	5.8	7.1	-:	9.0	9.	9.4	•	3.9	7.6	3.7	۳.	5.3	5.5	۵.	3.6	3.5	9.8	5.3	5.5	•	o. /	3.2	<b>8</b> .0	9.0
90	9	_	22	2297	2296	2299	2300	2301	2362	2363	2304	2365																															

USS ENTERPRISE (CVN-65,

Mart   Mart	ANSE ANSE ANSE ANSE ANSE ANSE ANSE ANSE														
4/5         4/5         4/5         4/5         4/5         4/5         4/5         4/5         4/5         1/5         4/5         1/5 <th>2.3 2.4 2.4 2.5 2.4 2.5 2.5 2.5 2.5 2.5 2.5 2.5 2.5 2.5 2.5</th> <th></th> <th>8</th> <th>AVG</th> <th>_</th> <th>FREE-FL</th> <th>1CH1</th> <th>\$</th> <th>2</th> <th>8</th> <th>&gt;</th> <th>OVER</th> <th>RAMP</th> <th>OVER RAMP</th> <th>d MA</th>	2.3 2.4 2.4 2.5 2.4 2.5 2.5 2.5 2.5 2.5 2.5 2.5 2.5 2.5 2.5		8	AVG	_	FREE-FL	1CH1	\$	2	8	>	OVER	RAMP	OVER RAMP	d MA
24         25         26         27         26         29         31         32         33         34         35         36         37         36         37         36         37         36         37         36         37         36         37         36         37         36         37         36         37         36         37         36         37         36         37         36         37         37         36         37         36         37         36         37         36         37         36         37         36         37         36         37         36         37         36         37         36         37         36         37         36         36         37         36         36         37         36         36         37         36         36         37         36         36         37         36         36         37         36         36         37         36         36         37         37         36         36         37         36         37         37         36         37         37         36         37         37         36         37         37         36         37<			¥	F/S	S K	٤/٤	s/m	DEG	8	DEC	8	E	3	E	3
6.9         2.1         9.1         2.8         7.5         2.3         3.6         0.65         3.6         0.69         3.6         0.69         3.6         0.65         3.6         0.69         3.6         0.69         3.6         0.69         3.6         0.69         3.6         0.69         3.6         0.69         3.6         0.69         3.6         0.69         3.6         0.69         3.6 </td <td>6</td> <td>•</td> <td>28</td> <td>29</td> <td>30</td> <td>2</td> <td>32</td> <td>33</td> <td>ŧ,</td> <td>33</td> <td>36</td> <td>37</td> <td>82</td> <td>82</td> <td>9</td>	6	•	28	29	30	2	32	33	ŧ,	33	36	37	82	82	9
7.4 2.3 6.7 2.6 7.5 2.3 7.1 2.2 2.4 659 3.3 657 15.6 6.8 1.8 6.7 1.8 6.3 2.8 7.1 5.6 6.8 2.8 7.4 2.3 5.6 6.8 2.8 7.4 2.3 5.6 6.8 2.8 7.4 2.3 5.6 6.8 2.8 7.4 2.3 5.6 6.8 2.8 7.4 2.3 5.6 6.8 2.8 7.4 2.3 5.6 6.8 2.8 7.4 2.3 5.6 6.8 2.8 7.4 2.3 5.6 6.8 2.8 7.4 2.3 5.6 6.8 2.8 7.4 2.3 5.6 6.8 2.8 7.4 2.3 5.6 6.8 2.8 7.1 2.3 6.8 6.8 2.8 6.8 6.8 2.8 6.8 6.8 2.8 6.8 6.8 2.8 6.8 6.8 2.8 6.8 6.8 2.8 6.8 6.8 2.8 6.8 6.8 2.8 6.8 6.8 2.8 6.8 6.8 2.8 6.8 6.8 2.8 6.8 6.8 2.8 6.8 6.8 2.8 6.8 6.8 2.8 6.8 6.8 2.8 6.8 6.8 2.8 6.8 6.8 6.8 2.8 6.8 6.8 2.8 6.8 6.8 2.8 6.8 6.8 2.8 6.8 6.8 2.8 6.8 6.8 6.8 2.8 6.8 6.8 2.8 6.8 6.8 2.8 6.8 6.8 2.8 6.8 6.8 2.8 6.8 2.8 6.8 6.8 2.8 6.8 6.8 2.8 6.8 6.8 2.8 6.8 6.8 2		2.8 7.6	2.3	 	2.5		<i>r</i> ,	<b>6</b> .	. 053	3.6	. 963	17.9	5.5	14.9	4.5
6.1 1.9 6.5 2.0 6.3 1.9 6.3 1.9 2.9 651 2.7 646 16.2 6.3 1.9 6.3 1.9 6.3 1.9 6.3 1.9 6.5 2.0 6.5 1.7 6.2 6.6 2.0 7.4 2.3 2.9 6.6 2.0 7.4 2.3 2.9 6.6 2.0 7.4 2.3 2.9 6.6 2.0 7.4 2.3 2.9 6.6 2.0 7.4 2.3 2.9 6.6 2.0 7.4 2.3 2.4 6.6 2.0 7.4 2.3 2.4 6.6 2.0 2.4 2.5 2.5 1.7 6.8 2.1 2.1 6.4 2.0 6.6 2.0 2.1 6.4 2.3 2.4 6.8 2.1 6.4 2.2 2.3 6.4 2.3 6.6 2.0 2.1 6.4 2.3 2.4 6.8 2.0 2.1 6.4 2.3 2.4 6.8 2.0 2.1 6.4 2.3 2.4 6.8 2.0 2.1 6.4 2.3 2.4 6.8 2.0 2.1 6.4 2.3 2.4 6.8 2.0 2.1 6.4 2.3 2.4 2.4 2.4 2.2 2.3 6.4 2.3 2.4 2.4 2.3 2.2 2.4 2.4 2.3 2.4 2.4 2.3 2.4 2.4 2.3 2.4 2.4 2.3 2.4 2.4 2.3 2.4 2.4 2.3 2.4 2.4 2.3 2.4 2.4 2.3 2.4 2.4 2.4 2.4 2.4 2.4 2.4 2.4 2.4 2.4		2.0 7.5	2.3	7.1	2.2		-,	<b>*</b> :	. 059	3.3	.057	15.6	<b>6.</b>	12.7	3.9
5.8         1.8         5.7         1.7         4.2         1.3         4.0         1.2         3.1         6.0         5.2         6.0         5.2         6.0         5.2         6.0         5.2         6.0         5.2         6.0         5.2         6.0         5.2         6.0         5.0         6.0         5.2         6.0         5.0         6.0         5.2         6.0         5.2         6.0         5.2         6.0         6.0         5.2         6.0         6.0         5.2         6.0         6.0         5.2         6.0         6.0         5.2         6.0         6.0         5.2         6.0         7.0         6.0         6.0         7.0         6.0         7.0         6.0         6.0         6.0         6.0         7.0         6.0         7.0         6.0         6.0         6.0         6.0         6.0         6.0         6.0         6.0         6.0         6.0         6.0         6.0         6.0         6.0 <td></td> <td>2.0 6.3</td> <td><del>.</del></td> <td>6.3</td> <td><u>.</u></td> <td></td> <td>•</td> <td>6:</td> <td>.051</td> <td>2.7</td> <td>. 048</td> <td>16.2</td> <td>ø. ₹</td> <td>13.7</td> <td>4.2</td>		2.0 6.3	<del>.</del>	6.3	<u>.</u>		•	6:	.051	2.7	. 048	16.2	ø. ₹	13.7	4.2
6.3 1.9 8.5 2.6 6.6 2.0 74 2.3 3.9 652 3.4 665 2.9 6.5 3.6 6.6 3.2 1.8 8.5 2.9 16.6 3.2 16.4 2.3 16.4 2.4 2.3 16.4 2.3 1		1.7 4.2	7.7	0.4	1.2			-:	.037	1.7	. 029	8.6	2.6	8.2	6.
6.2 1.9 6.8 2.1 6.4 2.9 6.6 2.0 2.7 .047 2.6 .045 16.2 7.9 2.8 2.8 2.8 2.8 2.8 2.8 2.8 2.8 2.8 2.8		2.6 6.6	2.0	7.4	2.3		٠,	9.	. 052	4.5	. 059	23.0	7.0	18.9	5.7
9.8         3.2         10.1         3.1         10.1         3.4         .059         4.1         .071         10.2         2.6         .046         3.2         .056         14.1         .071         12.2         3.6         .056         14.9         15.0         .056         16.8         15.0         .056         14.9         15.0         .056         14.9         15.0         .056         14.9         .056         14.9         .057         .056         14.9         .056         14.9         .057         .057         .056         14.9         .056         14.9         .057         .056         14.9         .057         .056         14.9         .057         .056         .056         .058         .056         .058         .058         .058         .058         .058         .057         .057         .057         .058         .057         .057         .058 <td></td> <td>2.1 6.4</td> <td>2.0</td> <td>9.9</td> <td>2.0</td> <td></td> <td>•</td> <td>7.</td> <td>.047</td> <td>2.6</td> <td>. 045</td> <td>16.2</td> <td>ø. <del>1</del></td> <td>7.7</td> <td>4.3</td>		2.1 6.4	2.0	9.9	2.0		•	7.	.047	2.6	. 045	16.2	ø. <del>1</del>	7.7	4.3
7.2 2.2 8.4 2.5 5.5 1.7 6.8 2.1 2.3 .040 2.8 .046 1.8 16.6 16.8 2.4 6.8 12.1 8.6 2.6 7.6 2.3 3.6 10.046 3.2 .056 116.8 2.4 7.8 2.4 7.8 2.4 7.7 2.3 10.1 2.5 7.1 2.2 3.6 .046 3.2 .056 116.8 2.7 13.1 4.8 2.4 7.7 2.3 10.1 2.5 7.1 2.2 3.6 .046 3.2 .056 116.8 2.7 13.1 4.8 2.4 7.7 2.3 10.1 2.5 7.1 2.2 2.7 13.1 13.1 13.1 13.1 13.2 2.8 8.8 2.7 7.2 2.2 6.9 1.8 2.4 8.8 2.7 7.2 2.2 7.7 2.3 10.0 12.1 13.1 13.1 13.1 13.1 13.1 13.1 13.1		2.9 10.6	3.2	19.1	J. 7		<b>F</b> )	<b>+</b> :	.059	+:	.671	19.3	5.9	17.0	5.2
7.9         2.4         6.9         2.1         8.6         2.6         7.9         2.6         .046         3.2         .056         16.8           7.9         2.4         5.9         1.8         2.5         7.1         2.2         3.6         .062         3.2         .056         14.9           7.9         2.4         3.9         2.5         10.7         3.5         .062         3.2         .056         14.9           8.0         2.5         7.2         2.5         10.7         3.5         .056         3.7         .057         17.7           8.0         2.6         2.6         2.6         0.6         2.7         .047         17.7         17.7         2.2         0.5         0.5         0.5         17.7         17.7         17.7         2.2         0.6         0.6         3.7         0.6         0.6         3.7         0.6         0.6         3.7         0.6         0.6         3.7         0.6         0.6         3.7         0.6         0.6         3.7         0.7         0.6         0.6         0.6         0.6         0.6         0.6         0.6         0.6         0.6         0.6         0.6         0.6		2.5 5.5	1.7	8.8	2.1		.4	٦.	.040	2.8	. 948	16.6	5.1	4.4	<b>+</b> . <b>+</b>
7.9         2.4         5.9         1.8         6.3         2.5         7.1         2.7         .94         2.7         2.5         10.7         2.5         2.7         2.2         2.7         2.6         0.46         2.5         10.7         2.7         2.2         2.7         2.2         2.7         2.6         0.46         2.3         3.1         3.1         3.2         3.1         2.2         3.2<		2.1 8.6	2.6	7.6	2.3		~	9:	.046	3.2	.056	16.8	5.1	14.3	4.4
7.9         2.4         7.0         2.4         7.7         2.3         8.1         2.5         8.6         2.5         10.7         7.3         8.1         2.5         8.6         2.7         2.2         3.6         9.6         3.2         3.7         9.7 <td>2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2</td> <td>1.8 8.3</td> <td>2.5</td> <td>7.1</td> <td>2.5</td> <td></td> <td>~</td> <td>7.</td> <td>.047</td> <td>2.9</td> <td>. 050</td> <td>14.9</td> <td>4.5</td> <td>12.3</td> <td>3.7</td>	2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2	1.8 8.3	2.5	7.1	2.5		~	7.	.047	2.9	. 050	14.9	4.5	12.3	3.7
8.8 2.7 13.1 4.0 8.2 2.5 10.7 3.3 2.8 2.8 2.8 2.8 2.8 2.8 2.8 2.8 2.8 2.8	8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	2.4 7.7	2.3	<b>8</b> .1	2.5		-,	9.	. 062	3.2	. 057	17.7	5.4	15.3	4.6
2.5         7.4         2.3         7.2         2.2         6.0         1.8         2.6         3.1         655         17.2         2.2         6.0         1.8         2.5         6.4         3.1         655         17.2         2.2         8.1         2.5         8.1         2.5         8.1         2.5         8.1         2.5         8.1         2.5         8.1         2.5         8.1         2.5         8.1         2.5         9.2         3.1         9.5         1.7         2.2         3.2         9.5         1.2         3.2         9.5         1.7         2.2         2.6         9.6         3.3         9.5         1.7         2.2         2.6         9.6         3.3         9.5         1.7         3.3         9.5         1.7         2.2         3.2         9.6         1.8         3.3         9.6         1.8         3.3         9.6         1.8         3.3         9.6         1.8         3.3         9.6         1.8         3.3         9.6         1.8         3.3         9.6         1.8         3.3         9.6         1.8         3.3         9.6         1.8         3.3         9.6         1.8         3.3         9.6         1.8         3.3 </td <td></td> <td>4.0 8.2</td> <td>2.5</td> <td>10.7</td> <td>3.3</td> <td></td> <td></td> <td></td> <td></td> <td><del>-</del>-</td> <td>. 671</td> <td></td> <td></td> <td></td> <td></td>		4.0 8.2	2.5	10.7	3.3					<del>-</del> -	. 671				
8.5         2.6         8.0         2.7         7.3         2.2         8.1         2.5         3.1         .055         17.2         8.1         2.5         8.1         2.5         8.1         2.5         8.1         2.5         8.1         2.5         8.1         2.5         8.1         2.5         8.1         2.5         8.1         2.5         8.2         8.2         8.2         1.2         8.2         8.2         1.2         8.2         8.2         1.2         8.2         8.2         1.2         8.2         1.2         8.2         1.2         8.2         1.2         8.2         1.2         8.2         1.2         8.2         1.2         8.2         1.2         1.2         8.2         1.2         8.2         1.2         1.2         8.2         1.2 </td <td>2.5.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2</td> <td>2.3 7.2</td> <td>7.7</td> <td>6.9</td> <td>8.</td> <td></td> <td>~</td> <td>80:</td> <td>.049</td> <td>2.5</td> <td>. 043</td> <td>15.7</td> <td><b>4</b>.8</td> <td>13.2</td> <td>4.0</td>	2.5.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2	2.3 7.2	7.7	6.9	8.		~	80:	.049	2.5	. 043	15.7	<b>4</b> .8	13.2	4.0
7.8         2.4         9.9         3.9         7.8         2.4         8.8         2.7         3.9         .655         3.7         .665         17.2           8.1         2.5         8.1         2.2         2.2         7.7         2.3         .657         16.0           8.2         3.9         2.1         2.2         1.9         2.2         1.9         2.2         .695         1.3         2.6         .695         1.3         .696         13.3         .696		2.7 7.3	7.5		2.5					3.1	. 055				
8.1 2.5 8.1 2.5 7.2 2.2 7.7 2.3 2.6 .946 3.3 .657 16.0 8.2 1.8 6.9 2.1 5.4 16 6.2 1.9 2.2 .939 2.3 .041 13.3 8.8 2.3 8.1 1.8 7.3 2.7 8.7 2.8 2.8 2.1 8.7 2.2 8.7 2.8 8.7 2.8 8.7 2.8 8.7 2.8 8.7 2.8 8.7 2.8 8.8 1.7 8.4 1.8 5.5 1.7 8.4 1.8 5.5 1.7 8.4 1.8 5.5 1.7 8.4 1.8 5.5 1.7 8.4 1.8 5.8 1.7 2.8 8.8 1.7 2.8 8.8 1.7 8.4 1.8 5.8 1.7 2.8 8.8 1.8 8.1 1.8 5.8 1.7 2.8 1.8 1.8 1.8 1.8 1.8 1.8 1.8 1.8 1.8 1	2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.	3.0 7.8	2.4	80.	2.7		,	9.	. 052	3.7	. 065	17.2	5.2	14.5	<b>†</b> .
8.2         1.9         6.9         2.1         5.4         1.6         6.2         1.9         2.2         .059         2.3         .041         13.3           7.5         2.3         6.1         1.8         7.3         2.2         6.7         2.9         2.1         .057         2.8         .041         13.7           8.6         1.7         2.9         2.7         2.9         3.5         .061         3.4         .069         19.3           7.4         2.2         9.2         1.7         2.3         1.7         2.8         .041         1.7         9.6         1.7         9.6         1.7         2.8         .045         1.2         9.6         1.3         1.3         1.3         1.4         9.6         1.2         9.6         1.3         1.2         9.6         1.3         9.6         1.3         1.2         9.6         1.3         1.2         9.6         1.2         1.3         9.6         1.2         1.4         9.3         1.4         1.2         2.2         2.9         1.1         1.2         9.6         1.3         1.2         9.6         1.3         1.3         9.6         1.3         1.3         1.3         1.		2.5 7.2	7.7	7.7	2.3			9:	. 946	3.3	. 657	16.0	6.4	13.5	<del>-</del> -
7.5         2.3         6.1         1.8         7.3         2.2         6.7         2.0         2.1         .037         2.8         .048         13.7           9.8         3.9         2.7         8.5         2.6         3.5         .061         3.4         .060         19.3           7.4         2.2         9.2         2.3         2.6         .062         4.0         .059         15.3           7.4         2.2         9.2         1.7         2.3         .061         3.4         .060         19.3           7.4         2.2         9.2         1.7         2.3         .062         4.0         .062         11.7           9.2         2.8         7.7         2.4         5.6         1.7         2.6         .045         2.5         .044         11.7           5.0         1.3         6.1         1.9         6.2         1.4         2.2         .040         1.8         0.3         10.2         10.2         10.2         10.2         10.2         10.2         10.2         10.2         10.2         10.2         10.2         10.2         10.2         10.2         10.2         10.2         10.2         10.2         10.	2.6 6.6 6.6 6.6 6.6 6.6 6.6 6.6	2.1 5.4	1.6	6.2	6.		•	7.5	.039	2.3	.041	13.3	<b>+</b> .4	1.0	J. J.
9.8         3.9         7.2         2.2         8.9         2.7         8.5         2.6         3.5         .061         3.4         .060         19.3           5.6         1.7         5.7         1.7         6.4         1.8         5.5         1.7         2.3         .061         3.4         .060         11.7           7.4         2.2         9.6         5.1         1.8         6.1         1.9         9.5         1.7         2.4         .062         3.3         3.5         1.7         2.4         .062         3.3         3.5         0.4         1.7         2.4         .062         1.7         3.5         0.4         1.7         2.4         0.6         0.6         0.6         1.7         3.5         0.6         1.7         3.5         0.6         1.7         3.5         0.6         1.7         3.5         0.6         1.7         3.5         0.6         1.7         3.5         0.6         0.	6.6 6.7 6.6 6.7 6.6 6.7 6.7 6.7	1.8 7.3	2.5	6.7	5.0				. 037	2.8	.048	13.7	4.2	1.3	J.5
5.6         1.7         5.7         1.7         6.4         1.9         5.5         1.7         2.4         .045         2.2         .039         15.3           7.4         2.2         2.2         2.3         2.4         .045         2.2         .035         11.7           8.2         1.3         6.1         1.9         6.1         1.9         2.7         2.6         .045         2.2         .046         11.2           4.3         1.3         6.1         1.9         4.9         1.2         2.6         .045         2.9         .046         11.2           5.0         1.3         6.1         1.9         6.1         1.9         2.2         .046         1.8         0.3         10.2         10.4         11.2         0.46         11.2         0.46         11.2         0.46         11.2         0.46         11.2         0.46         11.2         0.46         11.2         0.44         11.2         0.44         11.2         0.44         11.2         0.44         11.2         0.44         11.2         0.44         11.2         0.46         1.6         0.45         11.2         0.44         11.2         0.44         11.2         0.44	7.6 6.7 6.7 6.7 6.7 6.7 6.7 6.7	7	2.7	8.5	<b>5.8</b>		۳,		.061	4.5	. 969	19.3	9. 9.	16.8	5.1
7.4         2.2         9.2         2.8         5.1         1.5         7.6         2.3         2.4         .043         3.3         .058         11.7           9.2         2.8         7.7         2.3         1.8         6.1         1.9         2.7         3.6         .062         4.8         .059         13.6           4.3         1.3         2.1         5.9         1.2         2.3         .041         2.8         13.9           5.6         1.5         2.2         3.6         1.5         2.3         .041         1.8         .032         10.2           5.0         1.5         2.2         3.6         1.6         3.7         .065         10.2         10.2         11.2 <td>4.6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6</td> <td>۲.</td> <td><u>.</u></td> <td>5.5</td> <td>1.7</td> <td></td> <td>•</td> <td></td> <td>.048</td> <td>2.2</td> <td>. 039</td> <td>15.3</td> <td>4.7</td> <td>12.9</td> <td>G. B</td>	4.6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	۲.	<u>.</u>	5.5	1.7		•		.048	2.2	. 039	15.3	4.7	12.9	G. B
9.2         2.8         7.7         2.3         10.0         3.1         9.0         2.7         3.6         .062         4.0         .069         13.6           6.4         1.3         6.1         1.9         6.2         7.2         2.6         .045         2.5         .044         11.2           5.0         1.5         6.1         1.9         4.9         1.2         4.5         1.4         2.3         .040         1.8         0.35         10.2         11.2         10.2         10.2         10.2         10.2         10.2         10.2         10.2         10.2         10.2         10.2         10.2         10.2         10.2         10.2         10.2	2.6.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.	•	5.5	7.6	2.3		•		. 043	3.3	.058	11.7	3.6	<b>8</b> .0	2.7
6.4 1.9 6.8 2.1 5.9 1.8 6.1 1.9 2.6 .045 2.5 .044 11.2 5.0 1.3 6.1 1.9 4.0 1.2 4.5 1.4 2.3 .040 1.8 .032 10.2 5.0 1.5 2.6 .038 2.0 .035 13.9 2.0 1.5 2.3 .040 1.8 .032 10.2 13.9 2.3 .041 2.5 .044 9.1 1.9 6.9 2.1 6.4 1.9 2.7 2.2 .038 2.0 .035 13.9 13.9 2.1 1.9 6.7 2.4 8.8 2.7 2.5 .043 2.7 2.6 .043 2.7 2.6 .043 2.7 2.6 6.7 2.9 10.1 2.1 9.1 2.5 .043 2.7 2.6 .045 2.9 11.5 11.5 11.4 3.5 10.5 2.0 10.1 3.1 3.1 3.1 3.1 3.1 3.1 3.1 3.1 3.1 3		'n	۵.۲	9.6	2.7		۳,		. 062	4.0	. 969	13.6	<b>+</b> .1	10.9	3.3
4.3 1.3 6.1 1.9 4.0 1.2 4.5 1.4 2.3 .040 1.8 .032 10.2 5.0 1.5 2.6 6.1 6.2 6.1 6.1 1.9 6.1 1.9 6.1 1.5 2.2 5.0 1.5 2.2 6.038 2.0 6.035 13.9 7.0 2.3 9.6 3.0 7.7 2.4 8.8 2.7 2.5 .041 2.5 .044 9.1 1.4 5.5 10.5 3.0 1.0 5.1 1.9		-	<b>-</b>	<b>.</b>	6.				.045	2.5	. 044	11.2	4.6	8.6	5.6
5.0 1.5 2.6 .8 7.2 2.2 5.0 1.5 2.2 .038 2.0 .035 13.9 7.0 6.1 1.9 6.1 1.9 6.1 1.9 6.1 1.9 6.1 1.9 6.2 2.1 6.4 1.9 2.3 .041 2.5 .044 9.1 7.5 6.2 3.0 7.7 2.4 8.8 2.7 2.5 .043 3.7 .065 16.3 11.4 3.5 10.5 3.2 9.6 2.9 10.1 3.1 9.5 4.2 .041 2.5 .044 9.1 11.4 3.5 10.5 3.2 9.6 2.9 10.1 3.1 9.5 4.2 .045 4.2 .074 18.3 4.7 1.4 9.8 3.0 4.1 1.3 4.9 1.5 2.6 .046 1.6 .026 9.5 11.5 9.8 3.0 9.7 2.9 9.7 2		•	1.2	4.5	<b>+</b> .		•		.040	<b>.</b>	. 032	10.2	J. 7	7.1	2.5
6.1 1.9 6.1 1.9 6.9 2.1 6.4 1.9 2.3 .041 2.5 .044 9.1 7.6 2.3 9.8 3.0 7.7 2.4 6.8 2.7 2.5 .043 3.7 .065 16.3 11.4 3.5 11.6 6.7 2.0 5.8 1.8 6.3 1.9 2.7 2.5 .043 3.7 .065 16.3 11.4 3.5 11.6 6.7 2.0 5.8 1.8 6.3 1.9 2.7 2.6 .045 3.7 .065 16.3 11.4 3.5 11.6 5.8 1.8 5.8 1.1 1.3 4.9 1.1 2.1 0.54 4.2 0.74 18.3 11.6 5.8 3.0 0.7 2.9 0	1.0. 1.0. 1.0. 1.0. 1.0. 1.0. 1.0. 1.0.	.8 7.2	2.5	5.0	5.5		•		. 038	5.0	.035	13.9	4.5	1.3	J. 5
7.6 2.3 9.8 3.0 7.7 2.4 8.8 2.7 2.5 .043 3.7 .065 16.3 11.4 3.5 10.5 3.2 9.6 2.9 11.5 11.4 3.5 10.5 3.2 9.6 2.9 10.1 3.1 3.1 0.54 4.2 0.052 11.5 5.8 10.5 3.0 0.052 11.5 5.8 10.6 5.9 10.1 3.1 0.54 4.2 0.052 11.5 5.8 10.1 2.8 0.05 2.9 0.05 2.9 0.05 2.0 0.05	7.6 4.7 4.7 4.7 4.7 6.8 6.8 6.8 7.9 7.9 7.9 7.9 7.9 7.9 7.9 7.9	1.9 6.9	7.	4.9	<del>.</del>		•		.041	2.5	.044		2.8	ص ص	<b>.</b>
5.1 1.6 6.7 2.6 5.8 1.8 6.3 1.9 2.6 .045 3.9 .052 11.5 11.4 3.5 10.5 3.2 9.6 2.9 10.1 3.1 3.1 0.54 4.2 .074 18:3 5.8 1.8 6.2 1.9 4.1 1.3 4.9 1.1 2.8 0.46 1.6 0.25 9.5 5.9 0.5 2.9 0.7	6.1 6.7 6.7 6.8 6.8 6.8 6.9 7.9 6.1 7.9 6.1 7.9 6.1 7.9 6.1 7.9 6.1 7.9 6.1 7.9 6.1 7.9 6.1 7.9 6.1 7.9 7.9 7.9 7.9 7.9 7.9 7.9 7.9	3.0 7.7	7.4	<b>8</b> .	2.7		.,		.043	3.7	.065	16.3	9.	14.2	4.3
11.4 3.5 10.5 3.2 9.6 2.9 10.1 3.1 .054 4.2 .074 18.3 5.8 1.1 2.8 10.8 3.0 1.0 2.8 1.1 2.8 1.0 6.2 4.2 .074 18.3 5.8 1.1 2.8 1.0 6.2 6.0 6.0 6.0 6.0 6.0 6.0 6.0 6.0 6.0 6.0	4.4. 6.6. 6.7.	2.0 5.8	<b>.</b>	6.3	<del>.</del>		•		.045	3.0	. 052	11.5	J. 5	<b>9</b> .0	<b>5.</b>
4.7 1.4 9.8 3.9 1.9 .3 3.8 1.1 2.6 .946 1.6 .928 9.5 5.8 1.8 1.8 6.2 1.9 4.1 1.3 4.9 1.5 2.9 .935 2.9 .935 2.9 .935 11.6 5.9 8.3 9.7 2.9 9.8 13.7 9.8 13.7 9.8 13.7 9.9 1 2.8 9.9 2.7 8.7 2.7 9.1 2.8 9.9 656 18.2 9.8 14.6 14.9 14.9 14.9 14.9 14.9 14.9 14.9 14.9	6.6 4.7 4.8 6.8 6.8 6.8 6.8 6.8 6.8 6.8 6.8 6.8 6	3.2 9.6	5.8	10.1	и Г.		۳,		. 054	4.2	.074	18.3	5. 6	15.8	<b>4</b> .
5.8 1.8 6.2 1.9 4.1 1.3 4.9 1.5 2.0 .035 2.0 .035 11.6 11.6 11.8 3.0 8.7 2.9 9.8 13.7 10.9 2.7 8.7 2.7 8.1 2.8 9.0 2.7 8.7 2.7 8.1 2.8 9.0 2.5 9.6 14.6 14.0 14.0 14.0 14.0 14.0 14.0 14.0 14.0	5.8 6.6 7.0 7.0 9.1 9.1 9.1 9.1 9.1 9.1 9.1 9.1	3.0 1.0	ij	3.8	-:		.4		. 046	9.	. 028	9.S	2.8	6.3	<del>-</del>
9.8 3.9 9.7 2.9 9.5 2.9 9.7 2.9 3.4 .059 4.1 .072 16.0 4.7 2.6 10.9 3.3 7.8 2.4 9.1 2.8 2.3 .041 3.3 .058 13.7 4.0 2.1 8.3 2.5 8.0 2.4 9.1 2.8 2.5 .041 3.3 .058 14.6 4.6 4.1 2.8 9.0 2.7 8.7 2.7 9.1 2.8 3.2 .056 3.8 .066 18.2 4.1 2.5 7.2 2.2 6.0 1.8 6.7 2.0 2.9 .056 3.8 .066 18.2 4.1 3.1 10.9 3.3 7.6 2.3 8.7 2.7 3.1 .054 3.6 .063 13.4 4.6 4.7 8.9 2.1 2.6 .8 5.0 1.5 2.3 .040 1.9 .033 12.1 3.1 1.6 2.7 8.7 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0	9.8 7.0 7.0 9.1 9.1 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1	•	1.3	4.9	5.5		•		. 035	5.0	. 035	1.6	ы. Б	<b>.</b>	2.7
8.4 2.6 10.9 3.3 7.8 2.4 9.1 2.8 2.3 .041 3.3 .058 13.7 7.0 2.1 66.3 2.5 8.0 2.5 8.2 2.5 2.5 .043 3.3 .058 14.6 9.1 2.8 9.0 2.7 8.7 2.7 9.1 2.8 5.2 2.5 .043 3.3 .058 14.6 14.6 1.1 2.5 7.2 2.2 6.0 1.8 6.7 2.0 2.9 .056 3.8 .066 18.2 10.1 2.5 7.2 2.2 6.0 1.8 6.7 2.0 2.0 .056 2.5 .044 14.0 10.1 3.1 10.9 3.3 7.6 2.3 8.7 2.7 3.1 .054 3.6 .063 13.4 14.0 1.5 2.3 .049 1.9 .033 12.1 2.0 1.8 2.4 5.3 1.6 2.0 2.0 2.0 2.2 .038 12.3 2.2 2.0 2.0 2.2 .038 12.3 2.2 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0	7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0	•	<b>5.8</b>	6.7	5.8		-,		. 059	<del>-</del> -	. 072	16.9	<b>6. 4</b>	13.5	<del>-</del> -
7.0 2.1 6.3 2.5 8.0 2.5 8.2 2.5 2.5 .043 3.3 .058 14.6 9.1 2.8 9.0 2.7 8.7 2.7 9.1 2.8 5.2 .056 3.8 .066 18.2 6.1 2.5 7.2 2.2 6.0 1.8 6.7 2.0 2.9 .056 2.5 .044 14.0 16.1 3.1 10.9 3.3 7.6 2.3 8.7 2.7 3.1 .054 3.6 .063 13.4 5.4 1.7 6.9 2.1 2.6 .8 5.0 1.5 2.3 .049 1.9 .033 12.1 6.1 1.9 2.7 6.0 2.3 .049 1.9 .033 12.1 6.1 1.9 2.7 6.0 2.0 0.0 2.0	7.0 9.1 9.1 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1	2	7.7	<b>.</b>	2.8		~		.041	J. J	. 058	13.7	4.2	11.2	4.6
9.1 2.8 9.0 2.7 8.7 2.7 9.1 2.8 3.2 .056 3.8 .066 18.2 8.1 2.5 7.2 2.2 6.0 1.8 6.7 2.0 2.9 .056 2.5 .044 14.0 10.1 3.1 10.9 3.3 7.6 2.3 8.7 2.7 3.1 .054 3.6 .063 13.4 2.4 1.7 6.9 2.1 2.6 .8 5.0 1.5 2.3 .040 1.9 .033 12.1 8.1 1.9 2.7 8.2 4.5 5.3 1.6 2.0 0.035 2.2 0.03 12.3 8.1 1.9 2.7 8.2 4.5 5.3 1.6 2.0 0.035 2.2 0.038 12.3 12.3 12.3 12.3 12.3 12.3 12.3 12.3	9.1 2.8 9.9 16.1 2.5 7.2 16.1 3.1 16.9 6.1 1.9 6.9	2.5 8.0	2.5	8.2	2.5		.4		.043	3.3	. 058	14.6	4.5	12.0	3.7
8.1 2.5 7.2 2.2 6.0 1.8 6.7 2.0 2.9 .050 2.5 .044 14.0 4.0 10.1 3.1 10.9 3.3 7.6 2.3 8.7 2.7 3.1 .054 3.6 .063 13.4 4.0 1.7 6.9 2.1 2.6 .8 5.0 1.5 2.3 .040 1.9 .033 12.1 6.1 1.9 2.7 8 2.4 5.3 1.6 2.0 2.0 2.0 2.0 2.0 2.1 2.3 6.4 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0	6.1 2.5 7.2 16.1 3.1 16.9 5.4 1.7 6.9 6.1 1.9 2.7	2.7 8.7	2.7		2.8		Γ,		.056	3.8	.066	18.2	5. 5.	15.8	<b>4</b> .
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5.4 1.7 6.9 2.1 2.6 .8 5.9 1.5 2.3 .040 1.9 .033 12.1 6.1 1.9 2.7 .8 7.8 2.4 5.3 1.6 2.0 .035 2.2 .038 12.3 8.5 8.5 8.5 8.5 8.5 8.5 8.5 8.5 8.5 8.5	5.4 1.7 6.9 6.1 1.9 2.7	2	2.3	8.7	2.7		۳,	-	.054	3.6	. 063	13.4	<b>-∵</b>	10.8	3.3
6.1 1.9 2.7 .8 7.8 2.4 5.3 1.6 2.0 .035 2.2 .038 12.3 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	6.1 1.9 2.7 .6	<del>-</del> :	æ.	5.0	1.5		~	r.	. 640	<b>6</b> .	. 033	12.1	3.7	9.6	5.8
8 4 7 8 8 4 1 9 8 6 7 9 8 4 1 9 8 9 7 9 8 9 8 9 1 9 8 9 8 9 1 9 9 9 9 9 9 9 9	** ** ** **	.8 7.8	7.4	5.3	9.		~	•	.035	2.5	. 038	12.3	3.7	9.7	2.9
		1.6		7	9				929	2.6	.045	11.0	4.5	4.8	2.6

Mark   Mark	990			AIMCAN	•		}												
4/5         4/5 <th></th> <th>2</th> <th>SE</th> <th>8</th> <th>RT</th> <th>S</th> <th>8</th> <th>¥</th> <th>•</th> <th>FREE-FI</th> <th>CIGHT</th> <th>8</th> <th>*</th> <th>б</th> <th><b>≥</b></th> <th>8</th> <th>RAMP</th> <th>OVER RAMP</th> <th>RAMP</th>		2	SE	8	RT	S	8	¥	•	FREE-FI	CIGHT	8	*	б	<b>≥</b>	8	RAMP	OVER RAMP	RAMP
2.3         2.4         2.5         2.6         2.7         2.8         3.9         3.1         3.2         3.8         3.5         3.6         3.7         3.6         3.6         3.7         3.6         3.7         3.6         3.7         3.6         3.7         3.6         3.7         3.6         3.7         3.6         3.7         3.6         3.7         3.6         3.7         3.6         3.7         3.6         3.7         3.6         3.7         3.6         3.7 <th></th> <th>5/2</th> <th>Ş</th> <th>23</th> <th>Ş</th> <th>2</th> <th>K/S</th> <th><b>F/S</b></th> <th>N/S</th> <th>F/S</th> <th>M/S</th> <th>DEG</th> <th>3</th> <th>DEG</th> <th>2</th> <th>E</th> <th>3</th> <th>E</th> <th>3</th>		5/2	Ş	23	Ş	2	K/S	<b>F/S</b>	N/S	F/S	M/S	DEG	3	DEG	2	E	3	E	3
9.9         3.6         1.9         2.9         2.7         .046         2.6         .045           5.1         1.6         4.9         1.1         6.2         1.9         2.7         .046         2.6         0.4           6.6         2.9         9.4         2.9         5.2         1.6         7.1         2.2         6.4         1.9         2.4         .045         3.1         .055         2.5         .043           6.6         2.9         9.4         2.9         5.2         1.6         7.1         2.2         6.4         1.9         2.4         .045         3.1         .055         3.1         .055         3.1         .055         3.1         .055         3.2         .055         3.2         .055         3.1         .055         3.2         .055         3.2         .055         3.2         .055         3.2         .055         3.2         .055         3.2         .055         3.2         .055         3.2         .055         3.2         .055         3.2         .055         3.2         .055         3.2         .055         3.2         .055         3.2         .055         3.2         .055         3.2         .055         3.2<	~	23	34	22	<b>38</b>	23	28	<b>53</b>	30	5	32	33	ň	25	36	37	82	39	6
7.8         2.4         4.8         1.5         7.4         2.3         6.1         1.8         4.6         1.6         2.5         6.4         2.5         6.6         2.5         6.6         2.5         6.6         2.5         6.6         2.6         6.7         6.6         2.5         6.6         2.6         6.6         2.6         3.1         6.6         2.6         3.1         6.6         2.6         3.2         6.6         3.2         3.2         6.6         3.2         3.2         3.2         3.2         3.2         3.2         3.2         3.2         3.2         3.2         3.2         3.2         3.2         3.2         3.2         3.2 <th>_</th> <td>6.0</td> <td>3.0</td> <td><b>.</b> •</td> <td>9.9</td> <td>3.6</td> <td>-:</td> <td>6.2</td> <td>9.1</td> <td></td> <td></td> <td>2.7</td> <td>.048</td> <td>2.6</td> <td>.045</td> <td>9.6</td> <td>2.9</td> <td>7.0</td> <td>2.1</td>	_	6.0	3.0	<b>.</b> •	9.9	3.6	-:	6.2	9.1			2.7	.048	2.6	.045	9.6	2.9	7.0	2.1
5.1         1.6         4.9         1.5         4.6         1.4         4.6         1.4         2.3         3.0         3.0         1.8         5.0         9.0 <th></th> <td>7.8</td> <td>7.4</td> <td>4.0</td> <td>5.5</td> <td>7.4</td> <td>2.3</td> <td><b>.</b></td> <td><b>8</b>.</td> <td></td> <td></td> <td>J.1</td> <td>. 055</td> <td>2.5</td> <td>.043</td> <td>12.5</td> <td>3.8</td> <td>9.7</td> <td>3.0</td>		7.8	7.4	4.0	5.5	7.4	2.3	<b>.</b>	<b>8</b> .			J.1	. 055	2.5	.043	12.5	3.8	9.7	3.0
6.6 2.0 9.4 2.9 5.2 1.6 7.1 2.2 6.4 1.9 2.4 .042 5.0 .055 6.1 1.054 6.6 2.0 10.1 2.0	_	5.1	1.6	4.0	1.5	4.5	+:-	<b>4</b> .6	<b>+</b> .	4.6	<b>+</b> :	2.3	. 039	<b>8</b> .	. 032	13.0	4.0	10.8	3.3
9.1         2.8         7.5         2.3         9.2         2.4         3.2         .055         3.1         .064         3.2         .065         3.1         .064         3.2         .065         3.1         .064         3.2         .065         3.1         .065         3.1         .065         3.1         .065         3.1         .065         3.2         3.2	•	9.9	2.0	4.0	5.9	5.5	9.	7.1	2.5	4.9	9.	7.7	. 942	3.0	. 053	12.7	3.9	6.6	g.6
6.6         2.0         10.1         3.1         6.9         2.1         8.4         2.6         6.6         5.2         6.0         5.2         6.0         5.2         6.0         5.2         6.0         5.2         6.0         5.2         5.2         5.2         5.2         6.0         5.2         6.0         5.2         5.0         6.0         5.2         6.0         5.0         6.0         5.2         6.0         5.2         6.0         5.2         6.0         5.2         6.0         5.2         6.0         5.2         6.0         5.0         6.0         5.2         6.0         5.0         6.0         5.2         6.0         5.0         6.0 <th>_</th> <td>9.1</td> <td>2.8</td> <td>7.5</td> <td>2.3</td> <td>8.2</td> <td>2.5</td> <td>7.8</td> <td>2.4</td> <td></td> <td></td> <td>3.2</td> <td>.056</td> <td>3.1</td> <td>. 054</td> <td>13.3</td> <td><del>-</del></td> <td>10.9</td> <td>3.3</td>	_	9.1	2.8	7.5	2.3	8.2	2.5	7.8	2.4			3.2	.056	3.1	. 054	13.3	<del>-</del>	10.9	3.3
14.6         4.5         11.1         3.4         16.1         4.9         13.7         4.2         4.3         .076         5.4         .096           7.7         2.3         8.7         2.7         8.6         2.1         8.3         2.5         3.1         .065         3.2         .095           7.7         2.3         8.6         2.4         7.5         2.3         3.2         .065         3.2	_	6.6	5.0	19.1	 	<b>6</b> .0	2.1	4.6	5.6			2.6	.045	3.2	.056	12.2	3.7	<b>8</b> .6	2.7
7.5         2.3         8.7         2.7         6.8         2.1         8.3         2.5         3.1         .054         3.4         .069           7.7         2.3         8.1         2.5         8.6         2.9         3.1         .055         3.2         .055           7.8         1.5         3.9         1.5         4.1         1.3         2.4         .042         3.2         .055           7.1         2.2         2.7         3.5         2.3         3.9         2.6         6.6           7.1         2.0         2.7         3.2         2.2         3.3         .062         3.2         .055           6.7         2.0         7.2         2.2         7.4         .054         2.9         .055         3.2         .065         3.2         .065         3.2         .065         3.2         .065         3.2         .065         3.2         .065         3.2         .065         3.2         .065         3.3         .065         3.3         .066         3.3         .066         3.3         .066         3.3         .066         3.3         .066         3.3         .066         3.3         .066         3.3         .066	_	4.0	4.5	1.1	4.5	16.1	<b>6</b> .	13.7	4.2			<b>4</b> .4	.076	5.4	. 095	15.4	4.7	1.8	3.6
7.7         2.3         8.1         2.5         8.6         2.4         7.5         2.3         3.1         665         3.2         6.6         4.6         2.4         6.7         3.3         6.9         2.4         7.5         2.3         3.1         665         3.2         6.05         3.2         3.2         6.05         3.2         3.2         6.05         3.2         3.2         3.2         6.05         3.2         3.2         3.2         3.2         3.2         3.2         3.2         3.2         3.2         3.2         3.2         3.2         3.2         3.2         3.2         3.2         3.2         3.	_	7.5	2.3	8.7	2.7	<b>9</b> .9	2.1	B. 3	2.5			J. 7	.054	4.5	.060	17.1	5.5	14.5	+.+
7.6         2.1         9.6         2.6         7.5         2.3         3.6         .652         3.2         .665         3.2 </td <th>•</th> <td>7.7</td> <td>2.3</td> <td> </td> <td>2.5</td> <td><b>9</b>.0</td> <td>5.6</td> <td><b>8</b>.3</td> <td>2.5</td> <td></td> <td></td> <td>3.1</td> <td>.055</td> <td>3.5</td> <td>.057</td> <td>20.5</td> <td>6.2</td> <td>18.2</td> <td>5.5</td>	•	7.7	2.3	 	2.5	<b>9</b> .0	5.6	<b>8</b> .3	2.5			3.1	.055	3.5	.057	20.5	6.2	18.2	5.5
4.8         1.5         3.9         1.2         4.9         1.5         3.9         1.6         6.2         9.9         9.5         9.9         9.6         9.9         9.9         9.6         9.9 <th>_</th> <td>7.0</td> <td>2.1</td> <td><b>9</b>.6</td> <td><b>5</b>.8</td> <td><b>9</b>.0</td> <td><b>5. 4</b></td> <td>7.5</td> <td>2.3</td> <td></td> <td></td> <td>3.0</td> <td>. 052</td> <td>3.2</td> <td>. 055</td> <td>14.0</td> <td>4.4</td> <td>11.2</td> <td>4.6</td>	_	7.0	2.1	<b>9</b> .6	<b>5</b> .8	<b>9</b> .0	<b>5. 4</b>	7.5	2.3			3.0	. 052	3.2	. 055	14.0	4.4	11.2	4.6
9.0         2.7         10.7         3.3         6.9         2.7         9.6         2.9         3.9         .053         3.8         .066           6.7         2.2         7.4         2.2         7.4         2.2         3.3         .056         2.6         3.9         .055         3.3         .056         2.9         .055         3.3         .056         2.9         .055         3.3         .056         2.9         .056         3.3         .056         2.9         .056         3.3         .056         2.9         .056         3.3         .056         2.9         .056         .056         3.3         .056         .056         3.3         .056         .056         3.3         .056         .056         3.1         .056         .056         3.1         .056         .056         3.3         .066         3.3         .066         3.3         .066         3.3         .066         3.3         .066         3.3         .066         3.3         .066         3.3         .066         3.3         .066         3.3         .066         3.3         .066         3.3         .066         3.3         .066         3.3         .066         3.3         .066         3.3	_	4.8	 5:	d.0	1.2	<b>6</b> .	5.	<del>-</del>	J.3			2.4	. 042	 6.	. 029	12.1	3.7	9.5	2.9
7.1         2.2         6.9         2.1         7.2         2.2         7.4         2.2         3.3         .056         2.6         .045           4.9         1.5         5.4         1.5         2.3         3.3         .056         2.6         .045           4.9         1.5         5.4         9.4         2.9         3.4         .053         2.1         .056           9.3         2.6         1.6         4.9         1.5         2.7         .047         3.6         .052           9.6         1.8         2.7         9.7         3.9         2.7         .047         3.6         .062           9.6         1.8         3.2         9.4         2.9         3.4         .053         3.1         .057         .064         3.1         .055         9.6         9.7         .056         9.7         9.	_	•	2.7	10.7	3.3	8.8	2.7	9.6	2.9			3.0 0.0	.053	S. S	. 966	12.6	а. В	10.0	J. 0
6.7 2.6 7.6 2.1 6.2 1.9 7.5 2.3 3.1 6.54 2.9 .051 2.9 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5	~	7.1	2.5	<b>0</b> .	2.1	7.2	2.5	7.4	2.2			n.	.058	5.6	.043	13.2	4.0	10.7	رن دن
4.9         1.5         5.4         1.6         5.6         1.7         2.4         9.45         2.1         9.35         2.1         9.35         2.1         9.35         2.1         9.35         2.1         9.35         2.1         9.35         9.45         2.9         3.4         9.69         3.2         1.0         4.9         1.2         9.7         3.0         9.57         3.6         9.65         9.7         3.0         9.65         3.7         9.65         9.65         9.7         3.0         9.7         9.6         9.6         9.7         3.0         9.7         9.6         9.65         3.7         9.6         9.65         3.7         9.6         9.65         3.7         9.6         9.6         3.7         9.6         9.6         3.7         9.6         9.6         3.0         9.6         3.0         9.6         9.6         9.6         9.7         9.6         9.6         9.7         9.6         9.6         9.6         9.7         9.6         9.6         9.7         9.6         9.6         9.7         9.6         9.6         9.7         9.6         9.6         9.7         9.6         9.6         9.7         9.6         9.6         9.7	_	6.7	7.0	7.0	2.1	6.2	<b>o</b> .	7.5	2.3			٠. ا	.054	6.9	.051	22.4	<b>8</b> .9	9.8	<b>9</b>
9.3         2.8         10.3         3.1         8.8         2.7         3.9         2.7         3.6         3.6         3.6         3.6         3.6         3.6         3.6         3.6         3.6         3.7         3.6         3.6         3.7         3.6         3.6         3.7         3.6         3.6         3.7         3.6         3.7         3.6         3.7         3.7         3.7         3.6         3.7         3.7         3.6         3.7         3.7         3.7         3.6         3.7         3.7         3.7         3.6         3.7         3.7         3.6         3.7         3.7         3.6 <th></th> <td>6.4</td> <td>- .5</td> <td>4.0</td> <td><b>•</b></td> <td>•</td> <td> S:</td> <td>5.6</td> <td>1.7</td> <td></td> <td></td> <td>7.4</td> <td>.043</td> <td>2.1</td> <td>.036</td> <td>- -</td> <td>4.6</td> <td>80 10.</td> <td>5.6</td>		6.4	- .5	4.0	<b>•</b>	•	 S:	5.6	1.7			7.4	.043	2.1	.036	- -	4.6	80 10.	5.6
8.6         2.6         19.7         3.3         8.4         2.9         3.4         2.9         3.7         964         3.7         964         3.7         964         3.7         964         3.7         964         3.7         965         3.7         965         3.7         965         3.7         965         3.7         965         3.7         965         3.7         965         3.7         965         3.7         965         3.7         965         3.7         965         3.7         965         3.7         965         3.7         965         3.7         965         3.7         965         3.7         965         3.7         965         3.7         966         3.7         966         3.7         966         3.7         966         3.7         966         3.7         966         3.7         3.8         3.7         3.8         3.7         3.8         3.8         3.7         3.8         3.8         3.7         3.8         3.8         3.7         3.8         3.8         3.8         3.8         3.8         3.8         3.8         3.8         3.8         3.8         3.8         3.8         3.8         3.8         3.8         3.8         3.8 <th></th> <td>D. G</td> <td>7.8 7.8</td> <td>7.0</td> <td></td> <td><b>6</b></td> <td>2.7</td> <td>2.7</td> <td><b>6</b></td> <td></td> <td></td> <td>2.7</td> <td>.047</td> <td>ופו</td> <td>.962</td> <td>13.8</td> <td>7.5</td> <td>2.5</td> <td></td>		D. G	7.8 7.8	7.0		<b>6</b>	2.7	2.7	<b>6</b>			2.7	.047	ופו	.962	13.8	7.5	2.5	
6.5 2.6 6.5 2.6 6.5 2.8 6.5 2.6 6.7 3.0 5.7 5.1 5.0 5.2 5.1 5.0 5.2 5.1 5.0 5.2 5.1 5.0 5.2 5.1 5.0 5.2 5.1 5.0 5.2 5.1 5.0 5.2 5.1 5.0 5.2 5.1 5.0 5.2 5.2 5.2 5.2 5.2 5.2 5.2 5.2 5.2 5.2			5 7 9	7.9	, ,		7.4	4.0	8.4			٠ • •	80. 61.	· ·	499.	 		 	÷ c
6.6       1.6       4.4       1.5       4.7       1.4       4.6       1.4       2.2       0.36       1.7       0.35         7.6       2.3       7.9       2.7       1.4       6.2       2.5       2.7       0.47       3.2       0.65         8.3       1.9       4.7       1.4       6.2       2.5       1.6       2.7       0.47       3.2       0.65         8.3       1.9       4.7       1.4       6.2       1.6       3.9       3.5       0.66       4.1       0.71         8.6       2.1       5.2       1.6       2.2       2.7       0.49       2.9       0.95         8.6       2.4       6.5       2.1       7.2       2.2       2.4       0.45       3.9       0.65       3.9       0.65         8.4       1.7       7.6       2.3       5.6       1.6       7.1       2.2       2.2       0.98       3.9       0.65       3.9       0.65       3.9       0.65       3.9       0.65       3.9       0.65       3.9       0.65       3.9       0.65       3.9       0.65       3.9       0.65       3.9       0.65       3.9       0.65       3.9				) «		7 0						4 F	5.50	- e	6 6 7	- 17	•	4 6	
7.6         2.3         7.9         2.4         9.6         2.7         6.2         2.5         2.7         .047         3.2         .055           9.8         3.9         2.7         10.6         3.6         3.6         4.1         .071           6.3         1.9         4.7         1.4         6.2         1.9         5.2         1.6         2.3         .046         2.0         .035           6.8         2.1         5.2         1.9         5.2         1.6         2.3         .046         2.0         .035           7.8         2.4         6.3         2.5         1.3         4.1         1.2         2.4         .043         1.6         .028           6.4         2.7         7.6         2.7         7.4         2.2         2.4         .043         1.6         .055           6.4         2.7         7.2         2.2         2.2         2.2         .048         2.9         .058           6.4         2.3         2.5         10.3         3.1         .055         2.8         .068           8.9         2.7         7.9         2.4         6.5         2.9         7.4         2.2         3.6 <th></th> <td></td> <td>-</td> <td>4</td> <td></td> <td></td> <td>*</td> <td>. 4</td> <td>*</td> <td></td> <td></td> <td>2.5</td> <td>638</td> <td>1.7</td> <td>929</td> <td>9.</td> <td>3.5</td> <td>6</td> <td>2.7</td>			-	4			*	. 4	*			2.5	638	1.7	929	9.	3.5	6	2.7
9.8         3.9         19.8         3.3         8.8         2.7         16.9         3.9         3.5         .060         4.1         .071           6.3         1.9         4.7         1.4         6.2         1.3         4.1         1.2         2.3         .040         2.9         .058           7.8         2.1         5.6         1.7         4.2         1.3         4.1         1.2         2.4         .043         1.6         .028           8.6         2.4         8.3         2.7         7.6         2.3         8.6         2.4         .043         1.6         .052           8.6         2.4         8.3         2.7         7.6         2.3         8.6         2.4         .053         3.9         .056           8.4         2.2         5.1         1.6         7.2         2.2         3.2         .043         3.9         .053           8.9         2.7         7.9         2.4         6.5         2.9         7.4         2.2         8.6         2.7         .041         2.7         .042           8.9         2.7         3.2         8.4         1.8         7.5         2.2         8.6         2.7 </td <th></th> <td>7.6</td> <td>2.3</td> <td>7.9</td> <td>2.4</td> <td>0.</td> <td>2.7</td> <td>8.2</td> <td>2.5</td> <td></td> <td></td> <td>2.7</td> <td>.047</td> <td>3.2</td> <td>.055</td> <td>8.8</td> <td>2.7</td> <td>6.9</td> <td><b>6</b>.</td>		7.6	2.3	7.9	2.4	0.	2.7	8.2	2.5			2.7	.047	3.2	.055	8.8	2.7	6.9	<b>6</b> .
6.3 1.9 4.7 1.4 6.2 1.9 5.2 1.6 2.3 .040 2.0 0.035   6.8 2.1 5.6 1.7 4.2 1.3 4.1 1.2 2.4 .043 1.6 .028   7.8 2.4 6.3 2.5 7.0 2.1 7.4 2.2 2.1 .037 2.9 .050   8.6 2.6 9.0 2.7 7.6 2.3 8.0 2.4 2.2 2.1 .037 2.9 .050   6.4 2.0 6.1 2.3 5.1 1.6 7.2 2.2 2.2 2.2 0.38 3.0 .053   6.4 2.0 6.1 2.3 2.5 1.0 7.4 2.2 2.2 3.0 .052 2.8 .045   10.6 3.2 12.2 3.7 8.3 2.5 10 7.4 2.2 8.6 2.6 3.1 .054 2.7 .047   12.2 3.7 13.8 4.2 9.5 2.9 11.6 3.5 3.6 .052 3.9 .065   8.0 2.4 8.3 2.5 6.4 1.9 7.3 2.2 8.6 2.5 .044 2.9 .051   8.0 2.4 7.0 2.4 6.5 2.0 7.6 2.3   5.0 1.8 8.4 2.5 4.2 1.3 5.8 1.8 2.5 .044 2.9 .051   8.0 2.4 7.0 2.4 6.5 2.0 7.6 2.3 2.7 .048 3.1 .055   9.0 2.4 7.0 2.3 7.5 2.2 7.6 2.3 2.7 .048 3.7 .048   9.0 2.6 7.8 2.3 7.5 2.3 7.5 2.5 2.9 .055 3.1 .055   9.0 2.8 7.8 2.4 7.2 2.2 7.6 2.3 3.0 .055 2.9 .055   9.0 2.8 7.8 2.4 7.2 2.2 7.6 2.3 3.0 .055 2.4 .041   9.0 2.8 7.8 2.4 7.2 2.2 7.6 2.3 3.0 .055 2.4 .041   9.0 2.8 7.8 2.4 7.2 2.2 7.6 2.3 3.0 .055 2.4 .041   9.0 2.8 7.8 2.4 7.2 2.2 7.6 2.3 3.0 .055 2.4 .041   9.0 2.8 7.8 2.4 7.5 2.1 5.8 1.8 2.5 2.5 2.8 .055 2.4 .041		9.8	3.0	10.8	3.3	8.8	2.7	10.0	3.0			3.5	990.		.071	13.7	4.2	11.3	4.6
6.8 2.1 5.6 1.7 4.2 1.3 4.1 1.2 2.4 .043 1.6 .028 7.8 2.4 6.3 2.5 7.0 2.1 7.4 2.2 2.1 .037 2.9 .050 8.6 2.6 9.0 2.7 7.6 2.3 8.0 2.4 2.4 2.0 3.0 .052 3.0 .051 3.0 .052 3.0 .051 3.0 .05		6.3	<del>.</del>	4.7	<b>+</b> :	8.5	<u>.</u>	2.5	<b>9</b> .			2.3	.040	5.0	. 035	9.5	2.9	7.0	2.1
7.8         2.4         6.3         2.5         7.9         2.1         7.4         2.2         2.1         .650         2.9         .650           6.6         2.6         2.7         7.6         2.3         5.9         2.4         3.9         .653         3.9         .652           5.4         1.7         7.6         2.3         5.1         1.6         7.2         2.2         3.9         .653         3.9         .653           6.4         2.9         5.6         1.6         7.1         2.2         3.0         .652         2.9         .653           10.6         3.2         2.4         6.5         2.6         3.1         .652         2.9         .668           2.0         2.7         3.9         3.1         .654         2.7         .647         2.7         .647         2.7         .647         2.7         .647         2.7         .647         2.7         .647         2.9         .668         2.9         3.6         .651         2.9         .668         2.9         3.6         .647         2.9         .644         2.9         .644         2.9         .644         2.9         .644         2.9         .644		8.8	2.1	3. <b>6</b>	1.7	4.2	1.3	<del>-</del> -	1.2			2.4	.043	÷.	. 028	16.2	4.0	13.5	÷.
8.6         2.6         9.9         2.7         7.6         2.3         8.9         2.4         3.9         .953         3.9         .953         3.9         .953         5.9         .953         3.7         .944         2.9         .951         .951         .951         .951         .951         .951         .951         .951         .952         .953         .953         .953         .953         .953         .953         .953         .952         .953         .952         <		7.8	7.4	8.3	2.5	7.0	2.1	7.4	2.5			2.1	. 037	5.8	. 050	12.3	3.7	<b>8</b> .	ъ. Э.
5.4 1.7 7.6 2.3 5.1 1.6 7.2 2.2 2.8 39 3.6 .053 3.6 .053 3.6 .053 3.6 .053 3.6 .053 3.6 .053 3.6 .053 3.6 .053 3.6 .053 3.6 .053 3.7 8.3 2.5 16.3 3.1 2.2 2.8 .045 2.9 .068 2.7 7.9 2.4 6.5 2.9 11.6 3.5 3.1 .054 2.7 .047 2.9 11.6 3.5 2.4 11.6 3.5 2.4 11.8 2.4 2.5 1.3 5.8 1.8 2.5 2.8 .044 2.9 .051 5.9 1.8 2.4 7.9 2.4 6.5 2.9 1.8 2.5 2.9 1.8 2.5 2.9 1.6 2.7 .044 2.9 .051 5.9 1.8 2.4 2.5 2.9 1.8 2.7 .044 2.9 .051 5.9 1.8 2.4 2.5 2.9 2.9 1.8 2.7 .048 4.7 .003 5.4 1.6 5.7 1.7 3.2 1.9 4.4 1.4 2.9 2.7 .048 4.7 .003 5.9 1.5 7.7 2.3 7.5 2.3 7.9 2.4 8.2 2.5 2.9 .059 3.1 .055 5.9 1.5 7.7 2.3 7.5 2.2 7.6 2.3 3.9 2.6 2.8 .045 2.9 .051 5.9 2.9 2.9 2.9 2.9 2.9 2.9 2.9 2.9 2.9 2		9.0	5.6	•	2.7	7.8	2.3	8.0	7.4			8. 8.	. 853	9.0	.052	13.1	<b>4</b> .0	4.6	3.2
6.4 2.6 6.1 2.5 5.6 1.6 7.1 2.2 3.8 .632 2.8 .848 19.6 5.2 12.2 3.7 8.3 2.5 16.3 3.1 5.6 3.1 6.5 2.8 .848 19.6 5.2 12.2 3.7 8.3 2.5 16.3 3.1 5.6 3.1 6.5 2.9 .868 12.2 3.7 13.8 4.2 9.5 2.9 11.6 3.5 3.5 3.6 .862 4.3 .876 15.9 1.8 8.3 2.5 6.4 1.9 7.3 2.2 2.5 .844 2.9 .851 5.9 1.8 8.4 2.5 2.4 7.3 2.5 8.4 2.5 .844 2.9 .851 5.9 1.8 8.4 2.5 2.4 8.5 2.4 8.5 2.9 1.8 2.4 8.5 2.7 8.4 2.4 8.4 2.5 2.9 1.8 2.4 2.5 2.9 1.8 2.7 8.4 2.7 8.4 2.4 8.4 2.5 2.9 1.8 2.7 8.4 2.7 8.3 2.7 8.5 8.1 8.5 2.9 1.8 2.7 8.5 8.1 8.5 2.9 1.8 2.7 8.5 8.1 8.5 2.9 8.5 8.1 8.5 8.1 8.5 8.1 8.5 8.1 8.5 8.1 8.5 8.1 8.5 8.1 8.5 8.1 8.5 8.1 8.5 8.1 8.5 8.1 8.5 8.1 8.5 8.1 8.5 8.1 8.5 8.1 8.5 8.1 8.5 8.1 8.5 8.1 8.1 8.5 8.1 8.1 8.1 8.1 8.1 8.1 8.1 8.1 8.1 8.1		4.0	1.7	7.6	7. 7.	 	•	7.2	7.5			2.2	.038	<b>8</b> .0	. 65	15.3	4.7	12.5	
19.6     3.2     12.2     3.7     6.3     2.5     10.3     3.1     3.9     .952     3.9     .966       12.2     3.7     13.6     6.5     2.9     17.4     2.2     8.6     2.6     3.1     .964     2.7     .947       12.2     3.7     13.6     1.6     3.5     2.6     4.3     1.9     7.3     2.7     .944     2.9     .951       5.9     1.8     2.4     2.5     2.9     7.6     2.3     2.7     .948     2.4     .941       5.9     1.8     2.4     3.5     2.9     7.6     2.3     2.7     .948     4.7     .941       5.9     1.6     3.7     2.9     3.3     2.7     .948     4.7     .943       5.4     1.6     3.7     3.2     1.9     4.4     1.4     2.9     .948     4.7     .983       5.9     1.5     7.7     2.3     7.9     2.4     8.2     2.5     2.9     .959     3.1     .955       5.9     1.5     7.7     2.3     7.9     2.4     8.2     2.5     2.9     .956     3.1     .955       9.0     2.6     2.7     2.7     2.7     2.7 <t< td=""><th>•</th><td>4.</td><td>7.0</td><td><b>9</b></td><td>2.5</td><td>10 (</td><td><b>-</b> (</td><td>7.1</td><td>2.2</td><td></td><td></td><td>۵. و</td><td>.052</td><td>2.8</td><td>. 649</td><td>2. 2. 6</td><td><b>*</b> (</td><td>2.5</td><td><b>⊕</b> •</td></t<>	•	4.	7.0	<b>9</b>	2.5	10 (	<b>-</b> (	7.1	2.2			۵. و	.052	2.8	. 649	2. 2. 6	<b>*</b> (	2.5	<b>⊕</b> •
12.2       3.7       13.8       4.2       9.5       2.9       11.6       3.5       3.6       962       4.3       975         12.9       2.4       1.3       1.6       3.5       1.6       2.5       944       2.9       .045         5.9       1.8       2.5       2.2       2.5       .044       2.9       .045         5.9       1.8       2.5       2.9       7.6       2.3       2.7       .048       2.4       .041         6.0       2.4       7.9       2.4       1.6       2.7       .048       4.7       .083         5.4       1.6       5.7       1.7       3.5       9.1       2.4       1.4       2.9       2.7       .048       4.7       .083         5.4       1.6       5.7       1.7       2.3       7.9       2.4       8.2       2.5       2.9       .056       3.1       .055         5.9       1.5       7.7       2.3       7.5       2.3       7.9       2.4       8.2       2.5       2.9       .056       3.1       .055         6.6       2.9       7.7       2.2       7.6       2.3       3.6       .055       3.	_	9 6	 	7.7	· ·		. · ·	. P		•	•	) r	200. 45.4	, c	000.		, r	, T	. 7
6.6       2.4       6.4       1.9       7.3       2.2       2.5       .044       2.9       .051         5.9       1.8       6.4       2.5       4.2       1.3       5.8       1.8       2.7       .044       2.4       .041         5.9       1.8       2.4       7.6       2.3       2.7       .048       4.7       .041         9.5       2.9       1.6       2.3       2.9       7.6       2.3       2.7       .048       4.7       .083         5.4       1.6       5.7       1.7       3.2       1.9       4.4       1.4       2.9       2.9       .083       1.7       .030         5.9       1.5       7.7       2.3       7.5       2.3       7.9       2.4       8.2       2.5       2.9       .056       3.1       .055         5.9       7.6       2.3       7.6       2.3       7.6       2.3       7.6       2.9       .056       3.1       .055       3.2       .056         9.0       2.8       7.8       2.4       7.7       2.2       7.6       2.3       3.6       .055       3.2       .056       2.4       .041       2.6       2.	•	,				) u		: =	1 K	) )	;	•	962		978	. e	4	13.4	-
5.9 1.8 6.4 2.5 4.2 1.3 5.8 1.8 2.7 .044 2.4 .041 6.5 2.9 1.8 2.4 7.9 2.4 6.5 2.9 7.6 2.3 2.7 .048 3.1 .055 9.5 1.8 5.4 1.6 5.7 1.7 3.2 1.9 4.4 1.4 2.9 2.5 2.9 .055 1.7 .030 5.4 1.5 7.7 2.3 7.5 2.3 7.9 2.4 8.2 2.5 2.9 .056 3.1 .055 6.6 2.9 7.8 2.4 7.2 2.2 7.6 2.3 3.0 .055 3.2 .056 6.5 2.9 4.7 1.4 6.9 2.1 5.8 1.8 2.4 7.2 2.2 7.6 2.3 3.0 .055 2.4 .041	•		7.6		2.5	4	-	7.3	2.5			2.5	944	2.9	.051	11.2	4.6	8.7	2.7
6.0     2.4     7.6     2.3     2.7     .048     3.1     .055       9.5     2.9     11.6     3.5     9.1     2.8     10.9     3.3     2.7     .048     4.7     .083       5.4     1.6     5.7     1.7     3.2     1.0     4.4     1.4     2.0     .035     1.7     .030       5.0     1.5     7.7     2.3     7.5     2.3     7.9     2.4     8.2     2.5     2.9     .056     3.1     .055       6.6     2.0     7.6     2.3     5.6     1.7     6.5     2.9     2.8     .049     2.9     .051       9.0     2.8     7.8     2.4     7.2     2.2     7.6     2.3     3.0     .052     3.2     .056       6.5     2.0     4.7     1.4     6.9     2.1     5.8     1.8     2.6     .045     2.4     .041		9	-	4.6	2.5	4.2		8	<b>8</b>			2.5	110	7.4	140	16.8	5.1	14.8	4.5
9.5     2.9     11.6     3.5     9.1     2.8     10.9     3.3     2.7     .048     4.7     .083       5.4     1.6     5.7     1.7     3.2     1.0     4.4     1.4     2.0     .035     1.7     .030       5.0     1.5     7.7     2.3     7.5     2.3     7.9     2.4     8.2     2.5     2.9     .050     3.1     .055       6.6     2.0     7.6     2.3     5.6     1.7     6.5     2.9     2.8     .049     2.9     .051       9.0     2.8     7.8     2.4     7.2     2.2     7.6     2.3     3.0     .052     3.2     .056       6.5     2.0     4.7     1.4     6.9     2.1     5.8     1.8     2.6     .045     2.4     .041		9.0	7.4	7.9	2.4	6.5	2.0	7.6	2.3			2.7	. 648	J.1	. 055	15.7	4.8	13.3	÷.
5.4 1.6 5.7 1.7 5.2 1.0 4.4 1.4 2.0 2.0 .035 1.7 .030 15.0 1.5 2.0 1.5 2.0 2.5 2.0 2.5 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0		9.5	2.8	11.6	3.3		2.8	10.9	3.3			2.7	. 648	4.7	. 083	14.1	4.3	11.3	4.6
5.0 1.5 7.7 2.3 7.5 2.3 7.9 2.4 8.2 2.5 2.9 .050 3.1 .055 16.6 2.0 7.6 2.3 5.6 1.7 6.5 2.0 2.0 2.8 .049 2.9 .051 19.0 2.8 7.8 2.4 7.2 2.2 7.6 2.3 3.0 .052 3.2 .056 16.5 2.0 4.7 1.4 6.9 2.1 5.8 1.8 2.6 .045 2.4 .041		5.4	<b>9</b> .	5.7	1.7	3.5	<u>-</u>	<b>†</b> .	<del>*</del> :			2.0	. 035	1.7	. 030	12.4	3.8	10.2	J. 7
6.6 2.0 7.6 2.3 5.6 1.7 6.5 2.0 2.8 .049 2.9 .051 19.0 2.8 7.8 2.4 7.2 2.2 7.6 2.3 3.0 .052 3.2 .056 19.0 5.5 2.0 4.7 1.4 6.9 2.1 5.8 1.8 2.6 .045 2.4 .041	_	5.0	<del>.</del>	7.7	2.3	7.5	2.3	7.9	7.4	8.2	2.5	2.8	. 050	٠. ۲.	. 055	15.8	<b>4</b> .8	13.5	<b>+</b> .
9.0 2.8 7.8 2.4 7.2 2.2 7.6 2.3 3.0 .052 3.2 .056 1 6.5 2.0 4.7 1.4 6.9 2.1 5.8 1.8 2.6 .045 2.4 .041	_	6.6	2.0	7.6	2.3	5.6	1.7	6.5	2.0			2.8	.049	5.9	.051	18.1	5.5	15.6	<b>4</b> .8
6.5 2.0 4.7 1.4 6.9 2.1 5.8 1.8 2.6 .045 2.4 .041	_	•.	2.8	7.8	7.7	7.2	2.2	7.6	2.3			3.0	. 052	3.2	. 056	15.0	4.6	12.7	J. 9
		6.5	2.0	4.7	4.	<b>6</b> .0	2.1	S.8	1.8			2.6	.045	4.5	.041	<b>4</b> .0	<b>4</b> .4	9.=	ы Б.

USS ENTERPRISE (CVN-65)

DAY LAN
USS ENTERPRISE (CVN-63)
LANDING DATA - MODEL T-2C

		3	LANDING D	DATA -	- MODEL T-20	) - - -	5	SS ENTE	USS ENTERPRISE (CVN-65)	₹ (3	(c9			DAY L	DAY LANDINGS			
200			AIRCR	AFT SI	NKING SI	AIRCRAFT SINKING SPEED AT TOUCHDOWN	TOUCH	NO			GLIDE	GLIDE PATH ANGLE AT TD	NGLE /	T T0	WHEEL	WHEEL HEIGHT	HOOK HEIGHT	EIGH
2	MOSE	SE	PORT	RT	S	STBO	AVC	•	FREE-FLIGHT	IGHT	B) #	ŧ	8	>	OVER RALLP	RAMP	OVER RALL	RAMP
	Ş	Ş	2	Ş	5	Ş	F/S	K/S	F/S	K K	DEG	2	DEC	8	E	3	E	3
22	23	*	22	<b>58</b>	22	28	53	90	3.	32	ĸ	Ř	35	36	37	800	39	4
2498	7.2	2.5	5.1	-	6.9	2.1	8.0	6.			2.0	.034	2.4	.041	16.5	5.0	<u>-</u> -	*
2566	7.8	7.4	7.5	2.3	7.4	2.5	7.6	2.3			2.4	.042	4.5	.059	15.3	4.7	12.7	n
2501	<b>.</b> .	6.	10.9	3.3	7.0	2.9	7.9	7.4			2.8	. 035	3.2	. 056	12.4	3.8	9.5	8
2503	7.7	2.3	7.7	2.3	7.9	4.7	7.8	2.4			2.3	.040	3.6	. 062	13.0	<b>6</b> .4	10.7	2
2564	5.6	1.7	6.7	2.1	6.1	<b>-</b>	4.9	9.7			2.0	.035	5.6	. 646	12.5	3.8 8.0	10.1	'n
2565	3. 9.	<b>.</b>	10.0	e.	S.9	<b>-</b>	7.9	2.4	4.8	2.6	2.5	.044	4.6	. 060	15.3	4.7	12.7	'n
2506		1.7	2.5	<b>9</b> .	<b>.</b>	7.6	<b>4</b> .6	<b>+</b> .			2.5	. 039	2.1	.037	<b>5</b> . 9	4.6	S.	7
2587	<b>6</b> .7	7.	7.0	2.1	. d	o. (	7.0	2.1			5.6	.045	٠. ا	.054	4.5	<b>+</b> (	Z :	'n
2269	-:	7.7	B 1	-	9.5	e	7 1	<u>ه</u> .	•	,	5.5	440.	2.7	. 647	16.9	2.5	14.7	ᢤ .
2514 2513	- 0 • r			* °	B. 7	7.7	\	· ·	o.	1.7	7.7	90.00 00.00	, . , r	. 44.4 2.44.4	+ · ·	9 Y	5. e	• •
2512					) P	? =		- «			• «	550				) r		
2513	. 2	-					. 4				2.7	948	2.0	.035	13.2	• •	6.00	
2515	7.6	2.3	-	6.	10.5	3.2	7.6	2.3			2.7	.047	9.	.052	4.0	7.4	2.8	'n
2516	4.4	1.3	3.3	•	5.3	8.	4.7	<b>+</b> .			1.7	. 030	2.5	. 039	9.9	a.6	7.3	7
2517	8. 8.	1.8	<b>8</b> .9	2.1	8.8	2.1	5.5	1.7			2.5	.044	4.2	.042	14.3	<b>+</b> . <b>+</b>	1.9	'n
2518	8. 8.	<b>9</b> .	7.5	2.3	6	1.7	6.7	<b>5</b> .0			6.	. 033	2.7	.046	<b>1</b> .8	3.6	8.6	ĸ
2519	6.7	7.0	<u>.</u>	7.8	7.1	2.2	8.1	2.5			2.7	.046	3.1	.053	16.7	5.1	7.7	<del>,</del>
2520	9.0	8.8	8.3	2.5	•. =.	3.3	9.6	2.9			2.9	. 050	+:	.671	14.6	<b>4</b> .8	11.7	'n
2522	<b>.</b> .	2.5	9.5	2.5	<b>†</b>	<del>.</del>	♦.	6.			2.2	. 038	n.	.058	15.6	4	13.2	4
2523	4.1	0 0 0	<b>9</b> .0		بر در	2.8	4.0	6.0			2.9	.049	4.5	.073	16.4	o. •	14.0	÷,
2524	) ·	9.7		7.7	2.5	2.5	2.5	5.5	,	•	, . • .	.042	. v	aca.		4 H	2.2	
25.25	) ) )		, ,	- 0		-	• • •	- °		<u>.</u>	2.5 4.0	1 6	- 5	96.		. 4	1.0.1	'n
2527	9.0	-		2.8	7.7	2.3	7.8	4.			2.5	446	3.0	.052	9.8	ارى ھ	16.4	'n
2528		2.8	8.8	2.7	4.0	2.6	8.3	2.5			5.6	.046	3.8	990.	14.1	4.3	1.5	'n
2529	7.4	2.2	8.6	7.6	<b>6</b> .9	2.1	7.8	7.4			2.5	. 639	3.1	. 053	15.2	4.6	12.8	'n
2536	5.7	1.7	6.3	6	5.0	<b>-</b> .	<b>6</b> .0	8.			2.3	.041	2.5	.043	16.8	5.1	14.9	<del>+</del>
2531	6.7	5.0	<b>9</b>	7.6	5.0	<b>.</b>	7.6	2.3			2.5	0 7	2.7	.047	7.5	<b>4</b> .4	12.1	'n
2532	4.	<b>9</b> .	<b>.</b>	2.7	4.7	<b>*</b> :	6.7	9.			7.4	.042	2.7	.047	17.5	. S.	e. 4 6. 4	*
2533	4.	•		<b>9</b>	4. 60.		•	S.			e. •	. 032	<b>6</b> .	.034	12.6	ю. •	10.7	n i
2534		•	7.2	7.7	r) (	<b>.</b>	<b>9</b> .	9.			5.9	. 635	2.7	.047	4.6	4. 0.	12.2	'n.
2535	٠. د د	7.7	9 1	- ·	<b>4.</b>	2.3		<b>.</b>			2.5	.043	2.5	. e4.	16.0	4 I	5.3	٠.
2536		9. 1	7.7	2.5		<b>.</b>	0.	2.1	,	,	2.1	. 636	2.9		9.9	. ·	e :	•
2537	4:4	`.'	9.	2.5	÷ ;	- (	<b>+</b> •	J.5	<del>4</del> .	* •	2.2	929.		5.5		• •	2:	÷ r
2536	5	2.3	- c		י פ	2.0	. d.	e .	5.	9.	2.3	929.	2.5	2.0	5.0	4 t	7.1.	, c
255	 		9 6	- 0	n (		÷ •	<del>+</del> (			ю. - «	. 632	7.7	929.	77.7	` ·	o r	i c
2246	» .	- c	? ;	* 1	9 0		0 t	9 ·			۲.۶ د د	940	, r		9.0		: ;	<b>,</b>
2541		7 . 6	, r	, ,	7.4	- c	) t				- c	200. ATA	, c	9.6	0. 4 0. 4	7 0	 	, 4
7107	7.,	7.7	?	7:7	D .	۸.۸	٠./				٨.٥	000	۲.0	2	•	)  -	2	÷

IGHT	d a	3	\$	3.1	2.8	2.5	4.5	3.1	3.8	3.7	9.0	<b>4</b> .8	<b>4</b> .0	<b>4</b> .	4. U	g.5	4.0	3.1	3.5	4.6	3.6	3.0	3.8	4.6	3.1	3.1	3.2	3.9		g.8	4.4	J. B	3.6	3.7	4.6	3.1	<b>+</b> . <b>+</b>	3.5	4.0	3.0	3.3	4.5	3.8
ноок нетсит	OVER RAMP	t	39	10.1	9.2	8.1	14.9	10.0	12.4	12.2	9.7	15.6	13.3	13.0	14.2	11.6	11.3	19.2	11.5	11.0	11.8	10.0	12.5	11.2	10.2	10.2	10.4	12.8		12.7	14.0	12.6	11.7	12.2	11.3	10.1	13.5	11.5	13.0	8.8	19.7	14.9	12.4
WHEEL HEIGHT	RAMP	æ	8	S.8	3.6	3.2	5.2	3.8	4.6	4.5	3.7	ທ. ທ່າ	<b>4</b> .	<b>4</b> .	 -	<b>4</b> .4	4.2	۵. ت	4.5	4.2	4.4	3.7	4.5	<b>-</b> ∵	J. B	ы. В.	о. Ю	4.6		4.5	0.	4.0	4.4	4.4	<b>+</b> . <b>+</b>	3.7	<b>4</b> .8	<b>+</b> .+	4.7	3.7	4.2	5.1	4.5
WHEEL	OVER RALLP	E	37	12.5	11.7	10.4	16.9	12.4	15.1	14.6	12.0	17.9	5.8	15.7	16.7	14.2	13.8	12.7	13.8	13.7	14.2	12.3	14.8	13.4	12.6	12.5	12.9	15.1		14.8	16.4	14.8	14.0	14.2	13.6	12.3	15.9	14.3	15.4	12.1	13.7	16.8	14.9
VT T0	₽V.	3	38	.044	. 036	.040	.040	. 627	. 046	.054	.039	. 985	. 056	.651	.047	.046	.045	. 055	. 030	. 063	.015	. 032	. 949	. 075	. 036	. 042	. 053	. 056	101	. 057	. 968	.072	. 968	.040	. 045	.048	.052	. 028	. 057	. 033	.043	.050	.051
WGLE /	6	DEC	33	2.5	2.1	2.3	2.3	5.5	5.6	J.	2.5	<b>4</b> (	3.5	2.9	2.7	5.6	5.6	J. 1	1.7	3.6	ø.	<b>6</b> .	2.3	4.3	2.1	4.7	3.0	3.5	S.	J. J	3.9	4.2	g.	2	5.6	2.7	3.0	1.6	3.3	9.	2.5	2.9	5.9
GLIDE PATH ANGLE AT TO	BHW.	8	*	. 034	. 035	. 035	. 947	. 028	. 039	.046	.045	. 964	.043	. 942	. 938	. 936	. 036	. 037	. 036	.035	.037	.037	. 037	.044	. 637	.631	. 637	. 039		. 038	.036	.045	. 035	. 028	.032	.034	.046	.028	.035	.037	.037	.038	.033
GLIDE	65	DEG	23	2.0	9.9	2.0	2.7	1.6	2.2	2.8	5.6	3.7	2.8	2.4	2.5	2.1	2.1	2.1	2.1	2.0	2.1	2.1	2.1	2.5	2.1	8.	2.1	2.2		2.2	2.0	2.6	2.0	9	1.8	9.1	2.6	1.6	2.0	2.1	2.1	2.2	6:
	IGHT	S/N	32						2.0	2.4																9.							2.6	1.8	2.0								
	FREE-FLIGHT	F/S	E						<b>9</b> .	7.9																5.3							8.5	5.9	6.7								
NWOC	(3	¥	99	<del>.</del>	1.7	6.	1.9	1.2	7.0	2.3	1.7	۵. د	5.6	<b>.</b>	2.1	<b>.</b>	6.	2.3	1.3	5.6	۲.	5.	6.	3.1	9.	1.7	2.5	2.3	3.2	2.3	7.6	G	2.7	1.7	7.0	2.0	₩.	-:	2.4	5.	2.0	2.2	2.5
INKING SPEED AT TOUCHDOWN	AVG	F/S	28	6.1	5.6	6.3	6.3	3.9	6.5	7.4	9.	11.7	æ •	<b>4</b> .	6.7	<b>6</b> .9	<b>4</b> .	7.6	<del>-</del> -	8.6	7.4	<b>4</b> .8	6.2	19.1	5.3	5.5	7.2	7.6	10.5	7.6	8. S.	6.0	89.08	5.7	6.5	6.6	9.9	80.00	8	6.4	6.5	7.3	7.2
EED AT	2	K K	28	<del>•</del>	<b>7</b> .0	9.7	<b>1</b> .0	<b>+</b> :	9.	2.2	2.1	4.0	7.6	7. <b>0</b>	<b>.</b>	<b>5</b> .0	<b>.</b>	6.	7.7	2.5	=	2.1	1.8	2.7	1.7	<b>+</b>	2.0	2.6	3.2	2.1	2.3	5.6	2.9	<u>.</u>	6.	7.7	9.	۲.	3.2		2.5		2.3
CING SE	STBO	F/S	23	5.3	5.1	6.7	5.4	4.7	5.2	7.1	<b>9</b> .0	۲. <u>-</u>	<b>8</b> .6	<b>6</b> .5	<b>6</b> .1	6.5	3. 9.	6.3	<b>+</b> .+	<b>8</b> .1	3.5	6.8	5.8	8.8	5.7	4.7	6.7	6.5	4.0	<b>6</b> .9	7.7	9.0	9.6	6.1	6.2	7.2	5.1	2.2	4.0	9.0	9.9	4	7.5
S	H	K K	26	2.2	2.1	1.7	<del>.</del>	J. J.	2.5	2.3	<b>.</b>	9.0	7.7	<u>.</u>	2.5	1.7	2.6	2.7	1.2	2.8	€.	œ.	2.0	4.5	5.5																		2.1
AIRCRAFT	PORT	5/2	22	7.3	6.9	5.6	6.2	4.2	8.3	7.4	S.8	ø. -	7.8	 	8.2	5.4	8.7	8.8	3.9	5.7	2.6	2.9	9.9	J.3	5.0	6.5	8.5	7.8	6.7	8.4	4.0	1.5	8.3	5.4	6.5	5.1	6.3	5.6	7.4	4.4	6.4	•	0.0
	w	\$	54	2.1	9.	5.0	1.7	5.5	2.5	<b>.</b> .	7.7	J. W.	2.8	<del>.</del>	7.4	2.1	<b>.</b>	2.3						_					·		2.9	2.7	<b>8</b>	9.	9.	1.7	4.	5.	2.5	5.	4.	4	2.3
	NOSE	5,5	23	6.7	5.2	9.9	5.6	4.8	7.3	6.3	7.4	o. •	9.5	o. •	7.7	7.0	5.8	7.5	3.6	9.6	•	6.1	3.5	7.5	4.4	5.2	5.2	8.8	8.8	7.8	4.0	8.8	5.9	5.2	5.4	5.6	4.7	5.0	7.3	0.4	4.5	~	7.6
200	ş		22	2543	2544	2545	2546					_																															2585

USS ENTERPRISE (CVN-65)

		3	AMDING D	DATA - MODEL T-2C	MODEL 1	2 -	ž	SS ENT	USS ENTERPRISE (CVN-65.)	(C <b>\</b>	(1)			DAY L	DAY LANDINGS			
995			AIRCR	WFT SII	NK ING S	PEED AT	RCRAFT SINKING SPEED AT TOUCHDOWN	N C			GLIDE	GLIDE PATH ANGLE AT TD	WGLE A	5	WHEEL	нетсят	HOOK HEIGH	호 :
2	¥	MOSE	8	PORT	SI	STBO	AVG		FREE-FLIGHT	LIGHT	唟		8	>	OVER	RAMP	OVER	3
	2	\$	\$	Ş	F/S	S/n	F/S	S/N	F/S	M/S	DEG	8	DEG	3	E	3	E	
22	23	<b>5</b>	23	<b>36</b>	23	<b>5</b> 8	<b>53</b>	90	2	32	S	Ř	35	38	37	38	88	•
2586	7.5	2.3	4.6	1.7	<b>9</b>	2.9	7.5	2.3			€.	.031	2.9	.050	13.0	4.0	10.6	P)
2587	4.6	<b>5.8</b>	10.0	3.3	4.8	1.5	7.9	7.4			2.1	.036	3.3	.057	14.3	4.4	11.5	<b>P</b> )
2588	8.8	2.7	12.8	3.0	5.0	1.5	8.5	2.5			2.1	.036	3.2	.056	10.6	3.2	8.2	~
2589	7.8	7.4	<b>8</b> .8	7.0	6.9	2.1	æ.	2.1			e. -	.032	2.7	.047	12.6	3.B	10.1	<b>P</b> )
2590	6.3	<u>.</u>	7.1	2.7	4.8	<del>7</del> .	<b>9</b> .	<b>8</b> .			8.	.034	4.7	. 042	13.9	4.2	11.5	P)
2591	7.9	7.4	7.0	2.1	7.2	2.2	7.1	2.5			9.7	.034	J. 7	. 055	15.5	4.7	12.8	-,
2592	6.2	 	6.2	<b>a</b> :	7.1	2.1	<b>9</b> .9	2.1			2.1	.037	2.7	. 048	11.7	3.6	4.6	
2593	4.9	 S	6.5	7.0	6.3	<b>o</b> :	6.9	<b>.</b> 8.	6.2	6.	₩. 80.	.031	2.5	.044	12.3	3.7	8.6	۳,
2594	9. 9.	<b>.</b>	7.6	2.3	5.1	<del>1</del> .6	5.8	<b>.</b>			2.2	. 039	2.9	.050	15.3	4.7	12.5	۲,
<b>404</b>	<b>9</b> .	7.4	6.5	7.0	7.8	7.4	7.3	2.2			<b>4</b> .0	.070	2.8	. 649	18.4	5.6	16.1	•
4063	<b>9</b> .9	2.1	7.0	2.1	<b>.</b>	- •	6.7	7.0			J	. 053	4.7	. 042	16.7	5.1	14.3	•
4177	<b>9</b> .9	2.1	<b>9</b> .5	5.6	7.8	<b>•</b> 0	5.5	1.7			2.5	. 038	2.5	. 038	15.0	4.6	12.5	-,
4313	14.8	4. 8.	12.5	3.8	12.9	8.8	12.4	J.8			4.2	. 673	5.6	. 689	18.6	5.7	15.5	•
4331	9.3	2.8	9.0	2.6	<b>8</b> .	3.0	8.5	2.6			3.1	.055	3.3	. 058	21.9	6.7	19.6	·
4336	7.8	2.3	7.7	2.3	4.9	5.0	7.5	2.3			4.6	. 059	3.2	. 057	16.9	5.2	14.2	•
4435	<b>9</b> .0	2.8	<b>8</b> .9	2.1	4.0	2.2	7.5	2.3			2.7	.047	J. 7	.053	14.0	n.4	11.4	۳,
4705	7.9	7.4	8.6	2.6	7.9	7.4	7.7	2.3	8.0	7.4	2.6	.046	2.5	. 044	16.6	5.1	14.1	•
4953	2.3	۲.	5.2	<b>.</b>	5.2	<b>9</b> .	5.4	9.			4.4	. 058	2.3	. 040	19.8	6.9	17.0	•,

RAD DEG 49 50 1035 -1 - 1046 -2 5 1047 -1 - 1017 -1 - 1018 -2 8 - 1018 -2 8 - 1019 -2 8 - 1122 -4 4 - 1016 -9 6	8 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	<b>▼</b>	11.0 DEG 45 46 45 46 45 46 45 46 45 46 46 46 46 46 46 46 46 46 46 46 46 46	OR FF DEG RAD DEG 44 45 46 4 6.3 .110 6.3 .110 6.5 .113 7.9 .122 7.9 .122 7.9 .122 6.5 .113 6.5 .113 6.5 .113 6.5 .113 6.5 .113 6.5 .113 6.7 .099 6.1 .166 6.1 .166 6.1 .166 6.1 .166 6.2 .168	08 FF 45 48 45 48 45 48 45 48 45 48 45 48 45 48 45 48 45 48 48 45
1444 422 4884 7 8 44 87 74 8 8 8 8 8 8 8 8 8 8 8 8 8 8	AAA 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	RAD DEG RAD 47 48 49 2.6 635 2.3 646 -1.8 -631 1.9 -617 1.9 -617 4.7 -682 -2.3 -646 -1.1 -619 7.9 -122 7.9 -165 6.9 -165	45 46 47 48 49 45 46 47 48 49 45 119 2.9 635 119 2.9 635 112 -1.2 -2.9 646 113 -1.12 -1.8 -017 103 -2.3 -046 104 4.7 -082 105 -2.3 -046 105 -2.3 -046 113 -1.1 -019 115 -1.1 -015 115 -1.1 -015 115 -1.1 -022 115 -1.1 -025 115 -1.1 -025 115 -1.1 -025 115 -1.1 -025 115 -1.1 -025 115 -1.1 -025 115 -1.1 -025 115 -1.1 -025 115 -1.1 -025	DEG RAD DEG RAD DEG RAD  44 45 46 47 48 49  6.3 .110 2.0 .035  6.5 .1139016  5.9 .103017  5.9 .103017  5.4 .0942.3040  5.4 .09411019  6.5 .11311019  6.6 .07012040  6.7 .09912040  6.8 .154054  6.91314024  6.110612  6.213120055  6.313005  6.400912  6.513005  6.7005  6.813005  6.9105  6.9105  6.1009	43 44 45 46 47 48 49 43 44 45 46 47 48 49 49 6.3 .116 2.6 .035 .113 8.7 .152 2.3 .046 .107 6.5 .113 -1.8016 .052 7.0 .1229016 .054 5.4 .094 4.7 .082 .059 5.5 .1032.3040 .055 6.5 .1131.1019 .056 6.5 .1131.1019 .152 6.8 .154 .094 .152 6.8 .154 .094 .152 6.9 .103 .006 .009 6.5 .1131.1019 .152 6.8 .154 .099 .108 6.5 .1131.1016 .152 6.8 .154 .099 .108 6.9 .108 .109 6.9 .109 .109 6.9 .109 .109 6.9 .109 .109 6.9 .109 .109 6.9 .109 .109 6.9 .109 .109 6.9 .109 .109 6.9 .109 .109 6.9 .109 .109 6.9 .109
	648 648 648 648 648 648 648 648 648 648	2.6 647 6417 6	46 47 48 49 2.0 .035 2.3 .046 -1.9 .016 -1.6 .017 -1.6 .017 -1.1 .082 -1.1 .084 -1.1 .084 -1.1 .084 -1.1 .084 -1.1 .084 -1.1 .084 -1.1 .084 -1.1 .084 -1.1 .084 -1.1 .084	6.3 .116 2.6 .035 6.3 .116 2.6 .035 6.5 .113 2.3 .046 6.5 .113 -1.8031 7.8 .064 4.7 .082 5.4 .094 -2.3046 5.4 .094 -1.1019 6.5 .113 -1.4024 6.5 .113 -1.4024 6.5 .113 -1.4024 6.5 .113 -1.4024 6.5 .113 -1.4024 6.5 .113 -1.4024 6.5 .113 -1.6 -1.1019 6.5 .113 -1.6 -1.1016 6.5 .113 -1.0 -1.0 -1.05 6.5 .113 -1.0 -1.0 -1.05 6.5 .113 -1.0 -1.0 -1.05 6.5 .106 -1.0 -1.0 -1.05 6.5 .106 -1.0 -1.0 -1.0 -1.05 6.5 .107 -1.0 -1.0 -1.0 -1.05 6.5 .108 -1.0 -1.0 -1.0 -1.0 -1.0 -1.0 -1.0 -1.0	6.3 .116
	1411 455 -864 1	2. 3	2.00352.3046 2 2.3046 2 2 2.3046 2 2 2 2 3046 3 2 2 2 3 2 2 3 2 2 3 2 2 3 2 2 3 2 2 4 3 3 2 2 4 3 3 2 2 4 3 3 2 2 4 3 3 2 2 4 3 3 2 2 4 3 3 2 2 4 3 3 2 2 4 3 3 2 2 4 3 3 2 2 4 3 3 2 2 4 3 3 3 2 3 3 3 3	. 116	6.3 .116
		. 635 . 646 . 617 . 617 . 618 . 618 . 618 . 619 . 619 . 618 . 618 . 618 . 618 . 618 . 618 . 618 . 618 . 618	2.3	. 116 . 152 . 152 . 13 . 113 . 122 . 18 . 193 . 994 . 994 . 994 . 994 . 113 . 999 . 99	6.3 .116 6.5 .113 7.6 .129 7.6 .122 7.6 .122 7.7 .002 7.8 .004 6.5 .113 6.5 .103 6.7 .004 6.8 .014 6.9 .014 6.9 .012 6.1 .106 6.2 .108 6.3 .108 6.4 .009 6.5 .113 6.6 .114 6.7 .009 6.8 .014 6.9 .014 6.9 .120 6.1 .106 6.1 .106 6.2 .108 6.3 .108 6.4 .009 6.5 .113 6.6 .108 6.7 .009 6.8 .108 6.9 .108 6.9 .108 6.9 .108 6.9 .108 6.9 .108 6.9 .108 6.9 .108 6.9 .108 6.9 .108 6.9 .108
			2.3	. 152 2.3 . 046	6.5 . 152 . 2.3 . 646 6.5 . 113
				. 129	7.4 . 129
	1 1 1	- 100.1 - 101.4 - 101.6 - 101.	1.6 - 0.57 - 0.6	. 113	6.5 .113
	1 1		1.6	. 122 1.0 .017 .064 4.7 .082103 .9 .016 .094 -2.3 -040 .095 -1.1019 .070 .8 .014 .113 -1.4024 .113 -1.99 .113 -1.99 .154 6.0 .105 .106 -3005 .107 .905	7.6 .122 1.6 .617  4.8 .684 4.7 .682  5.9 .1639 .616  5.4 .694
	1 1		.8 .914 .7 .982 - .3 .916 .1 .1 .946 .1 .1 .944 .1 .1 .94 .1 .4 .924 .1 .4 .199 .2 .916 .3 .916	. 684	6.5 113 - 1.05 -
	1 1	- 688. - 616. - 619. - 614. - 624. - 616. - 616. - 616. - 616. - 616.	4.7	. 183	4.8 .084 4.7 .082 - 5.9 .103
<b></b>			. 9	. 193	5.9 .103 5.4 .094 5.4 .094 6.5 .113 6.5 .113 6.5 .113 6.6 .103 6.7 .093 6.8 .154 6.9 .106 6.1 .008 6.2 .106 6.3 .106 6.4 .001 6.5 .113 6.6 .105 6.7 .003 6.8 .124 6.9 .105 6.1 .106 6.2 .106 6.3 .106 6.4 .001 6.5 .106 6.6 .105 6.7 .106 6.8 .124 6.9 .106 6.9 .106 6.1 .106 6.1 .106 6.2 .106 6.3 .106 6.3 .106 6.4 .106 6.5 .106 6.6 .106 6.7 .106 6.8 .106 6.9 .1
			-2.3040 -1.1019 -1.4024 -1.4024 -1.5024 -1.902 -1.902 -1.0503 -1.0505	. 694 . 694 . 676 . 113 . 113 . 114 . 113 . 695 . 695 . 113 . 154 . 168 . 168	5.4 .094 .2.3 .046 5.4 .094 .094 .1.1 .019 6.5 .113 .1.4 .199 6.7 .099 .7.0 .122 6.5 .113 .014 6.6 .154 .095 .122 6.7 .099 .122 6.8 .154 .095 6.9 .106 6.1 .141 .095
	1 1		1.1 - 619 8 614 11.4 - 624 11.4 - 199 7.6 - 122 - 616 6.6 - 105 6.7 - 616	. 694 . 676 . 113 . 106 . 106 . 107 . 699 . 699 . 113 . 113 . 108 . 108	5.4 .094 6.5 .113 .1.4 .024 6.1 .106 .11.4 .199 6.2 .113 .099 7.0 .122 6.3 .113 .012 6.4 .199 6.5 .114 .016 6.6 .154 .016 6.7 .006 6.8 .154 .016 6.9 .106 6.1 .106 6.1 .106 6.2 .106 6.3 .106 6.3 .126 6.4 .106 6.5 .126
	1 1		.8 .014 -1.4024 -11.4 .199 7.6 .122 - -9016 6.0 .105	. 676 . 8 . 614 . 1131.4624 . 166 . 11.4 . 199 . 699 . 7.6 . 122 - . 1132.616 . 154 . 6.6 16.65 . 1683665 -	6.5 .113 8 914 6.5 .113 11.4 199 6.7 699 7.6 12.2 11.3 1.9 1.0 1.2 11.3 1.9 1.0
~~~		. 199 . 122	11.4024 11.4199 7.6122 - 6.6105 6.7	. 113	6.5 .113 -1.4024 6.1 .106 5.7 .099 6.5 .113 6.8 .154 6.9 .105 6.2 .106 5.1 .008 6.1 .104 6.1 .104 6.2 .106 6.2 .106 6.3 .104 6.4 .104 6.5 .113 6.6 .105 6.7 .005 6.7 .006 6.8 .120 6.9 .120
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	1 1		7.0 .122 - 9016 6.0 .105 3005 -	. 699 . 113 . 154 . 154 . 166 . 165 . 168 . 168 . 168 . 168 . 169 . 169 . 169 . 169	6.5 .113
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	ī	- 665 -	1-39 2	.3865 -13865 -1689 1.6 .017	6.2 .1663665 - 5.1 .689 1.6 .617 8.1 .141 6.9 .126 4.7 .682 1.5 .626
		.017		9.1	5.1 .069 1.0 .017 5.1 .141 6.9 .120 4.7 .062 1.5 .026
		6	/19. 9.1		8.1 .141 6.9 .128 4.7 .082 1.5 .026
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		007	4007	.1194007	6.8 .1194007
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		035	-2.0035	.086 -2.0035	4.9 .086 -2.0035
4	.183		10.5	.101 10.5	5.8 .101 10.5
	- 040 -	040	-2.3040	.103 -2.3040	5.9 .103 -2.3040
	. 982	. 082	4.7 .082	.110 4.7 .082	6.3 .110 4.7 .082
		944	2.5 .044	.136 2.5 .044	7.8 .136 2.5 .844
		- 042	-2.4 842	-2.4642	-2.4042
		676	679 - 679	127 - 4 4 - 728	ACA - A - A - A - A - A - A - A - A - A
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	035	i	-2.6	.115 -2.8	6.6 .115 -2.9
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	924	1.4 .024	7.	7.1	8.0 140
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		3	LANDING DATA	1	MODEL T-	1-20	_	USS ENTERPRISE (CVN-65)	SRPRIS	ie (cw	(€9)			ð	DAY LANDINGS	INGS				
3		PIT	I O	Ŭ Z <				ROLL	<	N G L	w	<b>a</b> .	PITCH RATE	RATE	ROLL RATE	RATE	F. P. A.	÷	YAW	
2	5		8		4		10		క		Ŀ		¥	5	AT TO	2	AT TD	۾	AT TD	٥
	DEG	3	DEG	3	930	3	DEG	3	DEG	8	DEG	3	DEG	\$	DEG	<b>8</b>	DEG	8	DEC	8
<b>∓</b>	42	\$	‡	<b>5</b>	\$	41	<b>\$</b>	64	20	51	25	53	54	55	56	22	28	29	99	19
1778	₩. 13.	.075	6.5	.113				.005 -1.		. 021		*	-		3.4			091	<b>8</b> .0	.140
1779	4.0	. 659		. 886		١		669 -1.B		031		1				.079 -1			3.0	. 052
1786	9	.007	4.6	. 980		7				. 002		1 9					_		3.7	.065
1782	2.5	169.	8 . 1 . 8	.049		ī'		<b>6</b> 28 2		. <b>9</b> 63		9	6 6 6	900 000 000					7.7	134
1784	9 9	886	ים יחים	620		( î		040 -3.9 040 -2.6		1.045 0.045		. ~			-7.55	- 131 - 5- 131 -		966 	5.0	99.
1785	4.4	.075	4.60	147						.021		*	<b>-</b>						4.9	.112
1786	5.2			101		_		.023 -1.6	1	028		7	7						6.9	. 120
1787	<b>D</b>		5.2	.091		€)	5.7			. 002		_	<b>6</b> .							. 984
1788	9.5		4.4	. 129		•	•			.031		φ.				7	<u>.</u>			086
1789	ب د م			888		'		•		059		7	•			7			5.5	.044
1/96		98		6::		-, <b>4</b>		.9619		916		_		. 658 769	7.5		7.7		5.7	686.
1794		3 5	•	 		· 1	١	942 69		120		0				7- 2/0		- 620		. 024 956
1795	7		מי	858		-				. 993		-				692 -2			. B.	898.
1796	0.4			166		ניו		ī		023		7	1						2.5	.044
1797	4.0			.131		_				012		4								007
1798	* <b>*</b>			.112						021		-7							9.9	.115
1799				888		Ϋ,		1		044 56		7 7		042 LE	- 6	٠	-	042	÷.	.679
1887	• «	100	0 17	5. 8. 8. 8.		Ī		626 3.7 1992 4.1		.000		F 10	• •	_		211 -		919	6 6	9.6
1863	7.5		*	.077		. •		9.99		.002		→		•				023	2.1	.037
1884	8.8		5.4	. 994		7		•	·	042		7	1	_				019	₹.	.007
1805	<b>.</b>		5.1	. 989		_				. 059		!	ı					051	5.9	. 183
1807	4 I		4.6	486		7	-5.0 -	087 -2.0	ŀ	035		. 2			'			031	7.7	.038
	7.8	921.	 	727		•				650		• -	. ·	9 6	) e	2- COI.	-2.4	1.650	- 6 • 4	2/0.
1810	4.0		5.2	169.		-		1	•	033		'n							5.0	. 687
1812	4.5	•	4.7	. 682		ī	ı			.010		n							2.8	.049
1813	5.0	_		.117		7		049 -1.	i 0	<u>0</u> 33		'n	<b>+</b> .		_				<b>+</b> :-	.072
1814	<b>.</b>		7.3	. 127		44			<b>+</b>	. 997		~	-						6.2	. 108
1815	7.2	_		. 165		, '	nj (		ni i	061		~				7			7.1	.124
1817	- (	.072	9.0	2		7	<b>1</b>			.120					י. מיני				2.2	. 838 638
1618	7.5	166	• •	21.		. <u></u>		2.4.2 - 824 2		رائ. درائ	0	+ 6 A 6		0.00		710.	i ;	- 6/9. i		901
1822	5.3	685	. B	145		7				023		-						_	19.1	.176
1823	5.7	680	8.2	.143		7		047 -1.	i 6	033					4.1	.024 -2	-2.0		3.8	990.
1891	4.7	. 982	7.0	.122		-		. 023		600.		6	9.6		3.9		6		6.1	. 166
1893		886	٠ • •	.15		``	-2.3			033		ı	, ,	012	• c	.024 -3	دن د		8. d	.101
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RAD         DEG         RAJ         TD         AT         AT         TD         AT         AT         TD         AT	LANDING DATA	NIGNYI	2	<u>د</u> د	ı	MODEL T	1-2C	_	USS ENTERPRISE (CVN-65)	IERPR I	SE (CVI	N-65)			ă	DAY LANDINGS	INGS				
RAD         DEG         RAD         DEG         RAD         DEG         RAD         DEG         RAD         DEG         RAD         DEG         RAD         DEG         RAD         DEG         RAD         DEG         RAD         DEG         RAD         DEG         RAD         DEG         RAD         DEG         RAD         DEG         RAD         DEG         RAD         DEG         RAD         DEG         RAD         DEG         RAD         DEG         RAD         DEG         RAD         DEG         RAD         DEG         RAD         DEG         RAD         DEG         RAD         DEG         RAD         DEG         RAD         DEG         RAD         DEG         RAD         DEG         RAD         DEG         RAD         DEG         RAD         DEG         RAD         DEG         RAD         DEG         RAD         DEG         RAD         DEG         RAD         DEG         RAD         DEG         RAD         DEG         RAD         DEG         RAD         DEG         RAD         DEG         RAD         DEG         RAD         DEG         RAD         RAD         RAD         RAD         RAD         RAD         RAD         RAD         RAD <th>PITCH ANGLE</th> <th>ITCH ANGL</th> <th>CH ANGL</th> <th>N G L</th> <th>_</th> <th></th> <th></th> <th></th> <th>0</th> <th></th> <th>z</th> <th>L,J</th> <th>•</th> <th>P11CH</th> <th>RATE</th> <th>ROLL</th> <th>RATE</th> <th></th> <th>₹</th> <th>*</th> <th>_</th>	PITCH ANGLE	ITCH ANGL	CH ANGL	N G L	_				0		z	L,J	•	P11CH	RATE	ROLL	RATE		₹	*	_
RAD         DEG         RAD         DEG         RAD         DEG         RAD         DEG         RAD         DEG         RAD         DEG         RAD         DEG         RAD         DEG         RAD         DEG         RAD         DEG         RAD         DEG         RAD         DEG         RAD         DEG         RAD         DEG         RAD         DEG         RAD         DEG         RAD         DEG         RAD         DEG         RAD         DEG         RAD         DEG         RAD         DEG         RAD         DEG         RAD         DEG         RAD         DEG         RAD         RAD <th>TP 90 0T</th> <th></th> <th></th> <th></th> <th><b>1</b></th> <th>•</th> <th></th> <th>2</th> <th></th> <th>క</th> <th></th> <th>Ħ</th> <th></th> <th></th> <th>Ð</th> <th></th> <th>ę</th> <th>AT T</th> <th>٥</th> <th>AT 1</th> <th>۾</th>	TP 90 0T				<b>1</b>	•		2		క		Ħ			Ð		ę	AT T	٥	AT 1	۾
2.7         .044 <th>DEG RAD DEG RAD DEG RAD DEG</th> <th>DEG RAD DEG RAD</th> <th>RAD DEG RAD</th> <th>DEG RAD</th> <th>2</th> <th></th> <th>2</th> <th>ပ္</th> <th>8</th> <th>DEC</th> <th>SA O</th> <th>DEC</th> <th><b>2</b></th> <th>DEG</th> <th>\$</th> <th>DEG</th> <th>8</th> <th>DEG</th> <th>8</th> <th>DEG</th> <th>3</th>	DEG RAD DEG RAD DEG RAD DEG	DEG RAD DEG RAD	RAD DEG RAD	DEG RAD	2		2	ပ္	8	DEC	SA O	DEC	<b>2</b>	DEG	\$	DEG	8	DEG	8	DEG	3
2.7         .047        2        003         1.1         .019        8        014         1.2           2.5        044        3        023         2.9         .051        3        056         4.7           2.8        049        03         3.5         .061         -4.0         -070         -0.1        047         2.4          1        054         1.8         .031         -3.5        061         -4.0         -070         -0.1        047         2.4          1        073        052         1.8         .049         1.1        047         2.4        052        1        047         2.4          1        077        08         1.3        056         -1.3        053         7.4        055        053        142        047         2.4        056        13        061        14         1.12        041        142        142        142        142        142        142        142        142        142        142        142        142        142        142        142        142        142 <t< th=""><th>42 43 44 45 46 47 46</th><th>44 45 46 47</th><th>45 46 47</th><th>1 46 47</th><th>41</th><th></th><th>\$</th><th></th><th>6</th><th>20</th><th>5</th><th>22</th><th>53</th><th>\$</th><th>55</th><th>26</th><th></th><th>58</th><th></th><th>99</th><th>19</th></t<>	42 43 44 45 46 47 46	44 45 46 47	45 46 47	1 46 47	41		\$		6	20	5	22	53	\$	55	26		58		99	19
-2.5         -844         -1.3         -023         2.9         -651         -3.8         -666         4.7           2.6         -034         3.5         -661         -1.9         -6.6         -1.9         6.6           3.1         -054         1.8         -051         1.9         -061         -1.9         -6.6           3.1         -054         1.8         -051         -1.6         -104         2.4           -1.3         -053         -0.1         -0.54         -1.9         -6.6         -1.9         -6.6           -1.1         -0.07         -0.0         0.00         3.1         -054         1.9         -0.05         7.4           -1.1         -0.07         -0.0         0.00         -1.6         -0.05         -1.8         -0.05         7.4           -1.1         -0.07         -0.0         0.00         -1.1         -0.05         -1.4         -0.05         7.4           -1.2         -0.03         -1.5         -0.05         -1.6         -0.05         7.4         -0.05         7.4         -0.05         7.4           -1.2         -0.03         -1.1         -0.03         -1.1         -0.03         -1.1 </th <th>9 .163 6.7 .1172</th> <th>63 6.7 .1172</th> <th>6.7 .1172</th> <th>.117</th> <th>2</th> <th>2</th> <th>. 7</th> <th>ľ</th> <th></th> <th>7.7</th> <th>.047</th> <th></th> <th>•</th> <th>.2</th> <th>. 003</th> <th>1.1</th> <th></th> <th>i 80</th> <th>914</th> <th>1.2</th> <th>. 021</th>	9 .163 6.7 .1172	63 6.7 .1172	6.7 .1172	.117	2	2	. 7	ľ		7.7	.047		•	.2	. 003	1.1		i 80	914	1.2	. 021
2.8         .049         2.9         .051         .1         .002         -1.9         -033         1.2           -2.2         -033         3.5         .061         -4.0         -6.6         -1.05         6.6           -1.1         -062         1.8         .031         -2.5         -6.6         -1.05         6.6           -1.1         -062         2.8         .049         12.1         .211         -4.2         -063         6.6           -1.1         -017         -0.65         1.9         .031         -2.7         -063         7.4           -1.1         -013         -0.26         -1.8         -031         -3.7         -063         7.4           -1.2         -013         -0.26         -1.9         -0.33         -7.4         -0.26         -7.5         -0.66         -7.9         -7.4         -0.65         -7.4         -0.65         -7.4         -0.65         -7.4         -0.65         -7.4         -0.65         -7.5         -0.66         -7.5         -0.66         -7.5         -0.66         -7.5         -0.66         -7.5         -0.66         -7.5         -0.66         -7.5         -0.66         -7.5         -0.66         -7.5	1.6	5.3 .092 1.6	.092	1.6				-		1	.044		ī		. 023	2.9		-	990	4.7	. 982
-2.2 - 0.033	9 +98 . 64.6	4.6 .864	9	<b>5</b>							.049		•4					-		1.2	. 021
3.1         .034         1.8         .031         -3.5         -1041         2.4         -3.5         -1041         2.4         -3.5         -1041         2.4         -3.5         -1041         2.4         -3.5         -1041         -3.5         -1042         -3.5         -1042         -3.5         -1042         -3.5         -1042         -3.5         -1043         -3.5         -1043         -3.5         -1043         -3.5         -1043         -3.5         -1043         -3.5         -1043         -3.5         -1043         -7.5         -1056         -1.9         -3.5         -1043         -7.5         -1056         -1.9         -3.5         -1043         -7.5         -1043         -3.5         -1043         -7.5         -1043         -7.5         -1043         -7.5         -1043         -7.5         -1043         -7.5         -1043         -7.5         -1043         -7.6         -1056         -7.5         -1043         -7.5         -1043         -7.5         -1043         -7.5         -1043         -7.7         -1042         -804         -1042         -804         -1042         -804         -1042         -804         -1042         -804         -1042         -804         -1042         -1042 <th>1.5 484 6.1 1.96</th> <th>6.1 .106</th> <th>.106</th> <th>5. T</th> <th></th> <th></th> <th></th> <th></th> <th></th> <th>1</th> <th>.038</th> <th></th> <th>., ·</th> <th>ر د رو</th> <th></th> <th></th> <th></th> <th></th> <th></th> <th>9.0</th> <th>£ 5</th>	1.5 484 6.1 1.96	6.1 .106	.106	5. T						1	.038		., ·	ر د رو						9.0	£ 5
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-1.3      923      36      963       5.5      996       -2.8      949       8.1         3.6       .952      49      986       16.5      288       -2.2      938       1.1         3.5       .961      13      923-21.1      368       -5.5      993       10.1         4.9      961      159      928      3.2      991       8.8         1.6      923      36      963      961      964       4.8         1.6      928      15      965      966       3.9       14.3         1.7      928      966      965       2.9      161      959       14.3         1.2      928      16      3.7      965       3.9      161      959       14.3         1.2      928      933       9.3      162      3.4      959       13.1         3.3      958      933      3.5      966       3.9      969       13.1         3.1      958      933      958      17      959       13.1         3.1      959	.698 4.7 .682 -2.6	4.7 .082 -2.0	2 -2.0	2 -2.0					635 -	-	. 992		•	1			T	8		, n	. 005
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3.3       .058         3.3       .058        5      003       3.5       .061       -3.7      065       4.5        5      009       3.5       .061       -3.7      065       4.5         3.0       .052       3.9       .068       4.7       .084       -5.7      093       13.1         3.1       .065       3.9       .068       4.7       .082       -1.1      018      1         3.1       .065      065      7      086       4.7      089       4.6         3.1       .064      7      089       -4.7      082       8.7        052      17      007       5.8       .101       -2.5      061       6.9        052      17      009       7.4       .129       -3.5      061       6.9        064      052      17      039       7.4       .129       -3.5      061       6.9        069      069      7      039       7.4       .129       -3.5      061       6.9        07      052      038      1      028	4.0 .070	4.0 .070	.1.1-	-1.1					,	•	.021		· 7			. e				. 6	.087
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3.6       .652       9.6       4.7       .652      0      1      0      1      0      0      0      0      0      0      0      0      0      0      0      0      0      0      0      0      0      0      0      0      0      0      0      0      0      0      0      0      0      0      0      0      0      0      0      0      0      0      0      0      0      0      0      0      0      0      0      0      0      0      0      0      0      0      0      0      0      0      0      0      0      0      0      0      0      0      0      0      0      0      0      0      0      0      0      0      0      0      0      0      0      0      0      0      0      0      0      0      0      0      0      0      0      0      0      0      0 <td< th=""><th>3.9 .068</th><th>3.9 .068</th><th>.068 -1.1-</th><th> a</th><th></th><th></th><th></th><th>-, -</th><th></th><th>1</th><th>. 958 96</th><th></th><th>•</th><th></th><th></th><th></th><th></th><th>- '</th><th>•</th><th>o +</th><th>. 679 979</th></td<>	3.9 .068	3.9 .068	.068 -1.1-	a				-, -		1	. 958 96		•					- '	•	o +	. 679 979
-3.7      065       3.9       .068       3.3       .058       -2.2      038       4.6         3.1       .064       1.12       3.1       .064       -3.8      066       3.6         3.1       .064      7      069       -4.7      062       8.7         2.4       .062      4      007       5.8       .101       -2.5      044       5.4         -3.6      052      17      030       7.4       .129       -3.5      061       6.6         -0.0       0.009       .7      026      016       -3.5      061       6.6         -2.6      045       .7      028       -1.6      023       4.3         -2.6      045       .3       .062       -4.0      070       3.7        9      016      0      016       -3.6      016       -3.6      063       5.4        9      016      0      010       -3.6      063       4.3      066       5.4        9      016      0      016       -3.6      016       -3.6      063       5.3	- 6.4-	- 2.7	- 7.4	7.7	•	•	•	Ö			.052		•								8
0.0       0.000       1.5       0.0       -0.00       3.6       -0.00       3.6       3.6       3.6       3.6       3.6       3.6       3.6       3.6       3.6       3.6       3.6       3.6       3.6       3.6       3.6       3.6       3.7       3.7       3.7       3.7       3.7       3.7       3.7       3.7       3.7       3.7       3.7       3.7       3.7       3.7       3.7       3.7       3.7       3.7       3.7       3.7       3.7       3.7       3.7       3.7       3.7       3.7       3.7       3.7       3.7       3.7       3.7       3.7       3.7       3.7       3.7       3.7       3.7       3.7       3.7       3.7       3.7       3.7       3.7       3.7       3.7       3.7       3.7       3.7       3.7       3.7       3.7       3.7       3.7       3.7       3.7       3.7       3.7       3.7       3.7       3.7       3.7       3.7       3.7       3.7       3.7       3.7       3.7       3.7       3.7       3.7       3.7       3.7       3.7       3.7       3.7       3.7       3.7       3.7       3.7       3.7       3.7       3.7       3.7	4. 654 6.6 .115	4. 6.6 .115	4. 2115	4.	₹.	₹.		•	,				~)	_		ņ	7	'n		<b>9.</b>	. 686
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2.4       -0.95       -1.7       -0.90       7.4       -1.9       -5.5       -0.94       5.7         2.6       -0.95       -1.7       -0.90       1.6       -0.91       -5.9       -5.9       -5.9       -5.9       -5.9       -5.9       -5.9       -5.9       -5.9       -5.9       -5.9       -5.9       -5.9       -5.9       -5.9       -5.9       -5.9       -5.9       -5.9       -5.9       -5.9       -5.9       -5.9       -5.9       -5.9       -5.9       -5.9       -5.9       -5.9       -5.9       -5.9       -5.9       -5.9       -5.9       -5.9       -5.9       -5.9       -5.9       -5.9       -5.9       -5.9       -5.9       -5.9       -5.9       -5.9       -5.9       -5.9       -5.9       -5.9       -5.9       -5.9       -5.9       -5.9       -5.9       -5.9       -5.9       -5.9       -5.9       -5.9       -5.9       -5.9       -5.9       -5.9       -5.9       -5.9       -5.9       -5.9       -5.9       -5.9       -5.9       -5.9       -5.9       -5.9       -5.9       -5.9       -5.9       -5.9       -5.9       -5.9       -5.9       -5.9       -5.9       -5.9       -5.9       -5.9	.676 7.0 .122	7.0 .122 -5.3	-3.5	2.5							40. 6.			ь.		_		i :•	790		201.
3.     -1.7     -0.36     -1.7     -0.36     -1.6     -0.36     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3     -0.3	- 9 808. I.C 9/9.	1 a.l	1 p.1		ı	ı	ı				240.		, •			n -	-	ن ا ا	¢ • •	t d	100
6.6     6.000       7.     6.1       -2.6     -0.00       7.     6.0       -2.6     -0.00       -3.     -0.05       -3.     -0.05       -4.     -0.00       -5.     -0.00       -6.     -0.00       -7.     -0.00       -7.     -0.00       -1.     -0.00       -1.     -0.00       -1.     -0.00       -1.     -0.00       -1.     -0.00       -1.     -0.00       -1.     -0.00       -1.     -0.00       -1.     -0.00       -1.     -0.00       -1.     -0.00       -1.     -0.00       -1.     -0.00       -1.     -0.00       -1.     -0.00       -1.     -0.00       -1.     -0.00       -1.     -0.00       -1.     -0.00       -1.     -0.00       -1.     -0.00       -1.     -0.00       -1.     -0.00       -0.00     -0.00       -0.00     -0.00       -0.00     -0.00       -0.00     -0.00       -0.00     -0.00 <th>626 6.9 .126</th> <th>6.9</th> <th>120</th> <th>. ·</th> <th></th> <th></th> <th></th> <th> '</th> <th>7</th> <th></th> <th>700.</th> <th></th> <th>ī '</th> <th></th> <th></th> <th></th> <th></th> <th>ن ۱</th> <th>- 6</th> <th>» «</th> <th>971.</th>	626 6.9 .126	6.9	120	. ·				'	7		700.		ī '					ن ۱	- 6	» «	971.
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6.6 6.666 -1.7636 4.6 .686 -3.1654 4.2 . -2.46421.4624 5.5 .696 -3.0652 4.4 .		4. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1.	4 64					Ŭ			,004 997		<b>→</b> F		- 040. - 148			•	20 G	. d	942
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	2. 086 3.6 .063 2.0	3.6 .063 2.0	2.0	2.0						•	.042		ī	*	.024	3.00			952	*	.677

<b>&gt;</b>	£	2	19	.072	960.	. 686	. 063	.049	.019	.138	. 059	. 005	040	.003	. 021		.19	023	.061	. 992	051	689	9.000	•	5	023	.077	044	.049	.13	. 037	¥2.	. 122	. 851	.012	047	. 038	.113	.087	.007	131	.019	. 682
XVM	14	DEG	99	<del>-</del> -	5.5	4.6	3.6	2.8	-:	7.9	4.6	r.	-2.3	7	7.7	7.5	6.8	L. 1.	3.5	<del>-</del>	-2.9	5.7	<b>e</b> .	80 i		-1.J	4.4	-2.5	7.8	<b>6</b>	2.1	7.7	7.0	2.9	۲.	-2.7	7.7	6.5	5.0	₹.	7.5	1:	4.7
خ ٠	5	3	28	. 042	075	. 968	. 945	052	044	. 051	. 942	007	023	051	052	982	. 966	038	033	900.0	- 000	072	030	- 049	152	. 026	030	416	047	- <b>6</b> 88	014	982	644	049	012	. 037	058	051	049	040	. 072	010	082
r.	¥	DEG	58	-2.4	4.4	- 6.5-	-2.8 -	6	-2.5 -	-2.9	-2.4 -	<b>+</b>	'n	Ġ	-3.0	'	ر وي	-2.2 -	- 6.1	9.0	ا ان	-	•		- 7:9	 5.		<b>6</b>		-5.6	-			-2.8	_	_	- 5.5	_		_	·	9	4.7
RATE	5	8	22	. 805	. 030 -	. 698	.232 -		- 858 -	.183 -	- 150.									.175	. 028	-				040	- 141					-			. 038		. 924 -	.230 -	-	-		.124	. 984
ROLL RATE	¥	DEC	26	ņ	- 1.1	3.9	13.3	8.3	3.3	9.5	2.9	9.5	_	_	8.8	7.5	ę. 6.	3.7	1.7	10.0	9.7	¥.4	и. В.	<b>6</b> .	+ + +	ח	 	9.9	<b>9</b> .0	2.5	2.5	. v. =	ı.i	<b>4</b> .0	-2.2	8.8	<del>*</del> :	3.2	7.3	2.3	-	7.1	8.4
RATE	5	8	22	. 999	052 -	. 023	061 1		.051	. 698	019	. 026	•	•	021	. 058	. 124	.058	. 984		. 021	.016	.054	.040			. 954	. 962	. 692	. 023	.073	. 092-1	. 669	026	960	. 617	9.66	1481.	.038	684	033	648	.059
PIICH KAIE	7	DEC	4	ĸi	. 9.5	7.3	5.55	'n	2.9	5.6		5.		6.	-1.2	3.3	7.1	3.3	8.4	. 2.	1.2	6.	3.1	2.3	2.3	7	3.1	<b>-</b>	S. J.	٠. د.	4.2	5.3	ĸ.	. 5.	5.5	<b>6</b> .	9.9	5.5	2.5	60	-		4.6
		3	53		•		. 995 -				•		,	•	٠				019	•														- 924 -				. 824 -	i	•	603 -		
44 	1	DEG	25																-															- <del>+</del> -				<b>+</b> :-			2	ļ	
- : :	~	3	5	663	609	023	. 999	.002	056	021	024	.070	966	.019	. 035	007	016	.080	019	003	.044	012	. 003	014	031	.040	049	.040	628	007	028	054	410.	. 993	600.	. 054	021	075	610	045	- 945	024	990.
	8	DEG	20	2	. 5	-1.3	'n	-	-3.2	-1.2	4.7	4.0	. 8.5	-:	2.0	· •	6.	<b>4</b> .6		7	2.5	. 7.	ų	89.	_		_		9. T	4.	•	- -	€0.	7.	ĸ.	J. 7	-1.2	_	-		-2.6		3.8
2	۵	3	49	.072	014	- 994	026	026				066	. 686	14	. 068	600	049	699	623 -	010	152	.098	012	986	063 -				•	.031	•	-	. 136	024	. 049	059		. 031	-, 035	063			- 909
	5	DEG	<b>\$</b>	<b>+</b>		-	5.1.5	.55				_	4.6	₩.	3.9	ĸ.	-2.8				_				_	_		0. T	<del>-</del> .	<b>.</b>	<b>+</b> .	<del>-</del>	7.8	· •	2.8		9.7					a	
	<b>L</b>	3	47			·	.124		•			•					•	•	. 196		•			•	•	•	•	•						. 065		•	•	660	-	•	160	·	
0 L	۱.	DEG	9				7.1												6.1															3.7				5.7			5.4		
z <	8	2	\$	.072	119	. 687	.112	.087	1.0	. 673	. 692	989	.124	. 122		191	.13	960.	<b>.</b>	. 163	.165	3	. 128	.677	. 679	.152	<b>5</b>	986	3	.115		<b>66</b>	.676	. 105	.115	9	. 063	119	106	984	.115	195	103
Z C	J	DEC	‡	<del>-</del>	8.8	S.	4.9	S.	6.3	4.2	5.3	<b>4</b> .	7.1	7.0	8.5	S. 38	6.5	5.6	S.	0. 0.	9.	5. 0.	7.2	<b>+</b> .	÷.5	8.7	4.6	<b>4</b> .0	7.6	<b>9</b> .0	<b>5</b>	5.7	<b>•</b> •	<b>9</b> .	9.9	6.1	3.6	8.8	6.1	4			5.9
<b>-</b>	ę	8	2	3	. 966	. 045	7.	.070	.072	. 635		1	<b>.</b>	=	.127	8	\$	.113	3	40	<b>466</b>	980	.077	. 662	8	986	\$	.07	3	<b>3</b> .	. 112	.07	<u>.</u>	88	.061		.075	.10	.667	926	20	6	.052
	-	DEC	42	2.5	3.8	2.6	7.7	•		2.0	4.6	<b>9</b> . 1	2.7	8.1	7.3	3.5	4.5	6.5	9. 9.	ر ا	4.	5.5	<b>†</b> .	4.7	<b>.</b>	6.4	7.7	•	<b>4</b> .	2.7	<b>†</b> .	•.	5.5	3.7	3.5	5.3	4.3	<b>6</b> .3	5.0	3.2		2.8	9. 9.
3	2		7	1949	1950	1951	1953	1955	1956	1957	1958	1959	1961	1964	1965	1966	1967	1969	1976	1971	1972	1973	1974	1975	<b>707</b>	2046	2047	2648	<b>7878</b>	2020	202	202	2053	2024	2055	2026	2057	2058	2059	2060	2961	2863	2065

		3	LANDING DAT,	1	MODEL T-2C	-3C		uss en	(ERPR )	USS ENTERPRISE (CVN-65)	F-65)			DAY	DAY LANDINGS	NGS				
995		P 1 4	I O	<b>3</b> ✓	<b>W</b>			ROL	۱ ۸	N G L	w	•	PITCH RATE		ROLL RATE	MTE	F. P. A	÷	YAW	
2	5	_	8		1	ė.	đ		8		Ŀ		AT TD	٥	AT T	5	AT TD	۾	AT TD	0
	DEG	3	DEC	3	DEG	8	DEC	8	DEG	<b>8</b>	DEG	8	OEC	3	DEG	SAD O	DEG	3	DEG	\$
<b>∓</b>	42	2	‡	\$	\$	41	\$	<b>6</b>	20	5	22	53	<b>*</b>	25	26	22	88	29	99	5
2066	4.2	.073	5.9	391.			ĸ.	. 669		.019		ī				ī	ĸ.		3.3	. 858
2067	7.4	. 129	6.1	. 106				.042 -2	+	. 942		9					_		8.6	.115
2069	, d , d	= {	 	88		1	     	687 	eo 4	.614 874		ų d		096 -2 - 112 -1	-2.7	047 -3 - 061 -3	÷ 4	059 	ر د د د	. 961
2072		700	7 K	966		1	1		i ed	631		-							. o. r	968
2673	4.0	8	. <del>.</del>	.075		ı	1			.052		-					_		5.9	.103
2074	3.2	929	8.8	.145					•	021		91							5.8	101
2	• •	.052	e. e	 			÷.	. 626 -1	-1.7 -	938 5.1		י ני		.058 -7.3		127 -5 - 126 -		- 193 9 5 5		120
7878	· ·	5 6	7.0			•				944		4 1	_				۰ -		) o	.968
2679	-	196	**	. 129			; <b>†</b>		: -:	. 037		-							6.0	.155
2000	6.	. 633	3.0	. 968					_	. 030		ĸ							5.1	.089
2063	2.7	7	5.5	960					1	059		60					-2.8		 	110
2 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	6.7	156	4. e	.079				1 600.		. 636		1 7	. I	010 -6 - 116 11	 	1 9 1 ° -	i (	080	0. u	122
2007				2 6		1	2.7			.026		7						-	9 6	227
2002	5.0	.667	9.0	<u>.</u>		-		667		.054		7							5.4	. 694
200	<b>9.</b>	8	6.3	=:				011.	4	056		9 (	•		<b>.</b>		α.	-	9.5	178
200	<b>+</b>			966		,	1	128	 	. 623 - 684		N 1	2.5 5.45	. 948	t a	- 909 -	' 	. es.	9 G	700
2662	9.0	8		2 2						935		1	i •				-2.3	040	t. 5	.023
2007	5.7	80	4.7	.062	5.4	<b>*60</b>	•		•	- 603 -	· -	662 -1	_					052	4.7	. 082
2002	2.8	3		51:						.056		יי מי	4.4	.059 2		.051 -3.		054	e .	÷ 5
2 <b>69</b> 7	• •	65	9.4	5 4			-2.7	070 - 047 -		-, 856 -, 856		? -			2.4			. 010	. 2	. 838
2008	9.0	984	. e.	101						003		†	ı			•		035	3.3	.058
200	5.8	101	6.5	.113		i			9.4	. 686		•			۰ م	.192 -1.	<b>+</b> .		9 · 0	.045
212	 	5.6	7.5 0.7	3 5		: <b>!</b>	- 2.6	1.640	* -	954		- <b>•</b> ?				7 928	t KO	679	- 17	. 682
2163	9	115		115				940	יי	500		8		7				089	6.8	119
2105	3.0		4.0	.070				- 999	· -:	002		7						056	9.3	.162
2106	2.3	÷.	5.9	. 163			1			982		-	•	•				075	S. 5	<b>2</b>
2107	ن د زه	5	• •	<u>.</u>						023		1			3.2	.056 -2		<del>0</del> 51		
2188	, ,		• •	?				919.1	֓֞֝֞֜֜֜֝֜֝֜֜֜֝֓֜֜֝֜֜֜֜֝֓֓֓֓֜֜֜֜֜֝֓֓֓֓֜֜֜֜֝֡֓֜֜֝֡֜֜֜֜֝֜֜֜֝	- e e		7		1.000 1.000 1.000			- 6	1 6	7 F	200
2 6	7 E					. 1						•		.019			. ~	- 993	9	10.
2171	9.0	3	6.7	.17						.031		•	_			•		033	2.1	.637
2173	4.0	999	5.5	980			_	- 150.	-	002		ı	2		•	-	·	659	a	. 033
2174	7.9	38	5.5	980			8.2			929		•	÷.		<b>.</b>	.192 -3.	٠	1.956 676	 	. 196
2175	10	191	6.J	130			·	002	-2.8	64g		n		. 2	i D	-	?	J. 638	:	Š.

		3	LANDING DATA	ı	MODEL 1-20	ģ	_	USS ENTERPRISE (CVN-65)	ERPRIS	E (CVN	<del>(</del> -65)			ργ	DAY LANDINGS	SON				
997		P 1 4	X O	S Z V	n m			R 0 L	۱ ۸	N C L	ш	ā	PITCH RATE		ROLL RATE	MTE	F. P. A.	خ :	YAW	*
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	DEG	2	930	3	DEC	3	DEC	8	DEG	3	DEG	3	DEG	8	DEG	\$	DEG	3	DEG	8
ŧ	7	3	‡	\$	<b>\$</b>	47	\$	49	20	5	25	53 9	54	22	26	27	28	28	99	5
12	5.4		_	.129		ī	1.1	019 1	•	.017		<u>*</u>	<b>о</b>	.269 8	8.6	.150 -2	•	035	4.5	.059
<b>.</b>	2.7			. 1 <b>96</b>		_		ï	ı	035		ĸ,						-	10.4	.181
į	2.5		_	986		••		.054	<b>ن</b>	.005		7						035	2.8	.049
2				<b>8</b>			0.0			. 030		-1.7							7.8	.136
2207		0 / <b>0</b>				7		. <b>6</b> 24.5		6/3 644		` ₹		/ 919. .070 .5		- 124 - 698 2	9 P	- 163 - 184		981.
\$	*		6.7	117		**		-		045		89			•	-		077	7.3	.127
•	÷.		6.2	20		7				662		'n		•	_		-3.2 -	056	5.	. 026
Ξ	3.4	628	9.2	.161		-,	_	•		047		'n				.131 -3.	4	059	9.3	. 162
23	2.6	\$45	5.8	101		•	~	003 2.	_	. 042		4.	_			7	₩.	031	r.	. 995
Ž	÷.	3	8.2	3		_			7	005		2.6			1	T	•	686	5.7	660
5		40	<b>4</b> 1	70		7'	ا •		<b>.</b>	017		2.0				.691 -5.	_	- 699	7.2	.126
	, t	3		. 661			• • • •	1- 469.	eir I	e17		-7.9		849 Z		4 C 4 C 4 C 4 C 4 C 4 C 4 C 4 C 4 C 4 C		070	- ·	889.
9 9	. 7	279		988		ľ	' '	.016 -2.3		. 940		9 9		. 185 – 5	- 25.69				4.6	460
2	3.2	926	<b>4.4</b>	.075		7	4.4			.044		2.7					-3.0	052	7.4	.042
5	5.5	986	5.7	686		7		•	•	038		5.7				. 1552	'n	040	4.0	. 070
22:	4 t	. 675	• •	. 1 <b>6</b> 5		7 °				054		•	٠,				, ,	075	ø :	.120
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27	3.0		3.0	163		_				637		, b			1			026	<b>. 5</b> 0	.014
28	6.5	•	7.0	. 122		•				044		7					•	035	2.5	.044
8	8. 6		S.5	986		44 (	. 6	7	•	035		9						659	4 i	.079
3 5	, ,		• •	211.		·' 'ì		2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	i i	- 6988 676		 			 	. 621 	i 1 ? °	1.965	* · •	821.
32		•		122		•	. ~	.073	9	9. 8.		1			•		•	077	4.	147
3	3.0	-		.072		7		_		. 023		2.5		-			•	949	2.4	. 042
충	3.8		5.5	986		ī		024 -1	i •	024		7.4					-2.4	042	2.3	.040
8	4.2		4.6	100		• `		T		075		1	ŧ			-				989.
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3	7.7		· · ·	. I.		Ī '	7.1	021	יי מ	989.		÷	? •	/ C/0.		5. T.		900.0	֓֞֜֜֜֜֜֜֜֜֓֓֓֓֓֓֓֜֜֜֟֜֓֓֓֓֓֓֓֓֓֓֡֜֜֜֓֓֓֡֓֜֝֓֡֓֡֓֡֓֡֓֡	100
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3	2.8		5.0	.087		7	n	4		. 686		•	· ·				'	045	6.2	168
ŧ	3.5	_	6.8	119		٠,		.103 -5.7		699		٠	· •				1.7		11.8	.206
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¥	5.3	_	9.0	.115		7	٠. ٢.ك		_	.012		<del>-</del>	~	.021 24.8				.017	60.	014
<b>₹</b>	4.	•	4.5	.679		•	7.	.082 -5.	_	639		÷	ī. m	=======================================	i -	-	n	040	8. B.	. 966
<b>5</b>	6.5	.113	9.1	¥.		ī	ı <b>89</b>	031	•••	914		-		. 924 4	n.	<b>07</b> 5 -2.	9	035	2.9	.051

EG         RAD         DEG         RAD	LANDING DATA - MODEL T-2C I T C H A N G L E OR FF	l Z	l Z	00EL T-2C L E FF	27		- 0	USS ENT	TERPRIS  L A  OR	USS ENTERPRISE (CVN-65) ROLL ANGLE OR F	N-65)	<u>.</u>	PITCH RATE	DA RATE TO	DAY LANDINGS  ROLL RATE AT TO	INGS PATE	F. P. A.	<b>₹</b> _e	YAW AT TO	_ 0
49         56         51         52         53         54         55         56         57         58           -024         2.1         -037         -1.2         -021         .5         -064         -2.5           -039         -7.4         -1.23         -049         6.3         .119         -6.6         -115.3         -069         -2.5           -039         -7.4         -1.29         -1.2         -0.21         -3.5         -069         -2.5         -001         -1.5         -0.21         -3.2         -0.21         -0.2         -0.21         -1.5         -0.21         -0.2         -0.21         -0.2         -0.21         -0.2         -0.20         -0.3         -1.2         -0.21         -0.2         -0.21         -0.2         -0.21         -0.2         -0.2         -0.2         -0.2         -0.2         -0.2         -0.2         -0.2         -0.2         -0.2         -0.2         -0.2         -0.2         -0.2         -0.2         -0.2         -0.2         -0.2         -0.2         -0.2         -0.2         -0.2         -0.2         -0.2         -0.2         -0.2         -0.2         -0.2         -0.2         -0.2         -0.2         -0.2	RAD DEG	<b>క</b> బ్జ		3	t 230	2	966		<b>8</b> 9		DEG	8	AT DEG	£ 3	DEG	5 8	AT 1 DEG	<b>2</b>	AT T DEG	2
1.2         .063         .7         .012         2.6         .045         3.1         .054         2.5           1.4         -024         2.1         .037         -1.2         -021         .5         .069         2.5           1.1         -039         -2.3         -046         6.3         .1         .093         -2.5         .069         -2.5           -1.3         -053         -1.6         -029         -2.6         -010         -1.6         -017         -1.5         -017         -1.5         -017         -1.5         -017         -1.5         -017         -1.5         -017         -1.5         -017         -1.5         -017         -1.5         -017         -1.5         -017         -1.5         -017         -1.5         -017         -1.5         -1.7         -017         -1.5         -017         -1.5         -017         -1.5         -017         -1.5         -017         -1.5         -1.6         -1.7         -010         -1.7         -010         -1.7         -1.6         -1.7         -1.6         -1.7         -1.6         -1.7         -1.7         -1.6         -1.7         -1.7         -1.8         -1.7         -1.8         -1.7         -	45 44 45		\$		\$	41	<b>\$</b>	6	20	2	52	53	4	22	26		28	28	99	5
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	ŗ.	A	DEC	88	6.9	-5.8		4		_	+	<b>.</b>						9				<b>n</b>							- •						<b>.</b>	-2.1	1.7	-3.0	- 6:1-	-3.6	- 7.2-	-3.2	- 6.5-
OINGS	ROLL RATE	5	RAD	22	. 954	. 108	.086			- 986 -	037-11.					. 986	- 1961	199										2 6												. 623		092 -	- 190
DAY LANDINGS	ROLL	AT	DEG	26	3.1	6.2	6.4				-2.1						n.	<b>-</b> . •	<b>so</b> !			15.1													- 8.5-	. 8.1.	. 5.4		-3.8	n	2.5	5.3	3.5
۵	RATE	5	RAD	22	. 082	9.000	051	026												017								107							. 926					023	127	. 638 -	.031
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NTERPR		8	DEG	20	<b>1</b>	-1.3	4.6	ø.	ا. ان	₹.	S: T				2	-3.7	<b>.</b>	<b>.</b>	7	ĸi.	9	_		-2.7	Ξ.	2.5	-2.3						2.9	'n	1.2	-2.3	1.5		J. 0	2.4	-2.6	8.	-
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LANDING DATA	× 0	O	DEG	‡	9.9	3.6	<b>9</b> .0	5.8	4.6	<b>-</b>	<b>6</b> .3	<b>a</b> .	7.5	8.5	ر. د.	<b>6.</b>	<b>.</b>	÷.5	•	<b>*</b> : <b>*</b>	<b>0</b> .0	4.		<b>.</b>		<b>.</b>		o .	7.0			-	3.5	+	5.8	6.7	8.8		<b>.</b>	<b>5</b> .8	4.4	6.1	5.5
3	<b>-</b>	ę	3	3	496	28.		<b>98</b>	3	.115	3	929	3	.124	<b>5</b>	. 124	3	3	<b>5</b>	.127	<u>\$</u>	.173	.075	<b>5</b>	51.	131	124	2	3			113	5	920	9.	.052	. 692	.112	. 965	. 859	.143	.054	.079
		-	DEG	42	4.8	9.5	4.5	<b>9</b> .+	4.0	9.0	<b>4</b> .8	4.0	٠. د	7.	<del>ا</del> .	7.1	7.6	3.6	<b>₹</b>	7.3	<b>8</b> 9	<b>6</b>	4.3	<b>3.</b>	7.5	7.5	7.1	ים פינו	e (			6	3.7	3.2	•	3.0	5.3	<b>†</b> .	3.7	4.5	8.2	3.1	4.5
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	YAW	AT TD	8	2	.017	. 044	. 038	.126	. 033	.112	.024	. 035	. 903	440	. 635 845	828	910	.017	.042	.077	770		. 021	.017	. 087	. 989	9. 4 4. 4	.017	.687	. 103	626	. 995	.630	489.	90.0	. 024 PAR	410.	.092	117
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DINGS	RATE	5	3	22	198				916		. 175				. 260	- 60						. 024					. 629		.051			. 992				675			258
DAY LANDINGS	POLL	AT	DEC	98	6.2				• 0						0. <del>4</del> . 0	) r	. 4	2.7				÷ 0			_ ,		?.	3.2	2.9	17.2	5.0	7	11.2		2.1	, t	15.3	5.8	-
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		3	LANDING DAT	   <b>5</b>	MODEL 1	1-20		SS	ENTE	RPRIS	USS ENTERPRISE (CVN-65)	F-65)			5	<b>₹</b>	DAY LANDINGS				
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Ť	3.2	. 926	5.6	886			9.	010	1		963				003	<b>9</b>			068	4.3	. 075
2584	2 4 2 4	25 5	* *	= = =	<b>4</b>	₩20		982	6 - C	•	016 944	9	916	7 7	- 921	1.5 2.1	. 637	5.4	<del>0</del> 40	4 5:4	. 679 786
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2511 2	* •	242	7.2	.126			<b>D</b>	909.			.026			* 6	.024	9,		N (	938 	1.7	. 636
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Ĭ	•		-	100			a.	986		_	965			3.3	.058	11.4		n	058	9.0	.063
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2529	•		6. 0	98			- 9	019	2.5		446				002		. 987	2.7	026	4.7	.073
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-	•		6.1	.106			-1.2	021		7	012		'	ĸ.	696	3.5			851	3.1	.054
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2536	•	672		120	•	•	7.8	949	-77. B	1 n d	044 007	•			124	D . 0	191	-2.8		4.5	. 67.
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2540 0	1.7		5.7	660.			-2.5	044	, N +	٠. 9	.063		1	. 5.1	023	4.4	.147	1.2	. 021	• †	670
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r. G	7	DEC	28	2.2	2.9	<b>+</b> .	2.2		_		<b>+</b> :		_				1 8: T		_	1.6.	·		-2.5	1		_	•	•	-	-		-		-2.3	3.3	-2.8 -	1.8	-	-3.6		1.55	•	5.0
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J S Z		2	51	.030	0.000	035	037	.026	077	. 059 -	. 963	. 667	.021	. 023	.007	031	.047	.042	024	072	005	. 059	070	.117	916	- 680	. 023	. 989		. 021	686	054	•		916 -	.127	9.66	. 003	. 026	.047	051	016	049
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T U	8	DEG	•	~	•		•	•	•	•	5.3	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•		•	•	•	•	•	•	•	•	•	•	•	•	•	•
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	YAW	AT TD	3	2	. 103	<b>. 894</b>	660	.072	. 026	. 232	. 984	. 654	. 061	. 010	. 826	. 120	103	.045	. 128	. 672	. 003	. 038
	<b>)</b>	AT	DEG	99	5.9	5.4	5.7	+:	1.5	13.3	4.8	3.1	3.5	9.	5.5	6.9	-5.9	2.6	7.2	<del>-</del> -	7	2.5
	F. P. A.	5	3	29	091	051	082	096	031	190	061	047	028	077	031	065	. 094	033	072	061	. 003	042
	Ŀ	AT	DEG	86	-5.2	-2.9	7	-5.5	1.8	10.9	5.5	-2.7	1.6	<b>+</b> .	1.8	-3.7	4.5	-1.9	- †	-3.5	7	-2.4
DINGS	ROLL RATE	5	8	22	225	333	.352	019 -	. 129 -	010-	865 -3.5	.049	. 077	058	.075	316	047	. 002	.016	689	. 103	019
DAY LANDINGS	ROLL	AT	DEG	26		_	29.2	_	7.4	<b>9</b> .	-2.7	2.8	<b>+</b> .	-3.3				-		-5.1		
ò	RATE	5	S.	33	070-12.9		833	. 961	007	.075	017	117		. 628 .				. 042		. 106		
	PITCH RATE	AT	DEC	40	• •		-	3.5							•		•	2.4	3.8	6.1	6.1	-2.1
			8	53	•		•				•	042 -			•						030	•
/N-65)	w	9	DEC	25								-2.4									-1.7	
USS ENTERPRISE (CVN-65)	Ω Χ <b>∀</b>	~	SA S	2	. 646	. 003	082	9.000	016	017	016	. 865	. 921	660.	607	056	.012	. 056	024	. 038	- 620 -	.031
ITERPR	, , ,	8	DEG	80	2.3	7	4.7	9.9	•	-1.0		r.	1.2		• • •	-3.2	۲.	3.2	•	2.5	- 4.6-	
uss ed	0 8	_	3	49	699	. 003	. 141.	003	_			045	.056		. 628						926	
		2	DEG	84	ĸ.	7	9.1	2 -	٠	- 5.1-			3.2	_	9.1	_	4.5	4.2	9.1	œ.	1.5	•
2 -			3	41						•	•	.124 -						1			.072 -	
MODEL T-2C	6 L E	T.	9	9								7.1										
TA - N	Z		3	<b>\$</b>	.117	134	100	119	196	. 129	191	.117	.133	. 679	. 691	110	119	. 080	108	.115	. 105	.112
LANDING DATA	<b>∓</b> 0	8	050	‡	6.7	7.7	6.1	6.8	6.2	7.4	5.8	6.7	7.6	4.0	5.2	6.3	6.9	4.6	6.2	9.9	9.9	4.9
3	P 1 T	_	8	\$	3	986	. 056	.058	. 687	196	.963	138	960	.164	. 072	10.	.175	3.	. 082	<b>6</b> 8	. 072	. 698
		2	DEG	42	3.6	<b>6</b> .4	3.2	3.3	5.0		3.6	7.9	5.5	4.0	<del>.</del> .	•	10.0	9.	4.7	4.0	-:	3.6
	200	2		<b>∓</b>	2586	2587	2588	2589	2590	2591	2592	2593	2594	4044	4063	4177	4313	4331	4336	4435	4705	4953

DAY LANDINGS	
USS ENTERPRISE (C.M-65)	
LANDING DATA - MODEL T-2C	

9	85																																										
REREAD	NUMBER			•	•	•	•	•	•	7	•	•	•	•	<b>©</b>	•	-	•	•	•	-	•	•	_	•	•	•	•	- (	• •		- •	- «	-	_	-	•	•	· <del>-</del>	• -	- •	- 0	
ARR GEAR	RUNOUTS	8	82	9.	9.9	9.0	9.0	0.	9.	9.6	9.9	365.8	406. ⁴	416.6	<b>6</b>	<b>9</b>	<b>6</b>	414.0	9.0	414.0	0.0	337.8	386.1	406.4	388.6	304.8	<b>6</b>		461.3	2.080	9 6	Tag.	- 6	6	375.9	403.9	393.7	6		369.7	1005	231.2 418.8	1
**	\$	X	2	•	6	•	•	0	•	•	•	<del>*</del>	160	164	•	0	0	163	0	163	•	133	152	160	153	120	•	•	158	90	9 6			•	148	159	155	•	) <b>C</b>	142	7 7	5 4	>
BAROMETRIC	PRESSURE	¥.	88	769.7	769.7	769.7	769.7	769.7	769.7	769.7	760.7	769.7	769.7	769.7	760.7	760.7	769.7	769.7	769.7	769.7	7.69.7	760.7	769.7	7.69.7	760.0	760.0	761.0	761.0	9 2	9. 6	10/	76.10	761.6	761	761.0	761.0	761.0	761.0	761.0	761.8	761.0	761.0	
BARO	PRE	IN HG	79	29.95	29.95	29.95	29.95	29.95	29.92	29.92	29.92	29.92	29.92	29.92	29.92	29.92	29.92	29.92	29.95	29.92	29.92	29.95	29.92	29.95	29.92	29.92	29.96	29.96	29.96	28.82	8.87	20.00	20.00	20.02	29.96	29.96	29.96	20 9K	29.06	29.98	20.06	20.00	
164		ပ	78	9	19	19	6	19	<b>6</b>	19	6	6	19	6	6	6	6	6	19	19	19	19	19	4	22	22	20	79	20	97	9 6	9 6	9 6	9 6	29	20	20	60	9 6	2 6	3 6	3 6	3
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DECK ROLL		SAD.	78	. 021	. 003	. 033	. 802	9.666	. 058	.044	. 061	. 033	.033	. 939	.045	.019	. 002	. 003	.047	.044	. 026	. 021	. 038	.014	. 636			002		-	979.						- 992	919	9 6	1.014	949	- 636 416	
DEC		DEC	75	1.2	.2	1.9	-	9.0	u. u	2.5	J. 55	6.	1.9	1.7	2.6	-	Ξ.	ä	2.7	2.5	5.	1.2	2.5	₩.	1.7		L	ï	<b>.</b>		<u>.</u>			1	7	1	-		1 1	- 1		: «	•
DECK PITCH		2	74	863	003	009	005	007	009	010	. 005	003	. 007	669	003	007	007	005	005	007	667	005	005	018	669	003	009	007	007	600.	e1e		200	1 6	- 99.7	9.6		9			3 6	9.6	>  - 
DEC		DEC	22	2	2	5.5	J	<b>†</b>	ij	•	'n	7.5	₹.	.5	2	<b>†</b>	Ť	ا. ن	J. J.	+	<b>†</b>	٦.	J. J.	.6	S.	2	i.	<b>♥</b> .	1	ر. د	, ,	î I			•		1		. 1	) M	) 4	9	) 
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SIDE	2		8	919	985	957	963	985	957	963	985	963	983	329	307	981	981	307	328	358	347	981	321	347	329	635	983	957	983	296	200		2 6	3	8	9	2 0	402	0.00	2	7	2 6	200
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OFF-CENTER	DISTANCE	E	3	-10	7	-1	9	4	*	-19	-10	-	F	÷	=	-13	-17	-15	7	-10	7	=	7	7	-12	-13	97	-12	7	<b>P</b> :	<u>.</u>	2 9		<b>.</b>	. 5	5	រ	• •	P	2 4	P (	91	3
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ETRIC ARR GEAR REREAD SURE RUNOUTS NUMBER
BAROWETRIC ARR GE PRESSURE RUNOUT
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P DECK PITCH ED
FLAP SHIP
NO. TYPE CO
. OX
DISTANCE
DISTANCE

	3	LANDING DATA	1	MODEL T-20	1-2C		uss E	<u> </u>	RPR 15	USS ENTERPRISE (CVN-65)	¥-65)			_	γ	DAY LANDINGS				
ક્ર	OFF-CENTER	R RAMP TO	5 5	WIRE	SIDE	NDC	3	SHIP		DECK PITCH	P11CH	DECK ROLL	ROLL	¥	TEMP	BAROMETRIC	TRIC	ARR	ARR GEAR	REREAD
5	DISTANCE	DISTAN	TANCE	Š	2	TYPE	CODE	8	SPEED							PRESSURE	URE	2	RUNOUTS	NUMBER
E	3	E	3					₹	S/X	930	8	DEG	8	L.	ပ	IN HG	<b>₹</b>	2	₹	
3	2	2	8	67	2	8	70	7	22	22	*	75	78	11	78	79	89	2	82	
7	32		1	n	647	50120		12	•	. s	005	6.	016	67	9	29.95	769.7	147	373.4	•
7	-7		\$	*	325	58288		5	^	2 -	003	1.4.	007	67		29.95	760.7	58	401.3	•
-	•		<u>-</u>		647	69129		5	7				007	67	6	29.95	760.7		<b>0</b> .0	•
7,	7.	258	2;	n (	3	56166		2:	<u>ر</u> ر				037	67	6	29.95	760.7	156	396.2	•
7			<b>.</b> 2	4 6	98	50200		<u> </u>	, r	9.0	999		963	68	20 -	30.01	762.3		391.2	<b>-</b>
?	·		2	: <b>→</b>	96	50200		5	- 40		. 995	; r?	.005	8	3 2	39.91	762.3		403.9	• •
T)			8	n	676	80120		5	€	9.9			028	89	<b>50</b>	30.01	762.3		414.0	_
T	-		3	*	342	50200		5	80	2			003	89	20	30.01	762.3	163	414.0	-
7	·		2	4	302	50120		5	80	. 1.1	002	1.5	009	68	70	30.01	762.3	59	419.1	•
٣ :			2		24	70100		5	€0	٠	003		. 665	88	20	30.01	762.3	0	0.0	-
7			<b>Z</b> :	•	655	70200		16	∞ (				600	89	50	30.01	762.3		9.9	•
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ן ק	•		8 2		9	79196		9 5	o «	Y F		1.4		0 E	9 8	38.63	762.3	9 6	9 6	<b>-</b>
9	·		82	r	3	50120		9	•	-2			.003	89	79	30.01	762.3	163	414.0	•
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-12	•		82	*	993	50200		16	80	-	002	+:	007	89	<b>50</b>	30.01	762.3		411.5	•
7	•		2	~	329	50100		9	₩			1.3-	023	89	59	30.01	762.3	152	386.1	•
= '			2 3		3	50123		9 :	<b>6</b>	·	995 605		867	8	8 8	30.01	762.3	<b>o</b>	e e	<b>o</b> o
7	7 7		2 2		5 5	69199		9 5	D 60	- 49	799.		919	8 8	9 6	30.01	762.3	9 6	9 6	• •
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7			2	n	200	50100		2	•		005		.014	89	20	30.01	762.3		353.1	<b>,</b> ,
7	•		₽;	י מ	3	8 8 8 8		٤ :	<b>6</b> 0 (	•	007		002	8	9 6	39.91	762.3	19	416.6	- •
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_			2 6	*7	97.9	80200		2 12	۰ د	٠.		•	766	3 %	2 8	30.01	762.3	166	421.6	•
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7		275	\$		77	79199		5	•	'n	995	-:	.019	8	20	39.91	762.3	•	<b>9</b> .0	•
7	7 -2	291	8		328	66266		5	60	٠	003	-	969	89	70	30.01	762.3	•	<b>6</b> .	•
7		262	2	n	328	<b>Sele</b>		5	•	2	963	ø.	910	88	<b>30</b>	30.01	762.3	145	368.3	-
7		<b>586</b>	24		5	<b>7018</b>		5	€0	' - '	002		010	89	<b>50</b>	30.01	762.3	0	<b>6</b>	•
7		<b>701</b>	2	,	3	70100		5	•0	-	.002	2	003	89	<b>50</b>	39.91	762.3		9.	<b>S</b>
7		223	2	<b>(1</b>	949	28286		2	_	٠	963	ų.	. 995	80	70	39.91	762.3		406.4	<b>-</b> - (
7		261		מ	55	50120		2	•	6. 6.	9.00		939	80	20	30.01	762.3	160	406.4	<b>5</b>
7		23	7	•	20	70100		2	•	N	. 993		995	89	29	30.01	762.3		9.9	7
<b>?</b> '	7	8	3	◀ ·	328	50100		2	•	2.			. 995	89	50	39.01	762.3		388.6	<b>S</b>
T	7	<b>730</b>	8	*	635	50100		2	6	2	003	-1.2 -	. 021	<b>8</b>	20	30.01	762.3	3	388.6	<b>5</b>

	REREAD	NUMBER			•	-	•	<b>6</b>	9 6	9 6	· <del></del>	•	6	7	<b>o</b> (	9 6	9 6	•	•	-	•	<b>9</b>	<b>©</b> 6	۰ د	ı –	-	•	<b>©</b> (	N 6	• •	• •	•	8	-	•	-	_	-	
	ARR GEAR	STO	₹	82	386.1	9.	9.0	378.5	9.9		0.0	0.0	381.0	411.5	401.3	410.0	398.8	373.4	414.0	350.5	406.4	368.3	±			414.0	9.	9	9 6		393.7	401.3	468.9	414.0	421.6	345.4	468.9	391.2	
	ARR	RUNOUTS	Z	<b>8</b>	152 3	•	•	149	֓֞֞֞֓֞֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֡֓֓֓֓֓֡֓֓֡		•	•											162 1	•	•	163 4	•	•	<b>P</b> 4	<b>,</b>	155.3							154	
	BAROMETRIC	PRESSURE	¥	80	762.3	762.3	762.3	762.5	762.5	762.5	762.5	762.5	762.5	762.5	762.5	763.5	762.5	762.5	762.5	762.5	762.5	762.5	762.5	761.7	761.7	7.197	761.7	761.7	7.10/	761.7	761.7	761.7	7.197	761.7	761.7	7.197	761.7	761.7	
DAY LANDINGS	BARON	PRES	IN HC	78	30.81	30.01	30.01	30.02	30.02	30.02	30.02	30.02	30.02	30.02	30.02	20.02	30.02	30.02	30.02	30.02	30.02	39.95	30.02	20.00	29.00	29.99	29.88	29.89	58. 87 00 00	20.00	29.99	29.89	29.99	29.89	29.99	29.88	29.99	29.89	
DAY 1	TEMP		ပ	78	<b>50</b>	79	20	<b>6</b> (	<b>P</b> 9	2 5	6	5	19	5	<u></u>	2 .	9 5	5	5	49	5	<b>5</b>	5 5	3 5	3 23	23	2	23	3 5	200	2 2	23	23	23	23	23	23	23	
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	DECK		DEG	22	-	2	-	7.			6				6. T	7.	- 0			-	<b>1</b> .3		1 4		7	σ.	.7	7	Đ, M	; -	. 7	1.3	•	લ	J.			€0	
USS ENTERPRISE (CVN-65)	DECK PITCH		3	*	003	003	003	993	7997	- 663	003	005	003			799.	- 003	.002	002	662	003	002	. 995	200	. 903	007	002	002		200	. 965	965	667	003	003	003	993	.002	1
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RPR IS	SHIP	SPEED	¥S	22	^	7	7	۲ ۱	- 1			~	7	•	<b>6</b>	۰ م	<b>.</b>	•	6	•	•	•	•	) e	9	40	80	<b>6</b>	n 4	) <b>r</b>	<b>1</b> 0	10	ĸ	10	S	80	60	40	,
ENTE			Š	7	5	5	2	2 :	2 :	2 12	2	5	13	7	7	2 :	2 2	12	12	12	12	2	2 5	9 0	<b>a a</b>	0	0	<b>o</b>	<b>D</b>	• •	. =	•	9	•	0	0	•	Œ	,
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ARR CEAR	RUNOUTS	8	82	9.9	0.0	403.9	378.5	411.5	419.1	419.1	419.1	424.2	424.2	424.2	<b>6</b> .6	<b>0</b> .0	414.0	375.9	<b>6</b> .0	<b>6</b> .0	<b>6</b> .	<b>9</b> .	396.2	9.	368.3	393.7	391.2	393.7	401.3	9 0	9.0	7. 4		186	- •		9. E	9.6	•	<b>.</b>	<b>.</b>	<b>0</b> .	9.
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286         79         3 228         6228         29         10         -1         -002         -4         -007         66         19         29         79         79         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75	7		3	~	35	56266		<b>5</b>	•	~	.00	₹.	.007	99	5	29.97	761.2	-	101.3	•
293         896         75         896         75         193         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75         75 <th< td=""><td>1</td><td></td><td>82</td><td>~</td><td>328</td><td>50200</td><td></td><td>20</td><td>9</td><td></td><td>. 002</td><td>4.4</td><td>. 997</td><td>99</td><td>5</td><td>29.97</td><td>761.2</td><td></td><td>114.0</td><td>•</td></th<>	1		82	~	328	50200		20	9		. 002	4.4	. 997	99	5	29.97	761.2		114.0	•
219         64         329         78289         29         10         60         6.010         66         19         29.97         761.2         18           235         74         329         78289         29         10         1.00         0.00         -1.00         66         19         29.97         761.2         18           235         75         321         5010         21         11         -2         .000         -1.00         66         19         29.97         761.2         18           145         44         232         5010         21         11         -2         .000         -1.00         66         19         29.97         761.2         16           145         44         232         5010         21         11         -2         .000         -1.00         66         19         29.97         761.2         16           195         50         2 300         501         11         -2         .000         -1.00         60         19         2.00         19         19         19         19         19         11         10         10         10         10         10         10 <td< td=""><td>7</td><td></td><td>2</td><td></td><td>957</td><td>70120</td><td></td><td><b>5</b></td><td><u>.</u></td><td></td><td>. 666</td><td>'n</td><td>. 969</td><td>99</td><td>19</td><td>29.97</td><td>761.2</td><td>•</td><td><b>9</b>.0</td><td>•</td></td<>	7		2		957	70120		<b>5</b>	<u>.</u>		. 666	'n	. 969	99	19	29.97	761.2	•	<b>9</b> .0	•
255         76         3 857         3 857         3 857         3 857         3 857         3 857         3 857         3 857         3 857         3 857         3 857         3 857         3 857         3 857         3 857         3 857         3 857         3 857         3 857         3 857         3 857         3 857         3 857         3 857         3 857         3 857         3 857         3 857         3 857         3 857         3 857         3 857         3 857         3 857         3 857         3 857         3 857         3 857         3 857         3 857         3 857         3 857         3 857         3 857         3 857         3 857         3 857         3 857         3 857         3 857         3 857         3 857         3 857         3 857         3 857         3 857         3 857         3 857         3 857         3 857         3 857         3 857         3 857         3 857         3 857         3 857         3 857         3 857         3 857         3 857         3 857         3 857         3 857         3 857         3 857         3 857         3 857         3 857         3 857         3 857         3 857         3 857         3 857         3 857         3 857         3 857         3 85	T'		3	(	329	78286		9.	<b>9</b> :	_	. 999	ė.	919	8	<u>e</u> :	29.97	761.2		0.	6
2.5.5         7.5         7.6         7.5         7.6         7.7         7.6         7.7         7.6         7.7         7.6         7.7         7.6         7.7         7.6         7.7         7.7         7.7         7.7         7.7         7.7         7.7         7.7         7.7         7.7         7.7         7.7         7.7         7.7         7.7         7.7         7.7         7.7         7.7         7.7         7.7         7.7         7.7         7.7         7.7         7.7         7.7         7.7         7.7         7.7         7.7         7.7         7.7         7.7         7.7         7.7         7.7         7.7         7.7         7.7         7.7         7.7         7.7         7.7         7.7         7.7         7.7         7.7         7.7         7.7         7.7         7.7         7.7         7.7         7.7         7.7         7.7         7.7         7.7         7.7         7.7         7.7         7.7         7.7         7.7         7.7         7.7         7.7         7.7         7.7         7.7         7.7         7.7         7.7         7.7         7.7         7.7         7.7         7.7         7.7         7.7         7.7 </td <td>7 1</td> <td></td> <td>2</td> <td>r) r</td> <td>957</td> <td>50200</td> <td></td> <td>, G</td> <td>• • •</td> <td></td> <td>. 662</td> <td>- 1</td> <td>. 962</td> <td>9 9</td> <td>D 0</td> <td>29.97</td> <td>761.2</td> <td></td> <td>5.191</td> <td><b>.</b></td>	7 1		2	r) r	957	50200		, G	• • •		. 662	- 1	. 962	9 9	D 0	29.97	761.2		5.191	<b>.</b>
155         47         358         762.00         21         1         4         1.00         0.00         0.0         0.00         6         1.00         6         1.00         1.00         0.00         0.0         0.00         0.0         0.00         0.0         0.00         0.0         0.00         0.0         0.00         0.0         0.00         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0	1		\$ 5	) r	7 7	27100		3 5	· : :		90.		2	9 9	2 5	79.97	781.2		1 0	۰ -
145         44         2         328         50100         21         11         0.0         0.005         -1.3         -0.23         66         19         29.97         761.2         165           153         53.0         23.0         52.00         21         11         .3         .005         -1.3         -023         66         19         29.97         761.2         156           153         53.0         2         66.0         50.200         21         11         -1         -0.02         -1.4         -0.07         66         19         29.97         761.2         163           214         65         2         32.0         50.00         22         11         -1         -002         -2         -003         61         29.97         761.2         163           214         65         2         32.0         50.00         22         11         -1         -0.02         -2         -0.03         61         29.97         761.2         163           220         11         2         2         22         11         -1         -002         -1         -1         -1         -1         -1         -1         -1	1		: 5	1		7828		: 5	: =	. •	7	•	912	99	9	29.97	761.2		6	- ~
167   51   2   515   50200   21   11                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               .	7		; ‡	~	328	59100		. 5	: =		999		999	99	. <u>.</u>	29.97	761.2		19.1	٠-
195         59         2         358         59200         21         11         3         .005	<b>'</b> T		5	8	818	56200		2	=				.023	99	2	28.97	761.2		196.2	•
173         53         2         646         50200         21         11        1        002        4        007         66         19         29.97         761.2         162           214         51         2         328         50200         22         11        002        6         19         29.97         761.2         161           214         67         2         328         50200         22         11        002        5        004         66         19         29.97         761.2         162           220         67         2         328         50200         22         11        002        5        005         66         19         29.7         761.2         165           184         39         2         328         50200         21         11        002        5        005         66         19         29.7         761.2         165           184         39         2         328         50200         22         11        002        5        005         66         19         29.7         761.2         165           184         39 <td>1</td> <td></td> <td>8</td> <td>8</td> <td>22</td> <td>59200</td> <td></td> <td>53</td> <td>=</td> <td></td> <td></td> <td></td> <td>.014</td> <td>99</td> <td>19</td> <td>29.97</td> <td>761.2</td> <td></td> <td>126.7</td> <td>•</td>	1		8	8	22	59200		53	=				.014	99	19	29.97	761.2		126.7	•
167         51         2         328         58200         22         11                     167         51         2         3.57         561.2         167         2         2         3.58         56100         22         11                 192         29         7         761.2         167         167         167         167         167         167         167         167         167         167         167         167         167         167         167         167         167         167         167         167         167         167         167         167         167         167         167         167         167         167         167         167         167         167         167         167         167         167         167         167         167         167         167         167         167         167         167         167         167         167         167         167         167	7		3	7	978	58288		5	=		002	4.1	. 997	99	19	29.97	761.2		14.0	_
214         65         2         25.56         50100         22         11         0.00         0.000        5        000         66         19         29.97         761.2         167           221         67         2         355         50100         22         11        1        003         66         19         29.97         761.2         152           159         40         2         325         50200         22         11        2        003         66         19         29.97         761.2         162           184         56         2         325         50200         22         11        2        004         66         19         29.97         761.2         162           184         56         2         2.00         22         11        1        002        9         66         19         29.97         761.2         162           183         59         2         2.00         2.0        00        00        01         66         19         29.97         761.2         162           183         59         2         11        1        002	7		2	8	328	50200		22	<u>-</u>		. 002		. 914	99	<u>5</u>	29.97	761.2		68.8	•
221         67         2         557         56166         22         11        1        662        3        665         18         29         751.2         153           236         46         2         32         600        1        662        3        665         19         29.97         761.2         165           184         26         2         328         58260         21         11         6.0         6.00        1        662         6.1         29.97         761.2         167           184         56         2         345         59260         21         11         6.0         6.00        7        605         6.1         29.97         761.2         167           183         56         2         2.00         2.1         11         6.0         6.00         7.0         16.0         6.0         6.0         7.0         16.0         761.0         761.0         761.0         16.0         16.0         16.0         761.0         761.0         761.0         761.0         761.0         761.0         761.0         761.0         761.0         761.0         761.0         761.0         761.0	7		3	~	33	26 188 8 188		22	=		.000		. 669	99	<u>6</u>	29.97	761.2	-	124.2	_
226         67         2 328         59200         22 11         3 900         -1.1 - 619         50 19         25.37         761.2         152.1           159         40         2 321         59200         21 11         -2.0         -0.003         -8 - 014         66         19         29.97         761.2         152.1           184         56         2 329         59200         21 11         -1.0         0.002         66         19         29.97         761.2         167.1           181         56         2 646         50120         21 11         -1.0         -0.005         66         19         29.97         761.2         167.1           181         56         2 865         50200         22 11         -0.002         -0.016         69         21         29.05         61.0         761.0         165.1         761.0         165.1         761.0         165.1         165.1         761.0         165.1         761.0         165.1         761.0         165.1         761.0         165.1         761.0         165.1         761.0         165.1         761.0         165.1         761.0         165.1         761.0         165.1         761.0         165.1         761.0	Τ'		6	~	957	56166		22	= :				. 985	99	<u></u>	29.97	761.2	-	93.9	~ 0
153         56         2         321         322         321         322         321         322         322         322         322         322         322         322         322         322         322         322         322         322         322         322         322         322         322         322         322         322         322         322         322         322         322         322         322         322         322         322         322         322         322         322         322         322         322         322         322         322         322         322         322         322         322         322         322         322         322         322         322         322         322         322         322         322         322         322         322         322         322         322         322         322         322         322         322         322         322         322         322         322         322         322         322         322         322         322         322         322         322         322         322         322         322         322         322         322	۲°		6	7	228	58288		2 :	= :				819	8 4	2 9	/R. R.7	761.2		- 4	N 6
184         56         2         646         50120         21         11	ĭŤ		? ?	4 6	328	2070G		; =	: :		6	1	6	8 8	2	29.97	761.2		124.2	4 6
181         55         2         965         50200         22         11         .3         .005        9        9         .6         .9         .6         .9         .6         .9         .6         .9         .6         .6         .6         .6         .6         .6         .6         .6         .6         .6         .6         .6         .6         .6         .6         .6         .6         .6         .6         .6         .6         .6         .6         .6         .6         .6         .6         .6         .6         .6         .6         .6         .6         .6         .6         .6         .6         .6         .6         .6         .6         .6         .6         .6         .6         .6         .6         .6         .6         .6         .6         .6         .6         .6         .6         .6         .6         .6         .6         .6         .6         .6         .6         .6         .6         .6         .6         .6         .6         .6         .6         .6         .6         .6         .6         .6         .6         .6         .6         .6         .6         .6	1		8	• ~	9	50120		5	: :=		. 992		8	99		29.97	761.2		24.2	. 6
213         65         70126         22         11         600         7         605         21         29         761.0         60           193         59         606         70100         22         11         600         7         612         69         761.0         60           196         60         70100         22         11         1.00         600         7.012         69         761.0         60           152         46         70100         21         11         1.00         600         7.012         69         761.0         60           229         641         70100         21         11         1.00         600         76.010         69         761.0         60           229         70         60         70100         21         11         1.00         600         76.010         69         761.0         761.0         761.0         761.0         761.0         761.0         761.0         761.0         761.0         761.0         761.0         761.0         761.0         761.0         761.0         761.0         761.0         761.0         761.0         761.0         761.0         761.0         761.0	1		8	1	8	50200		22	=	_	.005		.016	69		29.96	761.0		1.61	~
193         59         606         70100         22         11         0.00         7         012         69         761.0         0           194         60         325         70200         21         11         .1         .002         .2         .003         69         21         29.96         761.0         0           152         46         50200         21         11         .1         .002          .010         69         21         29.96         761.0         0           216         60         70100         21         11                                                         <	1		2		325	70120		22	=	_	. 999	ņ	. 005	69		29.96	761.0	•	<b>.</b>	•
196         60         325         70200         21         11         .1         .002         .2         .003         69         21         29.96         761.0         0           163         50         641         70100         21         11         .4         .007          6.010         69         21         29.96         761.0         0           229         70         2         646         50100         21         11         .1         .002          6.010         69         21         29.96         761.0         6           216         64         3         325         50120         21         11           6.010         69         21         29.96         761.0         157           274         84         3         325         50120         21         11           6.010         6.02           6.010         6.010         6.02          6.010         6.010         6.010         6.010         6.010         6.010         6.010         6.010         6.010         6.010         6.010         6.010         6.010         6.010	7		8		3	70100		22	=	_	.000	۲.	.012	69	5	29.96	761.0	•	<b>6</b> .	•
152         46         70100         21         11	Τ,		3 :		325	70200		2 :	Ξ:	÷.	86. 19.	ų,	. 993	8	7 2	29.96	761.0	•	9.0	•
229         76         26         26         26         26         26         26         26         26         26         26         26         26         26         26         26         26         26         26         26         26         26         26         26         26         26         26         26         27         28         27         28         27         28         26         27         28         26         26         27         28         27         28         27         28         27         28         28         27         28         28         27         28         28         28         28         28         29         28         28         29         28         28         29         28         29         28         29         28         29         29         29         29         29         29         29         29         29         29         29         29         29         29         29         29         29         29         29         29         29         29         29         29         29         29         29         29         29         29         29         29	1		3		3			<b>.</b> .	= :	• •	) }		9 4	<b>8</b> 0	7 7	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	761.0	•		<b>&gt;</b> -
216         66         2         666         50100         21         11         0.0         0.000        2        003         69         21         29.96         761.0         156           274         84         3         325         50120         21         11        1        002        7        012         69         21         29.96         761.0         156           301         82         4         329         50100         26         16              2         156         21         29.96         761.0         156           272         83         321         50100         20         10         0.00           6         20         20         20         20         20         20         20         20         3         3         3         3         3         3         3         3         3         3         3         3         3         3         3         3         3         3         3         3         3         3         3         3	7		? ?	~	3	50200		5 5	: =	-	200	9	9	8		29.96	761.0		8.86	- 6
274         84         3         325         59120         21         11        1        092        7        912         69         21         29.96         761.0         156           391         92         4         329         59120         21         11        1        092         .7         612         63         21         29.96         761.0         156           391         92         4         329         59100         20         10         0.00         .7         612         63         21         29.96         761.0         156           293         83         4         670         50230         20         10         0.00         -0.00         -1.3         -0.23         63         21         29.96         761.0         156           210         64         50200         20         10         0.00         0.00         -1.3         -0.03         21         29.96         761.0         156           246         75         246         56200         20         10         0.00         -1.3         -0.03         21         29.96         761.0         156           248 <th< td=""><td>1</td><td></td><td>2</td><td>8</td><td>3</td><td>50100</td><td></td><td>5</td><td>=</td><td></td><td>. 999</td><td>2</td><td>. 963</td><td>69</td><td>21</td><td>29.96</td><td>761.0</td><td></td><td>98.8</td><td>-</td></th<>	1		2	8	3	50100		5	=		. 999	2	. 963	69	21	29.96	761.0		98.8	-
369         94         641         70200         21         11        1        002         .7         .612         63         21         29.96         761.0         .6           301         92         4         329         50100         20         10         0.00         .7         .615         6         29.96         761.0         156           293         8         4         670         50230         20         10         0.00         -1.3         -023         6         29.96         761.0         153           210         64         50230         20         10         0.00         -1.4         -007         69         21         29.96         761.0         153           246         75         20         10         0.0         0.000         -4         -007         69         21         29.96         761.0         153           246         75         2         10         0.0         0.000         -4         -007         69         21         29.96         761.0         151           246         75         2         10         0.0         0.000         -4         -007         69	7		\$	n	325	50120		5	=	_	002	7-	.012	89	2	29.96	9.192		196.2	•
301         92         4         329         50100         20         10         0.00         .3         .005         69         21         29.96         761.0         156           272         83         3 21         50100         20         10         .1         .002         .6         .010         69         21         29.96         761.0         156           293         84         50230         20         10         .1        002         .4         .007         69         21         29.96         761.0         153           246         75         2         50200         20         10        002        4         .007         69         21         29.96         761.0         153           246         75         2         10        902        4         .007         69         21         29.96         761.0         151           246         75         2         20         10        4         .007         6         21         29.96         761.0         151           217         66         2         2         10        9        4        07         6	ï		ž		3	78286		7	=	·	. 662	.,	. 012	69	5	29.96	761.0		•	-
272         83         3 221         50100         20         10         .002         .6         .016         63         21         29.86         761.0         163           293         4         670         50230         20         10         0.00         -1.3         -023         63         21         29.96         761.0         163           260         64         5020         20         10         0.00         -1.4         -007         63         21         29.96         761.0         153           246         75         2         3646         50200         20         10         0.00         -4         -007         63         21         29.96         761.0         151           246         75         2         364         50200         20         10         0.00         0.000         .4         .007         69         21         29.96         761.0         151           248         76         2         606         60120         20         10         .000         0.000         .6         0.000         .2         29.96         761.0         169           256         76         2         600 </td <td>ï</td> <td></td> <td>8</td> <td>*</td> <td>320</td> <td><b>8</b> <u>18</u></td> <td></td> <td>2</td> <td>=</td> <td>_</td> <td>. 66</td> <td>ņ</td> <td>.005</td> <td>8</td> <td>5</td> <td>29.96</td> <td>761.0</td> <td></td> <td>396.2</td> <td>-</td>	ï		8	*	320	<b>8</b> <u>18</u>		2	=	_	. 66	ņ	.005	8	5	29.96	761.0		396.2	-
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DAY LANDINGS	BAROMETRIC	PRESSURE	IN HC	78	29.96	29.96	29.96	29.96	29.86	29.96	29.96	29.96	29.96	29.82	29.95	29.95	29.95	20.00	29.95	29.95	29.95	29.92	29.94	29.94	29.84	29.94	29.94	29.94	29.94	20.00	29.94	29.94	29.94	29.84	29.84	29.94	29.94	29.84	29.94 29.94
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REREAD	NUMBER			-	•	-	-	•	•	-	7	-	-	-	_	_	•	-	•	-	•	_	•	-	•	_	<b>.</b>	- •	- •		• •		_			~ ~ ~ ~						
ARR GEAR	RUNOUTS	5	82	•.	383.5	496.4	406.4	426.7	388.6	403.9	403.9	419.1	386.1	<b>9</b> .	<b>9</b> .	386.1	383.5	381.0	<b>6</b> .	401.3	<b>9</b> .	401.3	401.3	398.8	381.0	393.7	396.2	386.2	3/6.5		393.7	0.0		393.7	393.7 398.8	393.7 398.8 414.0	393.7 398.8 414.0	393.7 398.8 414.0 0.0	393.7 398.8 414.0 6.0 386.1	393.7 4.4.0 6.0 386.1 386.1	393.7 4.4.6 6.6 386.1 396.1	393.7 398.3 4.4.0 6.6 386.1 396.2 1.9
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ETRIC	SURE	¥	88	761.2	761.2	761.2	761.2	761.2	761.2	761.2	761.2	761.2	761.2	761.2	761.2	761.2	761.2	761.2	761.2	761.2	761.2	761.2	761.2	761.2	761.2	761.2	761.2	761.2	761.2	761.2	761.2	761.2	761.2		761.2	761.2	2.5.5	761.2	761.2 761.2 761.2 761.2	261.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.	761.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2	761.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2
BAROMETRIC	PRESSURE	N H	79	29.97	29.97	29.97	29.97	29.97	29.97	29.97	29.97	29.97	29.97	29.97	29.97	29.97	29.97	29.97	29.97	29.97	29.97	29.97	29.97	29.97	29.97	29.97	29.97	29.87	29.87	20.97	29.97	29.97	29.97		29.97	29.97	29.97 29.97 29.97	29.97 29.97 29.97	29.97 29.97 29.97 29.97	29.97 29.97 29.97 29.97	29.97 29.97 29.97 29.97 29.97	29.97 29.97 29.97 29.97 29.97 29.97
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DECK ROLL		8	76	005	. 016	.010	. 002	410.	.005	007	010	600	. 002	9.00	010	002	003	9.66	021	0.000	.007	002	. 003	. 662	.003	019	<b>9</b>	012	200.		66 7	410.1	.002		<u>+10</u> .	19. 10.		- 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1			4.00.0 4.00.0 4.00.0 4.00.0 6.00.0	4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0 4.00.0
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LANDING DATA -	-	DDEL 1	1-2C		USS E	MT ES	PRISE	USS ENTERPRISE (CVN-65)	<b>(</b> 29)			۵	<b>∑</b>	DAY LANDINGS				
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BAROMETRIC	SURE	¥	88	761.2	761.2	761.2	761.2	761.2	761.2	761.2	761.2	761.2	761.7	761.7	762.3	761.2	761.0	761.0	760.5	769.7	762.5
BAROM	PRESSURE	¥	79	29.97	29.97	29.97	29.97	29.97	29.97	29.97	29.97	29.97	29.99	29.99	30.01	29.97	29.96	29.96	29.94	29.95	30.02
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	PISI	E	2	273	276	<b>5</b>	275	247	246	232	243	298	218	273	320	178	317	212	222	275	273
OFF-CENTER	DISTANCE	2	3	1	7	†	7	7	ŋ	†	†	7	ī	7	7	ę	-	7	1	†	7
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995	8		83	2586	2587	2588	2589	2596	2591	2592	2593	2594	‡	<b>4</b>	4177	4313	3	33	4535	4705	4953

DAY LANDINGS

USS ENTERPRISE (CVN-65)

LANDING DATA - MODEL T-2C

## **TA-4F DAY**

				χ	21	6678	6078	66/8 6811	5988	5988	6124	6365	6486	6486	3	6124	7	6033	6124	6124	6396	6396	6124	6350	6358	6124	6486	6124	6878	6305	6486	6486	6396	6486	6833	6385	6305	6305
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uss e	- MODEL TA-4F	WIND-VEL	ā	3	60	•	•	• •	•	80	<b>50</b> 4	9 43	*	*	• •	• •	2 9	2	-	= :	2 :	2 2	n	<b>10</b>	n r	'n	IO.	<b>5</b> 0 (	O 4	· –	-	-	-	-	- •		-	-
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USS ENTERPRISE (CVN-65)

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	WEIGHT		<b>TBS</b>	<b>50</b>	14200	14100	13800	14100	13688	13580	14100	14300	14300	14300	14388	14666	13788	14388	14300	14300	14200	14000	13/88	14388	14200	14300	14300	14300	14300	14300	14300	14200	14300	14300	13766	13788	14999	14666	14366
SOUL	LIFT	u.		61									1.00			9	1.00	:	1.00					1.00								1.20	1.1	;	- 66				
DAY LANDINGS	un	5		€	1.00	1.00	9	<del>-</del> -	1.18	1.10	1.20	<b>-</b>	- 00	- ·	9	9 6		1.10	- - -	1.00	1.20	1.20	99.	. 60	1.99	- 8.	 90 :	1.20		1.20	1.00	1.10	- - -	 	ee	1.66	1.10	9.7	9. t.
	\$	۲		11																																			
	KVPA	Z		<b>5</b>	1.06	1.09	1.12		3.1	1.09	1.12	1.09	=	+ 0. + 0.	)  -  -	79.1	. 6.	1.03	1.04	1.22	1.09	- 68	1.16	1.12	1.07	1.06	99.	• •	=======================================	1.00	1.14	1.15	<del>-</del>	70.	1.07	± :	1.20	1.02	1.16
(§2	V.dSA		N/S	5																																			
USS ENTERPRISE (CWI-65)	\$		\$	<b>±</b>																																			
ISE	VPAMIN		M/S	5	9	99	90	9 4	9	8	99	67	67	6	3	9 4	3	67	67	67	9	8	2 E	6	8	67	6	) (	6	67	67	96	67	67	8	92	9	9 !	67
TERPR	<b>₹</b>		3	7	129	129	128	2 5	127	126	23	2	2	2	2	120	2	3	2	2	129	128	12/	2	129	136	2	3 5	3	2	2	129	<b>8</b>	3	127	127	128	128	<u>5</u> 5
SS	VEOR		s/	Ξ	5	57	<b>5</b> :	5 2	<b>.</b> 3	3	8	8	8	<b>3</b> 3	79	8 2	8	2	62	69	62	8 (	8 8	3	62	3	25	\$ 8	8 8	8	3	62	3	<b>S</b>	20	S	٤ ج	<b>4</b> 1	8
<b>5</b>	VE		\$	•	118	Ξ	<b>9</b>	e :	12.5	124	128	2	13	2 5	871	2 6	5 8	2	121	77	120	9	211	2	121	ţ	<u>.</u>	C =	127	8	125	120	122	197	90	126	5	9	2 2
		•	K/S	•	•	•	•	•		•	•	•	•	•	<b>D</b> (	<b>.</b>		•	•	•	•					_				•	•	•	•	•	•	•	•		<b>.</b>
Ĭ	Ą	PERP.	3	•	•	•	•	• •	•	•	•	•	•	•	•	•	•	•	•	•	•	~	N 6	. ~	~	7	~	<b>,</b>		•	•	•	•	•	•	•	•	•	<b>D G</b>
1300	WIND-VEL	<b>.:</b>	¥	7	2	2	<b>~</b>	r) r	י י	, <b>2</b> 7	n	n	<b>7</b> 7	n,	· ·	2 r	) P7	, m	~	n	<b>m</b>	י מ	n #	, ra	•	<b>+</b>	<b>+</b> 1	2 m	, n	, ,	~	~	~	~	~	8	~ (	7	2 2
4 - 4	=	PAR.	2 2	•	25 1	23	23	 5 %	2 22	23	23	23	- :2:	23	8 8		2 2	23	25	25 1	23	2 2	 	2 2	27	27 1	22	 2 %	26	28	26 1	_	_	_	23	24	<del>-</del> :	*	 * *
ING DATA - MODEL TA-4F	3		M/S	so.																	_	.,								_						~			- 0
NIOW	VE-F1		<u>3</u>	•	200	3	6	4 t	} =	28		_	_		_	5 5					_		n 4					g o r			_	3		8				52	13 50 50
2	_				=	=	= ;	= =	? =	=	_	_	2 12	_ '				_	_	_	_	•		_	_	_	•		_	_	_	-	_	_	= :	5	= :	1	<del>-</del>
	VPAF	2	Ş	r) ~				2 2								)	_		_	_	•		2 2 2 2	-	•	•			•	-			_	<b>.</b>	~ ·	5	*	<b>9</b>	38 7
			3	7	7	_	_		_	_	_	_	_	- '	- '		_	_	_	_	-	-		-	_				_	_	_	_	_	_	_	_	_	_ `	
	200	ğ		-	1611	1612	1613	1615	1618	1619	1626	1621	1622	1623	1624	1623	1627	1628	1629	16.	183	1634		1637	1638	1639	1640	1641	1644	1645	1646	1647	1648	1649	1656	1651	1652	165	1654

			W.	21	6486	<b>±</b>	98	6486	82	6486	Ŧ	6214	98	6486	50	98	86	98	88	86	86	6385	80	6441	88	86	<b>5</b> 4	78	8	6486	6486	6214	<b>*</b>		6486	ſ	6486	<b>=</b> (	86
	WEIGHT			••	3	6214	6486	40	3	<b>4</b>	644	62	<b>3</b>	<b>9</b>	63	₹	<b>3</b>	\$	40	<del>3</del>	<b>4</b>	3	3	\$	\$	2	5	9	3	\$	<b>₹</b>	62	62		3	į	<b>1</b>	Ď	ě
	¥		SS	70	14300	13700	14300	14300	13900	14300	14200	13700	14300	14300	14000	14300	14300	14300	14300	14300	14300	13900	14100	14200	14300	14300	13500	13400	14000	14300	14386	13766	13700		14388		14399	14200	14388
INCS	HII	7.		<u>e</u>		1.99				1.10	1.10																										;	1.20	
DAY LANDINGS	HII	10		92	1.20	- 99	1.30	1.20	1.10	<u>-</u>	- - - -	- - - - -	1.10	1.10	- - -	1.10	1.10	1.10	<b>8</b> .	- 10	<b>9</b> 	<b>8</b> .	1.10	<b>8</b> .	- 8	- 10		<b>2</b>	<b>3</b> .	 	1.20	1.10	1.10	1.10	<b>2</b>	<b>9</b> .1	<b>1</b> . 1	1.10	- 8 -
	\$	<b>⋖</b>		11																																			
	KVPA	Z		•	1.0	1.01	1.10	1.05	1.02	= -	- - -	1.07	1.06	1.02	- - -	1.08	1.12	1.07	1.08	1.05	1.13	1.13	1.69	 •	1.05	- 98	- 65	<b>.</b>	1.01	1.17	1.08	1.03	1.98		1.12	,	<b>.</b>	90.	<b>.</b>
65)	V.dsA		N/S	5																																			
<b>(</b> C <b>V ⊢</b>	Ş		ž	<b>±</b>																																			
RISE	VPAMIN		<b>K</b>	5	67	8	67	67	99	67	99	65	67	67	9	67	67	67		_	_	99	99	99	67	67	9	65	99	67	67	65	8		67	!	67	8	67
NTERP	Š		\$	12	130	127	130	130	128	5	129	127	130	130	128	130	50	5	138	130	5	128	129	129	5	130	126	126	128	130	130	127	127		136		2	129	138
USS ENTERPRISE (CVN-65)	VEOR		Ş	=	S	55	<b>9</b>	88	Š	29	8	80	8	28	8	3	33	65	62	90	3	57	8	8	20	8	22	20		8	99	9	26	27		5	8	8	
	>		\$	•	103	106	116	106	105	=======================================	113	112	115	168	132	122	103	127	120	100	13	11	115	107	1	\$	102	8		129	117	118	109	=		= :	7	113	
u. T		PERP.	¥	•	•	•	•	•	•	-	-	-	-	-	-	-	_	-	<b>,-</b> -	-	-	-	-	-	<b>-</b>	-	-	_	7	4	<b>-</b>	~	8	8	n	<b>m</b>	<b>+</b> (	N.	<b>-</b>
<b>≵</b>	WIND-VEL	2	\$	•	•	•	•	•	•	7	~	~	~	8	8	~	~	8	7	~	~	N	~	8	N	~	~	~	*	₹	~	*	*	4	'n	<b>10</b>	<b>80</b> (	<b>13</b> (	7
<u> </u>	MIN	PAR.	\$	7	12	2	12	72	<b>*</b>	2	2	2	2	7	2	5	2	5	<b>*</b>	<b>*</b>	<b>*</b>	13	12	12	7	7	2	<b>±</b>	2	7	2	2	2	5	5	€ ;	<b>5</b>	9	77
DATA – MODEL TA-4F		_	₹	•	74	74	24	74	27	<b>58</b>	<b>70</b>	22	23	22	22	<b>5</b> 0	<b>50</b>	22	<b>58</b>	28	<b>9</b>	<b>58</b>	*	23	23	7	7	77	<b>5</b>	7	<b>5</b>	23	22	22	2	3	20	32	<b>5</b>
LANDING	VE-FILM		\$	60	57	3	5	3	3	5	3	21	3	3	3	20	5	8	3	8	5	5	3	57	3	3	8	3	3	3	8	3	57	5	3	3	3	ģ	21
3	Ý K		₹	•	•	•	-		•	-	•	•	_	-	•	•	•	-	•	•	_	-	•	•	-	-	-	•		•	•	•	•	•	•	2	•		•
	VPAF	2	Ş	"										_		-	•	•	•	•	•	•	•	_	-		_	_		٠.		_		_	-	27		-	
	5	•-	\$	~	¥	121	<u>*</u>	2	7	₹	<u> </u>	2	2	3	¥	<u>*</u>	¥	Ŧ	=	7	=	ž	=	7	7	Ĭ	ij	¥	7	Ę	=	5	7	7	<u>∓</u>	5 5 7	Ž	2	7
	3	ğ		-	1656	1658	1659	166	1662	1665	1665	1666	1667	1668	1669	1670	1671	1672	1674	1675	1677	1678	1679	3	<u> </u>	3	3	3	<b>1</b>	3	4052	4251	4252	4259	<b>1</b> 7	#	120	1981	4993

				-	_		•	_	•	•	<b>.</b>	•	<b>o</b>	•	•	€0	n	so.	•	<b>+</b>	<b>.</b>	7	<b>6</b>	7	S.	<b>G</b>	<b>+</b>	<b>o</b>	•	•	o,	G.	*	so.	S.	9	<b>.</b>	7	S	*	∞	2	۱ 🛨
ноок нетснт	OVER RAMP	3	4	'n	'n		'n	'n	2.5	'n	2.	'n	3.8	÷.	5.8	4	'n	7	'n	.i	2.8	, 2	3.9	4	4.5	7	ri เ	5	7	7	<u>-</u>	તં	'n	'n	6	4.6	2.9	'n	J.5	7	2.8	<b>P</b>	'n
HOOH	Ø.	t	90	10.3	11.1	7.4	11.3	10.3	5.0	12.9	6.2	<b>0</b>	12.6	15.0	9.5	9.3	10.7	8.1	8. E	7.8	<b>9</b> .	7.2	12.7	<b>8</b> .	14.6	9.7	11.3	<b>.</b>	8.5	<b>8</b> .5	6.2	e.	11.3	11.5	8.3	12.1	<b>7</b> .	12.2	11.6	7.9	9.3	10.5	1.1
WHEEL HEIGHT	RAMP	2	8	4.2	4.4	P. 17	*	4.2	3.0	4.9	3.0	<b>4</b> .	<b>6</b> .	9.0	4.0	J. B	<b>4</b> .4	J. 6	4.8	3.5	<del>-</del> :	3.3	5.0	3.8	5.5	4.0	4.5	ы. В	3.6	ы. В.	9. 9.	<b>4</b> .0	<b>4</b> .0	4.6	۳. ت	<b>5</b> .6	<b>6</b> .4	<b>4</b> .8	4.6	4.6	3.8	4.2	4.5
WHEEL	OVER RAMP	E	37	13.7	14.2	10.8	14.5	13.9	12.9	16.2	8.0	13.1	16.2	18.5	13.0	12.6	1.1	1.8	15.6	₽. E	13.3	10.8	16.4	12.5	18.1	13.1	14.7	12.5	<b>a</b> :	12.4	9.7	13.1	15.1	15.2	11.9	18.5	13.1	15.7	15.2	11.2	12.4	4.5	14.8
T 70	<b>8</b>	3	36	.070	.058	.033	440	.051	.049	.070	. 033	.060	. 96	. 975	. 091	. 036	.043	. 051	. 050	. 063	.049	.045	.059	.045	.058	.044	.058	.044	.051	. 057	.049	. 050	.050	. 062	. 044	. 059	. 057	. 957	. 055	. 965	.054	945	.048
MCLE A	8	DEG	SS	<b>6</b> .	3.3	9.	2.5	5.8	2.8	4.0	<b>6</b> .	4.6	4.0	4.0	5.5	2.0	7.4	5.8	4.0	3.6	2.8	2.6	4.6	2.6	J. J	2.5	3.3	2.5	2.8	n.	2.8	5.9	5.0	3.5	2.2	4.6	3.3	3.3	3.1	3.7	3.1	9.6	2.7
GLIDE PATH ANGLE AT TD	2	3	Ř	<b>.064</b>	990.	.040	. e38	. 055	. 055	976	. 029	. 969	. 969	.074	. 694	.049	.063	.052	. 068	. 065	. 052	.054	.067	948	.058	.050	.050	.049	. 046	.049	948	. 057	.052	. 969	.044	. 062	.056	. 059	.048	.058	. 962	957	.049
GLIDE	<b>8</b>	DEG	2	3.7	3.8	2.3	2.2	3.1	J. 1	4.4	1.7	4.6	<b>4</b> .0	4.2	5.4	2.8	3.6	J. 0	3.9	3.7	3.0	3.1	3.9	2.8	3.3	2.9	2.9	2.8	2.6	2.8	2.8	3.3	3.0	3.9	2.5	3.5	3.2	3.4	2.8	3.3	3.6	P.	2.8
	IGHT	s/s	32				3.1				<b>1</b> .8		4.0	<b>4</b> . <b>4</b>		7.0							<del>-</del> :	7.6													3.8		2.7				
	FREE-FLICHT	F/S	2				10.1				5. 8.		13.2	14.0		6.7							13.3	8 9.													12.4		6.9				
N		Ş	8	4.2	3.3	2.1	3.0	5.8	9.0	4.3	<b>6</b> .	3.3	3.8	4.3	5. 5.	<b>7.</b>	<b>5</b> .0	5.8	J. 7	n. n	2.7	2.7	3.0	2.5	J. 5	4.5	ص ص	<b>7</b> .8	4.0	4.0	5.9	4.0	<b>5</b> .8	<b>6</b> .	5.8	3.8	3.7	3.7	5.8	<del>-</del>	3.7	8.	3.0
NETWO SPEED AT TOUCHDOWN	AVG	5/5	<b>58</b>	13.8	10.7	<b>0</b> .	9.7	7.0	<b>0</b> .	<b>.</b>	6.3	10.7	12.5	<del>-</del> -	17.9	6.7	<b>.</b> 5	<b>+</b> .	<u>=</u>			<b>8</b> .	12.7	8.5	<b>9.</b>	1.1	12.4	<u>-</u>	=:	=	9.0	1.2	S	-2. -2.	<b>9</b> .5	12.4	12.2	12.1	9.0	13.4	12.0	9.2	6
PEED AT	8	K/S	<b>58</b>	•	٠. د.	7.0	2.8	9.5	d. 5	4.4	<del>0</del> .	2.7	S. 0	<b>+</b> . <b>+</b>	5.3	2.1	2.5	ر ا	-	4.0	2.5	2.7	3.8	2.5	3.1	3.3	•	2.5	3.2	ر ا	<b>%</b>	ص	 -	•	2.8	4.5	3.6	3.5	5.8	4.2	4.5	2.7	0.
20	STBO	Ş	22	13.1	<b>6</b> .0	9.9	-	9.0	8.6	14.5	4.0	•.	12.4	¥.4	17.4	7.0	8.2		- -	<u> </u>	-	•	12.5	<b>9</b> .1	5.9	9.9	 	<b>*</b> .	6.5	• •	<b>6</b> .	1.7	<u>-</u>	3.0	5.0	11.2	8.5	1.6	9.0	13.8	5.2	•	. 60
	<u>.</u>	Ş	<b>38</b>	<b>*</b> :	3.0	2.5	3.2	5.8	۵.0	4.2	<b>.</b>	3.0	a.5	4.2	4.5	<del>.</del>	7. 9.	5.6	J. 7	3.5	5.9	5.6	•:	2.4	3.5	S. S.	n. 0.	<b>.</b>	۵. د.	J. 5	<b>5</b> .8	3.3	2.8	•	S.0	<b>•</b> •	3.8	g.2	5.8	0.0	0.5		. e.
AIRCRAFT SI	PORT	ž.	ន	14.5	12.8	7.3	<b>*</b> .•	9.0	<b>6</b> .0	13.7	6.3	12.3	12.7	3.8	7.8	<b>9</b> . <b>†</b>	<b>9</b> .0	8.7	<u>-</u>	9. •	9.6	8.5	13.0	9.4	<b>+</b> :=	2.3	<b>e</b> :		1.7	<b>+</b> :	9.2	19.7	<b>9</b> .3	5.1	9.7	3.0	12.6	12.7	9.0	12.9	12.7	0	
	w	\$	7	<b>-</b>	4.7	2.3	9.5	2.4	7.4	3.6	2.2	9.0	•	<b>9.</b>	• •	J	2.3	5.0	_	2.9	<b>5.6</b>	ر. ا	<b></b>	3.5	0.D	u.5	N.0	2.7	5.50	0.0	_	•		_		4.6	_	_	3.3	4.5	3.0		9 6
	NOSE	٤	23	13.4	•:=	7.6	•.•	7.7	9.0	e. E	7.1	<b>9</b> .0	13.0	5.6	3.3	٠. ت	7.7	<b>6</b> .3	<b>8</b> .0	9.0	8.5	- -	5.0	1.6	9.	9.	<b>9</b> .	•	<b>+</b> : =	2.9	8.9	<b>+</b> .	6.9	3.8	9.5		1.5	12.4	6.7	1.2	1.7	•	 
997	2		2		_		_	_			_		_	_								•	•	-	_	•	•		•	•		•	•		•	-	_	_	_	_	88	5	362

USS ENTERPRISE (CVN-65)

	НООК НЕТСНТ	OVER RAMP	3 E	39 40						i	7.3 2.	5.1 4.	8.5 2.	1.0	7.3 5.5	 			12.7	10.0	11.0 3.	7.5 2.	9.0	6.7	15.5	2.6	9.0 2.	8.8 2.	7.9		2.1	12.6 3.	10.6 3.	10.1 3.	9.7 2.	7.4 4.	•	7.	15.0 1.4.
		<u>s</u>	3	80		_	_		- a	<u>)</u>	4.6	5.6	3.7	•	4.6	~ `	~ •	_ •	1 8.				4.2		 				o.0		7.7	•	-		<b>6</b> .	4.5		٠ 	
DAY LANDINGS	WHEEL HEIGHT	OVER RAMP	E	37	14.2	14.0	16.0	15.4	2.5	<u>:</u>	11.0	18.5	12.0	15.4	15.1	14.7	16.2	0.5	15.0	13.8	14.4	10.9	13.7	12.1	÷ •	16.2	12.8	12.3	11.7	. ·	15.5	16.0	14.3	13.8	13.1	14.9	•	12.0	7.7
DAY L	0T T	₽	3	36	. 949	.051	.040	.051	5 6	.032	.032	.072	.060	.054	.035	. 65	9. 9.	55.6	549.	.026	.037	.039	. 044	<b>4</b> 26.	946	.052	.047	. 028	826		626	140	.057	. 051	.041	. 050	.038	100	909
	GLIDE PATH ANGLE AT TD	6	DEC	જ	2.3	2.8	2.8	6.6	7.4		9.	<del>-</del> -	4.6	J.	5. 9.		9.7	- e	. 6		2.1	2.3	2.5	<b>.</b> (	2.5 4.5	9	2.7	9.	7.7	7.0		2.4	3.3	5.8	2.3	5.8	6 1	٠. ا	ر د د
	PATH	<b>15 - 15</b>	8	*	. 85	.059	. 056	.057	• •		.047	.064	. 059	.061	.042	.052	3	, 60 A	7	.031	.050	.051	.042	240	3	. 663	.048	646	970	6	5	4	. 963	.057	.046	. 048	6	800	60
-65)	GLIDE	₩.	DEG	33	2.8	4.0	3.2	n. 0	2 . 2 .	!	2.7	3.6	4.6	ы Б	4.6	<b>D</b>			2.7	-	5.8	5.9	7.4	5.5	, c	9	2.7	7. 8.		- ·		5.5	3.6	3.2	<b>5.</b>	2.8	•	•	J. J
E (CV)		FREE-FLIGHT	M/S	32									3.5								2.5		1	<b>7</b> .	N.	3.1		2.6											
ERPRIS	-	FREE-I	F/S	31									1.3								8.3		!		o.	10.3		9.0											
USS ENTERPRISE (CVN-65)	NOO	AVG	K/S	2	2.6	3.0	3.3	9.0 0.0	, v	2.5	2.1	4.2	4.5	<b>u</b> .u	7.7	2.3	7 Y	? r	. 6	2.1	2.7	5.6	2.8	<b>7</b>	, v , w	9	0.0	2.5	7.5		- 0	2.0	3.0	3.0	2.6	3.2	2.8	<b>9</b> .	2.7
_	AIRCRAFT SINKING SPEED AT TOUCHDOWN	₹	Ş	29	8.5	9.8	10.7	0.0	* <b>*</b>	7.1	6.8	13.6	=	• =	7.2	7.6	?		. G	7.0	8.8	8.7	2	7.7	? "	9	7.0	7.3	7.2	- ·		•	0.0	8.0	4.0	10.4	, 0,		12.1
14	PEED A	STBO	K/S	28	2.6	<u>ئ</u> ۔	J. 0	2.8		7.0	1.8	3.7	J. 5	3.2	2.0	2.5	7.9	) <b>-</b>	2.3	2.1	2.7	2.7	2.8	2.5	y c	2.8	2.9	2.5	 	2.5	- 0	2.9	2.7	2.9	2.7	3.3	2.7	ر ا	
DATA – WODEL TA-4F	W INC	S	2	27	6.5	10.1	9.8	6.5		9	9.9	12.1	<b>1.6</b>	<b>†</b>	6.5		?		7.7		8.9	8.8		7.4		9.5	4.0	8.3	<b>9</b> .9	•		4	8.7	<b>6</b>	8.8	10.7	•	12.0	÷:
- ATA	MT SI	PORT	\$	<b>56</b>	2.6	<b>5.8</b>	d.5	3.2	2.2 4.0	2.5	2.3	8.P	3.2	4.0	2.4	7.7	, v	; e		2.1	2.7	2.6	2.5	2.5	7.7	3.2	2.9	2.0	N (	7.8	- 0	2.9	3.2	3.0	7.4	7.9	2.9	•	2
LANDING (	AIRCA	X	2	23	6.0	9.3	<b>.</b> :			4.0	7.6	12.5	<b>19</b> .5	=	•	7.3	* ;	? =	9	7.0	9.8	9.0	9.0	7.6	P 4	10.5	9.0	<b>†</b>	7.7			4	10.6	9.0	•	9.7		 	12.4
3		MOSE	\$	54	2.8		u.u	٠.,	, v , v	2.7	2.6	2.8	<b>0</b> .0	۵. د	2.5	2.3	7. S	, ,	2.4	2.8	3.5	1.1	3.2	o.	* r	9	J. 5	3.7	2.5	9 · 0	, v	'n	2.8	2.7	7.4		2.8		•
		¥	Ş	2	•	•	10.7	•	. e	9.0	4.	D. 0	12.8	11.7	<b>8</b>	7.7	0.5	2 0		4.0	11.3	3.5	<b>10.</b>			12.8	<b>19.0</b>	12.1	- 1	? (			2.0	•	9.	<b>.</b>	n. 0		13.2
	200	2		22	3	Š	3	3		312	313	450	316	31	27	322	724	320		3	ž	3	3	<b>X</b>	3 3	7	33	ž	725	3;	3 3	9	470	472	474	476	ţ!	2	2

9			AIRCRAFT		NKING S	PEED A	SINKING SPEED AT TOUCHDOWN	N O			GLIDE	PATH A	GLIDE PATH ANGLE AT TD	T T	WHEEL HEIGHT	EIGHT	HOOK HEIGHT	IGHT
2	NOSE	SE	PORT	RT	22	STBO	AVG	<b>.</b>	FREE-FLIGHT	LIGHT		<b>3</b>	\$	>	OVER RALLP	d N	OVER RAMP	d.
	Ş	Ş	2	Ş	٤	\$	23	<b>*</b>	<b>5</b> /s	K/S	DEG	3	DEC	2	E	3	E	3
23	23	74	23	<b>56</b>	22	28	29	2	5	32	2	ħ	SS.	8	37	8	39	<b>•</b>
<b>482</b>	7.3	2.5	9.0	2.9	8.8	2.7	5.6	2.8			3.5	198	2.6	. 946	12.9	g. S	9.3	8.8
į	<b>•</b> .=	3.3	10.2	3.1	=:	4.0	10.7	3.2			3.5	196.	3.5	.066	16.1	<b>4</b> .9	12.2	3.7
<b>\$</b> :	e :	n.,	12.2	7.5	2:	4.0	= : 8: !	S. 6	•	•	۵. ۵.	<b>.</b>	0.°	.063	15.9	<b>4</b> .8	12.6	8.8
Ì	2 · c	7.7	12.9	9.0	* :		13.2	9 v	2.5	-	Ž	98	? r	9/0-	7	,	:	•
\$ \$	12.0	, v		, n	•	, n	2.5	, w			, ,	3		. 85. 85.	÷.	<b>;</b>	<u>.</u>	p.
181	<b>9</b> .	2.8	<b>.</b>	3.1	7.0	2.8	0.0	0.n			3.2	.056	2.9	. 856	15.4	4.7	12.2	3.7
495	11.8	3.6	<b>.</b> 0.	3.3	9.	2.7	10.2	٠. ۲.	10.2	3.1	2.7	.047	<b>5</b> .8	.050	12.9	3.9	<b>†</b> .	8.8
497	5.0	2.8	7.5	2.3	8.2	2.5	8.	7.4	<b>8</b> .0	7.4	2.8	949	2.4	. 042	1.5	3.5	<b>9</b>	2.5
498	e: ::	<b>9</b> .0	1.6	J. 5	12.1	3.7	#. 6.	3.6			3.1	<b>.</b>	3.3	.057	13.4	<b>-</b> :	<b>8</b> .8	J. 0
<b>6</b>	• =	3.3	-	2.8	8.8	2.7	•	2.7			3.0	.052	2.3	940	16.3	5. <b>0</b>	12.9	a.5
3	S. 5	7.6	•	2.1	6.2	<b>.</b>	<b>9</b> .9	2.1	<b>6</b>	7.	<b>6</b> .	.052	•	.032	4.0	4.5	<b>=</b> .5	J.5
3	e:	9 .	12.8		• •		*:	- (			•	3	* •	.677		•	•	•
	• •	) r	? •	-		, c		) c	•	•	y . c		• •	700.	? <b>:</b>	; ;	9.7.	· ·
3 3	12.0	, w	. =	7	. e	, v	10.8		18.6		2.7 2.7	964		929	5.5		15.5	£.4
50	8.7	2.7	-	2.5	7.0	2.1	7.8	2.4		)	2.5	828	7.7	.037	16.7	5.1	13.3	•
9	9.0	7.6	10.5	3.2	10.5	3.2	10.6	3.2			9.0	.053	2.7	.047	17.0	5.2	13.6	<del>-</del>
587	•.	2.8	<b>†</b> .	•:	8.3	2.5	7.4	2.5	7.4	2.3	2.4	. 642	<b>.</b>	. 032	9.0	2.9	6.3	<b>.</b>
8	11.7	3.0	9.0	2.7	10.0	3.3	<b>6</b>	3.0	10.5	3.2	2.7	٠ ۲	2.4	. 042	<del>-</del> :-	<b>4</b> .3	10.6	3.2
200	5.0	J	9.5	<b>5.</b> 6	<b>9</b> .5	5.8	<b>†</b>	5.8	<b>9</b> .5	7.8	3.2	928	5.0	52	<b>5</b> .	9.0		2.5
511	10.2	 	<b>†</b> ;	5.0	5.5	3.2	o. ;	9.0	9	•	4.6	929	•	.052	<b>+:</b>	<b>+</b> (	10.7	n. n.
512	n:	n (	16.7	N. N	•	 	9.9	3.2	12.8	ю. В	4.2	24	4.	999.	21.7		17.9	ب ب ب
213	9 0	9 7 7	2.0	• •		9 r	12.3	· ·			? • • •			649		٠ د د	9. <del>4</del>	7.0
515	17.1	•	13.6	-	13.0	•	13.4	-			*	878	4.7	5	21.6	9.	17.5	. IS
516	4.0	7.0	2.0	2.8	8.3	2.5	8	2.7			5.0	.051	2.8	.050	13.5	7	0.0	9.0
517	7.0	2.1	9.	2.9	10.3	7.7	<b>0</b> .	о. У.			3.1	.054	8.8	.050	10.0	3.2	<b>6</b> .0	2.1
518	7.7	2.3	12.9	8. 8.	•:	J. 0	13.1	<b>.</b>			<b>+</b> :0	. 969	<del>-</del> -	.072	17.3	5.3	13.7	4.2
519	7.7	7.4	<b>5</b>	<b>9</b> .	10.3	3.2	<b>*</b> :	J.5			4.6	996.	3.2	. 656	12.1	3.7	<b>+</b> .	<b>7.</b> 0
<b>2</b> 50		o.	S	0	= - -	J. 5	<b>*</b> :=	3.5			J	. 855	5.8	150	18.8	5.7	15.6	<b>4</b> .0
521	<b>9. 4</b>	7.6	<b>1.3</b>	ы В.	10.2	J.	r.=	3.5	1.2	4.6	n 0.0	.061	4.0	.059	¥.3	<b>+</b> .+	10.7	n. n.
522	-	2.5	<b>9</b> .	2.1	9.5	<b>6</b> .	7.3	2.7			2.8	<b>9</b>	<b>.</b>	. 627	15.6	<b>4</b> .8	12.1	7.7
523	•	<b>9</b> .	<b>8</b>	2.7	10.2		<b>.</b>	٠, ٠			4.6	. 628	<b>.</b>	.054	6.6	<b>4</b> .0	12.4	۵. ن
224	G.	2.7	19.2	 -	<b>a</b>	9	e. e.	٠. -			ر ان	.657	7. 9.	5	17.3	5.3	13.6	4.2
525	D. 0	<b>7.8</b>	8.7	2.7	<b>0</b> .	7.7	<b>6</b>	2.7			۵. و		٠, و	. 853	5. 9.	<b>4</b> .6	= :	4.6
<b>2</b> 26	7.3	2.5	7.6	2.3	4.0	5.	7.3	2.5			2.5	.043	1.7	. 030	13.4	<b>+</b> .4	<b>9</b> .	۵. ف
527	6.2	<b>0</b> .	6.3	 	4.5	<b>.</b>	ر د د	<b>.</b>			2.5	838	9.	. 627	æ. :	<b>6</b> 0 1	æ ;	5.6
228	۵. در	<b>7.8</b>	12.3	3.7	7.	J. 5	12.5	<b>8</b>			÷.	.075	<b>6</b> .	. 676	18.7	5.7	14.00 0.41	4.5
538	7.1	2.1	7.4	2.3	8.7	2.6	<b>9</b> .2	2.5			2.5	.044	2.5	4 4	13.2	<b>+</b> .e	10 10	7.7

USS ENTERPRISE (CVN-65)

Ħ	•	3	6	3.5	2.7	2.8	3.3	2.7	3.6	4.0	3.0	9.8	4.1	<del>-</del> -	3.4	2.9	3.3	2.7	3.0	4.2	2.7	2.8	 8.	3.0	3.0	3.3	<b>8</b> .		2.3	3.1	2.2	3.3	2.7	3.8	2.1	3.0	2.3	3.7		3.4		2.3	3.6
HOOK HEIGHT	OVER RAMP	E.	80	11.4	<b>9</b> .0	<b>0</b> .0	11.0	<b>0</b> .0	11.6	13.1	ø. Ø	ø. Ø	13.4	13.4	11.1	4.0	10.8	8.8	9.7	13.8	<b>9</b> .0	n.0	<b>6</b> .0	o. O	<b>9</b> .0	11.0	5.0		7.4	10.2	7.3	10.9	<b>8</b> .0	12.6	6.7	8. 6	7.4	12.1		11.2		7.6	11.7
WHEEL HEIGHT	RAMP	3	88	4.5	8.S	a.v	4.5	3.8	4.6	<b>9</b> .	<b>+</b> . <b>+</b>	<b>-</b> .	5.2	5.5	4.4	<b>+</b> .1	<b>+</b> .+	и. В	<b>+</b> .1	5.2	3.8	8.S	<b>9</b> .0	<b>-</b> .4	4.2	<b>+</b> . <b>+</b>	2.8		4.0	<del>-</del> .+	u.u	<b>*</b> : <b>*</b>	0.0 0.0	<b>6. +</b>	3.1	+.1	4.0	4.7		<b>+</b> .		3.5	4.5
WHEEL	OVER RALP	E	37	14.9	12.5	12.9	14.8	12.6	15.2	16.2	13.4	13.5	16.9	16.9	14.5	13.3	14.5	12.5	13.4	17.2	12.6	12.7	6.7	13.5	13.7	14.3	<b>9</b> .0		11.1	13.5	10.8	14.4	12.5	16.1	10.2	13.4	11.0	15.4		14.5		11.5	14.8
5 7	₹	3	8	. 654	. 052	. 036	.051	. 029	. 042	.634	.633	.035	.961	. 055	.041	. 967	.656	. 072	. 029	.056	.060	. 053	.025	.049	.041	.633	.065	450	. 036	. 636	.012	. 636	.043	. 055	. 036	. 026	.016	. 032	.038	.028	.052	.035	.045
GLIDE PATH ANGLE AT TD	6	DEC	33	3.1	9.0	7.0	7.9	1.7	7.4	<u>.</u>	<b>o</b> .	<b>5</b> .0	3.5	J. 7	2.4	3.8	5.8	<del>-</del> :	1.7	3.2	4.6	J. 7	4.	2.8	2.3	<u>.</u>	3.7	2.7	2.1	2.1	۲.	7.7	2.5	3.5	2.1	5.	œ.	<b>8</b>	2.5	1.6	a. 6	7.0	5.6
PATH /	<b>1 1 1 1 1 1 1 1 1 1</b>	3	ħ	. 040	.040	.042	.065	.033	.048	.043	.043	.048	.069	. 059	.050	. 073	.058	. 962	.040	. 063	.050	. 858	.032	948	.046	.044	838		.048	.053	. 029	.043	.048	.052	.044	. 038	. 025	.052		.047		. 037	.051
GLIDE	8	DEC	S	2.3	2.3	2.4	3.7	<del>.</del>	2.7	5.6	2.5	<b>7</b> .8	3.9	4.5	2.9	4.2	3.3	3.5	2.3	3.6	5.8	5.8	£.8	2.8	2.6	2.5	3.3		2.8	3.0	<del>.</del> 6	2.5	2.8	3.0	2.5	2.2	<b>*</b> :-	3.0		2.7		2.1	2.9
	LIGHT	K/S	32				2.7		2.2										5.0		3.1		2.0			<del>.</del>			2.8		1.2		2.5			<del>.</del>	<del>.</del>		2.3			2.5	
	FREE-FLIGHT	5/3	ភ				<b>8</b> .0		7.2										9.0		<b>19.</b>		6.5			6.1			<b>6</b> .		3.8		<b>8</b> .3			<b>9</b> .	5.1		7.2			7.3	
N	c	¥	8	3.3	2.8	7.4	2.8	1.7	2.5	2.7	<b>7.0</b>	7.4	ы. В.	3.5	2.6	3.5	2.8	3.5	2.2	3.B	3.5	3.2	7.0	2.5	2.5	2.0	2.7	3.5	7.6	2.5	7.7	7.4	7.4	3.5	2.7	1.7	<del>1</del> .6	2.0	2.1	2.3	3.3	2.1	3.2
AIRCRAFT SINKING SPEED AT TOUCHDOWN	AVC	Ş	59	10.9	. a	7.8	 	5.7	7.1	•	6.5	7.8	12.4	11.6	<b>8</b> .5	#. #	9.5	11.5	7.1	12.4	10.5	₹.	6.5	8.2	7.2	6.5	8.7	<b>+</b> .=	9.0	<b>8</b> .3		7.9	7.9	1.5	7.3	5.7	 	6.7	7.0	7.6	10.9	<b>9</b> .9	10.6
PEED A	STBO	Ş	28	3.2	5.8	<b>.</b>	2.8	<b>9</b> .	<del>.</del> .	2.5	-	2.0	<b>5</b>	3.3	2.7	3.6	7.7	4.5	2.3	<b>•</b> •	3.5	2.8	7.7	2.6	2.5	<b>5.0</b>	2.8	8.B	2.7	2.5	-	7.4	2.5	2.2	7.0	1.7	<b>+</b> :	2.1	7.0	2.2	3.2	2.1	3.2
KING S	S	٤	22	10.5			9.5	5.1	6.3	7.3	<b>.</b>	<b>9</b> .	12.6	10.7	6. B	12.0	8.8	1.1	7.5	13.1	10.5	<b>.</b>	7.2	<b>†</b>	7.1	9.0	-	12.6	•	6.3	4.0	7.8	<b>.</b>	10.8	6.5	5.4	4.7	6.6	6.5	7.3	10.5	<b>9</b> .9	10.5
AIS FA	E	\$	28	4.6	2.8	5.6	8.8	7.0	7.4	٠ <u>.</u>	7.7	7.7	Q.B	3.B	2.5	3.5	ر. د.	3.6	<b>5.0</b>	9. 9.	3.2	3.2	<b>.</b>	7.4	7.7	7.0	7.6	J. 7	2.5	<b>5</b> .6	<b>+</b> :	2.5	7.7	3.7	2.5	<b>9</b> .	1.7	2.0	2.5	4.7	3.5	2.1	3.2
AIRCR	PORT	2	22	1.3	9.5	4.0	<b>†</b> .	9.0	7.9	10.2	7.2	5.7	12.3	12.5	8.2	<b>*</b> :=	5.3	<b>8</b> . E	9.0	1.7	•.e	6.	8.2	9.0	7.2	4.9	<b>+</b> .0	5.0	8.2	8.5	4.7	<b>9</b> .	7.7	12.2	9.1	<b>9</b>	5.6	6.7	7.3	7.9	3.E	8.8	9.6
	w	Ş	*	2.1	<u>د.</u>	<b>6</b> .	3.B	2.1																									3.7	3.0	2.8	2.8	٦.	2.5	3.0	2.8	3.5	a. 0.	2.9
	NOSE	٤	23	7.0	5.5	6.3	12.6	7.0	<b>9</b> .0	8.8		8.7	<b>8</b> .0	8.5	8.	5.3	8.9	•.	3.5	12.5	•:	8.2	9.0	8.6	7.8	7.3	5.9	11.7	9.0	9.0	2.5	<b>.</b>	12.0	<b>0.0</b>	9.2		19.1		9.7	<b>.</b>	9.6	9.7	4.0
9 3	2		22	3	532	3	33	3	3	3	3	3			•			•	•		•																			282			

USS ENTERPRISE (CNN-65)

EIGHT	RAMP	3	\$	4.6	3.6	3.1	J.1	3.3	9.°	<b>a</b> 6	ص ص	* ·	2.5	9 6	. 4	•	. 4	, b	0.7	4.5	5.0	3.0	g.6	5.1	<b>6</b> 0.0	n. 1		9 <b>4</b> 9	<b>6.</b>	<b>+</b> . <b>+</b>	4.0	3.0	4.6	3.7	2.7	g.5	5. <b>0</b>	3.7	g.6	3.8	5.1
HOOK HEIGHT	OVER RALP	E	8	1.1	11.8	10.3	10.3	10.8	<b>3</b> - <b>3</b>	12.7	12.7			n •		14.7	14.1	=	12.8	14.7	16.5	12.9	11.7	16.8	12.6	9.0	> <		18.1	14.3	15.2	a. a	15.0	12.2	8.8	12.9	6.5	12.2	12.6	12.3	16.6
WHEEL HEIGHT	OVER RAMP	3	8	4.5	4.0	4.3	4.2	<b>*</b> :	€.			n •		٠ • •	'n	, e	• • • • • • • • • • • • • • • • • • •	* <b>*</b>	9.0	5.5	6.2	5.1	4.7	6.1	<b>4</b>	<b>*</b> ·	- ^	. *	6.1	5.5	5.7	4.2	3. <b>6</b>	<b>8</b> . <b>4</b>	S. S.	5.0	9. 9.	<b>4</b> .	<b>⊕</b>	<b>4</b> .0	6.2
WHEEL	OVER S	E	37	14.7	15.9	14.0	13.9	<b>+.</b>	15.6	16.3	13.6	•	? ! :	· •			2.5	* <del>*</del>	16.4	18.2	20.3	16.7	15.3	20.1	15.8	<del>*</del> :	9 F	15.5	10.0	18.0	18.8	13.8	18.4	15.7	12.4	16.4	10.0	15.8	16.1	15.9	20.3
AT T0	<b>8</b>	3	38	<b>.</b>	. 042	.059	.639	. 639	. 649	.067	38.	020	?	740.		948	6.5	639	. 947	.050	. 964	.059	. 063	. 053	. 054	.042	30.	943	.063	. 043	.056	.043	. 048	.043	.043	.045	. 038	.044	.070	. 054	. 058
ANGLE	•	DEG	33	2.0	7.4	4.0	2.3	2.2	2.8	<b>6</b>	9 0	7.7	r. 7	• •				2.5	2.7	2.8	3.6	4.6	3.6	3.0	n	7 .		- 6	8.0	2.4	3.2	<b>5</b> .6	2.8	2.5	2.5	7.6	2.5	2.5	<b>4</b> .0	ر ا	3.3
GLIDE PATH ANGLE AT TO	基金	3	ħ	. 948	.053	.072	6 6	.062	. 052	. 968	5.6		/ 6	709.			55.0	649	964	.058	.055	. 868	690.	.061	.045	. 045	949	65.0	190	.047	.055	.047	.052	. 057	. 055	. 969	.045	.047	. 686	. 069	.056
CL IDE	8	DEG	33	2.8	0. 0.	<del>-</del> -	2.3	J. 3	0. 0.	e. 6	4.2	9 6	7.7	B <	•	0 -	· ·	. 6	3.7	n.	7.7	4.6	3.9	3.5	2.6	5. <b>6</b>	2.6		3.7	2.7	3.2	2.7	J. 0	u.u	3.2	4.6	5.6	2.7	4.6	3.9	3.2
	LIGHT	X/S	32	2.5	2.5	S. 6											0	2.7		2.7						,	2.3				3.3				2.5			3.2			
	FREE-FLIGHT	F/S	ភ	7.3	8.3	1.8											6		;	Ø.							<b>*</b> :				10.9				8.3			10.5			
N	ၒ	Ş	8	2.5	2.3	3.6	2.3	2.3	J. 1	7.7	- (	9.7	* .	9 0	, c	, ,		2.7	2.8	2.7	8.0	3.7	3.0	4.0	3.7	2.7	2.5		a n	3.0	3.3	2.5	٠. ت	2.8	2.5	J. 7	7.4	3.0	4.2	3.2	J. 5
SINKING SPEED AT TOUCHDOWN	AVC	F/S	82	7.3	7.5	1.8	7.7	7.5	19.2	12.3	13.5	e e	9.						9		12.7	12.0	11.7	<b>-</b>	12.0		*:	• •	12.8	9.7	10.7	6.3	<b>-</b>	D. 3	<b>9</b> .1	10.3	7.9	<b>10.0</b>	13.9	10.6 0	11.5
PEED A	STBO	\$	28	2.3	2.2	3.0	2.5	2.4	<b>5</b> .3	ر د ن	4.2	, v	7.7	, c	, .	- 6		2.8	2.8	6.	0.4	•	3.0	3.2	3.6	2.7	2.5		•	2.9	3.2	7.4	8. 9.	2.8	2.5	3.5	2.7	3.3	4.2	J. 7	3.5
KING S	ST	2	27	7.5	7.2	11.8	-	7.8	10.0	9:1	13.7	7 0	7.7	•	9 6	) d				4.	13.1	13.1	11.8	19.3	1.8	<b>.</b>	 		13.2	9.0	10.6	7.9	<b>0</b> .0	<b>.</b>	<b>.</b>	10.4	<b>0</b> .0	10.9	13.8	10.2	11.6
_	E	Ş	<b>38</b>	2.2	7.4	8.0	7.7	2.1	5.9	•	•	/:	 	, , , , ,	, .	, ,		. 6	2.8	7.0	7.5	3.5	3.5	3.6	3.7	2.8	7.5		8.5	9.0	3.3	<b>5.6</b>	J.7	5.9	2.6	J. 7	2.1	2.8	<b>4</b> .3	3.5	3.5
AIRCRAF	POR.	2	22	7.2	7.8	11.7	7.3	6.9	9.0		2.5	» ·	? (					•	7	4.0	12.3		9.5	12.0	12.2	- ·	 	? •	12.6	8.0	6.9	9.7	6.3	9.5	9.5	10.2	<b>6</b> .0	<b>.</b> .	• • •	 5.	9. E
	w	\$	24	2.8	2.5	3.0	2.5	5.6	<b>.</b>	<b>6.0</b>	•		<u>:</u>	9 ¢		_		3.2			_	3.7	_	_	_	_		• «		_	_				a. 0		٠. ت	4.0	4.2	 	3.7
	MOSE	2	23	5.0	8.3	6.	7.4	<b>6</b> .5	3. <b>8</b>	<b>.</b>	•	•	•	n •	• •				P. 6		•	2.0	-:	1:1	3.2	<b>.</b>	بر ا	)	0.0	6.7	1.0	9.1	•.	9.3	2.9	6.5	9.7	1.2	3.8	5.0	2.1
995	2		2																									3 \$												_	

USS ENTERPRISE (CVN-65)

200			AIRCRAFT		KING S	SINKING SPEED AT TOUCHDOWN	TOUCH	N O			GLIDE PATH ANGLE AT TD	PATH A	NGLE A	T T0	WHEEL HEIGHT	EIGHT	ноок нетонт	18 <del>4</del>
2	2	MOSE	PORT	RT	R	STBO	AVC	•	FREE-FLICHT	E E	<b>2</b>		8	>	OVER RAMP	\$	OVER RAMP	<b>A</b>
	٤	Ş	5	Ş	٤	Ş	2	Ş	2	¥	DEC	3	DEG	2	E	*	E	3
22	23	<b>5</b>	52	<b>56</b>	23	<b>58</b>	8	8	5	32	SS.	3	33	8	37	82	39	<b>\$</b>
3	11.3	4.	•	3.5	19.6	3.2	10.6	3.2	10.6	3.2	3.0	.052	3.4	.059	17.5	5.3	13.8	4.2
ž	7.0	4.4	6.5	2.0	7.0	2.1	<b>9</b> .9	2.1			2.3	5	5.	. 026	12.0	3.7	9.6	5.6
788	<b>=</b> .5	J.5	9.0	٠. د.	7.8	2.3	8.7	2.7	8.7	2.6	3.2	. 856	2.7	.047	16.5	5.0	13.1	<b>4</b> .0
788	7.6	2.3	7.4	2.3	8.8	2.7	<b>-</b>	2.5			2.7	.047	2.1	. 637	14.0	4.3	19.1	4.7
787	<b>9</b> .0	٠. د.	6.7	7.6	9.5	2.8	8.0	2.7			2.7	. 047	7.4	. 042	14.6	4.5	11.2	4.6
2	12.0	3.7	7.7	2.4	 -:	2.8	4.0	2.6			2.7	.047	2.0	. 035	15.2	4.6	11.7	3.6
78	9.5	2.8	7.5	2.3	7.9	7.7	7.7	2.3			2.7	946	2.0	.035	17.0	5.2	13.4	4.1
8	<b>.</b>	2.5	9.9	2.7	9.8	2.7	8.8	2.7			3.2	. 055	2.5	.043	12.8	a.s	 -:	2.8
2	4.8	5.	= •:	3.3	<b>.</b>	<b>9</b> .0	<b>19.</b> 4	3.2			3.2	.055	7.4	. 042	17.8	5.4	14.1	<b>4</b> .4
797	<b>9</b> .0	2.5	9.0	7.0	6.1	<del>.</del>	6.3	<b>.</b>			2.1	.037	 •	.028	11.3	4.6	7.4	2.3
2	9.	2.0	9.9	2.7	9.5	<b>5.8</b>	8.8	2.7			3.2	.055	2.7	.047	17.1	5.2	13.1	<b>4</b> .
<b>2</b>	<b>*</b> :-	*.	. S.	2.8	<b>-</b>	3.1	<b>-</b> -	 			3.6	.064	3.2	. 056	17.9	5.5	74.1	4.4
3	8.7	2.6	7.9	7.4	7.4	2.5	7.6	2.3			2.1	.037	<b>6</b>	.034	11.9	3.6	8.5	7.6
Ē	•	3.2	7.6	2.3	9.0	2.7	8.2	2.5			2.8	949	5.6	.045	16.8	5.1	13.2	<b>4</b> .0
<b>2</b>	<b>9</b> .	2.8	12.0	3.8	13.0	•.	13.5	<del>-</del>			4.3	.075	4.3	.075	16.6	5.1	13.1	4.0
3	<b>.</b>	2.5	9.7	3.0	= • •	4.0	10.4	3.2			3.0	.053	5.6	.045	15.4	4.7	#. E	J. 6
Ī	æ.	2.7	•	<b>5.0</b>	7.7	7.4	7.6	2.3	8.7	<b>5.6</b>	3.0	.052	2.5	. 639	15.6	4.8	12.3	3.7
3	•	<b>9</b> .	1.6	3.5	<b>=</b> .e	J. 5	13.6	3.5			3.1	.054	۵. ف	.053	16.2	4.0	12.8	a. 8.
3	11.7	0. 0.	9.0	7.0	8.0	7.4	7.3	2.2	6.5	2.0	2.4	243	<del>.</del>	. 032	14.9	4.5	<b>3.2</b>	4.6
į	<b>8</b> .0	2.6	2.0	<b>7.8</b>	=	٠. ٥.	<b>9</b> .	2.8			3.6	.063	<b>5</b> .8	. <b>6</b> 49	14.5	<b>+</b> .+	<b>9.</b>	5.5
=======================================	<b>+</b> .=	u.5	13.2	7.	12.6	3.8	12.9	3.9			3.9	996	3.7	. 065	17.0	5.2	13.6	<del>.</del> .
51	9.5	2.1	<b>5.</b> 2	 	10.2	٠. ۲.	==	ر. د.			3.1	.055	<b>5.</b>	.045	18.7	5.7	13.1	<b>4</b> .6
812	<b>5.9</b>	3.2	6.7	<b>5</b> .6	<b>8</b>	<b>5.8</b>	<b>9</b> .0	5.8	8.8	2.7			<b>5</b> .0	. 035				
813	7.0	2.1	7.8	2.4	8.8	2.1	7.5	2.3			3.3	.057	2.5	. 638	14.5	4.4	<b>10</b> .5	3.5
815	8.7	7.0	<b>4</b> .	<b>7.</b>	7.0	7.7	7.7	7.4			2.8	<b>3</b>	2.2	.038	13.0	4.0	<b>4</b> .	2.8
5	<b>.</b> .	2.1	16.7	3.3	<b>.</b>	2.5	4.0	5.8			2.6	.045	2.4	.042	11.3	4.6	7.6	2.3
818	12.5	<b>9.</b> 0	<b>+</b> .	<b>7.</b>	•.	2.7	8.7	2.7	8.7	2.7	3.4	996	2.7	.047	17.8	5.4	- - -	4.5
	7.7	7.4	<b>9</b> .	7.4	<b>9</b> .	<b>5.0</b>	7.7	2.3			2.8	. 649	1.7	. 030	15.1	<b>4</b> . <b>9</b>	<b>†</b> :	J.5
25	3.5	•:	9.	•	6.7	5.3	9.7				0.	. 652	2.7	.047	10.2	۲.۲	6.7	5. 0.
821	13.4	<del>-</del> :	12.2	2.7	12.9	G. 5	12.5	J. 8			4.2	.073	3.7	.064	18.2	5.5	14.6	4.5
822	7.8	7.7	<b>4</b> .	7.6	<b>+.</b>	3.5	. d	2.8			3.3	.057	2.7	.047	14.5	4.4	<u>=</u>	4.6
823	<u>-</u>	7.7	1.5	3.5	19.7	٦.	1.1	4.4			3.8	990	٠. ۲.	.055	18.6	5.7	4.9	<b>4</b> .5
824	13.5	<del>-</del>	13.0	÷.	12.0	3.7	12.5	3.8	13.0	<b>.</b>	3.0	990	4.6	.059	29.6	6.3	17.2	5.2
825	7.2	2.5	<b>5</b> .5	3.5	19.2	<u>ا</u> .	10.3	3.2			3.0	. 653	J. 7	.053	13.7	4.2	10.2	٠. ۲.
826	7.4	2.3	<b>8</b> .3	2.5	7.7	7.7	8.0	7.7			2.9	.051	2.3	. 039	12.1	3.7	<b>8</b> .6	5.6
828	12.8	3.0	12.2	3.7	12.3	3.7	12.8	0.D	13.0	3.9	4.2	.074	<b>4</b> .4	. 074	19.6	<b>6</b> .0	15.8	Ð. <b>♦</b>
828	11.2	4.0	13.2	<b>•</b> · •	13.9	4.3	14.0	4.3				.072	3.8	990	16.2	<b>4</b> .9	12.7	3.9
3	8.0	2.7	7.7	2.4	6.5	2.0	7.1	2.5			2.7	. 648	2.2	. 039	11.9	3.6	8.6	2.5
83	D. 3	2.8	9.5	5.8	12.9	3.9	10.9	3.3			3.5	. 961	2.8	. 048	15.0	4.6	<b>+</b> .=	3.5
832	10.9	<b>3.3</b>	12.4	3.8	11.3	4.6	11.8	3.6			3.7	964	2.8	.048	19.5	5.9	16.3	5.0

1041	<b>4</b>	3	\$	3.5	3.7	2.8	u.u	3.1	2.1	3.2	3.7	<b>8</b> .0	÷.	<b>+</b> .	4.0	 	7.4	4.6	2.5	<b>7.8</b>	o.,	2.1	٠. ا	<b>J</b> .	a.6	<b>5.6</b>	4.5	<b>†</b> .	4.8	o.,	2.5	4.5	3.7	1.5	•· •	5.2	<b>4</b> .8	5.4	4.0	4.3	4.0	6.3	3.6
HOOK HEIGHT	OVER RALP	E	8	1.4	12.1	9.5	10.7	10.2	ø. 9	10.4	12.1	12.5	13.0	13.1	<del>-</del> :	16.7	7.9	<b>1</b> .1		<b>6</b> .5	<b>.</b>	6.7	- 0 · 0	10.2	a. E	9. 9.	4.0	74.3	15.6	0	<b>9</b> .3	14.8	12.3	•	13.1	17.0	15.7	17.8	16.1	14.2	16.1	20.7	11.9
WHEEL HEIGHT	RALP	3	8	4.5	4.7	•.	4.5	4.4	4.5	<b>+</b> :	<b>4</b> .	<b>6.</b>	5.1	5.1	<b>4</b> .	<b>6</b> .1	9.N	<b>4</b> .5		a. n	4.7	n.n	4.2	4.4	4.8	3.7	9. <b>6</b>	5. 5.	5.7	<del>-</del> :	9.B	5.5	4.8	2.6	5.1	6.3	8. 8.	9.9	<b>9</b> .9	5.5	6.9	7.4	4.8
WHEEL	OVER RAMP	E	37	14.9	15.4	13.0	14.7	<b>+.</b>	<b>•</b> :	14.3	16.0	16.2	14.7	16.7	4.0	20.1	2. 8.	6. <u>*</u>	12.4	12.9	13.7	10.7	13.7	14.0	15.7	12.3	18.4	18.1	18.7	13.4	11.7	18.2	15.6	9.0	16.7	20.0	19.3	21.5	19.7	18.1	19.8	24.2	15.6
5 7	Ž	8	88	. 665	<b>1</b>	.044	. 047	.054	<b>4</b> 20.		. 961	940	646	. 046	.043	940	.047	. 653	.047	. 628	.071	. 961	. 965	. 052	.046	.041	. 058	. 052	.054	.043	. 028	.056	.062	.020	.047	990.	. 851	<b>.064</b>	. 964	.058	. 059	.676	. 048
GLIDE PATH ANGLE AT TD	6	DEG	Ŋ	3.7	2.5	2.5	2.7	J. 7	<b>.</b>	2.3	S. 5	7	7.6	7. 9.	2.5	<b>5</b> .8	2.7	- ·	2.7	1.7	•	ر در	7.7	9. 9.	5.6	7.4	3.3	0. 0.	٦. ت	<b>7.</b> <del>†</del>	•	3.5	3.6	1.2	2.7	3.8	5.8	3.7	3.7	4.6	4.5	<b>0</b> .	2.8
PATH	<b>B #</b>	3	\$	<b>.</b>	. 655	.056	549	.052	. 046	. 048		-96	.057	. 655	<b>6</b> 24	.067	.054	.062	6.	550	.67	. 689	.074	. 048	. 655	. 659	<b>.064</b>	.657	. 661	. 656	<b>.</b>	. 658	. 858	. 037	.057	. 068	. 657	690	.063	.063	.061	.067	.052
GL IDE	<b>&amp;</b>	DEG	22	3.7	3.2	3.2	2.7	o. 0.	<b>5.8</b>	2.7	9.	S. 50	J. 7	- -	ر ا	3.0	٦.	J. 5	2.8	5.0	<del>-</del>	<b>.</b>	<b>₽.</b>	2.7	3.2	4.5	3.7	3.3	3.5	5.8	2.5	3.3	3.3	2.1	3.2	3.0	3.3	<b>4</b> .	3.6	3.6	3.5	3.8	3.0
	LIGHT	K/S	32			₹.	2.7													<b>o</b> .						7.4					7.0			<b>+</b> :									3.1
	FREE-FLIGHT	<b>5/3</b>	ñ			1.2	8.7													<b>6</b> .3						7.8					<b>9</b> .			4.8									10.2
	v	Ş	3	3.7	2.8	2.8	2.8	 	2.7	2.7	7.7	2.9	7.0		7.4	J. J	T.	<b>9</b> .	2.5	<b>e</b> .	B.	5.8	N.6	2.8	5.6	2.5	3.5	3.2	3.7	5.8	<b>.</b>	3.7	3.7	J. 3	2.9	3.7	3.1	3.8	<b>.</b>	4.0	4.6	3.8	9.5
SINKING SPEED AT TOUCHDOWN	AVC	53	8	12.2	9.5	. G	•	=	7.3	8.7	• •	<b>†</b>	9	æ.	7.8	19.7	<u>-</u>	<b>.</b>	-	6.3	12.5	G	<b>=</b> .8	<b>9</b> .5	8.7	7.1	<b>1</b> .6	10.5	12.3	9.5	<b>9</b> .1	12.2	12.1	<b>4</b> .4	. e	12.2	10.3	12.6	13.2	==	11.3	12.5	9.7
PEED A	STBO	Ş	20	3.7	2.8	2.7	2.8	3.3	7.7	2.5		2.8	2.7		2.3	S. 55	3.2		2.5	-	9. 9.	7.7	J. J.		2.7	2.3	3.5		3.5	2.5	1.7	3.0	2.7	1.2	2.9	8. 8.	5.8	3.8	3.0	4.0	3.2	0	9.
KING S	S	23	27	12.0	9.7	•	•	10.7	7.1	<b>9.</b>	: :	2.0	•	<b>.</b>	7.7	<b>=</b> .	19.7	•••		•	12.4		<b>.</b>	=	8.0	7.6	10.5	<b>8</b> .	1.4	8.1	3. <b>6</b>	12.7	12.0	a.5	9.5	1.0	9.7	12.6	12.7	1.1	10.5	12.5	9.7
	<b>=</b>	\$	*	3.8	2.8	5.0	<b>5</b> .8	<b>5</b> .8	2.2	2.7	J. 5	7.9	5. 6.		7.7	<b>.</b>	7.8		2.5	7.0	<b>9</b> .	<b>.</b>	9.0	2.7	2.7	7.0	7.7	4.0	0. 0.	2.7	7.0	3.7	3.7	<b>*</b> :-	2.8	3.0	3.2	3.0	3.0	3.2	3.8	8.5	3.1
AIRCRAFT	<b>708</b>	٤	22	12.3	9.5	<b>9</b> .5	•		7.2	9.9	• =		•		7.0	<b>.</b>		9.7	-	6.3	12.5		12.7	<b>.</b>	•	6.7	12.1	1.2	12.8	9.0	6.7	12.0	12.1	4.6	5.0	12.8	4.0	12.8	12.8	10.4	12.4	12.5	10.2
	lu <b>j</b>	\$	<b>5</b>	3. 0.	2.7	4.8	7.7	2.5	•	2.7		J.5		2.7	3.2	3.2	7.0	2.7	 -	2.7	4.2	5.5	2.7	<b>5.8</b>	ď.	3.0		3.5	_	_	_	_	_	_		_	_	_		2.7		5.5	3.0
	NOSE	٤	2	12.7	6.7	13.8	12.1	8.2	<b>.</b>	9.9	<b>†</b> .	7	s: =	<b>.</b>	*. •	<b>†.</b>		•	7.	<b>8</b> .0	<u>3.0</u>	8.2	<b>8</b> .8	6.7	7.	e: =	<b>I.5</b>	<b>*</b> :=	12.9	<b>9</b> .5	9.0	3.4	12.6	9.9	9.2	13.5	9.2	9.1.	9.0	8.8	5.0	1.4	8.
201	ş		8							3																																	

USS ENTERPRISE (CVN-65)

NATT SIMILIAG SPEED AT TOLICHOMAN CLIDE PATH ANGLE AT TO WHEEL HEIGHT HOOK HEIGHT NAMED AT SIMILIAG SPEED AT TOLICHOMAN CLIDE TO THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE AND THE A		3	LANDING D	DATA -	- MODEL TA-4F	Ì	3	SS ENTE	uss enterprise (cvn—65)	¥ 3)	<b>(</b> 2			DAY L	DAY LANDINGS			
MAS         FYS         MAS         FYS         MAS         FYS         MAS         FYS         MAS         FYS         MAS         FYS         MAS         FYS         MAS         FYS         MAS         FYS         MAS         FYS         MAS         FYS         MAS         FYS         MAS         FYS         MAS         FYS         MAS         FYS         MAS         FYS         MAS         FYS         MAS         FYS         MAS         FYS         MAS         FYS         MAS         FYS         MAS         FYS         MAS         FYS         MAS         FYS         MAS         FYS         MAS         FYS         MAS         FYS         MAS         FYS         MAS         FYS         MAS         FYS         MAS         FYS         MAS         FYS         MAS         FYS         MAS         FYS         MAS         FYS         MAS         FYS         MAS         FYS         MAS         FYS         FYS         MAS         FYS <th>•</th> <th>•</th> <th>AIRCR</th> <th>IS TAN</th> <th>NECING SI</th> <th>PEED A1</th> <th>T TOUCH</th> <th><b>N</b></th> <th></th> <th></th> <th>GL IDE</th> <th>PATH A</th> <th>NGLE /</th> <th>VT 70</th> <th>WHEEL</th> <th>HEIGHT</th> <th>H XOON</th> <th></th>	•	•	AIRCR	IS TAN	NECING SI	PEED A1	T TOUCH	<b>N</b>			GL IDE	PATH A	NGLE /	VT 70	WHEEL	HEIGHT	H XOON	
26         27         26         29         31         32         33         34         35         36         57         38         39         31         32         33         34         35         36         37         38         39         31         32         33         34         35         36         37         38         39         39         39         31         32         33         36         36         37         38         39         39         39         39         39         39         39         39         39         39         39         39         39         39         39         39         39         39         39         39         39         39         39         39         39         39         39         39         39         39         39         39         39         39         39         39         39         39         39         39         39         39         39         39         39         39         39         39         39         39         39         39         39         39         39         39         39         39         39         39         39         39<	NOSE		2	RT	STI	2	¥		FREE-FL	IGHT.	*	•	6	>	<b>9</b>	RAMP	OVER.	3
24         17.4         3.5         13.5         33.         34.         35.         36.         37.         38.         39.         39.         39.         39.         39.         39.         39.         39.         39.         39.         39.         39.         39.         39.         39.         39.         39.         39.         39.         39.         39.         39.         39.         39.         39.         39.         39.         39.         39.         39.         39.         39.         39.         39.         39.         39.         39.         39.         39.         39.         39.         39.         39.         39.         39.         39.         39.         39.         39.         39.         39.         39.         39.         39.         39.         39.         39.         39.         39.         39.         39.         39.         39.         39.         39.         39.         39.         39.         39.         39.         39.         39.         39.         39.         39.         39.         39.         39.         39.         39.         39.         39.         39.         39.         39.         39.         39. <th>Ş</th> <th></th> <th>٤</th> <th>Ş</th> <th>Z.</th> <th>¥</th> <th>٤</th> <th>Ş</th> <th><b>F</b>/S</th> <th>Ş</th> <th>DEG</th> <th>3</th> <th>930</th> <th>3</th> <th>E</th> <th>3</th> <th>E</th> <th>3</th>	Ş		٤	Ş	Z.	¥	٤	Ş	<b>F</b> /S	Ş	DEG	3	930	3	E	3	E	3
3.4         11.4         3.5         11.6         3.5         11.6         3.5         11.6         3.5         11.6         3.5         11.6         3.5         11.6         3.5         11.6         3.5         11.6         3.5         11.6         3.5         11.6         3.5         11.6         3.5         11.6         3.5         11.6         3.5         11.6         3.5         11.6         3.5         11.6         3.5         11.6         3.5         11.6         3.5         11.6         3.5         11.6         3.5         11.6         3.5         3.6         11.6         3.5         3.6         11.6         3.5         3.6         3.6         11.6         3.5         3.6         3.6         11.6         3.5         3.6         3.6         3.6         11.6         3.5         3.6         3.6         3.6         3.6         3.6         3.6         3.6         3.7         3.7         3.6         3.7         3.7         3.6         3.7         3.7         3.6         3.7         3.7         3.6         3.7         3.7         3.7         3.7         3.7         3.7         3.7         3.7         3.7         3.7         3.7         3.7         3	24		22	<b>38</b>	27	<b>38</b>	8	8	3	32	3	\$	88	36	37	8	8	\$
2.7         8.7         2.6         8.8         2.7         3.5         944         2.2         945         3.9         13.8         4.2         4.2         4.3         3.1         945         2.8         945         3.8         945         3.8         4.2         4.7         3.1         945         2.8         969         14.7         3.1         945         2.8         969         14.7         3.1         945         2.8         969         14.7         3.1         945         2.8         969         14.7         3.1         945         2.8         969         14.7         14.7         14.7         14.7         14.7         14.7         14.7         14.7         14.7         14.7         14.7         14.7         14.7         14.7         14.7         14.7         14.7         14.7         14.7         14.7         14.7         14.7         14.7         14.7         14.7         14.7         14.7         14.7         14.7         14.7         14.7         14.7         14.7         14.7         14.7         14.7         14.7         14.7         14.7         14.7         14.7         14.7         14.7         14.7         14.7         14.7         14.7         <	2.8		11.2	4.5	11.4	3.5	11.6	3.5			3.3	.657	3.8	990.	16.9	5.2	13.1	*
4,3         13.9         4,2         14.1         4,3         13.9         4,2         15.9         2.8         2.8         2.8         2.8         2.8         2.8         2.8         2.8         2.8         2.8         2.8         2.8         2.8         2.8         2.8         2.8         2.8         2.8         2.8         2.8         2.8         2.8         2.8         2.8         2.8         2.8         2.8         2.8         2.8         2.8         2.8         2.8         2.8         2.8         2.8         2.8         2.8         2.8         2.8         2.8         2.8         2.8         2.8         2.8         2.8         2.8         2.8         2.8         2.8         2.8         2.8         2.8         2.8         2.8         2.8         2.8         2.8         2.8         2.8         2.8         2.8         2.8         2.8         2.8         2.8         2.8         2.8         2.8         2.8         2.8         2.8         2.8         2.8         2.8         2.8         2.8         2.8         2.8         2.8         2.8         2.8         2.8         2.8         2.8         2.8         2.8         2.8         2.8         2.8			9.0	2.7	8.7	2.6	<b>.</b>	2.7			2.5	<b>.</b>	2.5	. 639	13.8	4.2	10.2	ń
2.8         5.3         1.8         9.5         2.9         4.3         4.3         4.3         4.3         4.3         4.3         4.3         4.3         4.3         4.3         4.3         4.3         4.3         4.3         4.3         4.3         4.3         4.3         4.3         4.3         4.3         4.3         4.3         4.3         4.3         4.3         4.3         4.3         4.3         4.3         4.3         4.3         4.3         4.3         4.3         4.3         4.3         4.3         4.3         4.3         4.3         4.3         4.3         4.3         4.3         4.3         4.3         4.3         4.3         4.3         4.3         4.3         4.3         4.3         4.3         4.3         4.3         4.3         4.3         4.3         4.3         4.3         4.3         4.3         4.3         4.4         4.4         4.4         4.4         4.4         4.4         4.4         4.4         4.4         4.4         4.4         4.4         4.4         4.4         4.4         4.4         4.4         4.4         4.4         4.4         4.4         4.4         4.4         4.4         4.4         4.4         4.4 <td></td> <td></td> <td>14.2</td> <td>7</td> <td>13.0</td> <td>7</td> <td>14.1</td> <td>¥.4</td> <td></td> <td></td> <td>7.7</td> <td>865</td> <td><b>6</b></td> <td>999</td> <td>- 19 - 19 - 19</td> <td></td> <td><b>*</b>:<b>*</b></td> <td>÷</td>			14.2	7	13.0	7	14.1	¥.4			7.7	865	<b>6</b>	999	- 19 - 19 - 19		<b>*</b> : <b>*</b>	÷
2.9         10.0         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9         2.9 <td></td> <td></td> <td>• ;</td> <td>2.0</td> <td><b>8</b></td> <td><b>.</b></td> <td></td> <td><b>6</b> 6</td> <td></td> <td></td> <td>ص. ا</td> <td><b>5</b></td> <td></td> <td>8</td> <td>14.2</td> <td>4. U.</td> <td><b>.</b></td> <td>ri (</td>			• ;	2.0	<b>8</b>	<b>.</b>		<b>6</b> 6			ص. ا	<b>5</b>		8	14.2	4. U.	<b>.</b>	ri (
2.9         10.6         2.2         9.4         2.9         9.5         9.5         9.5         9.5         9.5         9.5         9.5         9.5         9.5         9.5         9.5         9.5         9.5         9.5         9.5         9.5         9.5         9.5         9.5         9.5         9.5         9.5         9.5         9.5         9.5         9.5         9.5         9.5         9.5         9.5         9.5         9.5         9.5         9.5         9.5         9.5         9.5         9.5         9.5         9.5         9.5         9.5         9.5         9.5         9.5         9.5         9.5         9.5         9.5         9.5         9.5         9.5         9.5         9.5         9.5         9.5         9.5         9.5         9.5         9.5         9.5         9.5         9.5         9.5         9.5         9.5         9.5         9.5         9.5         9.5         9.5         9.5         9.5         9.5         9.5         9.5         9.5         9.5         9.5         9.6         9.5         9.6         9.5         9.6         9.5         9.6         9.5         9.6         9.5         9.5         9.6         9.5 <td>9.0</td> <td></td> <td></td> <td>• •</td> <td>2.0</td> <td>- •</td> <td>2.8</td> <td>ب د د</td> <td></td> <td></td> <td>? •</td> <td></td> <td>· ·</td> <td></td> <td>20.0</td> <td></td> <td>17.0</td> <td>ri d</td>	9.0			• •	2.0	- •	2.8	ب د د			? •		· ·		20.0		17.0	ri d
4.2         12.6         5.8         13.4         4.1         5.2         1856         5.7         1856         5.7         1856         5.7         1856         5.8         5.8         5.8         5.8         5.8         5.8         5.9         5.8         5.9         5.9         5.9         5.9         5.9         5.9         5.9         5.9         5.9         5.9         5.9         5.9         5.9         5.9         5.9         5.9         5.9         5.9         5.9         5.9         5.9         5.9         5.9         5.9         5.9         5.9         5.9         5.9         5.9         5.9         5.9         5.9         5.9         5.9         5.9         5.9         5.9         5.9         5.9         5.9         5.9         5.9         5.9         5.9         5.9         5.9         5.9         5.9         5.9         5.9         5.9         5.9         5.9         5.9         5.9         5.9         5.9         5.9         5.9         5.9         5.9         5.9         5.9         5.9         5.9         5.9         5.9         5.9         5.9         5.9         5.9         5.9         5.9         5.9         5.9         5	-						•	• •				3		3	. v.	; <b>-</b>	. :	i
4.1         13.6         4.6         13.1         4.6         3.1         1854         3.4         1859         16.3         5.6         3.2         3.6         3.6         3.6         3.6         3.6         3.6         3.6         3.6         3.6         3.6         3.6         3.6         3.6         3.6         3.6         3.6         3.6         3.6         4.7         3.6         4.7         3.6         4.7         3.6         4.7         3.6         4.7         3.6         4.7         3.6         4.7         3.6         4.7         3.6         4.7         3.6         4.7         3.6         4.7         3.6         4.7         3.6         4.7         4.7         3.7         3.6         3.7         3.6         3.7         3.6         3.7         3.6         3.7         3.6         3.7         3.7         3.7         3.7         3.7         3.7         3.7         3.7         3.7         3.7         3.7         3.7         3.7         3.7         3.7         3.7         3.7         3.7         3.7         3.7         3.7         3.7         3.7         3.7         3.7         3.7         3.7         3.7         3.7         3.7         3.	7		13.8	4.2	12.6	9	13.4	+			3.2	926	7.7	196	22.0	6.7	18.2	i en
3.7         13.9         4.2         13.1         4.9         13.9         4.0         3.9         .060         4.3         .075         15.4         4.7           2.8         3.9         19.4         3.2         3.9         .052         2.7         .048         2.9         .057         2.9         .057         17.2         .057         .057         .057         .057         .057         .057         .057         .057         .057         .057         .057         .057         .057         .057         .057         .057         .057         .057         .057         .057         .057         .057         .057         .057         .057         .057         .057         .057         .057         .057         .057         .057         .057         .057         .057         .057         .057         .057         .057         .057         .057         .057         .057         .057         .057         .057         .057         .057         .057         .057         .057         .057         .057         .057         .057         .057         .057         .057         .057         .057         .057         .057         .057         .057         .057         .057	*		13.6	+	13.0	•	13.1	•			 	3	4.0	.059	19.3	9.	15.6	; →
2.2         2.9         3.2         3.6         3.7         3.6         2.7         3.6         2.7         3.6         2.7         3.6         2.7         3.6         2.7         3.6         2.7         3.6         2.7         3.6         3.7         3.6         3.7         3.6         3.7         3.6         3.6         3.6         3.6         3.6         3.6         3.6         3.6         3.6         3.6         3.6         3.6         3.6         3.6         3.6         3.6         3.6         3.6         3.6         3.6         3.6         3.6         3.6         3.6         3.6         3.6         3.6         3.6         3.6         3.6         3.6         3.6         3.6         3.6         3.6         3.6         3.6         3.6         3.6         3.6         3.6         3.6         3.6         3.6         3.6         3.6         3.6         3.6         3.6         3.6         3.6         3.6         3.6         3.6         3.6         3.6         3.6         3.6         3.6         3.6         3.6         3.6         3.6         3.6         3.6         3.6         3.6         3.6         3.6         3.6         3.6         3.6 <td>7.0</td> <td></td> <td>12.3</td> <td>3.7</td> <td>13.9</td> <td>4.2</td> <td>13.1</td> <td>•</td> <td>13.0</td> <td>4.0</td> <td>3.0</td> <td>986</td> <td>4.4</td> <td>.075</td> <td>15.4</td> <td>4.7</td> <td>11.5</td> <td>'n</td>	7.0		12.3	3.7	13.9	4.2	13.1	•	13.0	4.0	3.0	986	4.4	.075	15.4	4.7	11.5	'n
2.8         10.1         3.1         9.8         3.9         3.9         3.9         3.9         3.9         3.9         3.9         3.9         3.9         3.9         3.9         3.9         3.9         3.9         3.9         3.9         3.9         3.9         3.9         3.9         3.9         3.9         3.9         3.9         3.9         3.9         3.9         3.9         3.9         3.9         3.9         3.9         3.9         3.9         3.9         3.9         3.9         3.9         3.9         3.9         3.9         3.9         3.9         3.9         3.9         3.9         3.9         3.9         3.9         3.9         3.9         3.9         3.9         3.9         3.9         3.9         3.9         3.9         3.9         3.9         3.9         3.9         3.9         3.9         3.9         3.9         3.9         3.9         3.9         3.9         3.9         3.9         3.9         3.9         3.9         3.9         3.9         3.9         3.9         3.9         3.9         3.9         3.9         3.9         3.9         3.9         3.9         3.9         3.9         3.9         3.9         3.9         3.9 <td>2.5</td> <td></td> <td>+.•</td> <td>3.2</td> <td>0.0</td> <td>9.0</td> <td>+.</td> <td>3.2</td> <td></td> <td></td> <td>2.7</td> <td>. 046</td> <td>2.8</td> <td>.051</td> <td>17.8</td> <td>5.4</td> <td>14.4</td> <td>+</td>	2.5		+.•	3.2	0.0	9.0	+.	3.2			2.7	. 046	2.8	.051	17.8	5.4	14.4	+
2.8 8.2 2.5 8.7 2.7 9.8 2.7 2.5 .844 2.8 .835 14.3 4.4 2.8 3.8 11.2 3.6 12.2 2.8 2.4 7.5 2.9 2.8 .845 2.4 .842 13.4 4.1 3.8 11.2 3.6 12.2 2.8 2.4 7.5 2.9 2.8 .845 17.3 2.3 2.3 2.3 2.3 2.3 2.3 2.3 2.3 2.3 2	-		÷.	2.9	<b>=</b>	3.1	<b>9</b> .	3.0			3.0	.052	2.7	.047	17.2	5.2	13.6	*
2.5 8.1 2.5 7.8 2.4 7.5 2.3 2.9 .856 2.4 .842 13.4 4.1 2.5 7.7 2.6 8.2 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85 2.8 .85	<u>.</u>		9.5	2.8	8.2	2.5	8.7	2.7	<b>.</b>	2.7	2.5	#	2.0	.035	14.3	<b>+</b> .	= -	'n
2.8         11.7         3.6         12.2         3.7         4.0         .070         3.6         .062         23.6         7.0         7.0         7.0         7.0         7.0         7.0         7.0         7.0         7.0         7.0         7.0         7.0         7.0         7.0         7.0         7.0         7.0         7.0         7.0         7.0         7.0         7.0         7.0         7.0         7.0         7.0         7.0         7.0         7.0         7.0         7.0         7.0         7.0         7.0         7.0         7.0         7.0         7.0         7.0         7.0         7.0         7.0         7.0         7.0         7.0         7.0         7.0         7.0         7.0         7.0         7.0         7.0         7.0         7.0         7.0         7.0         7.0         7.0         7.0         7.0         7.0         7.0         7.0         7.0         7.0         7.0         7.0         7.0         7.0         7.0         7.0         7.0         7.0         7.0         7.0         7.0         7.0         7.0         7.0         7.0         7.0         7.0         7.0         7.0         7.0         7.0         7.	4.5		•.	2.5		2.5	7.8	2.4	7.5	2.3	2.9	929	7.4	.042	13.4	<del>-</del>	9.0	ri
2.5 7.7 2.4 6.6 2.4 2.7 2.8 2.7 2.3 2.6 2.2 2.8 2.7 2.3 2.6 2.2 2.8 2.4 2.3 2.8 2.3 2.6 2.3 2.6 2.3 2.6 2.3 2.6 2.3 2.6 2.3 2.6 2.3 2.6 2.3 2.6 2.3 2.6 2.3 2.6 2.3 2.6 2.3 2.6 2.3 2.6 2.3 2.6 2.3 2.6 2.3 2.6 2.3 2.6 2.3 2.6 2.3 2.6 2.3 2.6 2.3 2.6 2.3 2.6 2.3 2.6 2.3 2.6 2.3 2.6 2.3 2.6 2.3 2.6 2.3 2.6 2.3 2.6 2.3 2.6 2.3 2.6 2.3 2.6 2.3 2.6 2.3 2.6 2.3 2.6 2.3 2.6 2.3 2.6 2.3 2.3 2.3 2.3 2.3 2.3 2.3 2.3 2.3 2.3	ر د د		12.7	<b>8</b> 6	1.7	, 0	12.2	7.0			• •	.676	ب د د	3	23.0	 • .	4.0	ni ·
4.1       13.3       4.0       13.4       4.1         3.5       9.2       2.8       13.4       4.1         3.5       9.2       2.8       13.4       4.7         2.6       7.3       12.5       3.7       13.3       4.7         2.6       7.3       10.2       2.7       .047       15.3       4.7         2.7       2.8       2.7       .065       3.2       6.6       4.9         3.7       10.2       3.7       .065       3.2       6.6       4.9         3.7       10.2       3.7       .065       3.2       6.6       4.9         3.7       10.2       3.7       .065       3.2       6.6       4.9         3.7       10.2       3.7       .065       3.2       6.6       4.9         3.8       11.8       3.9       2.7       .065       3.2       6.6       6.9         3.8       11.8       3.9       3.7       .064       3.2       6.6       16.2       2.7       4.9       6.9       16.2       2.9       6.9       16.2       3.9       16.2       3.9       16.2       3.9       16.2       3.9       16.2			•	, c	9 P	9 4	7 <b>•</b>	5.4 6.4				700.	0.7	<u> </u>	?		o •	ė P
3.9       12.1       3.7       12.5       3.6         3.5       9.2       2.8       10.4       3.2       2.9       .050       2.7       .047       15.3       4.7         2.6       7.3       10.9       3.2       10.9       2.1       2.3       .041       1.8       6.9       4.9         3.3       10.9       3.3       11.2       3.4       3.7       .065       3.5       .061       16.9       4.9         3.7       10.2       3.1       10.4       4.1       3.7       .065       3.2       .062       16.2       4.9         3.7       10.2       3.1       10.4       4.1       3.7       .065       3.2       .056       16.2       4.9         3.7       10.2       3.7       .065       3.2       .056       16.2       4.9       5.0       6.8       16.2       4.9       5.0       6.8       16.8       5.1       4.9       5.0       6.8       16.8       5.1       4.9       5.0       6.8       6.0       16.8       5.0       6.8       6.0       16.8       5.0       6.8       6.0       16.8       5.0       6.8       6.0       16.8       5.0<	7		13.6	;	13.3	•	13.4	-			•		-	.07	23.7	7.2	20.1	•
3.5       9.2       2.8       19.4       3.2       2.9       .959       2.7       .947       15.3       4.7         2.6       7.3       2.2       6.8       2.1       2.3       .941       1.8       .931       16.1       4.9         3.3       14.1       4.1       3.4       3.4       3.4       .966       3.5       .961       16.9       4.9         3.3       19.6       4.1       11.2       3.4       3.4       .966       3.5       .961       16.9       4.9         3.7       19.6       4.1       11.2       3.4       .966       3.2       .961       16.8       5.1       6.8       16.2       4.9       5.1       6.8       16.2       4.9       5.9       6.8       16.2       4.9       5.9       6.8       16.2       4.9       5.9       6.8       16.2       4.9       5.9       6.8       16.2       4.9       5.9       6.9       5.9       6.9       5.9       6.9       5.9       6.9       5.9       6.9       5.9       6.9       5.9       6.9       5.9       6.9       5.9       6.9       5.9       6.9       5.9       6.9       5.9       6.9	9		12.8	0.0	12.1	3.7	12.5	3.8			3.3	.057	3.7	. 965	19.8	9.9	15.9	*
2.6       7.3       2.2       6.9       2.1       2.3       6.9       2.3       16.1       4.9         3.3       16.9       3.3       11.2       3.4       3.7       665       3.5       661       16.9       4.9         3.3       16.9       3.3       11.2       3.4       4.1       3.7       665       3.2       661       16.9       2.2       2.2       6.0       3.2       3.6       16.9       3.7       662       3.2       662       3.2       663       3.2       6.6       3.2       6.6       3.2       6.6       3.2       6.6       3.2       6.6       3.2       6.6       3.2       6.6       3.2       6.6       3.2       6.6       3.2       6.6       3.2       6.6       3.2       6.6       3.2       6.6       3.2       6.6       3.2       6.6       3.2       6.6       3.2       6.6       3.2       6.6       3.2       6.6       3.2       6.6       3.2       6.6       3.2       6.6       3.2       6.6       3.2       3.6       1.2       3.2       3.2       3.2       3.2       3.2       3.2       3.2       3.2       3.2       3.2       3.2	2.9		- E	d.5	9.5	2.8	19.4	3.2			2.9	929	2.7	.047	15.3	4.7	11.8	~
3.3       14.1       4.3       13.2       4.1       3.7       .665       3.6       3.7       .665       3.2       3.9       3.1       3.1       3.1       3.2       16.8       3.7       .665       3.2       .656       16.8       3.1       3.7       .665       3.2       .656       16.8       3.1       3.2       3.2       3.2       3.2       3.2       3.6       3.2       3.6       3.2       3.6       3.2       3.6       3.2       3.6       3.2       3.6       3.2       3.6       3.2       3.6       3.2       3.6       3.6       3.2       3.6       3.6       3.6       3.6       3.6       3.6       3.6       3.6       3.6       3.6       3.6       3.6       3.6       3.6       3.6       3.6       3.6       3.6       3.6       3.6       3.6       3.6       3.6       3.6       3.6       3.6       3.6       3.6       3.6       3.6       3.6       3.6       3.6       3.6       3.6       3.6       3.6       3.6       3.6       3.6       3.6       3.6       3.6       3.6       3.6       3.6       3.6       3.6       3.6       3.6       3.6       3.6       3.6						7.7	e (	7.	;	•	2.5	<u> </u>		5	. <u>.</u> .		12.4	י מ
3.7       13.2       4.9       3.7       965       3.2       6.8         3.2       19.2       3.1       10.4       3.2       2.4       .042       2.6       0.65       3.2       4.9         3.3       7.2       2.2       3.7       .064       3.2       .056       16.2       4.9         3.2       11.9       3.1       3.7       .064       3.2       .056       16.2       4.9         3.2       12.6       3.1       3.7       .064       3.2       .056       16.5       5.0         4.0       12.6       3.9       4.3       .07       .064       3.2       .056       17.6       5.4         4.1       10.1       3.1       12.6       3.9       .07       .07       3.4       3.7       .064       3.7       .064       17.6       5.4         4.1       10.1       3.1       12.6       3.7       .07       3.7       .064       3.7       .064       17.6       5.4         4.1       10.1       3.1       12.8       3.7       .07       3.7       .064       3.7       .064       17.8       5.4         4.2       12.8       2.7	, c			) e	2 :	? r		? •	7.	•	, w		) ×	E	. e	» -	1.7.1	? ◀
3.2       10.2       3.1       10.4       3.2       2.4       .042       2.6       .045       16.2       4.9         3.3       7.2       2.2       8.6       2.7       2.8       .049       2.5       .044       16.2       4.9         3.5       11.9       3.6       12.6       3.7       .064       3.2       .056       16.5       5.6         4.0       12.6       3.1       3.7       .064       3.2       .056       16.5       5.0         5.6       11.9       3.6       13.9       4.3       .07       .067       17.6       5.4         4.1       10.1       3.1       12.6       3.8       3.6       3.7       .064       3.7       .064       17.6       5.4         4.1       10.1       3.1       12.6       3.7       .07       3.7       .055       3.9       .051       17.8       5.4         4.1       10.1       3.1       12.8       3.7       .055       3.9       .051       17.8       5.4         4.1       10.1       3.1       12.8       3.7       .051       3.6       .052       3.9       .051       3.7       .051       <	2		12.3		13.6	•	13.2	•			3.7	965	3.2	920	22.2	. 60	18.5	מוי
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3.5       11.9       3.6       12.0       3.7       .064       3.2       .056       16.5       5.0         3.2       9.5       12.0       3.1       3.5       .061       2.8       .049       10.9       5.4         4.0       11.0       3.1       12.0       3.9       4.3       .064       3.1       .067       17.0       5.4         3.4       10.1       3.1       12.0       3.7       3.2       .055       3.9       .054       17.0       5.4         4.1       10.1       3.1       12.0       3.7       3.7       .055       3.0       .055       19.9       6.1       4.8         2.0       9.2       2.8       9.0       2.7       3.7       .055       3.0       .051       14.9       4.5         3.9       12.5       3.8       10.7       3.6       .063       3.6       .065       3.0       .051       15.0       4.6         3.9       10.3       3.5       3.5       .061       3.1       .053       12.6       6.6         3.0       11.9       3.6       11.9       3.6       13.9       .051       3.9       12.6       5.8 <td>9.</td> <td></td> <td><b>:</b></td> <td>3.3</td> <td>7.2</td> <td>2.5</td> <td>•.</td> <td>2.7</td> <td></td> <td></td> <td>2.8</td> <td>6 7</td> <td>2.5</td> <td><b>*</b></td> <td>18.3</td> <td>5.6</td> <td>14.6</td> <td>*</td>	9.		<b>:</b>	3.3	7.2	2.5	•.	2.7			2.8	6 7	2.5	<b>*</b>	18.3	5.6	14.6	*
3.2       9.5       2.8       10.3       3.1       3.5       .061       2.8       .049       18.9       5.8         4.0       12.6       3.9       4.3       .07       3.8       .067       17.6       5.4         3.6       11.9       3.6       3.9       4.3       .07       .07       4.8       5.4         4.1       10.1       3.1       12.6       3.8       4.3       .064       17.6       5.4         4.1       10.1       3.1       12.6       3.7       .07       .055       3.9       .052       19.9       6.1         4.1       10.1       3.1       12.6       3.7       .07       3.6       .064       2.2       .046       14.9       4.5       5.6         3.9       12.6       3.8       2.7       2.7       2.5       .045       2.2       .039       15.0       4.6         3.4       9.7       3.6       10.7       3.5       3.6       13.4       4.1       4.1         3.9       10.3       3.5       11.9       3.6       13.9       .051       3.9       12.6       5.0         4.5       12.8       3.9       12.8<	<b>*</b> :		<b>+</b> .=	S. 5	= •	3.6	12.0	3.7			3.7	<b>3</b>	3.5	. 856	16.5	9. 9.	13.2	•
4.0 12.6 3.8 12.8 3.9 4.3 .076 3.8 .067 17.6 5.4 3.6 11.9 3.6 11.8 3.6 4.3 .076 3.1 .055 17.6 5.4 3.4 10.1 3.1 12.6 3.8 4.3 .076 3.1 .055 15.7 4.8 5.4 11.9 1.0 12.6 3.7 .064 3.1 .055 15.7 4.8 5.4 4.1 10.1 3.1 12.0 3.7 3.7 .047 2.6 .046 14.9 4.5 2.7 3.8 12.6 3.8 2.7 .047 2.6 .046 14.9 4.5 2.7 8.6 2.6 8.8 2.7 3.6 .062 3.6 .062 18.3 5.6 3.4 9.7 3.0 10.7 3.3 3.5 3.4 .055 13.4 4.1 4.1 3.5 3.5 3.4 .055 2.8 .048 21.6 6.6 4.5 12.8 3.9 14.0 4.3 3.5 3.7 .064 3.8 .067 20.2 6.2 5.8 11.9 3.6 11.9 3.6 2.9 .051 3.0 .053 12.6 3.8 3.8 11.9 3.6 11.9 3.6 2.9 .051 3.0 .053 12.6 3.8 3.8 11.9 3.6 2.9 .051 3.0 .053 12.6 3.8 3.8 11.0 3.6 2.9 .051 3.0 .053 12.6 3.8 3.8 3.8 3.8 3.8 3.8 3.8 3.8 3.8 3.8	-		• •	3.2	<b>.</b>	<b>5.8</b>	2.2	<del>ر</del> ا			3.5	5	8. 7.	<b>5</b>	œ.		15.2	*
3.6       11.8       3.6       3.1       .054       3.1       .055       15.7       4.8         3.4       10.1       3.1       12.6       3.8       4.3       .07       .054       3.7       .064       17.8       5.4         4.1       10.1       3.1       12.6       3.7       .064       3.7       .064       17.8       5.4       5.4         2.6       9.2       2.7       9.1       2.8       2.7       .045       2.6       .046       14.9       4.5         3.9       12.5       3.8       2.7       2.5       .064       3.2       .039       15.0       4.6         3.4       9.7       3.6       10.7       3.3       3.5       3.4       .051       3.6       11.9       3.6       3.9       .051       3.8       3.8       3.8       3.8       3.8       3.8       3.8       3.8       3.8       3.8       3.8       3.8       3.8       3.8       3.8       3.8       3.8       3.8       3.8       3.8       3.8       3.8       3.8       3.8       3.8       3.8       3.8       3.8       3.8       3.8       3.8       3.8       3.8       3.8	7.			•	12.6	<b>8</b> .0	12.8	<b>0</b> .0			<b>4</b> .4	.076	8. 8.	.067	17.6	4.0	13.8	*
3.4 10.1 3.1 12.6 3.8 4.3 .076 3.7 .064 17.8 5.4 4.1 10.1 3.1 12.0 3.7 3.2 .055 3.0 .052 19.9 6.1 2.6 9.2 2.8 9.0 2.7 9.1 2.8 2.7 .047 2.6 .046 14.9 4.5 3.9 12.5 3.8 12.6 3.8 2.7 2.8 5.6 3.6 .063 3.6 .062 18.3 5.6 3.4 9.7 3.8 12.7 3.9 10.7 3.3 3.5 .061 3.1 .055 13.4 4.1 3.4 9.7 3.9 10.7 3.3 3.5 .061 3.1 .055 13.4 4.1 3.5 12.8 3.9 14.0 4.3 3.6 11.9 3.6 2.9 .051 3.0 0.53 12.6 5.8 3.8 11.9 3.6 11.9 3.6 2.9 .051 3.0 0.53 12.6 3.8 3.8 12.6 3.8 3.8 12.6 3.8 3.8 12.6 3.8 3.8 12.6 3.8 3.8 12.6 3.8 3.8 12.6 3.8 3.8 3.8 3.8 3.8 3.8 3.8 3.8 3.8 3.8	3.5		<b>6</b> . E	9.0	<b>:</b>	9.P	₽. ₽.	9.n			J. 7	. 654	٠. د.	. 855	13.7	<b>4</b> . <b>8</b>	12.3	n
4.1 10.1 3.1 12.0 3.7 3.2 .055 3.0 .052 19.9 6.1 2.6 9.2 2.8 9.0 2.7 9.1 2.8 2.7 .047 2.6 .046 14.9 4.5 3.9 12.5 3.8 12.6 3.8 2.7 2.8 .063 3.6 .062 18.3 5.6 2.7 8.6 2.6 8.8 2.7 2.7 2.5 .043 2.2 .039 15.0 4.6 3.4 9.7 3.0 10.7 3.3 3.5 .061 3.1 .055 13.4 4.1 3.5 12.8 3.9 14.0 4.3 3.5 3.7 .064 3.8 .067 20.2 6.2 6.2 4.5 12.8 3.9 14.0 4.3 3.6 11.9 3.6 2.9 .051 3.0 0.053 12.6 5.8 3.8 11.9 3.6 11.9 3.6 2.9 .051 3.0 0.053 12.6 3.8	7.		11.2	4.0	<u>-</u>	J. 7	12.6	3.B			4.3	.076	3.7	<b>*</b>	17.8	5.4	14.2	*
2.6 9.2 2.8 9.0 2.7 9.1 2.8 2.7 .047 2.6 .046 14.9 4.5 3.9 12.5 3.8 12.6 3.8 3.6 .063 3.6 .063 3.6 .062 18.3 5.6 2.7 8.6 2.7 8.6 2.7 8.6 2.7 8.6 2.7 8.6 2.7 3.0 10.7 3.3 3.5 .061 3.1 .055 13.4 4.1 3.4 9.7 3.0 10.7 3.3 3.5 .061 3.1 .055 13.4 4.1 3.9 10.3 3.1 11.5 3.5 3.5 3.4 .059 2.8 .048 21.6 6.6 4.5 12.8 3.9 14.0 4.3 3.6 3.9 .051 3.0 .053 12.6 3.8 3.8 11.9 3.6 11.9 3.6 2.9 .051 3.0 .053 12.6 3.8	5.5		13.3	<del>-</del> :	<u>-</u>	٠. ت	12.0	3.7			3.5	. 655	۵. و	.052	<b>9</b> .0	6.1	16.3	80
3.9     12.5     3.8     12.6     3.8     3.6     .063     3.6     .062     18.3     5.6       2.7     8.6     2.7     2.5     .043     2.2     .039     15.0     4.6       3.4     9.7     3.0     10.7     3.3     3.5     3.4     .061     3.1     .055     13.4     4.1       3.9     10.3     3.1     3.5     3.7     .064     3.8     .067     20.2     6.2       3.6     11.9     3.6     2.9     .051     3.8     .057     12.6     3.8	4.5		9.7	<b>5.8</b>	9.5	7.8	•	2.7	<b>.</b>	7. 8.	2.7	.047	5.6	.046	5. 5. 7.	<b>4</b> .00	T.	17)
2.7 8.6 2.6 8.8 2.7 2.5 .043 2.2 .039 15.0 4.6 3.4 9.7 3.0 10.7 3.3 3.5 .061 3.1 .055 13.4 4.1 3.9 10.3 3.1 11.5 3.5 3.5 3.4 .059 2.8 .048 21.6 6.6 4.5 12.8 3.9 14.0 4.3 3.7 .064 3.8 .067 20.2 6.2 3.6 11.9 3.6 11.9 3.6 2.9 .051 3.0 .053 12.6 3.8	7.		12.7	9.0	12.5	<b>8</b>	12.6	ص. ت			3.6		0	. 962	18.3	0.	13.1	•
3.4 9.7 3.9 10.7 3.5 3.5 3.5 .061 3.1 .055 13.4 4.1 3.9 10.3 3.1 11.5 3.5 3.5 3.4 .059 2.8 .048 21.6 6.6 1 4.5 12.8 3.9 14.9 4.3 3.7 .064 3.8 .067 20.2 6.2 1 3.6 11.9 3.6 2.9 .051 3.9 .053 12.6 3.8 3.6 11.9 3.6 2.9 .051 3.9 .053 12.6 3.8	2.5		<b>9</b> .	2.7	9.0	5.6	<b>8</b> .0	2.7			2.5	3.	2.5	.039	13.0	4.6	11.3	n
3.9 19.3 3.1 11.5 3.5 3.4 .959 2.6 .948 21.6 6.6 14.5 12.8 3.9 14.9 4.3 3.7 .964 3.8 .967 29.2 6.2 13.9 3.6 11.9 3.6 2.9 .951 3.9 .953 12.6 3.8 3.8	8		11.2	4.6	9.7	9. 9.	10.7	J. J.			3.5	196	J	. 055	13.4	-: +	<b>o</b> .	n
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3.00 11:00 5.00 11:00 5.00 2:00 5.00 5.00 5.00 5.00 5.00 5.00 5.00 5	7		4.6	4.0	12.8	<b>0</b> .	÷.	<b>4</b> .		,	3.7	964	٠, <del>١</del>	.067	29.2	6.2	9.9	<b>.</b>
	3.7		11.8 5	, d	e :	, o	e:	, ,	e. E	۵. ه	2.5 0.6			559.	12.6	ים ים		N

200			AIRCRAF	-	SINKING SPEED AT TOUCHDOWN	¥ 033	T TOUCH	MOC			GLIDE	PATH ,	GLIDE PATH ANGLE AT TO	17 TO	WHEEL	WHEEL HEIGHT	HOOK HEIGHT	194
ð	2	NOSE	PORT	ET.	STBD	2	AVC	<b>.</b>	FREE-FLIGHT	IGHT.	8	<b>8</b> +46	6	Š	SVER.	OVER RAMP	OVER RAMP	<b>M</b>
	2	\$	٤	\$	٤	Ş	\$	\$	5,5	Ş	DEG	3	DEC	3	E	3	E	3
2	22	*	22	<b>5</b> 8	27	<b>58</b>	8	8	5	32	2	3	35	88	37	8	e e e	•
Ē	10.9	3.3	12.1	3.7	1.0	3.6	12.0	3.7			4.2	.673	3.5	999.	15.0	<b>9</b> .	11.6	3.5
2	<u>.</u>		4.0	2.6	•	2.1	7.4	2.5			2.2	.639	2.1	. 637	13.6	<del>-</del> :	<b>8</b> .8	3.0
2	•	2.1	<b>*</b>	5.9	7.5	2.3	6. 9.	2.7			4.0	. 659	2.7	940	12.6	3.0 0.0	8.7	2.7
	7.9	2.5	16.2	'n	e :	• •	• •	e o	,	•	- ·	<b>4</b> 26.	9 .0	.045	14.3	<b>+</b> ·	= '	4.0
	12.0	, d		 	) e	1.7	• ·	) v.	· •	, v	9 °	9 Y	9 Y	65 <b>.</b>	* · ·	- 4	÷ •	2.8
<u> </u>	1.4	-	14.5	*	13.5	; ;	. <del>.</del>	. <del>.</del>	;	;		975	. +	. 673	20.4	6.2	- 1. - 1.	5.2
=	•	2.7	+.0	2.6	9.0	2.6	8.5	2.6			2.7	.047	2.1	. 036	17.5	5.3	13.9	4.5
1012	11.8	3.6	<b>8</b> .5	7.6	8.0	2.7	8.7	2.7	<b>0</b> .0	2.7	3.1	.054	2.5	***	13.0	<b>9.</b>	9.2	2.8
103	10.3	۲.	8.3	2.5	7.5	2.3	7.9	7.4			Q. P	.052	7.4	. 042	17.2	5.5	13.6	4.2
=	13.2	•	12.7	<b>0</b> .9	1.7	0. 0.	12.2	7.7	12.5	ы. В.	J. B	. 966	3.5	196.	20.5	8.5	16.7	5.1
9	- <u>.</u>	•	77.0	9. 9.	2.5		13.2	•			4.2	. 673	7.7	. 964	13.3	4.1	10.0	<b>9</b> .
101	= '	n (	6.2		<b>+</b> 1	2.5	- 6	5.5	7.9	7.4	2.5	7	7.5	629.	12.2	3.7	<b>4</b> (	5.6
	o. ;	2.3	- (	2.6		7.e	D (	7.7			9.6		9 '	. e4.	12:1	•	9. (d	2.9
182	11.2	, n		, v		2.0	. <u>.</u>	, n			9 S	2 t d	2.5	878. 176.	* :		D. G.	7 7
1021	9	2.1		2.5	7.4	2.5	•	7.4			2.5	943	0.	.032	15.8	4	12.4	3.0
1023	•	9.0	10.5	3.2	<b>.</b>	7.7	10.7	3.2			3.0	.052	2.5	3	18.6	5.7	15.2	4.0
1025	12.9	0. n	11.2	4.6	10.2	J. 1	10.7	<b>J.</b>	11.7	a.6	3.3	. 058	2.7	. 047	14.0	4.3	10.7	3.3
1027	= '		13.4	- (	2.0	 -	12.0	7.5			۵. و و	. 963	<b>8</b> .0	999	19.4	<b>6</b> . 6	15.8	<b>4</b> (
	n. •	- ·		9 7	o. ;	* *	e :	9 4			9 °C	9 6 6 6	6 6 7	559.	12.8	o. v		7 7 8 9
3	10.2	, r.		4		*	15.0	4			7.7	496		92	22.4			, r
555	12.0	3.0	12.3	3.7	11.7	9.0	12.0	3.7			4.6	.059	3.0	.053	<u>-</u>	5.5	4.0	4.5
1636	15.6	<b>4</b> .0	15.0	<b>4.</b>	14.3	4.	14.6	4.5	15.0	4.6	3.0	. 668	4.3	.074	21.7	9.9	17.9	5.5
2	÷ :	<b>+</b> :4	15.7	<b>4</b> 6	12.6	9	9.4	<b>*</b> •	15.d	<b>+</b> .0	n. •	679	٠,٠	496.	21.1	* *	17.5	n .
2 2	12.4	, D	5.0	4.2	=	5	13.0	•			) <del>-</del>	.072	, n	838	25.7	7.0	22.3	<b>6</b>
-	<b></b> :	4.3	15.2	4.0	14.2	4.3	14.7	4.5			4.2	.074	3.7	. 065	19.0	5.8	15.5	4.7
=	12.8	<b>0</b> .0	13.3	•	12.5	B. 6	13.2	<b>+</b> .			4.0	.070	<b>+</b> .1	.072	16.6	5.1	12.9	8.0
1042	•	2.7	2.5		9 .	2.0	9.5	2.8			4.2	578	2.8	909	28.5	6.2	17.2	2.5
3 3	12.4	n •	2.9	2.4	15.1	•		- 6			- · ·	57.	, i	0 C	16.2	o 4	13.2	0 m
1046	13.1	•	13.5		12.4	n.	13.1	4.0			4.2	.073	3.0	. 963	21.6	9.9	18.5	5.6
5	12.9	3.0	12.2	3.7	1.1	4.5	1.8	3.6	12.2	3.7	3.7	.064	3.5	.056	23.6	7.2	19.9	6.1
1049	12.5	3.8	12.7	3.9	<b>-</b>	J. 7	=:	4.6			3.5	.062	2.8	. 049	20.7	6.3	17.1	5.5
5	16.8	5.1	16.7	5.1	15.7	8.4	15.9	<b>4</b> .	15.9	<b>4</b> .8	÷.5	.078	<b>†</b> :	. 878	17.0	5.2	13.4	÷.
165			- (	2.6	7.8	7.4	<b>6</b>	<b>5</b> .0			2.7	978	7.7	.041	13.8	4.5	a (	9.0
100		* 6	• •	7.	, ,		- 4	- c	•	•	7.7	929		. 623	12.4	2	D .	/:
2	D	4.0	¥: R	۲.0	:	¥ .	?	F: 9		D	٠. د	700.	۲.۵	2	::	r o	1	<u>,</u>

USS ENTERPRISE (CVN-65)

		3	LANDING DA	DATA - L	- MODEL TA-4F	Ì	ደ	S ENTE	USS ENTERPRISE (CVN-65)	₹ (3	(2)			DAY L	DAY LANDINGS			
3			AIRCRA	AIS TA	KING SE	PEED A1	CRAFT SINKING SPEED AT TOUCHDOWN	2			GLIDE	GLIDE PATH ANGLE AT TD	NCLE /	0T TO	WHEEL	MEEL HEIGHT	¥	HOOK HEIGHT
2	NOSE	SE	PORT	<b>.</b>	STBO	8	AVC		FREE-FLIGHT	1 <u>8</u>	SH#	ž	8	>	8	OVER RAMP	<b>9</b>	OVER RAMP
	2	\$	2	Ş	5	¥	5	\$	5,5	¥	DEG	3	DEG	3	Ħ	2	E	
2	23	*	22	28	27	<b>99</b>	78	2	£	32	23	ň	z	38	37	88	38	*
1217	13.2	•	10.2	<b>6</b> .	15.2	4.6	15.7	4.0			3.5	.061	4.5	.078	20.2	6.2	16.6	40
1219	0.0	2.8	9.	2.5	7.6	2.3	7.7	4.7			2.8	.048	2.1	.037	=	4.6	7.2	; ~i
1220	10.8	3.3	6.7	9.0	19.7	7.7	<b>.</b>						2.4	.041				i
1221	<b>9</b> .3	2.8	7.8	7.4	<b>4</b> . <b>9</b>	<b>9</b> .	7.0	2.1			2.4	.043	1.8	. 032	1.1	4.5	7.5	7
1222	9.0	2.7	8.8	5.6	7.4	2.3	<b>.</b>	7.4			8.2	.050	2.3	.040	18.4	5.6	15.1	*
1223	<b>8</b> .	2.7	<b>8</b> .	2.7	9.5	2.8	•	2.7	<b>8</b> .8	0. 0.	2.0	. 036	2.2	. 838	1.4	3.5	8.0	7
1224	9.7	2.8	<b>9</b> .9	2.7	8.7	5.6	<b>0</b> .	2.7			2.8	.049	2.5	.043	1.8.1	5.5	14.6	₹
1225	12.0	2.7	= •:	3.3	1.1	4.6	1.3	4.5			J. 0	.053	3.5	. 056	20.5	6.2	16.7	'n
1226	12.2	7.7	7.7	<b>+</b> : <b>+</b>	12.8	8.0	5. 0. 1.	4.2				.071	<del>-</del>	.072	22.1	6.7	18.5	'n
1227	13.0	•	17.7	4.6	17.2	2.5	17.4				S. 6	.087	ر د د	960	29.6	<b>9</b> .	25.7	<b>,</b>
1228	13.5	<del>-</del> :	15.6	4	15.1	<b>.</b>	15.4	4.7			<b>*</b> (	9/8	4.7	. 982	20.4	9.7	16.7	ıń ı
8221	2.5		: :	7	- :	- ·	• •	5.7	•	•	7.7	. 046	2.7	. 646 6	4.5	<b>4.</b> 4	:	n e
25			 	)   		) r	- * :	, ,			y -	25.0	9	70 <b>0</b> .	*			ń ĸ
1236	. =	2.0	) - : =	4.5		2.0	: =	, 4.			. 6.	.051	2.0	. 159	18.5	9.0	15.0	•
1237	-	2.5		7.0	9	2.9	0.0	9.			4.5	. 059	2.6	.045	13.4	÷	4.	~
1230	€.=	4.6	6.9	3.3	11.2	4.5	1.0	4.5			3.2	.056	8.8	.051	16.2	4.9	12.6	n
1242	12.1	3.7	8.0	2.7	<b>†</b> .	5.9		2.8	9.5	2.8	2.7	. 846	2.5	. 039	17.0	5.2	13.6	*
1245	13.0	•.	12.4	3.8	1.9	3.0	12.5	3.8			3.6	.063	Q. D	. 968	24.2	7.4	20.5	•
1246	12.4	3.8	9.0	•.0	<b>+</b> .	3.2	<b>=</b> .	3.1	<b>.</b>	٠, ١.	2.9	.051	O.	. 052	15.4	4.7	11.7	ń
1247	13.8	4.2	13.1	<b>7</b>	15.9	<b>4</b> .	14.5	<b>+</b> ·	,	,	0.D	. 969	<b>4</b> .0	. 969	15.4	4.7	5.5	rý :
1248	7.7	o	• ·	9	<b>.</b>		<b>6.</b> 7		•	2.7	2.5	.043	5.9	.050	4.3	<b>+</b> ·	10.7	ימי
1248	13.4	<del>-</del> ;	12.0	7.	e: :		12.0	7.7	2.5	o.0	3.2	. <b>9</b> 55	n. 1	85. 85.	20.0	- 0	16.2	<b>+</b> •
	· ·		• •	2.5		7.5	? :	7.5				) (1)			9.50	9 C	? •	o e
	7.7.1	· ·	5.5	, e	9.71		5.5	- 6				. 600 7	- 6	7/9.	5.5	7.7	) C	
		3.1	=	, r	9.0	3.3	10.5	3.2			3.4	999	3.2	.057	19.2	G. 10	15.2	₹
1254	12.6	3.0	11.2	4.0	10.8	J. J.	₽	3.3			2.6	.045	2.7	.047	17.5	5.3	14.3	₹
1255	<b>+.</b> =	3.5	9.0	5.8	12.1	3.7	=:• •:=	4.6			3.8	990.	3.5	. 061	15.5	4.7	11.7	'n
	1.4	3.5	<b>9</b> .3	2.5	<b>.</b> .	<b>7</b>	4.6	7.6	<b>9</b> .	<b>5.</b>	<b>5.</b>	.046	2.4	. 042	15.1	<b>4</b> .0	11.7	'n
	₽.E	3.6	<b>=</b> .5	3.2	= 0.	n. n	10.7	y.3			3.0	. 053	5.8	.051	23.5	7.2	19.9	•
	<del>-</del>	2.5	<b>.</b>	5.8	19.6	3.2	<b>19</b> .1	J. T.			ر. 1.	.054	5.8	.051	18.4	9. 9.	14.7	÷
1259	7.5	2.3	1.2	4.6	10.2	J. 7	10.7	<b>3.</b> 2			4.6	. 96	J. 1	.053	12.6	3.8	<b>6</b>	٠i .
1260	<b>9</b> .E	u.s	12.5	<b>10</b>	11.7	<b>9</b>	12.1	7.7			J. 1	.055	3.0	. 962	17.1	.2 .2	13.5	÷ ·
1261	6.7	۵. ا	÷.	3.2	<b>→</b>	<b>6</b>	<b>6</b>	0			0. 0.	.053	2.7	.046	17.7	4.6	<del>+.</del> +.	<b>.</b>
1265	<b>9.</b>	 S:	÷.	<b>4</b> .4	12.0	7.7	13.0	<b>9</b> .			N. W	. 658	ر د.	. 961	17.2	5.2	13.6	•
1266	<b>10.</b> 4	3.2	÷.	3.5	<b>o</b> .	<b>9</b>		0. 0.			9.6	.046	5.6	. 046	15.7	4.	12.1	n ı
1267	<b>9</b> .9	2.1		J. J	10.5	3.2	10.6 1	3.2			۵. ف	.053	2.6	.046	15.0	4 (	÷ :	i r
1268	13.9	<b>*</b> .2	5.5	- (	5.8 0.0	7 .		- ;	•	•	<b>9</b> (	. 969	٠, د د د	8/6	26.8	D 4	50.CZ	
1209	Ð.	٠ •	•. •	5.X	D.	7.7	». »	D. 0	7.01		3.5	. <b>6</b> 22	7.7	/40.	71.1	÷.	P. / -	i

<b>≥</b> 9
F 25
DEG RAD 35 36
33 34
F/S M/S
F/S 14/S 29 30
F/S 14/S 1
~ }
ឌ ឧ

EIGHT	RAMP	3	<b>4</b>	4.	4.5	4.3	3.5	<b>*</b> .	3.8	3.8	2.8	<del>-</del> -	<b>*</b>	ر ا	5.8		J. 1	J. J	2.5	2.6	<b>4</b> .	3.0	2.7	3.5	3.3	y.3		•	7.7	, ,	0.0	2.1	3.2	3.7	3.2	3.6	4.8	3.8	<b>6</b> .4	4.6	J. 0	5. 80
HOOK HEIGHT	OVER RALP	t	39	15.9	14.8	7.7	11.5	14.4	12.5	12.4	9.7	13.4	15.0	10.3	0 .5		19.1	10.9	7.3	8.5	13.1	12.9	œ. œ.	11.3	10.7	10.8		,	. :	9 F	12.7	7.0	19.6	12.1	10.6	12.0	15.7	12.5	16.2	13.1	<b>6</b> .	19.0
MHEEL HEIGHT	RAMP	3	88	6.9	5.6	5.4	4.5	5.5	4.8	4.7	<del>-</del> .	 -	9.g	<b>4</b> .4	<b>4</b> .0		4.3	4.5	4.6	3.7	5.1	5.1	3.8	4.5	<b>+</b> . <b>+</b>	<b>+.</b>		,	S . 4	h a	. <del>4</del>	4.0	*	₩.	<del>-</del> :	4.8	5.8	€.	<b>9</b>	8.	<b>+</b> .	7.0
WHEEL	OVER RAMP	E	37	19.8	18.3	17.8	14.9	18.0	15.8	15.5	13.3	16.7	18.5	14.0	13.1		14.1	14.6	1.1	12.1	16.6	16.8	12.5	14.8	14.5	14.3		•	n •		15.7	11.3	14.5	15.6	13.6	15.6	19.1	16.0	19.6	18.4	13.4	22.9
T 10	>	3	8	.671	. 046	. 059	940	. 064	. 048	. 052	÷.	.035	.051	. 626	. 638	. 947	. 854	. 961	. 036	. 044	.061	. 049	.047	828	. 048	.053	. 034	.012	600 600 600 600 600 600 600 600 600 60	/70.	929	640	928	.025	.054	940	.677	.056	.031	.050	. 055	. 988
MCLE A	<b>&amp;</b>	DEC	2	<b>.</b>	<b>5.6</b>	4.6	<b>5.6</b>	3.7	2.8	9.0	•	<b>.</b>	7.8	5.8	7.5	2.7	٠. ۲.	S. 5	<b>7</b> .0	2.5	3.5	2.8	2.7	2.8	7.8	0. 0.	<b>a</b> .	•	9 .		6.2	2.8	<b>3.</b>	<b>+</b> .	3.1	2.3	<b>+</b> .	3.2	<b>4</b> .8	<b>5.8</b>	3.2	5.0
GLIDE PATH ANGLE AT TO	<b>18</b>	3	*	.676	. 053	. 963	.058	. 963	.057	.049	• •	. 651	.052	.052	.040		.051	. 052	836	.045	. 052	.045	.052	.051	<b>.</b>	. 658		;	2	. 4	990	955	. 657	<b>.0</b> 54	990	929	6.79	999.	. 666	.055	.067	. 085
GL IDE	8	DEC	33	<b>+</b> .	3.1	3.0	3.3	8.0 0.0	3.3	2.8	2.3	8 :	B. 1	9. 9.	2.3		5.8	3.0	1.7	2.6	3.0	2.6	3.0	2.9	2.5	3.3		•	9.9		- <del>+</del> .	3.2	3.5	3.1	3.8	4.5	4.5	3.4	3.4	3.2	3.8	<b>6.</b>
	LIGHT	N/S	32			<del>-</del> .			4.5		<b>9</b> .														8.8				•	.3												
	FREE-FLIGHT	5/2	ñ			13.4			11.2	,	5.2														8.5				•													
N	,,	¥	8	3.6	2.8	3.8	J. 0	<b>8</b> .8	3.2	3.7	1.2	2.3	3.7	и. В	5.6	3.7	J. J	a. 8	2.3	3.5	3.8	2.8	٦. ۲.	4.8	<b>9</b> .	3.8	<b>5.8</b>		۲. د د	- 6		2.8	8.0	<b>.</b>	3.2	2.5	4.7	3.5	2.4	3.8	3.6	5.1
AFT SINKING SPEED AT TOUCHDOWN	AVC	53	<b>53</b>	11.8	9.5	12.4	<b>.</b>	12.5	10.5	12.2	<del>-</del>	9.6	12.3	10.7	<b>8</b> .5	12.0	19.8	12.8	7.7	<b>+</b> .+	12.6	5.0	10.3	1.3	<b>.</b>	12.3	n :	? !	• •		9.2	9.2	12.6	<b>†</b> .	10.5	<b>9</b> .1	15.4	₽.	7.9	12.4	11.7	16.7
PEED AI	8	Ş	28	3.2	٠. د.	2.7	5.9	9. 9.	4.7	3.7	r. –	2.1	رم د	3.2	2.7	3.5	٠. ت	3.7	2.3	5.0	3.8	2.8	2.8	4.5	2.8	3.7			* c	, r	9	2.5	9	2.5	3.1	2.5	<b>4</b> .6	3.0	2.7	0.	7.7	5.0
KING SI	STBO	\$	22	10.6	6.7	12.2	<b>†</b> .	11.7	1.1	12.0	<b>4</b> .4	<b>.</b> .	12.4	10.4	•	1.6	10.2	12.3	7.5	8.7	12.5	9.5	6.7	11.2	-	12.1	4.			Y :	11.7	8.2	12.7	7.4	10.3		15.0	11.8	8.8	12.4	12.1	16.5
NIS T	7	Ş	<b>56</b>	3.8	2.7	3.0	5.8	•.	3.2	3.7	1.2	7.4	2.7	<b>5</b>	2.5	<b>9</b> .0	3.5	a. B.	2.5	2.7	3.B	2.8	4.5	3.5	J. J	3.8	- i	٠. د	7.7	. ,		2.8	8	9.	3.3	4.2	4.8	3.5	2.1	3.8	<b>8</b> 7	5.2
AIRCR	\$	2	22	12.5	8.9	12.5	9.0	13.0	<b>19</b> .0	12.2	<del>-</del>	7.8	12.1	10.7	•.	<b>6</b> . =	 •	12.9	9.7	12.0	12.6	5.0	 	11.3	10.7	12.6	5.5	4.2	?;		5.5	7	12.6	4.5	10.7	7.8	15.7	11.3	<b>6</b> .0	12.4	<b>1.</b>	16.9
	'n	¥	<b>C</b> •	• .	3.5	3.B	٠, ١.	٦.	3.B	3.6	•	2.8	<b>*</b> :	7.0	2.5	3.8	3.5	B. B	2.7	3.1	0.7	J. J.	9.0	3.7	3.0	4.6		<b>.</b> (	7.7	,	•	9	2.0	<b>*</b>	2.7	2.0	<b>-</b>	•	3.0	a. n	7.7	4.0
	NOSE	٤	23	13.1	19.4	<b>9</b> . E	0.0	=.	12.4	12.0	13.2	n.	÷.5	<b>†</b> .	7.2	12.5	*. •	12.4	<b>8</b> .0	10.2	12.7	9.9		12.1	12.0	1.1	<b>0</b>				3.2		10.7	•	8.8	9.0	13.5	13.2	<b>8</b> .8	12.7	<b>9</b> .9	13.2
200	£		22	1316	1317	1318	1319	1320	1321	1322	1323	1324														1340	3	1342	2		1548	1551	1354	1555	1557	1559	1566	1561	1562	35	1564	1565

DAY LANDINGS

USS ENTERPRISE (CVN-65)

		5	LANDING DA	<b>*</b>	- MODEL TA-4F	1. 1. 1.	ž	SS ENTE	USS ENTERPRISE (CVN-65)	(CVIFE	્ડ			DAY L	DAY LANDINGS			
200			AIRCRAFT		MKING	SINKING SPEED AT TOUCHDOWN	r TOUCH	<b>N</b>			GL 10E	GLIDE PATH ANGLE AT TD	NGLE A	5	WHEEL HEIGHT	HEIGHT	НООК НЕТСНТ	1641
2	NOSE	SE	\$	RT.	is	STBO	AVG		FREE-FLIGHT	IGHT.	18 FE	2	8	>	OVER RAMP	RAMP	OVER RAMP	SAMP
	53	\$	5	Ş	5	\$	٤/٤	M/S	F/S	s/m	DEG	2	DEG	3	E	2	E	3
22	22	<b>3</b>	22	<b>38</b>	27	28	53	8	3	32	S	*	25	36	37	80	39	9
1566	14.7	4.5		4.3	14.8	4.5	14.3	<b>*</b> :			4.5	.678	5. 10.	990.	18.8	5.7	15.4	4.7
1567	12.2	7.5	10.3		12.0	9.0 9.0	10.9	3.3			3.7	.065	3.0	. 053	15.2	4.6	11.2	3.4
568	13.0	•	12.2	5.7	1.8	e,	12.0	۵. ن	1.6	3.3	9.5	.067	3.5	.061	20.7	8.0	17.2	5.2
1369	- 6	, id	÷ :		9.5	2.5	. e	5.5			4.6	.969	2.1	.037	12.8	o.,	ø ;	5.0
1575		9 . C	n =	N 17		- 17		9 10			\ n	65.	0 F	3 t G	15.4	* ^	16.4	N 4
1572	12.6	9	16.2	+	15.9	<b>•</b>	. 1 . 1				) n	. 858	+.7	.082	19.2	. 0.	16.3	, v
1573	13.3	-	14.2	4.4	12.8	3.8	13.4	+			0.0	890.	3.0	.067	20.9	4.9	17.3	5.3
1574	<b>9</b> .0	5.8	9.7	2.5	<b>9</b> .0	2.9	9.0	2.7			3.3	.057	7.7	.041	15.7	4.8	12.2	3.7
1575	7.0	2.1	•	2.7	7.3	2.7	8.5	2.6			4.6	.059	2.7	.047	12.0	3.7	8.2	2.5
1576	7.0	2.1	•	7.4	S.	_ 	<b>9</b> .	2.1			2.7	.047	5.	. 627	16.6	5.1	13.6	<del>-</del>
1577	12.8	<b>6</b> .0	7. T	4.6	11.7	9.P	1.5	3.5			9.6	.053	5.8	.051	16.9	5.2	5.5	<b>+</b> :+
1578	6.		13.0	•	13.6	<b>-</b>	 -:-	<b>4</b> .			ا رو د و	. 963	<b>n</b>	.063	22.5	Ø (	<b>6</b>	5.7
1579	2.5	- ·	- 6	ر د د د	• •	 	= :	٠.٠ د د			۵. ب	. 655	5.5	. 044 446	13.0			* .
	9 9	o .	12.9	, c	2	•	2.0	9 1			<b>9</b> (	9/9		. 664 64	<b>*</b> :		2 : 2 :	*.
	9.9	7.7		, , ,	• •	, k		, , , ,			5.5	. 64.0 67.0	4 · 4	.042 067	- •	• v	- ¥	
	2 2		2.0	- 0	2 6	• «	. C					7 7 9 9 4 4	) r		. 6		2 5	, e
38				, n	10.7	, to		3.5			. 0.0	. 863	9.0	.053	15.7	4	12.0	3.7
1585	<b>+</b> .	2.6	1.3	3.5	10.4	3.2	10.9	3.3			3.3	.058	5.8	.051	19.2	9.0	15.5	4.7
1566	<b>9</b> .	7.4	8.2	2.5	9.9	5.0	7.4	2.3			2.3	.041	<b>.</b>	. 632	12.0	3.7	8.5	2.6
1567	10.0	9	 :		-: -:	4.6	10.8	<b>3.3</b>			3.5	.061	2.5	.044	17.7	5.4	<b>+.</b> +:	*
366	12.1	2.7	- - -	9	7.7	, ,	9.E	ы. С. С.			بر ا زو	.061	٠, ١	.052	18.1	ب بن بن	14.7	4.1
200	0. <del>4</del>	7.7	14.0	2 Y		- 4	13.8	7 7	13.0	1,0	/ Y Y	94.6	\ P	909.	15.5 23.1	7.4	. e	9 6
1591	£.	3.0	12.5	9.0	13.7	4.7	13.1	4		!	B.B	990	3.1	.055	17.4	5.5	14.0	4.5
1594	1.6	3.5	10.7	3.3	<b>1</b> .8	3.3	10.7	3.3			2.8	. 049	2.8	.050	16.2	<b>4</b> .9	12.9	0. N
1595	<b>9</b> . =	3.5	1.7		5.5	3.2	==	4.6			3.1	.053	0. 0.	.053	20.6	6.3	1.1	5.2
1596	<b>6</b>	2.8	6.7	2.6	7.9	4.	<b>9</b> .9	2.5			2.5	44.	4:4	.042	5.8	4.2	<b>29</b> :5	 
080	B. :	, ,		? .		• •	7.01	- I			7. 1.0	9	7.7	9			7 ·	•
		• •	10.4	• •		• •	 	, r			ع د د	50 6	) e	. 6/9.	22.2	- •	2.0	9 ~
1661	12.2	7.7	11.3	4	=	7	=	4				858	2.5	941	19.1	6	15.8	4
1602	7.6	2.8	4	2.8	•	2.7	9.5	2.8			2.3	639	2.5	944	12.3	3.7	80	2.6
1663	10.8	3.3	13.1	•	13.0	•.	13.0	<b>4</b> .0			3.6	.063	4.2	. 073	18.2	5.5	14.3	<b>+</b> : <b>+</b>
1604	9.0	5.8	6.2	<del>.</del>	6.1	<b>a</b> :	6.3	<del>.</del>	6.7	7.0	2.4	.043	1.7	. 629	13.0	<b>4</b> .	9.5	5.8
1685	<b>9</b> .	7.4	12.8	۵. د	<b>9</b>	5.6	1.0	4.0			3.7	.065	3.0	.053	4.3	<b>+</b> ·	<b>9.8</b>	<b>u</b> .u
566		D	12.0	۵.۷ د ر	: : :	4 . 4 .	9. ¢	u. v			. u	.063	9 Y	.046	15.7	<b>4</b> , 4	12.¢	υ. •
1619		. <del>.</del> .		, D	4. 6. 9. 9.	, n	. o.	, b			. 6 2.9	. 656 560	2 5	.038	16.9	5.2	13.5	, <del>,</del>

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	#		2 ci.e.v	8 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	2	N 9 9 4 - 4 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	31 31	M/S	DEC	-	-			3	t	
		g u4-u44004000000000000000000000000000000	2	8 45-455444545 - 27-456665655	2 42.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2	8 44-44499 9 44-44499	<u>.</u>	32		₹	DEC	2	E			3
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		4 - 4 0 4 0 0 4 0 0 0 0 0 0 0 0 0 0 0 0		n-45999999999	2	4-254 6756 6756 6756			2.2	.038	2.3	. 941	16.5	5.0	13.0	<b>.</b>
		- 4444444444444444444444444444444444444		~ 4 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	v. a = 1, a = a \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	- 2 H + H H H H H H H H H H H H H H H H H			3.0	.052	3.2	. 656	16.7	5.1	13.1	4.0
		<pre>uu + u u + u u u u u u u u uu + u u + u u u u</pre>	<u> </u>	4 2 2 2 2 2 2 2 2 2 2	2.1.2.0 0.0.0 0.0.0 1.0.0 1.0.0	25.5 25.4 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0			1.9	.033	1.3	.024	12.0	3.7		2.5
		u + u u + u u u u u u u u u u u u u u u		,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	12.5 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0	n + n n			2.4	.042	1.7	.030	12.7	6.5	0.0	2.7
		4 2 2 4 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2		2 4 4 5 4 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	2.50 6.60 6.60 6.60 6.60 6.60 6.60 6.60 6	+ n n			3.1	.055	3.2	.056	16.0	9.	12.6	8
	6 6 7 7 6 6 4 6 7 7 9 7 7 9 7 7 9 7 7 9 7 7 9 7 7 9 7 9 7 9 7 9 7 9 7 9 7 9 7 9 7 9 7 9 9 7 9 9 7 9 9 7 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9		0 0 1 0 0 1 1 0 0 0 4 4 6 0 0 0 0 0	8 8 8 8 8 9 9 9 9 9	6 6 2 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	. o. o.			9.5	. 967	3.5	.061	17.4	5.3	• •	4.4
	8 7 7 8 9 4 4 8 7 7 8 9 4 4 8 7 7 8 7 7 8 8 7 7 8 7 8	u 4 u u u u u u u u u u u u u u u u u u	0	******	e. 6. 6. 6. 6. 6. 6. 6. 6. 6. 6. 6. 6. 6.	3.0			2.8	. 649	4.7	. 042	18.7	5.7	15.4	4.7
	72 0 0 4 4 4 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	4 10 10 10 10 10 10 10 10 10 10 10 10 10	- 0 0 0 0 4 5 0 0 0 0 0	n a n n i	12.5 8.9 1.21				3.1	.053	2.3	.041	-:	4.4	10.5	3.2
	2 0 0 4 4 6 2 0 2 2 4 7 0 2 2	8845486		9 n n	9.9	3.8			3.7	. 065	4.6	.060	20.4	8 2	17.0	2.5
	4 4 6 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	242444		22.	12.1	_	10.2	3.1	2.3	.040	2.3	.040	16.9	5.2	13.5	<b>-</b> :
	0 4 4 0 12 2 0 2 2 2	40400		<b>5</b>					3.6	. 063	3.3	. 058	24.6	7.5	20.8	6.3
	12.2	, 4 ki	- 0 0 0 0 7	•	<b>9</b> .	2.9			2.8	.050	4.2	.041	12.1	<b>4</b> .0	11.2	4.5
	4112	2 12 14 4 14 14	<b>8</b> 6	٠. ص	12.1				3.5	. 061	4.6	. 059	21.3	6.5	17.6	5.4
		S. 1	<b>0</b> .5	٠, د.	10.2	3.1	9.7	2.9	2.1	. 637	2.8	. 949	12.3	3.7	8.2	2.5
	<b>→</b> =	•		7.8	<b>0</b>		1.0	 -:	3.2	. 056	2.7	.047	18.3	5.6	14.5	<b>†</b> : <b>†</b>
	<b>₹</b>	7.7	10.2	٠. ا	<b>†</b> .			1	3.3	. 658	5.9	.050	23.8	7.3	20.0	<b>.</b>
	7 12.0	7.7	<b>19.7</b>	3.2	11.2	_	= :2	ы Б	4.6	. 628	n.	.056	17.7	<b>4</b> .	13.6	4.2
	= 0	* ·	= '	* .	= ·	4 1			2.8	929	2.5	•	12.1	3.7	<b>9</b> .9	2.7
	P 6	 	D. 6	4.5 • •	 	, c			9 P		- c	979	9. 4. 2. 4.	9 r	12.4	0.°
		•			7.5	, -				.624	9	647	2 7	) e	18.2	- w
		, N				, P			9.0	962	. 6	150	13.8	. 4		9
	3.2 7.7	2.3	7.6	2.3	7.4	2.5	7.2	2.5	2.0	.035	1.7	.029	12.4	80.00	0.0	2.7
		<b>9.0</b>	8.8	2.7	<b>9</b> .3	2.8			2.4	.043	2.5	140.	11.6	<del>-</del> -	<b>0</b> .0	0.
		2.7	<b>9</b> .0	<b>5.6</b>	8.7	5.6			2.8	. 648	7.4	-04	15.6	4.0	<b>1</b> .8	3.6
2.5	4.6	3.2	= (		19.79 10.79	n .			2.7	949	8. 9.	940			13.3	÷ (
		9 F	•	7.7		7.7			8.7	<b>8</b> 0		629	<b>9.</b>	? •		9 9
					) r	; «			; c	848	- 6	45.6	. E	- <b>-</b>	13.5	) (r
		P	9		•	9			4.6	990	2.6	945	6.	9.0	6	2.4
11.0	4 10.3	3.1	5.9	3.2	10.4	3.2			2.4	.042	2.5	770	14.6	4.5	<b>+. -</b>	5.5
6.8 2.	1.3.6	-:	4.3	1.3	3.8	1.2	<b>+</b> .+	<b>+</b> :-	1.3	.023	₹.	. 967	e: =	3.6	9.0	7.6
8.6 2.	6 9.1	2.8	<b>9</b> .5	5.8	<b>9</b> .3	<b>5.8</b>	9.5	5.8	3.1	. 055	5.6	.046	17.7	5.4	13.8	4.2
1.8 3.	6 11.6	3.5	<b>+</b> .=	3.5	1.5	3.5			3.7	.064	3.0	. 052	16.2	<b>4</b> .0	12.2	3.7
1.3 3.	4 8.2	2.5	<b>8</b> .	2.7	<b>8</b> .5	<b>5. 6</b>	8.2	2.5	2.8	. 656	2.3	140.	15.6	<b>4</b> .8	12.0	J. 6
.e. 8	3 16.9	J. J	9.5	2.8	19.1	J. 1			2.7	. 047	2.5	.04	15.8	4.8	12.6	ري 100
 J.	2 11.4	J. 5	-	2.8	10.2	J. 7			2.7	.047	2.5	.038	13.4	<del>-</del> -	10.2	J. 1
8.0	9.0	7.0	7.0	7.7	9. 9.	2.1			2.3	.040	<b>.</b>	. 032	16.8	 	12.9	J.9
9.7 5.	- T.	J.5	=	n.	<b>7</b> . E	J. 5			8. 9.	.052	٦. ر د	. 055	12.5	<b>20</b> 1	<b>0</b>	2.7
1.4	6 12.2	3.7	10.2	رم 	11.2	4.0			<b>-</b> .	. 672	ر ا	.054	18.8	2.7	15.1	4.6

USS ENTERPRISE (CVN-65)

		3	LANDING DA	2	- MODEL TA-4F	u T	5	S ENTE	USS ENTERPRISE (CVN-65)	(C8+	(5)			DAY CA	DAY LANDINGS			
99			AIRCR	NIS TA	KING SP	EB A1	AIRCRAFT SINKING SPEED AT TOUCHDOWN	N.			CL IDE I	PATH A	GLIDE PATH ANGLE AT TD	5	WHEEL HEIGHT	EIGHT	HOOK HEIGHT	FR
2	2	NOSE	ğ	<b>.</b>	STBO	٥	¥C		FREE-FLIGHT	IGHT		•	BW		OVER RAMP	d.	OVER RALLP	3
	2	\$	2	\$	5/2	\$	5,5	¥	F/S	K/S	DEG	8	DEG	3	E	3	E	3
23	2	<b>5</b>	22	<b>58</b>	27	28	29	8	2	32	33	*	35	38	37	88	8	\$
1656	9.8	•	10.8	3.3	9.3	2.8	0.0	3.0			3.5	196	2.6		11.6	3.5	7.8	2.4
1658	12.5	, c	<b>o</b> ;	8.7	4:	2.8	۳: د د	9.7	5.0	2.8	2.8	.046	•	<b>9</b>	16.0	ø. 4 •	12.2	3.7
30	1.7		10.3		. •	, v	. •	. r.			- 17	858	•		12.9	- o	- e	9 6
1662	10.3	n. 1	11.3	3.5	13.4	÷	12.5	3.8			3.7	.065			17.2	5.2	13.3	<b>;</b>
3	7.3	2.2	5.1	•.	<b>6</b> .4	<b>5.0</b>	5.8	1.8	6.2	<u>۔</u>	<b>.</b>	.034			14.2	4.3	10.8	3.3
1665	<b>*</b>	5.6	<b>.</b>		• •	7.4	8.5	2.5	8.7	5.6		.050			17.4		<b>-</b> - :	4.4
1006	7.7	2.5	 				10.5	2.2			* *	9 6		. 640 643	16.6	- · ·	12.8 19.8	
1668		3.5	7.0		•	9 6		, r			, m	629	2.8		18.3	9	5.5	4 4
1669		3.2	9.7	-	10.0	3.2	10.1	3.1			2.9	.051			15.4	4.7	12.5	3.8
1670	<u>.</u>	J. 7	<b>•</b> :	•	10.2	3.1	10.6	3.2				. 656	•	.043	15.2	<b>4</b> .6	11.5	3.5
1671	10.3	3.5	<b>19.7</b>		11.7	9.°	11.3	3.5			3.7	. 965			16.0	<b>6</b> .	12.2	3.7
1672	<b>9</b> .0	2.8	9. 6.	•	10.8	n. n	9.9	3.2			3.5	. 969	2.6	970	12.6	ان ا	<b>8</b>	2.7
1674	•	5.8	e: -		5.5	n .	11.7	ю (			2.5	. <b>6</b> 56				o. 0	<b>.</b>	4 ¢
673	<b>.</b> .	• • •	? •	, c			2 · c	B . c			7.5	. 600 673	0.2 0.4		 	P ~		N 1
1678	13.0	•	12.6	•	12.6		12.6	9 9			9.0	.052			17.4	5.0	• •	. <del>.</del>
1679	- -	2.5	11.2	-	1:1	4.5	11.2	4.0				990			28.7	8.0	17.0	5.2
166	8.7	2.6	8.7		9.0	2.7	8.8	2.7				.046			14.7	4.5	10.7	3.3
1681	1.8 8.	3.6	<b>o</b> .		13.4	7	11.7	0.0 0.0				. 059			13.2	<b>4</b> .0	2.0	2.8
3	- -	ы. В	9.9		<b>5</b> .6	3.5	10.6 6	3.2			0.6	.052			12.0	۲. د ۲		9 0
	= 6	• •	9 ;			) r	7.0.5					809 609			25.5	- ^		
=	7	9	•	. 6		4.	8.2	2.5			•	3		9.	2	:	?	3
3	6.9	2.0	7.4		4.3	J. J.	5.8	<b>9</b> .			9.1	.028			14.2	4.3	10.7	3.3
4652	9.	7.4	12.4		10.6	3.5	12.4	3.8			-	.676			15.0	<b>4</b> .6	1.5	3.5
4251	12.1	3.7	10.7		11.1	4.6	10.9	3.3				.062			<b>.</b>	<b>4</b> .3	10.6	3.5
4252	9.7	٠. د.	10.3		19.2	J.	10.5	3.2			3.3	928			14.7	<b>4</b> .5	2.12	4.0
4259	- 9	6.		1.7	<b>4</b> (	e. (	9.0	~ . eo (			2.7	.047		40	11.3	4.6	7.4	2.3
*	2.	- -	<b>+</b>	7. 1.	D.	9	<b>9</b>	2.9					•	* 1	!		,	(
447	7.	5.0		, ,		2.9	ø ;	o.,			2.5	. 656	·	947	15.7	<b>4</b> .	12.1	7.
CR **	7.2	* •	 	• • • •	7.E	• •	- r - r	, c	1,0	,	0.6	929	•	#C#	15.5	- «		9 6
4993	13.4	-	13.4		12.3	3.8	13.1		:	•	?	3	3.5	190		;	;	i

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	-	2	3	5	.016	014	940	719	į	. 063	. 031	963	999.	. 961		7 60 1	. 665	669	.185	.028	.676	.675	1.044 6.04	017	. 679	.028	3	90	.056	.047	. 175	= :	25.		124	. 659	. 052	. 092	.061
	YAW	AT TA	DEG	99	٩	. 8.	2.3	6. 4	2.5	3.6		•					ij		<b>9</b> .	9.	<b>4</b> .	_	- 2.5 -		4.5	- •	7 15	6.2	.3.2	2.7	9. 6	0.0		- ·	, , , ,	- Y	. e.	5.3	3.5
	₹	5	3	28	637	047	052	678	059	084			023		. 824	944	065	051	672	040	066				101	070	950	- 140	075	687	178	660.			. 630	108	080	094	687
	. P.	4	DEC	88	-2.1 -	,	•	2 4	4.5	0. †	9.	٠. دن			• P		7.5	-2.9 -			-		2.5	-		•	2.4		4.3	•	N				79	) (	9.7	4.6	- 9.5
DINGS	RATE	5	8	22				9.6	.012	629 -	012 -	.421	826.	- 689. -			- 185 -	. 992	196				149		•	. 183	968	682	122 -	963	. e1 + 16	. 652				129	188	010	. 637
DAY LANDINGS	ROLL	AT	DEC	80	10.0	12.1	٠. د ۲	2.0		. 4.5-		24.1	<b>.</b> .		7.7		. 60	_		•		ر د ره	7 S	4.5	-7.4	 10.5	. a		_	0.5	•	٠, •	-			. 4. <u>7</u> -			_
٥	PITCH RATE	AT TD	8	22	.072	. 692	. 692	999. 959.							0.00		.082-10.	. 169				.692	. e				200				.131	. 169	799	2/0.	. 6			. 124	.068
	PITCH	AT	DEG	ž		5.3	n e	9 4	3.0	2.4	•	<u>-</u>	* 6	B			4.7	9.7	•	<b>5.3</b>	7.1		, r	4	5.0	 		6.7	<b>9. 4</b>	4.6	5.5	6.7	÷ ;	- r	, 6	9 17	, N	7.1	3.9
		44	8	53			;	2			. 021	;	9.6	016	. 613	•					,	042	012										3	. 61	900	- <b>. 66</b> 3			
USS ENTERPRISE (CVN-65)	الدا الب	•	DEG	25			•	<u>.</u>			1.2		- °		,	•					,	-2.4 1											•	•	•	;			
ISE (C	υ Ζ ∢	8	8	5	.033	939	616	956	019	019	012			919.	882 875	. I	68	. 063	031	003	035	948	. 626	037	. 122	14.	- 677	012	010	9.00	012	023	550.	919	.042	023	679	. 037	.010
ENT ERP			0 0 0 0	80	<b>6</b> .	1.7	<b>.</b>		7	7	7.7	ø.	<b>.</b>	<b>9</b> 1	7		, nj	a.6	<b>9</b> .7-	2	-2.0	-2.3	r	-2.1	7.0	- 0	1		9.	•.	7.1	L.	T		7.7		4	2.1	•
SS	<b>E</b>	ē	<b>%</b>	<b>9</b>	063	. 138	. 023	150	963	086	920	147	023	6	100		935	.0.		092	919	045	624	8	696		120	- 963	.023	1.038	692	- 966	867	. 662		1 2 2	916	052	040
		•	0000	\$	1.2	8.6	 		7	•	1.7	7	<u>.</u>		* *	9	2.0	•	•	-5.J			† •	5.7	-9.6	<b>9</b> (	, e	7	1.3	-2.2	. d	7	e ?	- ç	•			-3.0	-2.3
NODEL TA-4F		96	2	47			•	2			188	į	. 226	. 1/8	300							.236	. 236											. 22		78:			
MODEL	6 L E		930	\$			•	9. P			<b>10</b> .8	;		10.2	:	:					•	13.5	33.3										•	12.6	•	<b>.</b>			
DATA -	<b>Z</b>	8	<b>3</b>	\$	.223	. 19	.246	25.	255	.26	.281	.216	. 232	. 222	. 199		.267	.251	.262	.263	.25	25.	22.	230	.238	2	2 2	25	.244	.274	.243	.257	. 22	22.	.236	23.	188	. 222	.267
LANDING DATA	C	•	930 Q	‡	12.8		- ·	. · ·	14.5	11.5	16.1	12.4	2.5	12.7	* ·	2 2	15.3	+.+	15.0	13.1	<b>*</b> :	*:	9.4.				-	-	-	-	13.0	14.7	12.6	14.0 14.0	2.5	14.7		12.7	15.3
3	-	5	2	\$	181	181	55	222	.237	•	. 192	•	•	•	.211	•	• •	•	•	•	•	•	222		•	3	•	202	•	٠	•	•	•	.202	•	187	184	220	.227
		•-	DEG	7				12.8															12.7														4		13.0
	200	2		Ŧ	246	247	2 3		22	32	255	256	25	20	3 2	27.2	273	274	275	276	277	278	272	<b>5</b> 5	282	2 2	2 6	200	289	28	293	294	202	2 2	À S	0 0 0 0 0	9	9	302

		3	LANDING DATA	1	MODEL TA-4F	1		USS EN1	TERPRI	uss enterprise (CVN-65)	<b>⊢6</b> 5)			Ó	DAY LANDINGS	SON				
997		P I T	T U	O Z K	<b>.</b>			ROL	ر ۲	N G L	w	u.	PITCH RATE	RATE	ROLL RATE	MTE	9	<b>.</b>	YAW	
2	2		8		t		5		8		is.		4	2	4	2	AT TO	٥	AT TD	۵
	DEC	3	930	3	930	3	9	3	DEG	3	DEC	2	DEG	3	DEG	3	DEG	2	DEG	3
<b></b>	7	2	<b>‡</b>	\$	\$	<b>‡</b>	\$	\$	8	5	25	33	\$	88	26	22	88	8	2	5
28	11.7	_	_	.238			•	916	€.	. 631		W3	•	980	•	.010	ن. ب	~. 075	4.8	. 684
ž	12.2	.213 1	_	.228		τ	-2.8	- 159.		014		•	<b>.</b>	•	<b>.</b>	999	i a:	968	6.7	.117
3	<b>∵</b>	_	<b>.</b>	.218			۲.	. 210.	<b>*</b> :	. 059		•	7				•	105	<b>8</b> .4	.084
3	<b>9</b> :	•	<b>.</b>	.25		•	•	_		.115		▼ (	n,			. 187 - 3	9	999.	2.5	.04
3 5	13.7	224		.237		1 1	7.7	021	0 · c	S :		W &	<b>5</b> 4	. 945 1. 2.	25.5	896 - J. 888		066 	 	. 636 1.036
312	14.2			1		1			•			. •		105 1				012		5 6
212	12.1	•	5.7	.274				.026	1.2	691		<b>.</b>				•		047	ä	
714	12.8	•	_	.218		ï			1.2	.021		=	•	.185-16.		286-12.		220	8.8	171.
316	12.7	•	_	.239 1	•:	.244	~			838 -3	ن. ا	958 6	7		4.2	143 -9.8		171	7.4	. 129
317	12.1	-	_	.234		T	_		-2.5	044		מ	•		~		0.0	9.00	1.5.	995
320	9.2	•	<b>7.</b>	.286			•	.042 -1.	4	024		•	•		٠.		_	1 <b>0</b> 1	-	.019
322	e (	-	5.5	236		_		.147	- 1	50.		•	<b>1</b>	-	 	140 -1.1		- e19 -	+ ·	077
724		• •	• ·	202		•		956		996		α,	٠.		<b>10</b>	914 -6	i •			.056
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ñ		•	_					.045	•			<b>4</b> D	5.		3.2	.056	.2	073	2.6	.045
3				-	<b>n</b> .		~ .	956 -	7		_	059 7	<del>-</del> (		•			- 986	٠, در	.075
3				112.	2.	200			N 4	.2- 279.	_	. 53		0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	•	- 688		999	7.5	129.
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28		•			13.6	. 752.	•		~		J. 4.5-	059 8	•	₹	_	239 -5.2	٠.	691	0.4	.070
325		-	<u>.</u>	.286		T		878 -J.(	_	052		ונים	•		<b>.</b>			047	• •	.61
3			D ·	62.						219.		n i	•		i : T	0.7- 2/0·-		2	• •	740.
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474	13.0	_	3.9	.243		1	1.0.1	.631	•	.016		NO.	-			17 +	; •	080	3.5	. 061
476	12.7	-	. 6.4	.250		•	3.2	. 056	.7	.047		-	•			073 -2	i T	037	- 5 -	. 963
477	13.0					1	0.7					•	•		~	.038 -4	i +	677	œ.	.016
478	12.9		12.7	.222		•	9			196.		•	•			1- 859.	E .	631	٠. ن	.03
479	9.9	582		.258		ſ	1 0.0	661	1 1 1 9	010 		NF	ED 1	.049	 2.2	.056 -2	i i	042	ب. د د	926
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	۶	¥	DEC	2	6.	ا ا	• •	• ?	2.1			: -	2.0	3.3	<del>.</del>	+.	<b>4</b> .			? ?		2.3	-7.3	9 1	, 0	7.7	=	- -		4 3	2.5	•	9.7	7.5	<u>۔</u> ن	ر ا	֓֞֝֓֞֜֝֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֡֓֓֓֓֓֓֡֓֓֡֓֡֓֡֓	# #P
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	F. P. A.	AT TD	DEC	8	_		<b>.</b>						'n	•							_	; +	•	i •			<u>.</u>	i <b>+</b> ≀				i •	i •	7			i 1	. i.
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DAY LANDINGS	ROLL RATE	AT TO	DEG	57		•	. 656				•	990			'		'			251	239	035							•	•		698	'		023	<b>.</b>		202
DAY L				S.		•	-2.2		ŧ		18.6									. 956-14. 4	.686-13.7	.051 -2.0	1		5.5				ŀ	200		-5.6			1.0			
	PITCH RATE	5	3	8	. 961	.072	963	.03	.047	033	5	98	.040	.063	. 073	037	88	. 856	289.	85.0	8	.051	. 686	989	20.	Ξ	.010	5	/ <b>8</b> 8'-	98.	.031	.075	. 037	.087	. 105	989	799.	. 635
	PITC	AT	9	2	3.5	<del>-</del> ;	V. V.	8.	2.7	a (	ب د د		2.8	3.6	4.2	-2.1	0	3.5 1.2	? .	2.5	4	2.9	<b>4</b> .0	5.1	7 K		-	1.7	••	- 6	. 0	4.3	2.1	5.0	9.9		 	9.0
			3	3			- 965				- 851 854	3		056			002	019		012	624	035		672							038							
68)	w		DEC	22			-3.7 -															_									•							
USS ENTERPRISE (CVN-65)	ANGL		2	51	4	96 :		.157			? •	•	3	79 -3.2		. 965		77 -1.1	<b>9</b> [	77.			35	.028 -4.1	223	<b>:</b>	\$	5	.024	5 a	14 -2.2	37	.028	37	9	<b>9</b>	B (	<b>6</b> 23
PRISE	<	8	930		967		623	-		012	9 9	·					010	077			637	•	•	•	•	•		ı	•				•	037	016	059		i ·
	יור			8	1					<u>.</u> .		-				7	9		•		7		-	-	7	•		6.0	- 1	3 4		1		•		•		 
USS	ROL	٤	3	\$	865	002	2 2	8	047	3		652	037	056	052	052	.017	026	- 644	650	014	026	021	070	112	2.5	061	. <b>96.</b>	3	795	045	965	. 647	040	003	050	906	<b>9</b> 33
		_	930	\$	۲.5	7	7.7	-	-2.7	2.3	8.7.	3	-2.1	2.5	• ?	• • •	•	-1 -0 -0		9 6		-1.5	-1.2	•	÷ ;	1.0	5.5	7.5		ì	-2.6	5.7	2.7	-2.3	7	4.0		. 6
Ì			3	<b>‡</b>	•		243		•		781:	-	'	286	•			. 2	•	. 46	215		•	241 -	•	•	•		•	•	230			•		•	,	•
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1	2 2 4		3	\$	8	279		72		•	248 T		3	236 11			241 13		3	225		_		251 13	2 =	2	3	3	Ţ	<u> </u>	_		246	157	<b>.</b>	<b>‡</b>	8	345
ANDING DATA	x	8	22		_	•	•					! "		~				•	•			•	•	•	•	•	•				: "		-		-		7.	! "?
26 N	1 1 0		3	\$	-		7.7.	5.5.		_	= :		_	-	_	_	•		2.5		_	_	_		3 12.3 12.4		`_	-	_ '			_	_	_	-	7:		
,	•	ē		3	.2	ភ្		3		-	197	•			•		.218					•	٠	.243	•	• •	٠	٠	•	¥ \$	227	237	.234	2	-18	.218		.23
			DEG	7	12.1	12.4	12.1	16.5	7.	12.5	2.5	12.0	12.2	11.8	13.7	12.1	12.5	11.2		1.5	11.8	12.2	12.1	2.0	12.6	2	12.4	13.0	12.9	? :	13.	13.6	13.4	11.7	=	12.5		13.5
	200	ş		<b>=</b>	482	\$ :	3 3	\$	\$	3	<b>3</b> 5	ğ	\$	3	Š	200	3	<b>3</b>	8		3	3	511	512	2 5	515	516	517	5 5		521	522	523	524	525	<b>526</b>	220	3

	YAW	AT 10	3	5	. 968	077	.023	. 625	940	963	=======================================	. 654		.026	.127	.072	196.	.052	3	929	940	.026	- <del>-</del>	.021	896.	4.0	.023	160	. 656	940	168	110	. 169	. 968	. 115	084	
	2	AT	DEG	9	3.0	† ·	- ·	7	2.3	2	<b>6</b>	, n	8.5	1.5	7.3	<b>-</b> (	, ,	) a	9.7	4.0	2.3		3.1	1.2	0, r		1.3	4.0	N •	2.3	6.2	<b>6</b> .0	7.6	ы с о г	. 6	<b>6</b> .4	9
	۸	AT 10	3	20	056	624	045	- 042	101	019	054	9.6	. 103	965	110	677	072	909.	- 129	- 196	- 689	047	1.163	656	636.	. <b>8</b> 26	692	112	084	686	691	896	175	960-	. 699	.638	- 22 -
	r. 9.	7	DEC	8	-3.2	<b>+</b> . <b>-</b> .	9.7	7	5.8		٠, ا	25.5	9.5	2.7	6.3	+ : T	7	- 0	4.7	-	-5.1	-2.7	9	3.5	-5.7		-5.3	٠ ب	7 7		-5.2	s.	•	ب د د د	5.4	2.2	7
DINGS	ROLL RATE	ę	3	22	042	.073	9 6	145	175	.178	073	200	079	.007	012	. 103		6		698	288	026	924	.677	024	700	- 688	.023	80 60 60	047		101.	026-10	260	. 935	989	170.
DAY LANDINGS	BOLL	¥	DEC	28	-2.4	7	- Y		_	10.2	7 . 7 .	, c.	<b>9</b> .	*	7	0. 0.		7.7	-7.7	-5.0	16.5	5.7		4.4	<b>*</b> • •	22.6	-5.7	 	7.7	2.5	2.5	5.6		<b>a</b> .		5.7	7:7
٥	PITCH RATE	5	2	55	.051		559		100	010	990	466	.059	.047	138	.026		999			.045-16.	50	8			100		.122	.024	47	. 963	.052	.218	136-14.9	.672 2.	- 654	900.0
	P110	¥	DEG	Š	8.2	•		5.00	u	9	<b>8</b> 0	5.4°	4.0	2.7	7.9	٠. د	2.1	י י י	4	7	2.6	ر د د		<b>.</b>	0. C	. 4	•	7.0	÷ •	2.7	9.0	3.0	12.5	8.4		- 6	9.0
		le.	3	23	963	.002	.017										<b>04</b> 5	9/0.	.633	) ) )					.017			,	- 963			086		-		•	
WH-65)	u u	•	DEG	25	2	<del>-</del> (	- -									,	-2.0	<b>4</b> 9	9.						<u>.</u>			•	י מ			o. T			?		
USS ENTERPRISE (CVN-65)	Ω Ζ <b>∀</b>	8	8	2	635	.042		183	042	.00	867	031	080	<b>.</b> 014	.00	054	96	. e/e	651	688	186	073	1	002	3	. e39	. 082	- 638		. 617	.023	670	044	<b>§</b> §		850.	200.
NT CRPR	ו ר	0	DEG	3	-2.0	2.4		9	-2.4	*	- •	• •	•	•	₹.	ر ا	ų,	? "	-2.9	5.7	,	~ •	-2.5	_	2.3	, m	_	-2.2	9 7		1.3	•	-2.5	ri r	j æ	U.U.	٥
SS	8	2	2	9	024	00		2	.026	016	- 65 - 65 - 65		035	028	.883	021	S	798	5	028	÷.	656		-1.1	<b>5</b>	9	. 963	.012	2	9.0	.008				3	86	200
			960	\$	<b>+</b> : <del>-</del> <del>-</del> <del>-</del> <del>-</del> <del>-</del> <del>-</del> <del>-</del> <del>-</del> <del>-</del> <del>-</del>	<b>+</b> (		-2.8	5.	<b>6</b>	-2.8	, n	-2.0	-1.5	7	-1.2	- ! ?			9.7	•	-3.2 1.2	. 60	•	<u>*</u> ;	- 7	3.7	۲.	• •	9 0	5.5	4:4	_	-	. B.	10 P	
Ţ		بو	3	41	200	.218	.216											68	8						.215				.187			32.		9	-		
MODEL	9 1 9	•	230	\$	11.8	12.5	12.4									•	5.5	11.Z	10.0	)					12.3			;	10.7			14.5		•			
DATA -	<	8	2	\$	.253	8		248	.267	.234	58 (	28.	200	.281	. 260	. 248	* :	22.2	239	265	. 269	.241	218	. 255	5	269	.263	. 269	, 50 50 50 50 50 50 50 50 50 50 50 50 50 5	236	.239	.255	.237	2 2 2 2	3 = 5	.232	207
ANDING DAT	1 C E	•	930	‡	14.5	17.7	• · ·	14.2	15.3	13.4	• :	16.1	1.0	16.1	14.0	14.2	*		13.7	15.2	15.4	13.8	12.5	14.0	15.3	15.4	13.1	15.4	÷:	3.5	13.7	14.6	13.0	7.7	12.1	13.3	». <del>•</del>
3	-	5	3	2	.213	2	176	. 225	.206	.218	. 175	22	.187	.25	. 192	.227	761	2	3	.213	199	25	36	.216	.215	211	.215	10.	. 187	197	.220	.251	.255	192	 8 6 8 5	.236	2
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99	2		=	\$	<b>8</b>	_	<u> </u>	3	_			7.5							1021				3	3	3	3 5		85	929	3	<u> </u>	25	2	<b>5</b> 43	970	949	649	1050	159	1054	933

USS ENTERPRISE (CVN-65)

	AVA	AT TD	D DEG RAD	60 61	7012	7		•		7.1. 05/	,	0.1	٠, د.	, , ,	5.5 6.6 6	3.5	1.3	1.7	6.	! =	7.7		, .	-2.5	-5.0	-5.1689	-2.4	• •	-5.0	9 (	-/.2	200. A		-	9.6	1.7	-2.1037
	F. P. A.	AT TD	DEC RAD	58 59	-2.2038	i o	-2.2038	i	-1.2021	7.4 - 1.67	-5.6098	-5.0067	~	-1.2021	2.8049	4.0670	1.7 636	٠. ا	-5.5- -6.60 - 7.4-	-2.5044	3005	i i	13.1 - 181	i i	i •	1.2 921	-3.5061	1002	i •	i 6 1	-3.5861	C/A - C - 41			4.1072	6.1106	5.1 689
DAY LANDINGS	ROLL RATE	AT T0	DEG RAD	\$ 57		.033	.241	.110	1.166	2007:				2113		. 607	- 210. /				1 124		1.005			487	. 147			. 042	3:	1 288	- 173	.031	3 .237		- 858 -
DAY 1	PITCH RATE R	AT TD	2	55 56	.051 15.7		_		804 8. 5 - 50 - 60 -	777		.666 1.1	.631 7.	.185		9.00		.126 1.5	127 - 2.			.101 -7.4				.056 27.9		.072 3.5	_		_	878	. 117 -9.9		.686 13.6	.087 1.2	.086 3.3
	PITCH	ΤΑ	RAD DEG	53 54	2.9	•.4	9. 9.	w	7	2.5	-:	3.8	935 1.8	. e.	- -	0.0	•	7.5	<u> </u>	919 3.4	2.5	eo .	- 2. 2. 2.	<b>-</b>	031 -1.0	7.5	6.5	012 4.1	6 6 7			. •	935 6.7	9.3	4.9	5.0	ø. <del>†</del>
(CW+-65)	. L E	11	D DEG	52									-2.0(							1.1.1					-1.89	_		7					-2.0	:			_
USS ENTERPRISE (CVN-65)	LANG	8	DEG RAD	56 51	1.0017	8.7 .152	5.4 .094	<b>+</b> 1	-2.7047	070'- 0'- 1 4 824	5.6 .095	-3.5061		500.: 0.0-	6.0° 6.1	1.7 082		<b>.</b>	-2.0 - 0.03 -4 + -	٠ ~		2.6 .045	1.8 - 8.1-		5.0 .087		2.7 .047	_	-3.7065		1	2.2 -1.5 - 8.54				3665	3.2 .056
USS EN	ROL	5	OEG RAD	64		024	ï	656	•		198		_	7	- 858	673 -			220.	026	019					679		026	047	012		016			673	651	014
1A-4F		L.	3	47 48	Ť	7.	Ť	-3.2	7		; ;	9.9	.264 -1.4	•	7	Ť	ï	•	- 1	.211 -1.5	7		' <b>†</b>	•	.237 -2.4	7	=	.276 -1.5	7.7	 	**	ī -	.208 -	•	7	-2.5	ï
1 - MODEL	ANGLE	15	RAD DEG	55 84	Ŧ	2	<b>9</b>		2		2	80	32 11.7	2 3	2 2	62	32	8 :		132 12.1	2	2	3	30	45 15.6	70	*	82 15.8	513		22	7 <b>9</b>	144 11.9	302	3	157	101
ANDING DATA	1 C H /	8	930 0	;	13.8	13.0	<b>9</b> . E	12.6			13.3	13.5	13.3	5.5	10.2	10.7	13.3	12.5	• •	13.3	<b>+.</b> +	9:	13.2	13.7	43.0	D.C.	13.4	15.3	12.3	7.5	12.7			17.3	12.1	14.7	16.3
3	4	5	DEG RAD	42 43									11.0 .192		11.3 . 197								10.1 .176					15.6 .272			15.4 .234		11.7 .204	•	9.6		•
	300	ş		Ŧ																			1 682				_	•					•	•		•	•

	*	9	3	5	. 858	120	017	.042	082	760	.03	033	. 033	.024	986	. 667	2/8.		1	.075	. 666	. 654	996	9,9	989	.952	.00	.076	929.		.024	.031	106	. 024	038	070	010	.012		909
	YAW	OT TA	OEG	•	3.3	_	•				-		<b>6</b> .	<del>*</del> :	<b>0</b> .	•	• ·	7 -	2.5	4.3	0.		9,			9.7	<b>+</b>	<b>.</b>			*	1.8	6.1	<del>+</del> :	٠.	•	9	۲.	i	ار د
	¥	2	3	28	968	052	677	- 961	692	1.00	- 968	031	966	070	965	677	. 168	. 945	666	692	677	679	<b>698</b>		. 69.	677	045	682	9/9		. 185	059	176	056	049	061	073	091	<del>8</del> 59	989.
	ŗ.	AT	DEC	23	•	•	+	G	?•	0 17	•		•	•		• •	· ·	- 4		'n	<b>+</b> :	ะ เก	•			+	- 		B r	. ,			_					-5.2	• •	ا 0
SS	ATE	_	3	21	.134 -3	.094 -3		-	. 145	1 4 6 5 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		.119 -1	.066 -3	1 659.	.082 -			193 -		673 -5	1.016 L		3635	7 120-		7 960		- 988 -	298	- 200	- 651 -6.		112-10.							.120
DAY LANDINGS	ROLL RATE	AT TD	DEG	200		· •	•		n				•	~ •	_	- 1	ָ ֓֞֞֝֞֜֝֞֝֓֞֝֞֝֝֓֞֝֓֞֝֓֓֓֞֝	` .		N	•	•	<b>20</b> (						<b>.</b>				•	•	•	•	7	- i	1	
DAY			3	55	661 7	218 5	•				_	49 6	.038	<b>672</b> 3.	+ 010	4 986		672 -S		.687 -4.		619 -5.		- 040 - 1- 040	113	.058 5	117 7.	1	926 3.0	A61 10.	866 -2.5		215 6.		968 13.5	021 14.	126	954 2	•	90
	PITCH RATE	AT TD	DEG		ij		•	- ;		966.6	98.	•	<b>.</b>	<b>e</b> .					. 6	•	9.0	•	<b>.</b>	9.0				•		. 4		•	•	•	•	•	•	<b>.</b>	9.000	900.
	d		<b>2</b>	*	7	12.	'n	'n.			•	-2.8	7	*	7	4		•		4 5.0	•	 	n (		- 6	n	•	7	- 1			3.5	12.3	r.	<b>0</b> .70	1.2	7.2	'n		D
<b>≅</b>		4	950 R	3					i	<u>+</u>						028				.024			8	. 624	5					110	3								•	628
¥	W.			22					٠	•					,	<b>9</b>				4.		r.	•	* °	•					•									•	<u>ء</u>
USS ENTERPRISE (CVN-65)	S Z A	8	8	2	012	. 684		.017	911	) TO	968	. 051	. 610	. 654	677	. 647	621	926	8	•	.012	007	- 636	2	131	.012			073	017.	1	033	.023	. 619	.163	. 995	. 85 85	- 699	919	637
NTERPR	<u>ر</u> د	0	DEG	8	7	4.8		- ;			9.5	5.8	•	۵. ـ	* ! † !	2.7	7. G	4	<b>†</b>	2.3	۲.	<b>+</b> 1	-1.7	•	.5		'n	•	7 :		2.6	1.0	<u></u>	<u>-</u>	9. 9.	r.	-1.7	-5.7	- ;	-2.1
a ssa	0	_	3	<b>\$</b>	014	075	026	129	7.0	<b>6</b> 5			03	631	.024		2 2			619	676	. 612	2		924	036	867	. 012			58	96	061	1.030	858				.678	. 55
		2	930	\$			. 5:1	<b>7.</b> 4			2.2	7	- 9:1-	•	<b>+</b> ·		\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \			1.1	•			<u>.</u> •	. <del>.</del>	-2.2	• •		•	, , ,	-	~	- S.S.	_	4.5	+	3.0 0.0	G.	÷ •	
Ì			3	41		1	•			3 '	ı	•	1	ī		192 -		ı <b>!</b>		202	•	237	•		27	1	-			200			•	•	•			·		- 202
100EL TA-4	1	1	930	\$					•						,	•				•		•	•	• •						•	•								•	D
ī	9 Z 4		3	\$	248	291		.263	222	= 3 <b>3</b>	7	236	248	241	25	232 11	<b>8</b> 776	3	3	236 11		_	272	_	-	277	257	<b>5</b>	222	3.50	248	262	244	252	225	248	262	250	257	200 11
LANDING DATA	Ξ U	8	930	‡	•	•						_								_	_	_	_			_					•			_	_	_	_	_		•
200			3	2	113 14.2	232 16		194 15.	12.1		_	.215 13.9	_	13 13	_	. 192 13		-	_	-	-	-			213 13.4	_	-	_		0.4 - 4.0 0.4 - 4.0 0.4 - 4.0		_	_	_	_	_	.181 15.	_	14.7	11 203
	•	5	DEC	42			•	- (				2					7.00			_	•	<b>10</b>		 		12.6 .2		•	, ,				_	_			_		_	-
	9	_		7	7 12.		-	•		-	_	•	7 13.0	_						•	5 13.	•				Ť	•	_		- •	-	_	_	_	_	_	_	•		=
	5	2		•	12	121	122	22	2 :	122	122	122	122	72	123	2	2 .	12	123	124	124	2	7	12.	125	125	12	7	2	7		125	125	126	12	126	126	12	12	12

			2	_	152	079	966	196		049	075	824	. 103	079	965	631	982	90.		3 5	660.	.021	016	035	652	.026	.017	.047	809.		.028	623	926	.021	2 6	642	117	984	631
	YAW	AT TD		5	i	ï		i	· ·	i	ï	ï	•	ï		•	•		i 1		i			ī ī	ii		٠. -				. ~	 	<u> </u>	•	i`	- ` ·	· ·	. ī	- -
		•	DEG	2	4	7	7.0	÷	1 4	7	7	7	8	7	?	D. 1	Ť	7.	- 4	7	5	1.2	ï	7.	7	±.	-	7.	7.5		-	-	3.2	-	7	7.	. 6	1	#.
	÷	2	3	60	676	106	.073	044	112 - A63	677	679	101	- 113	. 103	. 673	. 963	682	8/9		799	999	075	058	075	200	061	077	. 698	989	929	047	699	066	054	037	982	115	963	692
	ر. ان	AT TD	DEG	82	ı	-	•		1 1 <del>4</del> 6	i •	ı S	i 60	i So	1 G	•	•	•				ا م	•	•	_		1	<b>1</b> →				_	7	•	· .	- - 1	` '	i i	9	1
S	W		3		†	٠ •			י קייקי		7	5 -5.							, , ,		7	5 4.3		7 4		5.0			֓֞֜֞֜֜֞֜֜֜֜֜֓֓֓֓֓֜֜֜֜֜֓֓֓֓֓֜֜֜֜֜֓֓֓֓֓֜֜֜֡֓֓֡֓֡֓֡֓֜֡֓֡֓֡֓֡֡֡֡֓֜֡֡֡֓֜֡֓֡֡֡֓֜֡֡֓֡֓֡֓֡֡֡֡֓֓֡֓֡֡֡֓֜֡֓֜			7 -5.				-	6 i	•	
DAY LANDINGS	ROLL RATE	<b>T</b>		57	1	369	. 672	- 0%	3 5	122	. 028	1.865	229	. 389	- 158	. 163	108	CC9.	7.014 AAC	989	.115	065	092	136	318	. 129	117	929	5 6 -	929	-	007	.045	. 129	. 965	. 667	636	198	. 002
3 ≿	<b>3</b> 0	¥	DEG	8	٠. در	17.7	<b>-</b>	7.7	. 9	7.0	<b>9</b> .	ا. د	J. 1	7.7	٠ م	8. G	- c	7.	י ע	3 -	9.0	-3.7	-5.3		5.5	7.4	6.7	4.	• •		9.0	4.	7.6	4.4	y.,	<b>•</b> !	\ 0	6.2	-
3	ATE	۵	3	88	- 619	.163 1	• 14		98.4		021	660	677-13.		•		•	50.	7		679	947 -		35	_		- 989	2 2 2		937	979	924	105	120	616		1 616	910	.012
	PITCH RATE	AT TA	DEC		_	•	ľ		, ,	•	ï	<u> </u>	·.	•	 -	•	_, .		i 				~. ~	•	1		٠. 	•	. `			_	•	•		•			ï
	4			\$	_	3.	e,	si i	7		7	S	+	•	_	6	'n	,	,	•		7	<u>.</u>	?:		2.9	÷	-	D #		=	-	<u>.</u>	9		7	2.1		ï
		<b>L</b>	3	3						.054	047				005					- 821			. 010																. 002
£65)	w	1	DEC	22						3.1	-2.7												₩.																-
USS ENTERPRISE (CVN-65)	ANGL		3	5	.692	. 656	2	. 682	. 837 858	_	F	. 638	8			<u> </u>	.033	<b>e</b> :	2,5	946	. 040	. 667	92	799.	952	8	. 026	5 5	2 G	184	95	35	•	919	<u>ي</u>	686	2 S	599	;
RISE	<b>Z</b>	8	DEG	60	•	•	1. 036	•	837 856	11	•	•	99.	.028	- 631		•	9/9-			•	ė	002	799.		638	•	051	. 660		992	035	010	•	035	<b>.</b>	1.065		
25	-			8	5.3	3.2	-2.2	4.7	-2.	4	2.8	2.2	•	<b>.</b>	7	= :	<b>.</b>	•	7	7	2.3	*	ī	* ;	200	-2.2	1.5	-2.9	3		7	-2.0		(	-2.0	ų,	7.6		
SS E	8		3	\$	052	.017	072	3	.023	8	637	626	. 628	628	919		2.5	3			649	072	.021	<u>.</u>	1.963	965	.028	- 656	9.63	242	077	. <b>98</b> 9	610		077		1.042		.007
		5	DEC	<b>\$</b>		_	_	<b>,</b>	n a		_	r.	•	•	<del>-</del>	-				) w	1 50	<u> </u>	~									10				_			
ابيا			2		7	-	Ť	-	n	-	•	7	-	7	- •	<u> </u>	1.0	9 ·	<u>.</u> '			Ť	2 -	•	9 49 1 17	7	<b>1.</b>	ال ال		ำ	Ť	ï	i	7	Ť	-2.5	? ?	-2.8	
Ĭ		<u>.</u>		\$						.213	. 206				. 236					2.46	•		.222																.223
MODEL TA-4F	C L E		930	\$						12.2	11.8				13.5					<b>6</b> 7			12.7																12.8
1	Z		3	\$	251	276	230	232	3 2				246			2	2	2	- 4	•		262		3 3	2	218	246	22	6	2 5	246	223	216	25	218	212	, ,	222	
ANDING DATA	z	8	DEC	<b>.</b>	•			<b>.</b>		• •			•	_																						<b>~</b> .			
N. O.	1 0		2	\$	=======================================		5			=					2									16.2			_		7.4.	-			12.4			- '	7.4.5		
)	-	2		3	. 223	<u>=</u>	.223	<u>.</u>	181	216	<u>.</u>	3	2	3	.234	7	77	2	, 10,	215	5	¥.	.215	5	26	ž	178	178	C12.	. 2	237	1.	5	. 16	.23	17		2.5	.227
		_	930	42	12.8	= -	12.8	= :	* -	7.7	<b>★</b> :	<b>.</b> 5	1.8		13.4	<b>*</b>	5.6	• •		9 F	-	•	12.3	•	15.2	1.7	10.2	9.7	72.3		2		₹.	6.7	2.5	2.0	7.7	12.1	3.0
	997	2		Ŧ	2				1274												•			1284	•				7								312		315
	3					=	=	<b>∵</b> ∶	2 2	: 2	==	<b>=</b>	=	-	-		2 :	= :		<u> </u>	•	-	<u>=</u>		: :		-	= :	<b>-</b> :		: 2	~	_	-	<b>-</b> ;	<b>=</b> :		: =	_

•	10	3	19	.143	120	. 026	087	016	072	101	.677	016	.054	059	.051	099	042	<b>.080</b>	019	077	. 056	.044	.00	.00	88.	. 686	692	- 198 - 198	2	- 989	9		740.	.037	. 647	. 637	<b>4</b> 10.	. 035	. 679	986	. 042	037	. 963
YAN	¥	DEG	3	8.2		1.5		G.		-5.8	<b>*</b> :	•	٠. ۲.		5.8		-2.4	<b>4</b> .0		_		2.5	₹.	*.	4			9	~	T	i.		* .	2.1	2.7	2.	•	5.0	4.5	4.0	7.4	-2.1	3.6
٠	5	2	29	120	061	854	059	044	092	063	084	051	694	058	696	065	984	696	056	070	094	073	679	063	047	966	. 665	946	051	660.	. 65	36	. 666	- 828 - 828	073	047	065	963	966	689	676	028	077
Ľ.	AT	DEG	88			الم. الم	4.5	-2.5	-5.3	-2.6		-2.9	-5.4		-5.5	-3.7	7	5.5	7.5	•	4.6	7.7	5.7	5.6		-3.8	J.												8.5	-5.1	0.7	9.1-	* †
ROLL RATE	0 1	ο <b>Σ</b>	22	.161	119	. 030	108	. 122	.014	012		. 035	030	.012	105	030	052	.040	. 122	410	002	•	. 166	.014														. 886	061	269	.010	689	. 963
	Υ	D DEC	99	9.2	<b>8</b> 0.	1.7	6.2	7.0	•	1.7		5.0	-1.7	۲.	• •	-1.7	6.2			••		2.3		•	_	3.7	14.5	4	7. T	<b>6</b>		7	_		0. <del>*</del>	S. 0.	5.		-3.5	-15.4	•	<u>-5</u>	3.6
PITCH RATE	AT TD	9	33	. 686	689	939	.112	. 129	.023	028	- 188 - 188	.117	.028	016	. 672	.016	.070	. 856	98	869.	.077	. 698	. 162	989	999.	<u>.</u>	. 607			=		3	• • • • • • • • • • • • • • • • • • •	. 629	.327	1.058	. 175	101	.070	1 + 1 0 .	. 063	. 136	. 065
PITC		RAD DEG	\$	4.6	-3-	8 1.7	4.0	7.4	7 1.3	• •	7 10.3	6.7	<b>9</b>	6.	<del>-</del>	œ.	<b>•</b> .	3.2	•	5.6	<b>+</b> .+	5.6	9.3	4.6	4 3.0	5.8	₹.	0.0 0.0			•	7 .	•	4.0	18.5	7.7	10.0	5.8	<b>+</b> .	€.	3.6	7.8	3.7
	4	DEG R	53			106			047		047														.024					. 040													
GLE		9	22	•	2	2.9	•	7	13 -2.7		8 -2.7	7	λ	<b>5</b> 2	ž.		5	9	9	Ξ	2	2	<u>a</u>	Ì	1.4	2				9 -2.8	•	N S	<b>.</b>	2	•	9	2	7	9	•	52	50	
<b>z</b>	8	DEG	51	1 106	. es	992	3010	710.			•		3 045	i	7 .065		2 073	656			7 .012	500	019	3 84		662		,	ē.		_	210	120	7012		•		1 637	6 886	016	. 938	858.	3040
0 1 1		3	49 50	838 -6.1	912 1.6	1201	19	61 1.0	76 1.5	79 1.6	,			•	ņ	72	7.7 %	37 -3.2			11	3 3	.045 -1.1	862 2.5	3.1 +10.	.002	25	92		ı	5.0 5.0	.028	6/9 6.5	992 -	0146	•	047 3.6	961 -2.1	Ť	245	021 2.2	002 3.3	042 -2.3
œ	6	DEG	<b>\$</b>	70	70	i	1019	5 061					2021		6045		4 094					~	•		•.	•	_	_	_	<b>+</b> (	2 - ees	<b>.</b>	0	-	•		•		1037	•		i	i +
		3	47	Ť	i	255 -6.9	Ŧ	7	211 4.		297 -2.6	•	Ŧ	-2.5	-2.6	7	Ϋ́	-2.1	1.8	?	Ť	i	~	i	218	•	?	9		206 -2.	i	<b>-</b> ·	÷	i	•	-	2.7	5.5	-2.1	7	-1.2	i	-7
n n	11	DEG	9			•			-		•																																
Z V		3	5	268	244	251 14.0	236	237	220 12	202	269 17.	223	253	267	267		3	262	298	263	244	288	251	243	284 12.	.241				246 11	22	200	321	262	230	2	256	200	234	227	215	232	.248
Σ U	8	DEG	‡	•	_	·	•	•	٠	11.6	•	•	•	•	•				-					13.9							_	-						-	-				14.2
P I T	_	3	\$	-	_																						.213		•	•	_												.286 1
	5	DEC	7							<b>9</b> .0								_	_	_	<b>~</b>						12.2														_		1.8
S C	2		<b>∓</b>	1316	1317	1318	1318	1320	1321	1322	1323	1324	1325	1326	1327	1328	1329	525	2351	3	333	535	133	1336	<u>5</u>		7.5	1342	3	1345	1547	2	25	<b>1</b> 25	1555	1557	1559	1560	1561	1562	1563	1564	1565

DAY LANDINGS

USS ENTERPRISE (CVN-65)

LANDING DATA - MODEL TA-4F

YAN

F. P. A.

ROLL RATE

PITCH RATE

ANGLE

ROLL

ANGLE

PITCH

200

2	8	5	.072	.061	012	. 692	140.	. 682	.211	.636	.012	.038	.014	. 858	64	•	.072	. 023	. 084	.044	.077	. 686	.007	. 989	. 023	.045	.056	.113	.040	.00.	.00.	. 995	044	669	052	051	. <b>984</b>	002	687	968	037	. 044
¥	DEC	99	+:	3.5		5.3	2.5	4.7	12.1	1.7	۲.	2.2	<b>.</b>	и. В	2.3	2.5	<del>-</del> -	٠ <u>.</u>	<b>4</b> .8	5.5	<b>†</b> :	4.0	₹.	-	<u>د.</u>	5.6	3.2	<b>6</b> .5	2.3	ij	ij	n		<b>.</b>	6.7	6.7	<b>4</b> .0	- -	ė	o.	-2.1	2.5
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7	DEG	20	5.0	- 6.1	9.	+.4	6.7	5.6	2.5	1.3	5.7 -	. 0.1	5.1	5.0	- 5.1	5.5	-5.0	- 7	9.4	. 8.5	5.2	. 8.	D		- 8.7		- 7.5			:	89.	4.5	9.1	2.3	8.	. 6.	5.7	8.3	 	- 1.2	. 9.	6.
٥	3	22	080 -	276	.052 -	.021	020 -	124 -:	.030-1	.211	. 181 .	. 124 -	.302 -	070 -:	1.836 L		-	.152 -	1	<b>6</b> 23 –:	.051	.126 _	_	•	-	_	-				`` 980	<b>947</b>	. 152	<b>933</b> –;	942	926 -	<b>0</b> 28	<b>9</b> 28 –:	445 -	112 -	204 -	410
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۵	3	55	<b>673</b>	859-15	<b>691</b>	143 1	<b>884</b> -1	091 -7	1 986	059 12.	159-19	. 699	. 886 17	7 930	677 -2.2	023	985 -1	_	914 -2	831 1	108 2	_	_	927 -B	_	_	_	917 46.7		.88	_					848 J		134	7	194 6	_	860
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క	DEC		1019	•	-	e.	B014	2021		2 . 963	3.058	2 .021	5020	5 - 944	_	5 026	2 · . 96.	. eS	•		•	e	980.	058	616.	051	8 048	. e16	9 678	٠ د		.02	20.	1002	4024	2 .073	8 031	•		•.	<b>.</b>	6. 1.
	2	\$ \$	51 -1.		631 7.		<b>677</b>	31 -1.	57 -5.	624	984 3.	1.:	54 -1.	M7 -2.	). S3	SS -1.	021	 889	. 626	838 -2.	938 1.	2	049 4.	 	28	<b>367</b> -2.	52 -2.	 88	7 2	<b>193</b>	2	2	 -	2	57 -1.	016 4.	28 -1.1	37 2.1	36	963 2.(	995 2.1	962 -1.
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WDING DATA	CH	8	DEG	‡	14.7	14.5	17.5	15.7	13.3	12.7	4.2	12.7	14.1	a. <u>+</u>	7.5		15.3	15.3	15.6	2.9	· •	3.2	13.1	13.1			17.8	13.7	14.6	15.8	12.9	•	9.7	4.0	12.4	12.5	ç
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88	2	Z	5	•	•	•	169	•	•	•				169		9	•									•	167	170			-		-	-	-	-	-	•	•	169	•	167
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DAY LANDINGS

USS ENTERPRISE (CVN-65)

Lawling Data - MODEL TA-4F

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OFFICIATION DATA - MODEL 17-4F SIDE DISTRIPRISE (CON-65) BAY LONG INCOME. TO WIRE SIDE LUGG FLAP SIDE DISTRICT NAME TO D WIRE SIDE LUGG FLAP SIDE DISTRICT NAME TO D WIRE SIDE LUGG FLAP SIDE SIDE NO. TYPE CODE SPEED.  1-15 - 1-257 718		₹	æ		•					•	•											•	-				-		•						_	_					
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Cartillo DATA - MODEL TA-4   USS BITDRYRISE (CVN-65)	NDINGS	BAROM	PRES	E H	79	36.63	30.03	39.93	26.62	30.03	30.05	30.03	30.03	30.03	38.83	38.83	38.83	26.65	36.63	30.03	30.03	30.03	30.03	30.03		30.05	39.92	30.02	20.00	70.07 6.01	10.05	30.05	30.01	29.97	29.97	29.97	29.97	29.97	29.97	29.97	•
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	REREAD	NUMBER			•	•	-	• •	•	•	•	•	•	_	•	•	• •	- •	<b>-</b>	•	•	•	•	~ (	• •	•	•	•	- •	• -		•	•	•	•	•	- (	~	<b>9</b>	•
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	TRIC	URE		8	761.2	761.2	761.2	761.2	761.2	761.2	761.2	781.2	761.2	761.2	761.2	761.2	761.2	761.4	761.2	761.2	761.2	761.2	761.2	761.2	761.2	761.2	761.2	761.2	761.2	781.2	761.2	761.2	761.2	761.2	761.2	761.2	761.2	761.2	761.2	:
DAY LANDINGS	BAROMETRIC	PRESSURE	N H	79	29.97	29.97	29.97	29.97	29.97	29.97	29.97	29.97	29.97	29.97	29.97	29.97	29.97	20.00	29.97	29.97	29.97	29.97	29.97	29.97	29.97	29.97	29.97	29.97	29.97	20 07	29.97	29.97	29.97	29.97	29.97	29.97	29.97	29.97	29.97	10.07
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	TRIC	SURE	¥	8	761.2	761.2	761.2	761.2	7.107	7.197	761.2	761.2	761.2	761.2	761.2	761.2	761.2	761.2	761.2	7. 1.2.	761.2	761.2	761.2	761.2	761.2	7.1.57	761.2	761.2	761.2	761.2	761.2	761.2	761.2	761.2	761.2	761.2	761.2	761.2	781.2	761.2
DAY LANDINGS	BAROMETRIC	PRESSURE	N H	78	29.97	29.97	29.97	29.97	) C C C C C C C C C C C C C C C C C C C	20.07	29.97	29.97	29.97	29.97	29.97	29.97	29.97	29.97	29.87	20.07	29.97	29.97	29.97	29.97	29.97	20.07	29.97	29.97	29.97	29.97	29.97	29.97	29.97	29.97	29.97	29.97	29.97	29.87	79.97	29.97
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7 A F	SIDE	Š		8	222	727	512	217			797	\$	228	767	3	51	5	8			2	428	22	787	217	Ę	22	420	51	2	<b>4</b> 29	-	2	797	228	228	228	226	9 6	707
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	ARR GEAR R	RUNOUTS	5	82	429.3	•	429.3	426.7	7.6	426.7	431.8	429.3	429.3	429.3	429.3	429.3			420.3	429.3	•	•.	429.3	416.6	429.3		431.8	426.7	429.3	•	431.8	431.8	9	5.5		•			•	426.7
	AR.	2	Z	5	169			9 5		58						69	• •	•	169			•				•	176		69			9/1	•		•	•	•	•	•	168
	BAROMETRIC	PRESSURE	₽	8	761.2	761.2	769.7	7.69.7	766.7	760.7	760.7	760.7	760.7	760.7	7.69.7	760.7	769.7	7.007	7.007	760.7	760.7	760.7	760.7	760.7	769.7	7.00.	760.7	769.7	769.7	760.7	769.7	769.7	769.7	7.00/	7.99.	769.5	7.00.	760.7	7.69.7	7.69.7
DAY LANDINGS	BARON	PRES	IN HG	20	29.97	29.97	29.95	28.83	29.95	29.95	29.95	29.95	29.95	29.95	29.95	29.95	29.95	CR . 87	29.93	29.95	29.95	29.95	29.95	29.92	29.95	20.83	29.95	29.95	29.95	29.95	29.95	29.95	29.95		28.82	78.67	20.00	20.00	29.95	29.95
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DISTANCE	OISTA	TANCE	9	<b>9</b>	TYPE	300	SPEED	_						PRESSURE	J.R.E	2	RUNOUTS	NUMBER
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		2	20	2	50200		•	•	900		8	29	2 :	29.95	769.7		429.3	<b>-</b>
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•		R	8	118	50120		•	D. I.	005		026	3	8	29.94	760.5		426.7	_
		3	<b>→</b> (	2	56126		<b>.</b>		. 963		965	2	2	29.94	760.5		431.8	- ,
		8 8	י מ	217	56128		 D (	•	98.		- e	8 4	<b>8</b> 8	28.84	. <b>6</b> 6 7		429.5	
		2	• •	- 6	56128		, c	1 1		1 1	1.06	8 2	2 6	29.94	768.5		429.3	
		*	~ ~	217	80120		. ~	7	962	6	016	3	2	29.94	760.5		424.2	~ ~
		67		707	70120		<b>1</b>	<b>†</b> :	607		016	3	<b>79</b>	29.94	766.5	•	•.	<b>,-</b> -
		2		873	70100		_	9.1	010	-1.7	030	3	28	29.94	760.5	•	0.0	~
		3	*	78	<b>3618</b>		_	<b>†</b>	007		010	3	2	29.94	760.5	169	429.3	-
		3		į	2 2		_	; -	992	~	636	8	2	20.04	766.5	•	•	•
		2		512	20.00			2	. 963	-2.1	637	3 :	2	29.94	766.5	•	• •	~
		3	(	<b>1</b>	78266		<b>1</b> 0 (	•			•	3	9 9	28.82	768.5		D 1	- •
			N	22	20200				999		012	3 3	e c	28.84	0.00		426.7	- ,
		2	<b>7</b> 3	512	20100			7.7	1.003	9	01 <del>0</del>	8	8 S	29.94	768.5		429.3	- •
		9	-	?	20100		•		;			9	9 (	20.04	768.5		51.0	- (
			<b>+</b> :	2	<b>8</b>		•		010		- <b>9</b> 63	<b>13</b>	2	29.94	760.5		429.3	~
		=	n	2	50120		•	_				3	2	29.94	760.5		429.3	_
		3	n	512	<b>20200</b>		•					3	2	29.94	760.5	169	429.3	_
		82		217	70100		•	n. i	. 993		010	3	<b>5</b>	29.94	760.5	•	•	-
		3		718	70100		•	2	963	6.1	016	89	<b>50</b>	29.94	760.5	•	• •	•
		5		412	70100		•	1.5	- 999		.026	89	50	29.94	760.5		•	•
		2	n	412	56166		•	<b>†</b>	007		019	89	<b>5</b>	29.84	760.5		406.4	•
		3	-	118	50120		T	. i	009	ø.	. 016	88	50	29.94	769.5		424.2	•
		8	*	107	50100		8	_				89	70	29.94	760.5	169	429.3	6

10   0   15   1   1   1   1   1   1   1   1		Š	L. DING DATA	ī	DOEL	MODEL TA-4F		USS E	N CB	PRISE	USS ENTERPRISE (CVN—65)	65			3	3 >	DAY LANDINGS				
No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.   No.	OFF	SONTER	RAMP	0T 0T	WIRE	SIDE		ş	Ē		ECK P	<u> </u>	DECK	POLL	ā	•	BAROME	TRIC	<b>A</b>	***	REREAD
Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary   Mary	018	TANCE	0157	ANCE	€.		TYPE	3000	SPE	£							PRESSI	URE	2	UTS	NUMBER
64         65         67         70         71         72         73         74         75         76         77         76         76         76         76         76         76         76         76         76         76         76         76         76         76         76         76         76         76         76         76         76         76         76         76         76         76         76         76         76         76         76         76         76         76         76         76         76         76         76         76         76         76         76         76         76         76         76         76         76         76         76         76         76         76         76         76         76         76         76         76         76         76         76         76         76         76         76         76         76         76         76         76         76         76         76         76         76         76         76         76         76         76         76         76         76         76         76         76         76         76         76<	E	3	E	3				_			DEG	3	930	2	<b>L</b>		IN HG	£ 36	2	8	
-3         192         59         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718	3	3	3	2	67	2	60				2	*	22	92	11	78	92	8	5	82	
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-2 199 61 2 716 58190 8 4	-	7	990	2	*	520	50 50 50 50		•	4		.002		. 662	2		29.94	760.5		29.3	~
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-3 256 76 2 212 5612 6 44607 16 622 62 20 22.84 766.5 1682 236 76 20 20 20 20 20 77 5612 6 6 44607 16 62 62 20 20 20 20 77 5612 6 6 12 236 70 20 20 20 20 20 77 5612 6 170 20 20 20 20 20 77 766.5 170 20 20 20 20 20 77 766.5 170 20 20 20 20 20 77 766.5 170 20 20 20 20 20 77 766.5 170 20 20 20 20 20 77 766.5 170 20 20 20 20 20 20 77 766.5 170 20 20 20 20 20 20 20 77 766.5 170 20 20 20 20 20 20 20 20 20 20 20 20 20	7	7	255	2	~	710	2		•	•					2	2	29.94	760.5		29.3	•
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-2 264 83 4 528 56120 8 44607 .1 .602 563 22.94 766.5 178 -2 264 83 4 528 56120 8 436053605 563 20 20.94 766.5 178 -2 264 87 5 194 262 20 20 20 20 20 20 20 20 20 20 20 20 20	7	7	22	2	7	707	<b>2</b>		•	í +		8		.028	2		29.94	760.5		28.7	•
-3 283 62 1 712 26120 8 43065 6.5 6.8 20 22.94 766.5 176 2.20 6 6 70 20 177 20 170 20 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	7	7	Ž	3	•	<b>2</b> 50	50120		•	í ♥		29		. 862	3		29.94	769.5		31.8	•
-1         306         94         4         873         56200         8         4         562         29         74         760         71         71         71         56120         8         4         760         71         71         71         71         71         71         71         71         71         71         71         71         71         71         71         71         71         71         71         71         71         71         71         71         71         71         71         71         71         71         71         71         71         71         71         71         71         71         71         71         71         71         71         71         71         71         71         71         71         71         71         71         71         71         71         71         71         71         71         71         71         71         71         71         71         71         71         71         71         71         71         71         71         71         71         71         71         71         71         71         71         71         <	7	7	202	62	-	712	56128		•	1 +		599		86.	3		29.94	760.5		126.7	•
-2 284 87 3 184 58128 8 4 -1 261 88 22 78128 8 4 -2 2 2 73 2 520 78128 8 42083 63 2 0 29.4 768.5 178 -5 2. 73 2 520 78128 8 41862 1.6 .020 63 2 0 29.4 768.5 18 -5 2. 73 2 520 78128 8 41862 1.6 .020 63 2 0 29.4 768.5 18 -5 2. 23 77 3 718 50128 8 458894895 63 2 0 29.4 768.5 18 -5 2. 23 77 3 718 50128 8 458894895 63 2 0 29.4 768.5 18 -5 2. 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	7	7	200	ž	*	873	50200		•	+					2		29.94	760.5		31.8	•
-6         178         52         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718         718	7	7	284	84	n	Ī	50120		•	+					8	 20	29.94	760.5		31.8	•
-5 2 73 2 520 56100	-21	4	178	22		710	76188		•	•					8		29.94	760.5	•	0.0	~
-1         261         88         229         78120         6         4         -1         -082         1.6         .028         63         29         4         769.5         6           -3         2581         86         258         710         710         8         4         -1.5         -0899         -1.4         -0805         6         20.94         769.5         6           -3         2587         87         229         78100         8         4         -1.5         -0899         -1.4         -085         10.9         -1.5         -0899         -1.4         -085         10.9         10.9         -1.0         -1.0         -1.0         -1.0         -1.0         -1.0         -1.0         -1.0         -1.0         -1.0         -1.0         -1.0         -1.0         -1.0         -1.0         -1.0         -1.0         -1.0         -1.0         -1.0         -1.0         -1.0         -1.0         -1.0         -1.0         -1.0         -1.0         -1.0         -1.0         -1.0         -1.0         -1.0         -1.0         -1.0         -1.0         -1.0         -1.0         -1.0         -1.0         -1.0         -1.0         -1.0         -1.0 <td>-13</td> <td>ņ</td> <td>7)</td> <td>ĸ</td> <td>7</td> <td>520</td> <td>50108</td> <td></td> <td>•</td> <td>1 +</td> <td></td> <td>963</td> <td></td> <td>. 963</td> <td>8</td> <td></td> <td>29.94</td> <td>760.5</td> <td></td> <td>29.3</td> <td>~</td>	-13	ņ	7)	ĸ	7	520	50108		•	1 +		963		. 963	8		29.94	760.5		29.3	~
-3 281 86 518 78120 8 458894897 68 28 28.94 768.5 169 69 6.3 178 58120 8 4588988 68 28 28.94 768.5 169 6.3 178 58120 8 45889888 5 68 28 28.94 768.5 169 6.3 178 58120 8 4588988 18 28 28.94 768.5 178 58120 8 4588988 18 28 28.94 768.5 178 58120 8 4588988 18 28 28.94 768.5 178 58120 8 4589988 18 28 28.94 768.5 178 58120 8 4589988 18 28 28.94 768.5 169 6.3 178 58120 8 8 4589988 18 28 28 28.94 768.5 169 6.3 178 58120 8 8 4589988 18 68 28 28.94 768.5 169 6.3 178 58120 8 8 4589988 18 68 28 28.94 768.5 169 6.3 178 58120 8 8 4589988 18 68 28 28.94 768.5 169 6.3 178 58120 8 8 4589988 18 68 28 28.94 768.5 169 6.3 178 58120 8 8 4589988 18 68 28 28.94 768.5 169 6.3 178 58120 8 8 4589988 18 68 28 28.94 768.5 169 6.3 178 58120 8 8 4589988 18 68 28 28.94 768.5 169 6.3 178 58120 8 8 458999 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18 6.3 18	7	7	261	2		228	70120		•	í •	i T	907		.028	2		29.94	760.5	•	0.0	•
-5 253 77 3 719 50100	-	7	281	2		510	70120		•	1 +		88	1.4.	<b>60</b>	8		29.94	760.5	•	•	•
9         284         87         229         78100         8         4	97	ę	253	1	n	710	56166		•	ľ		600	- 5	963	88		29.94	769.5		29.3	7
-3         287         87         4         164         50100         8         4         -5         -009        6        018         57         20         22.94         760.5         170           -3         286         63         1         716         59120         8         4        5        005         -1.3         -623         62         20.94         760.5         160        6        6        6        6        6        6        6        6        6        6        6        6        6        6        6        6        6        6        6        6        6        6        6        6        6        6        6        6        6        6        6        6        6        6        6        6        6        6        6        6        6        6        6        6        6        6        6        6        6        6        6        6        6        6        6        6        6        6        6        6        6        6        6	7	•	<b>784</b>	87		228	70106		•	1 +		500	8.	014	8		29.94	769.5		•	•
-3 206 65 1 716 50120 6 45005 -1.3023 68 20 29.04 760.5 170 205 68 20 50100 6 4 400 70100 6 4 4.0 -0.0 6 6 20 29.04 760.5 169 69 20 60 20 20 20 4 760.5 169 69 20 60 20 20 20 4 760.5 169 69 20 60 20 20 20 4 760.5 169 69 20 60 20 20 20 20 20 20 20 20 20 20 20 20 20	F	7	287	6	*	ì	<b>29.58</b>		•	1 +				919.	er C	 50	29.94	760.5		31.0	•
1         265         67         4         229         56160         8         4        6        616        9        6         26         29         29         760.5         6           -2         269         8         4        6        616         6         26         29         29         4         760.5         6           -2         266         8         4        6        616         6         26         29         4         760.5         6           -3         254         77         3         460         50120         8         4        6        616         6         26         29         4         760.5         16           -3         254         77         3         400         50120         8         4        6        616        7        612         63         20         29         4        6        616        7        616         6         20         29         4        6        616        7        612         63         20         29         4        6        616        7        616        6	7	?	<b>586</b>	3	-	710	50120		•	<b>+</b>				.023	3	2	29.94	760.5		31.8	•
-1         210         64         409         70100         8         4        6        610        9        615         68         20         29.94         760.5         0           -2         280         80         40         70120         8         4        602        616         68         20         29.94         760.5         6           -3         254         77         3         400         20120         8         4        607        607        606         68         20         29.94         760.5         170           -3         281         86         3         5110         8         4        603        7        605         68         20         29.94         760.5         170           -2         200         85         4         107         50100         8         4        603        1        619        1        619        603        603        603        603        603        603        603        603        603        603        603        603        603        603        603 </td <td>~</td> <td>-</td> <td>285</td> <td>9</td> <td>*</td> <td>229</td> <td><b>3</b></td> <td></td> <td>•</td> <td>4</td> <td></td> <td></td> <td></td> <td></td> <td>2</td> <td> 8</td> <td>29.94</td> <td>760.5</td> <td></td> <td>29.3</td> <td>•</td>	~	-	285	9	*	229	<b>3</b>		•	4					2	 8	29.94	760.5		29.3	•
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ENTERPRISE (CVN-65)	DECK PITCH		3	*	005	003	- 669	993	700	. 963	662	002	003	995	005	003		200	566	007	992	003	005	662	<del>00</del> 7	. 663	965	003	. 669	799.	662	- 667	003	003	002	995	007	010	9.000	662
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PRIS		a	N/S	72	,	_	<b>,</b>	•						•	•	•	, ,					•	•	•	•				•	<b>D</b> (				•		•	•	•	•	, ,
NT ES	SH P	SPEED	_ ₹	7	5	2	2	2 :	<u> </u>	<u> </u>	: 2	12	=	=	=	7	2 9	2 5	2 5	2	7	7	2	2	2 5	: 2	12	2	2 :	2 :	2 5	2	7	12	12	7	7	2	2 :	12
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Ĭ	SIDE	ġ		8	107	707	718	167	3 5	118	412	8	412	118	197	118	2		7.8	718	412	797	118	718	412	<b>8</b>	118	718	167		2 5	412	118	\$	718	<b>5</b>	\$	220	412	873
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L. OING DATA	3	DIST	E	2	278	186	<b>52</b>	216		311	329	270	293	223	270	317	3		238	286	3	248	186	282	2 3	8	181	<b>508</b>	28	917	3	267	178	<b>36</b>	<b>3</b> 6	242	266	21	8	332
3	OFF-CENTER	DISTANCE	2	3	7	7	7	7 (	1	17	7	Ŷ	7	7	ņ	7	7.	7	?	7	•	7	7	•	• 7	•	1	-	7	t '	7 -	7	†	7	7	7	7	†	<b>~</b>	ī
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		3	LADING DATA	1	MODEL TA-4F	1A-4F		uss	NE	PRIS	USS ENTERPRISE (CVN-65)	+65)			٥	3 ≽	DAY LANDINGS				
9	Q T	OFF-CENTER	RAMP TO	<b>10 10</b>	WIRE	SIDE	20	\$	SHIP P		DECK PITCH	HDT.	DECK	DECK ROLL	7	104	BAROMETRIC	TRIC	AR.	ARR GEAR	REREAD
ġ	018	DISTANCE	DISTAN	TANCE	Š	ğ	TYPE	<b>800</b>	SPEED	8							PRESSURE	URE	RUNOUTS	UTS	NUMBER
	E	2	E	3					3	K K	DEC	3	DEG	3	۱.	ပ	N HG	꾶	Z	5	
62	3	•	3	2	67	2	69	2	17	22	2	*	22	92	12	82	8	89	<b>8</b>	82	
276	•	•	200	85	*	28	56186		12	•	.2.	. 993	•	.010	70		29.93	760.2	176 4	431.8	•
271	*	-	287	87	•	412	50120		12	•	- 5	005	₩.	.014	92		29.93	760.2	169	429.3	-
272	÷ '	1	200	3	•	\$	70100		77	•	ا. د د		4.5	024	2		29.93	760.2		•.	-
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278	ŋ	7	278	2	*	710	50120		12	•	4.4	007	-	.002	22		29.92	760.0		429.3	•
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28	-	•	22	6	•	511	70120		=		۱ ۲۰:	963		962	2		29.92	760.0			. •
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25	7	7	238	2	<b>м</b> ·	212	50120		<b>e</b> :		٠	- 995		995	21		29.92	760.0		426.7	•
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3	2	1	276	3	*	7:	50120		•	,	. v.	005		.003	22	52	29.92	760.0	168 4	428.7	•
Ē	-	9	251	2	1	873	70100		•	<b>S</b>	7	.963		010	2		29.92	760.0		•	_
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3	7	7	2	<b>5</b> 1	n	873	20.00		<b>.</b>		່	. 669	י הי	. 663	72		29.92	760.0		5	•
į	7	7	257	<b>P</b> (	3 1				2 :	n .	7. c	30.5	•	8	2 5		28.82	9.6		5.1.6	•
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\$	-	7	273	3	1	727	70108		. =					014	2		29.92	769.0		0	. ~
310	7	7	187	22		\$	70100		=	'n	2	. 963		.010	72		29.92	760.0	•		-
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312	7	7	173	3	~	504	59166		<b>6</b>	'n	- 5.1			012	72		29.93	760.2	168 4	426.7	•
313	-17	ę	263	2		512	76166		<b>.</b>	'n	9		-1.2 -	821	77		29.93	769.2			~
410	=	4	182	<b>S</b>	<b>~</b>	727	50.00		<b>£</b>		• •	667	- (	. 662	2	22	29.93	769.2	168 4	426.7	- (
212	n	_	326	B	*	516	50120		9	n	. 2.	663	<b>D</b>	• 14·	7.		29.83	7.097		429.3	Đ

REREAD	NUMBER			-	_	•	•	•	~	-	•	•	~	<b>-</b>	•	-	9	•	•	•	9	•	•	-	•	~	-	-	•	7	-	-	•	-	8	•	8	-	8	•	_	•	-
ARR GEAR	OTS	8	82	429.3	429.3	426.7	429.3	<b>.</b>	428.7	426.7	426.7	0.	•	•	<b>.</b>	29.3	0.0	0.	0.0	429.3	429.3	•	424.2	429.3	429.3	0.0	•	<b>6</b> .	429.3	431.8	•	431.8	•	431.8	0.0	129.3	•	0.0	431.8	431.8	0.0	0.0	31.8
ARR	RUNOUTS	2	5	169 4	169 4	168	169 4	•	168 4		168	•	•	•	•	169 4	•	•	•	169 4	169 4	_			169	•	•			170 4		176 4		179 4		169 4	•	•	176 4	179 4	•	•	179 4
TRIC	SURE.	E E	80	760.2	769.2	769.2	760.2	769.2	760.2	760.2	760.2	760.2	760.2	760.2	760.2	760.2	769.2	769.2	760.2	760.2	760.2	760.2	760.2	760.2	769.2	760.2	760.2	760.2	760.2	760.2	761.2	761.2	761.2	761.2	761.2	761.2	761.2	761.2	761.2	761.2	761.2	761.2	761.2
BAROMETRIC	PRESSURE	N H	78	29.93	29.93	29.93	29.93	29.93	29.93	29.93	29.93	29.93	29.83	29.93	29.93	29.93	29.93	29.93	29.93	29.93	29.93	29.93	29.93	29.93	29.93	29.93	29.93	29.93	29.93	29.93	29.97	29.97	29.97	29.97	29.97	29.97	29.97	29.97	29.97	29.97	29.97	29.97	29.97
TEM		ပ	78	22	22	22	22	22	22	22	22	23	23	23	23	23	23	23	23	23	23	23	23	23	23	23	23	23	23	23	23	23	23	23	23	7	7	5	21	2	7	21	71
-		<b>L.</b>	11	72	72	22	72	72	72	77	2	2	2	2	2	23	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	69	69	69	69	69	69	69	69
DECK ROLL		3	92	.054	. 967	007	965	. 969	.00	037	. 024	.00	.01	021	012	003	002	014	009	.012	014	033	007	.010	002	919	.03	005	1.036	026	1.885	.016	.002	<b>.</b>	350		<b>.</b>	.002	. 967	e18	.033	010	.021
DECK		930	82	3.1	₹.	+	_				<b>*</b> :	ņ				7	7			۲.		6.7		ø.	ī	-:				5. T		œ	-	ų	<del>.</del>		3.2	-	₹.				
P11CH		<b>3</b>	*	600	002	995	003	992	002	007	997	963	- 999	. 995	- <b>96</b> .	609	003	005	003	003	667	. 963	993	- 999	963	995	007	963	98.	003	007	997	9.00	010	999		003	007	002	969	010	007	007
DECK PITCH		930	2	ĸ.	-			· ;	· -	• •	• •	- 5	ر. د	ان ا	- 7	ė.	2	۵.	- 7	•	· •	.2	2		2		• •	~	•	2	• •		•	9.	. S.		2	+:	_			*	*
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SKIP PIN	8	Š	7	•	•	•	•	•	•	•0	•	•	•	•	•	•	•	•	80	80	•	•	₩	•	•	•	•	•	•	•	•	•	_	₩	•	4	*	+	4	*	*	4	•
2	<b>800</b>		2																																								
200	TYPE		8	50100	50120	<b>36</b> 18	50120	70100	<b>56</b> 1 <b>8</b> 8	<b>30108</b>	2	70108	70120	<b>3</b> = <b>3</b>	70100	<b>3</b> <b>3</b> <b>3</b>	70188	<b>3</b> 0.00	<b>3</b> 2 3 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	<b>S</b> e i <b>S</b>	<b>3618</b>	66128	20200	50120	50123	70120	218	78188	<b>36128</b>	3	70120	<b>36</b> 126	76286	56128	76120	56128	76266	76128	56126	50120	70120	70120	59120
SIDE	Š		3	512	\$	228	873	797	871	797	228	=	2	217	22	113	217	520	873	797	673	516	792	873	5	718	718	=	718	=	51	5	217	412	22	217	228	2	3	239	\$	520	412
WIRE	Š		5	n	*	~	7		~	n	~					~				~	n		8	n	~				~	n		n		8		n			n	n			7
RAMP TO TD	DISTANCE	3	9	5	85	72	3	F	2	2	2	87	9	2	8	2	2	77	8	7	2	9	3	2	9	3	2	\$	67	ž	57	67	ŝ	5	7	5	2	3	1	2	82	3	2
3	DIST	E	2	267	302	236	222	252	248	259	38	287	285	226	283	238	238	237	313	234	<b>76</b>	310	211	231	286	211	228	5	220	9	187	<b>5</b> 50	192	1 0 0	232	8	239	213	252	276	270	175	238
ENTER	ANCE	3	3	?	7	ņ	7	7	7	•	7	•	7	7	~	7	7	ņ	7	7	7	•	ņ	7	7	7	-	7	?	†	•	†	ş	†	•	†	7	7-	7	7	•	1	κ'n
OFF-CENTER	DISTANCE	E	3	7	7	-15	7	=	7	•	7	•	7	4	^	7	<b>*</b>	<b>9</b>	4	•	-13	7	9 -	=	7	7	7	-17	7	-12	7	-13	<u>-</u> 13	-12	-	<del>+</del> =	7	7	7	7	•	+1-	13
200	<b>9</b>		62																																								1565

DAY LANDINGS

USS ENTERPRISE (CVN-65)

L. DING DATA - MODEL TA-4F

	REREAD	NUMBER			•	•	•	_	7	- •	<b>-</b>		•	-	•	_	- •	•	•	•	• •	4 64	~	<b>~</b> •	- «	, <b>-</b>	•	•	•	•	~ (	N 6	•	•	•	-	_
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	APR CEAR	RUNDUTS	8	82	429.3	•	426.7	431.8	429.3	8. E.	7.00		5	426.	5.5	429.J	429.3	429.3	451.8	431.8	25	426.7	431.8	431.8	420.3		429.3	ě	426.7	•	•	9.6	429.3	424.2	431.8	•	•
	\$	\$	Z	5	169	•	168	_		178				168	-	-	200		-	-	92			170			169		168	•	•	•			_	•	•
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	BAROMETRIC	SURE	¥	•	761	761	761	761	76	761	2 2	761	761	761	761	76	761.2	761.2	76	761	76.	76.	761	761.2	7.107	92	761	761	761	761	761	197	781	78	761.0	761	781
INGS	AROL	PRESSURE	IN HG	79	29.97	29.97	29.97	29.97	29.9	29.97	20.07	29.97	29.97	29.97	29.97	29.97	29.97	29.97	29.97	29.97	29.97	29.97	29.97	29.97	70.07	29.97	29.97	29.97	29.97	29.97	29.96	29.85	20.00	29.96	29.96	29.96	20 06
DAY LANDINGS	•				29	8	23	20	20	9 78	2 6	2 5	<b>8</b>	58	28	8	2 2	3 8	8	2	8 8	3 8	29	8 8	9 0	2 2	28	20	8	2	2	2 8	,	2 2	7	28	29
DAY	TEM		O	78	2	7	2	2	7	5 5		7	2	7	2	7		7 2	7	2	;	7 2	5	5 5	, ,	: 5	2	7	5	5	<u>.</u>	2 9	2 5	2	-	=	2
	_		<b>L</b>	11	69	8	8	8	8	8	9	9	69	69	69	69	8	8	8	8	8	\$	8	8		8	8	8	8	9	62	2 6	3 6	6	67	67	67
	DECK ROLL		3	92	.00	8		.026	8	8 8	3	965		. 026	8	=	.021	3	. 021	.863	.68	3		8		924	919	8	<b>.8</b>	916	<b>016</b>			000	926	. 963	AIA
	ă		DEG	23	~	ĸ.	-	٠. دن	- <del></del> -	ų.	4	•	<b>:</b>	ĸ.		•	ú.	•	. ~	si.	-, ¢		-	<b>+</b> •		, <del>,</del>		7	-	e.	_	1 0 1	o a	•		7	œ
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USS ENTERPRISE (CVN-65)	DECK PITCH		3	7.	997	865	003	063	607	. 669		- 963		607	80	8	5		9	-	002	3	607	8	Ì	012	. 98.		962	. <b>. 8</b>	. 8		3	8			5
<u>Ş</u>	Ä		DEC	2	•	,	7.7	7	•	, ,	•	~	!	•	*	'n	•			•	· -, •	; <del>+</del>	*	'n,	•		~		-	'n	• (	0 1	, ,		-	~	4
¥R IS		a	K K	27	7	7	7	, 4	7	N 6	, c	,	ı «	7	7	7	, i	, ,	, 1	7	, ,	, ,	. 4	, 4	A C		, 1	7	7	7	' + '	• •		•	•	+	7
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DAY LANDINGS

USS ENTERPRISE (CVN-65)

LANDING DATA - MODEL TA-4F

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# **SYMBOLS**

DEPARTMENT OF THE NAVY
Naval Air Development Center
Warminster, PA 18974-5000

13410 Code 6042 24 Aug 87

LIST OF SURVEY SYMBOLS AND DEFINITIONS

Prepared by:

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Aerospace Engineer

Enclosure (4)

Code 6042 10 Jun 87

#### LANDING LOADS SURVEY DEFINITIONS

SINK SPEED - VV - The sink speed of the aircraft landing gear wheel just prior to touchdown. Sink speed is reported for each landing gear individually; that is for the port, starboard, and nose wheels just prior to individual deck contact. In addition, the Average Sink Speed of the aircraft main landing gear is calculated just prior to touchdown of the first main landing gear wheel. Sink speed is determined from film data.

The symbols used to identify aircraft sink speed are as follows:

V<sub>V<sub>A</sub></sub> - average sink speed

 $v_{v_c}$  - sink speed of the starboard main wheel

 $V_{V_{\mathcal{D}}}$  - sink speed of the port main wheel

 $\mathbf{V}_{\mathbf{V}_{\mathbf{N}}}$  - sink speed of the nose landing gear

The values of aircraft sink speed are reported in both feet per second (ft/sec.) and meters per second (meters/sec.).

For shipboard landings, the values of sink speed are reported with respect to the vessels flight deck.

WING LIFT FACTOR —  $^{K}LE$  — The Wing Lift Factor is calculated from the derivative of the aircraft average sink speed. It is calculated just prior to the touchdown of the first main landing gear. A value of 1.0 for the Wing Lift Factor indicates that a constant sink speed is being maintained. If the value of K is greater than 1.0, this indicates that the sink speed is decreasing and K wing lift is greater than 1.0 G. Conversely, if the value is less than 1.0, then the sink speed is increasing and the lift being generated is less than 1.0 G.

The value of Wing Lift Factor is calculated from the equation

$$K_{IE} = (2*C/32.2) + 1.0$$

where the value of 2\*C is the second derivative of the regression curve of the aircraft vertical position with respect to time, evaluated at touchdown (t=0). The regression curve is that calculated for the average vertical position of the aircraft main landing gear and has the form of the equation

Position = 
$$A + Bt + Ct^2$$

The symbol for WING LIFT FACTOR is  $K_{\mbox{\scriptsize LE}}$ . This quantity is dimensionless.

The value of wing lift factor is measured with respect to the flight deck. (This value could be referenced to the horizon by correcting it for deck pitch angle.)

WIND OVER DECK - V - Wind Over Deck is the wind velocity measured by the ships instrumentation with respect to the flight deck. For aircraft carrier landings, the wind component down the landing deck is utilized. The positive direction for Wind Over Deck is from the ships bow to the stern, down the angle deck.

The symbol for WIND OVER DECK is Vu.

The value of Wind Over Deck is reported in knots and meters per second.

ENGAGING SPEED - VE - The engaging speed is the speed with which the aircraft closes on the aircraft carrier's flight deck. Engaging speed is reported with respect to the flight deck. Engaging Speed is calculated from film measurements.

The symbol for ENGAGING SPEED is  $V_{\rm p}$ .

The value of Engaging Speed is reported in knots and meters per second.

The value of engaging speed measured at the "over the ramp" position is identified as Veor\*.

APPROACH SPEED - VP'AF - The value of Approach Speed reported is the algebraic sum of Engaging Speed and component of Wind Over Deck parallel to the centerline of the angle deck. The value of Approach Speed is the aircraft horizontal velocity with respect to the air mass.

The symbol for APPROACH SPEED is  $V_{P^*AF}$ .

The value of Approach Speed is reported in knots and meters per second.

MINIMUM POWER APPROACH SPEED VP Amin - This value is the minimum power approach speed for a jet aircraft in the power approach configuration (landing gear, flaps and other high lift devices deployed). This number is determined from the aircraft's aerodynamic characteristics and landing weight per criteria established by NAVAIR.

The symbol for MINIMUM POWER APPROACH SPEED is Vp-Amin

The value of minimum power approach speed is reported in knots and meters per second.

POWER APPROACH STALL SPEED -  $^{V}$ SP'A - This value is the power approach stall speed for a propeller driven aircraft in the power approach configuration (landing gear flaps and other high lift devices deployed). This number is determined from the aircraft's aerodynamic characteristics and landing weight per criteria established by NAVAIR.

The symbol for POWER APPROACH STALL SPEED is VSP-A.

The value of power approach stall speed is reported in knots and meters per second.

RATIO OF MEASURED APPROACH SPEED TO MINIMUM POWER APPROACH SPEED - KVP'Amin - The ratio of the jet aircraft approach speed determined from film data to the minimum power approach speed for the same landing weight.

The symbol for the RATIO OF VprAF/VprAmin is KvprAmin

This quantity is dimensionless.

RATIO OF MEASURED APPROACH SPEED TO POWER APPROACH STALL SPEED - KVSP'A - The ratio of the propeller driven aircraft measured approach speed, determined from film data, to the aircraft power approach stall speed, for the same value of landing weight.

The symbol for the RATIO OF VPAF/VSPA is KVSPA.

This quantity is dimensionless.

AIRCRAFT PITCH ANGLE  $-\theta_D$  - The aircraft pitch angle measured between the aircraft reference line and a line parallel with the aircraft carrier's flight deck. Positive values of pitch angle are reported for an aircraft exhibiting a nose up attitude. Pitch Angle is determined from film data.

The symbol used for PITCH ANGLE is  $\theta_{\rm D}$ .

The value of this quantity is reported in both degrees and radians.

The value of pitch angle is reported at two locations—just prior to first wheel touchdown, and as the aircraft flies "over the ramp" at the stern end of an aircraft carrier's flight deck.

SUBSCRIPTS: R - Over the ramp

td - At touchdown

AIRCRAFT ROLL ANGLE  $\cdot$   $\theta_r$  — The Aircraft Roll angle measured between the aircraft reference line and a line parallel with the aircraft carrier's flight deck. Positive values of roll angle are reported for an aircraft whose starboard wing is down. Roll Angle is determined from film data.

The symbol used for RULL ANGLE is -  $\theta_r$ .

The value of this quantity is reported in both degrees and radians.

The value of roll angle is reported at two locations; just prior to first wheel touchdown and as the aircraft flies "over the ramp" at the stern end of an aircraft carrier's flight deck.

SUBSCRIPTS: R - Over the ramp

td - At touchdown

AIRCRAFT PITCH RATE  $-\dot{\theta}_p$  - The aircraft pitch rate is calculated from the film data. It is reported just prior to the touchdown of the first main wheel. Positive values of this variable indicates that the aircraft nose is pitching down. This rate is determined with respect to the flight deck.

The symbol used for THIS QUANTITY is  $\dot{\theta}_{p}$ .

The value of this quantity is reported in both degrees per second (deg./sec) and radians per second (radians/sec.).

AIRCRAFT ROLL RATE -  $\dot{\theta}_r$  - The aircraft roll rate is calculated from the film data. It is reported just prior to the touchdown of the first main wheel. Positive values of this variable indicates that the aircraft is rolling to port. This rate is determined with respect to the flight deck.

The symbol used for THIS QUANTITY is  $\hat{\theta}_r$ .

The value of this quantity is reported in both degrees per second (deg./sec) and radians per second (radians/sec.).

AIRCRAFT OFF-CENTERLINE DISTANCE - Y - This is the perpendicular distance measured between the aircraft centerline and the centerline of the flight deck (or runway). This value is calculated from film data just prior to first main wheel touchdown. Positive values of this quantity indicate that the aircraft landed on the port side of the flight deck centerline.

The symbol for THIS QUANTITY is Y.

The value of this quantity is reported in feet (ft) and meters.

DISTANCE FROM RAMP TO FIRST MAIN WHEEL TOUCHDOWN - XW - For aircraft carrier landings the distance between the flight deck ramp (aft end of the flight deck) and the point of first main wheel touchdown is determined from the film data. For land based surveys, this distance can be determined from an appropriate reference line with respect to the camera.

The symbol for THIS QUANTITY is -  $X_W$ .

The value of this quantity is reported in feet (ft) and meters.

AIRCRAFT INSTANTANEOUS GLIDESLOPE ANGLE -  $\beta V_V$  - This angle is determined just prior to first main wheel touchdown. The value of average sink speed ( $V_A$ ) and engaging speed ( $V_E$ ) are used to define the instantaneous glideslope. These values are entered into the equation;

$$\beta_{V_V}$$
 = arctan( $V_{V_A}/V_E$ ) + deck pitch angle

NOTE: A Consistent set of units must be used in this equation.

The symbol for THIS QUANTITY is  $\beta_{V_{\, U}}$ .

The value of this quantity is reported in degrees and radians

AIRCRAFT GEOMETRIC GLIDESLOPE ANGLE  $-\frac{\beta H}{W}$  - This angle is determined by utilizing the Distance from The Ramp To Touchdown ( $X_W$ ) and Height Of Main Wheels At The Ramp ( $H_U$ ). These values are substituted into the Equation:

 $\beta H_U = \arctan{(Vetd-SS/Vetd)*(H_U/X_U)} + deck pitch angle$ 

Where SS is Ships Speed.

The Quantity (Vetd-SS/Vetd)is a correction factor for ships forward motion during the time the aircraft flies from the Ramp position to Touchdown.

NOTE: A consistent set of units must be used in this equation.

The symbol for THIS QUANTITY is -  $\beta_{H_{11}}$ 

LANDING WEIGHT - W - The landing weight reported in the survey is determined from aircraft basic weight and the reported fuel state on aircraft final approach (the "Ball State"). The type and quantity of any external stores is also included in the determination of landing weight.

The Symbol for THIS QUANTITY is W.

The value of this quantity is reported in pounds and kilograms.

AIRCRAFT YAW ANGLE - YAW TD - The Yaw Angle is the angle between the aircraft centerline and the aircraft flight path at the point of first main wheel touchdown. Positive YAW Angle is defined to be that orientation where a clockwise rotation of the yaw vector causes the vector to coincide with the aircraft centerline using a minimum angular rotation. Yaw Angle is determined from film data.

The Symbol for THIS QUANTITY is YAW, TD.

The value of this quantity is reported in degrees and radians.

AIRCRAFT FLICHT PATH ANGLE - F.P.A. - The Flight Path Angle is the angle between the aircraft flight path and the flight deck centerline at the point of touchdown. This measurement is determined from film data. Positive Flight Path Angle is defined to be that orientation where a clockwise rotation of the flight path vector causes the vector to coincide with the flight deck centerline using a minimum angular rotation.

The Symbol for THIS QUANTITY is F.P.A.

The value of this quantity is reported in degrees and radians.

HEIGHT OF MAIN WHEELS OVER THE RAMP - HW -. The average height of the aircraft main landing gear wheels as it flies over the aircraft carriers ramp (aft end of flight deck) is determined from the film data. This information can also be provided for land based surveys utilizing an apppropriate reference line on the runway.

The symbol for THIS QUANTITY is  $H_{\mathbf{W}}$ 

The value of this quantity is reported in feet and meters.

HEIGHT OF THE HOOK AT THE RAMP - HH - The height of the aircraft arresting gear hook as it flies over the aircraft carrier's ramp (aft end of flight deck) is determined from the film data. This quantity is only reported on carrier surveys.

The symbol for THIS QUANTITY is  $H_{\mathbf{u}}$ .

This quantity is reported in feet and meters.

ANGLE OF FLIGHT DECK PITCH - &Dp - This angle is the pitch angle of the aircraft carrier's flight deck with respect to the horizon. This data is recorded from the ship's inertial navigation system utilizing inputs to the Fresnel Lens (Mirror Landing Aid System). This data is reported at the time of the aircraft first main wheel touchdown. This parameter is reported only for carrier landings. The positive value of this quantity indicates that the stern of the ship is up.

The symbol for THIS QUANTITY is  $\delta D_D$ 

This quantity is reported in degrees and radians.

ANGLE OF FLIGHT DECK ROLL -  $^{\delta}$ Dr - This angle is the roll angle of the aircraft carrier's flight deck with respect to the horizon. This data is recorded from the ship's inertial navigation system utilizing inputs to the Fresnel Lens (Mirror Landing Aid System). This data is reported at the time of the aircraft's first main wheel touchdown. This parameter is reported only for carrier landings. The positive value of this quantity indicates that the starboard side of the ship is down.

The symbol for THIS QUANTITY is  $\delta_{Dr}$ 

This quantity is reported in degrees and radians.

#### LIST OF SUBSCRIPTS

- FFE Free flight Engagement
- F Indicates that the data source is film data
- R Indicates data reported at the "over the ramp" position.
- P Port
- S Starboard
- N Nose Wheel
- A Average
- r Roll
- p Pitch
- td Data reported at aircraft touchdown
- d Data referenced to the Flight Deck

#### STATISTICAL SYMBOLS

- N Number of observations (data points).
- $\overline{X}$  Mean value of a parameter.
- P Probability.
- S Standard deviation of sample distribution.
- A<sub>3</sub> Skewness factor of sample distribution.
- $\mathbf{A}_{L}$  Kurtosis factor of sample distribution.